

# Electronic Design

THE MAGAZINE OF ESSENTIAL NEWS, PRODUCTS AND TECHNOLOGY

VOL. 15 NO.

# 9

APRIL 26 1967

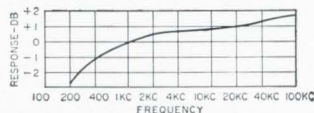
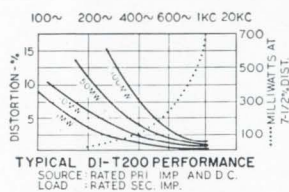


**Seek the right semiconductor** by starting here, and you'll find the devices that will make your circuit designs sparkle. Charts in this issue list more than 5000

transistors and microcircuits by function and key parameter. But don't stop there. Get detailed catalogs and application notes too. How? Turn to page 81.



# ULTRAMINIATURE TRANSISTOR TRANSFORMERS & INDUCTORS



- ➔ DUMET LEADS  
(gold plated, weldable and solderable)
- ➔ STRAIGHT PIN TERMINALS  
(printed circuit application)
- ➔ HIGHEST PERFORMANCE  
for size in the industry
- ➔ METAL ENCASED  
(Grade 4, Ruggedized)

**ALL STOCK UNITS MIL TYPE TF4RX  
Class "S" Available on Special Order**

High Power Rating ..... up to 100 times greater.  
 Excellent Response ..... twice as good at low end.  
 Low Distortion ..... reduced 80%.  
 High Efficiency ..... up to 30% better . . . compare DCR.  
 Moisture Proof ..... hermetically sealed to MIL-T-27B.  
 Ultraminiature Size ..... .5/16 Dia. x 3/8" H, 1/15 Oz.

Type No.	Pri. Imp.	DC ma <sup>†</sup> in Pri.	Sec. Imp.	Pri. Res.	Mw Level	Application
DI-T225	80 CT 100 CT	12 10	32 split 40 split	10	500	Interstage
DI-T230	300 CT	7	600 CT	20	500	Output or line to line
DI-T235	400 CT 500 CT	8 6	40 split 50 Split	50	500	Interstage
DI-T240	400 CT 500 CT	8 6	400 split 500 split	50	500	Interstage or output (Ratio 2:1:1)
DI-T245	500 CT 600 CT	3 3	50 CT 60 CT	65	500	Output or matching
DI-T250	500 CT	5.5	600 CT	35	500	Output or line to line or mixing
DI-T255	1,000 CT 1,200 CT	3 3	50 CT 60 CT	110	500	Output or matching
DI-T260	1,500 CT	3	600 CT	90	500	Output to line
DI-T265	2,000 CT 2,500 CT	3 3	8,000 split 10,000 split	180	100	Isol. or interstage (Ratio 1:1:1)
DI-T270	10,000 CT 12,000 CT	1 1	500 CT 600 CT	870	100	Output or driver
DI-T273	10,000 CT 12,500 CT	1 1	1,200 CT 1,500 CT	870	100	Output or driver
DI-T276	10,000 CT 12,000 CT	1 1	2,000 CT 2,400 CT	870	100	Interstage or driver
DI-T278	10,000 CT 12,500 CT	1 1	2,000 split 2,500 split	620	100	Interstage or driver
DI-T283	10,000 CT 12,000 CT	1 1	10,000 CT 12,000 CT	970	100	Isol. or interstage (Ratio 1:1)
DI-T288	20,000 CT 30,000 CT	.5 .5	800 CT 1,200 CT	870	50	Interstage or driver
DI-T204	Split Inductor (2 wdg)	§ .1 Hys @ 4 maDC, §§ .025 Hys @ 8 maDC, .02 Hys @ 20 maDC, DCR 25Ω				
DI-T208	Split Inductor (2 wdg)	§ .9 Hys @ 2 maDC, .5 Hys @ 6 maDC, DCR 105Ω §§ .2 Hys @ 4 maDC, .1 Hys @ 12 maDC, DCR 26Ω				
DI-T212	Split Inductor (2 wdg)	§ 2.5 Hys @ 2 maDC, .9 Hys @ 4 maDC, DCR 630Ω §§ .6 Hys @ 4 maDC, .2 Hys @ 8 maDC, DCR 157Ω				
DI-T216	Split Inductor (2 wdg)	§ 4.5 Hys @ 2 maDC, 1.2 Hys @ 4 maDC, DCR 2300Ω §§ 1.1 Hys @ 4 maDC, .3 Hys @ 8 maDC, DCR 575Ω				

<sup>†</sup>DCma shown is for single ended usage (under 5% distortion—100mw—1KC) . . . for push pull, DCma can be any balanced value taken by 5W transistors (under 5% distortion—500mw—1KC)  
 DI-T200 units have been designed for transistor application only . . . not for vacuum tube service.  
 U.S. Pat. No. 2,949,591 other pending.  
 Where windings are listed as split, 1/4 of the listed impedance is available by paralleling the winding.  
 §Series connected; §§Parallel connected.

## IMMEDIATE DELIVERY FROM STOCK

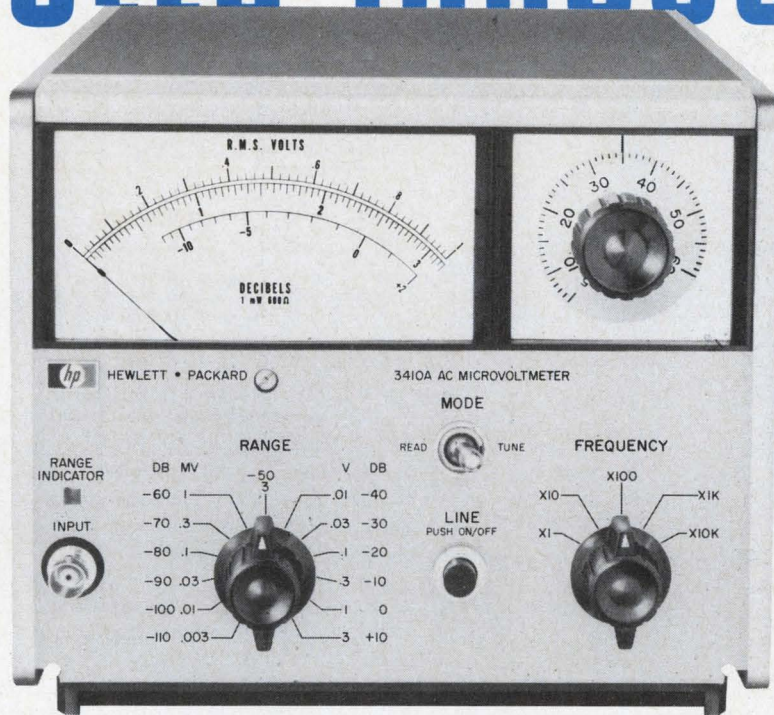
Write for catalog of over  
 1,300 UTC TOP QUALITY  
 STOCK ITEMS  
 IMMEDIATELY AVAILABLE  
 from your local distributor.



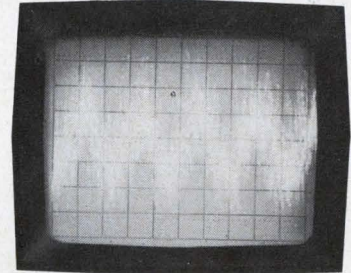
**UNITED TRANSFORMER CO.**  
 DIVISION OF TRW INC. • 150 VARICK STREET, NEW YORK, N. Y. 10013

# AC MICROVOLT METER

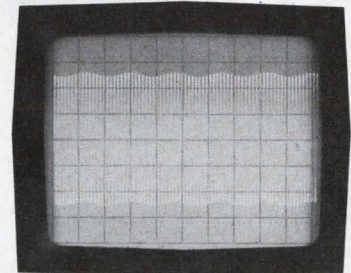
# SEES THROUGH NOISE!



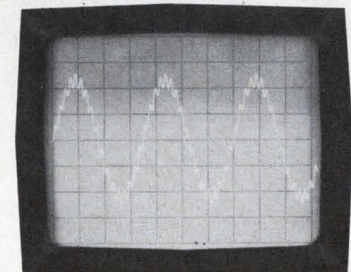
*New hp 3410A Measures  
300 nanovolts  
Buried in Noise*



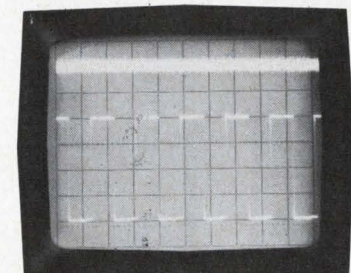
Measure 1  $\mu$ V, 500 kHz signal out of 40 dB noise.



Measure 10 mV, 5 Hz amplitude modulating  
1 V, 400 Hz.



Measure 300 nanovolts, 10 kHz  
signal superimposed on 10  $\mu$ V, 1 kHz.



Measure frequency of signal in noise up to 560 kHz  
by using square wave output,  
i.e. as a counter preamplifier.

New hp Model 3410A AC Microvoltmeter measures low level repetitive signals obscured by noise—3  $\mu$ V to 3 V full scale—accuracy  $\pm 3\%$ . RMS noise voltages up to 20 dB above full scale *do not affect* readings. Sensitivity, low cost and ease of operation are the 3410A's contribution.

This new microvoltmeter uses an hp designed phase-locked synchronous detector to separate effects of noise from signal. The detector is an electronic gate controlled by an oscillator phase-locked to the input signal. No external reference is required to lock to the input signal. Simply adjust front panel tuning control within 1% of signal frequency and phase-lock circuits *lock-on and track* input signal with  $\pm 5\%$  variation in the 5 Hz to 600 kHz frequency range. Phase-lock circuits track 0.5%/sec change in signal frequency without a change in voltmeter accuracy. Input impedance is 10 M $\Omega$  shunted by 20 pF.

The new Model 3410A has two outputs on the rear panel. One is a dc recorder output for monitoring long term drifting ac voltage amplitudes. The other is an output for driving an electronic counter to make precise frequency measurements.

For full specifications on the new hp Model 3410A AC Voltmeter, call your hp field engineer. Or, write to Hewlett-Packard, Palo Alto, California 94304, Tel. (415) 326-7000; Europe: 54 Route des Acacias, Geneva. Price: hp Model 3410A, \$800.00.

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An extra measure of quality

097/11

ON READER-SERVICE CARD CIRCLE 2



## Unit Citation

We're honored! Not that we've won our crusade yet...just another battle ribbon. A while back we scored a military victory with our Model 880, the *first* solid state Mil Spec counter. This time it's a fully-militarized 5MHz all-silicon solid state universal counter-timer. Call it USN /AN-245, sir.

There's a good reason you should be interested. You see, the military model had its basic reliability well proved by our original commercial version, Model 607A. Now *there's* the one for *you!* It offers more features and capabilities than even the Admirals asked for. And it's available on-the-double.

Now hear this: Our lowest-bidder-type price is only \$1,575. (Check *that* saving against our competitor!) Then check these features: Model 607A is ideal for wide-range frequency measurements, frequency ratio determination, period and multiple period or time interval measurements, and pulse count totalizing. Time base is a 1 MHz crystal oscillator (for 1 microsec resolution). Display is six decade inline with display storage. BCD output transfers directly to CMC Model 410 tape printer, computer systems, etc. Automatically positioned illuminated decimal. Either ac or dc coupling of input signal. Front and rear A and B channel inputs. Rugged, compact (approx. 3½" high). Available for bench or rack.

### THANKS

With all our pride and excitement over our USN/AN-245 award, and other new products, we haven't forgotten our fellow Crusaders who've made this success possible...YOU. A FREE Crusading Engineers medal is our fun-loving way of saying thanks. Get yours by writing for data so you can "Check the Specs" of our 607A. Your "chief" will be so proud of you at mail call!

12973 Bradley / San Fernando, California  
Phone (213) 367-2161 / TWX 910-496-1487



# Electronic Design

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## Departments

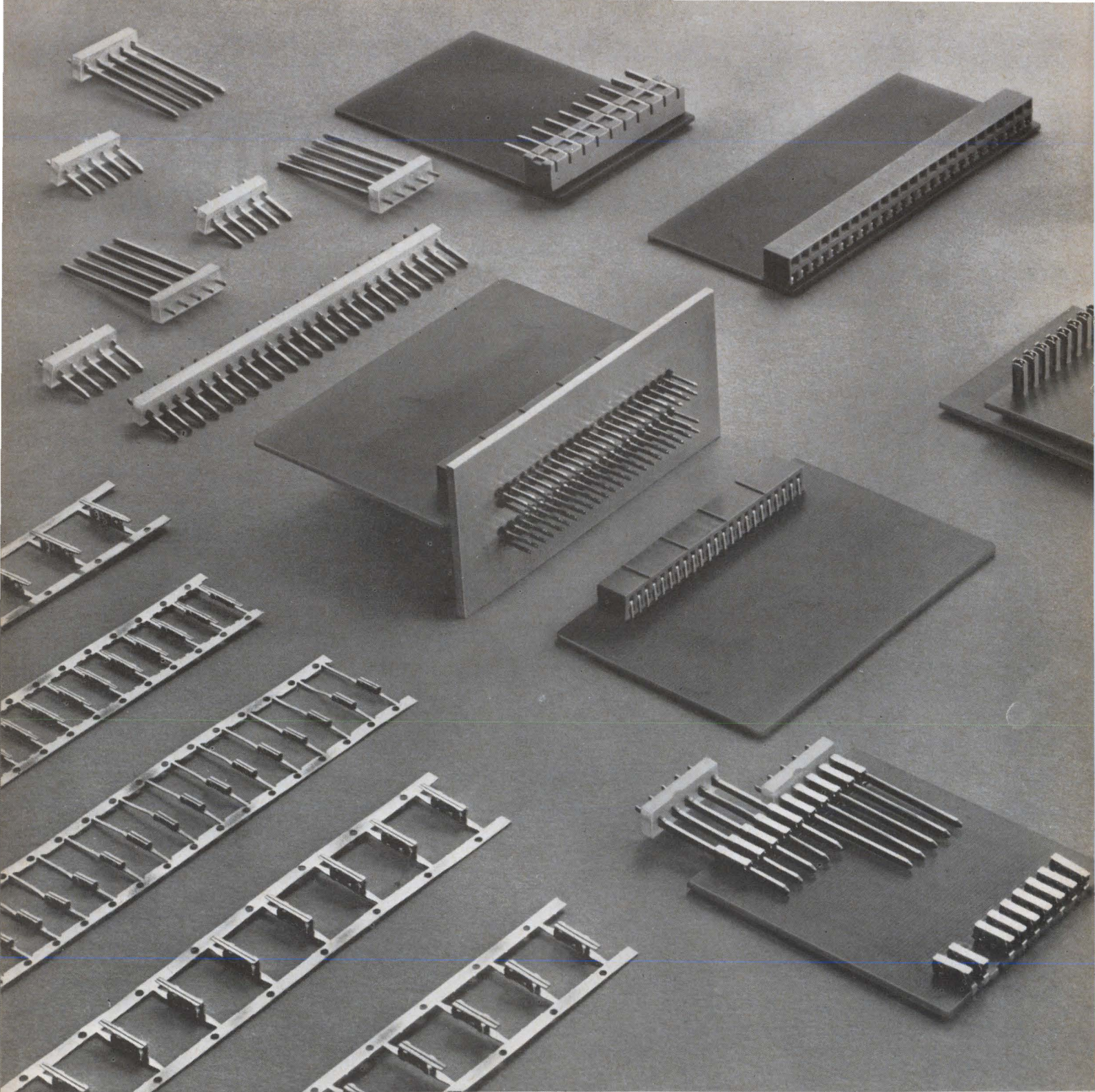
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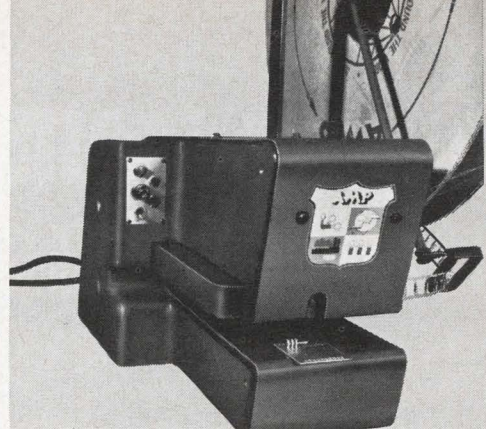
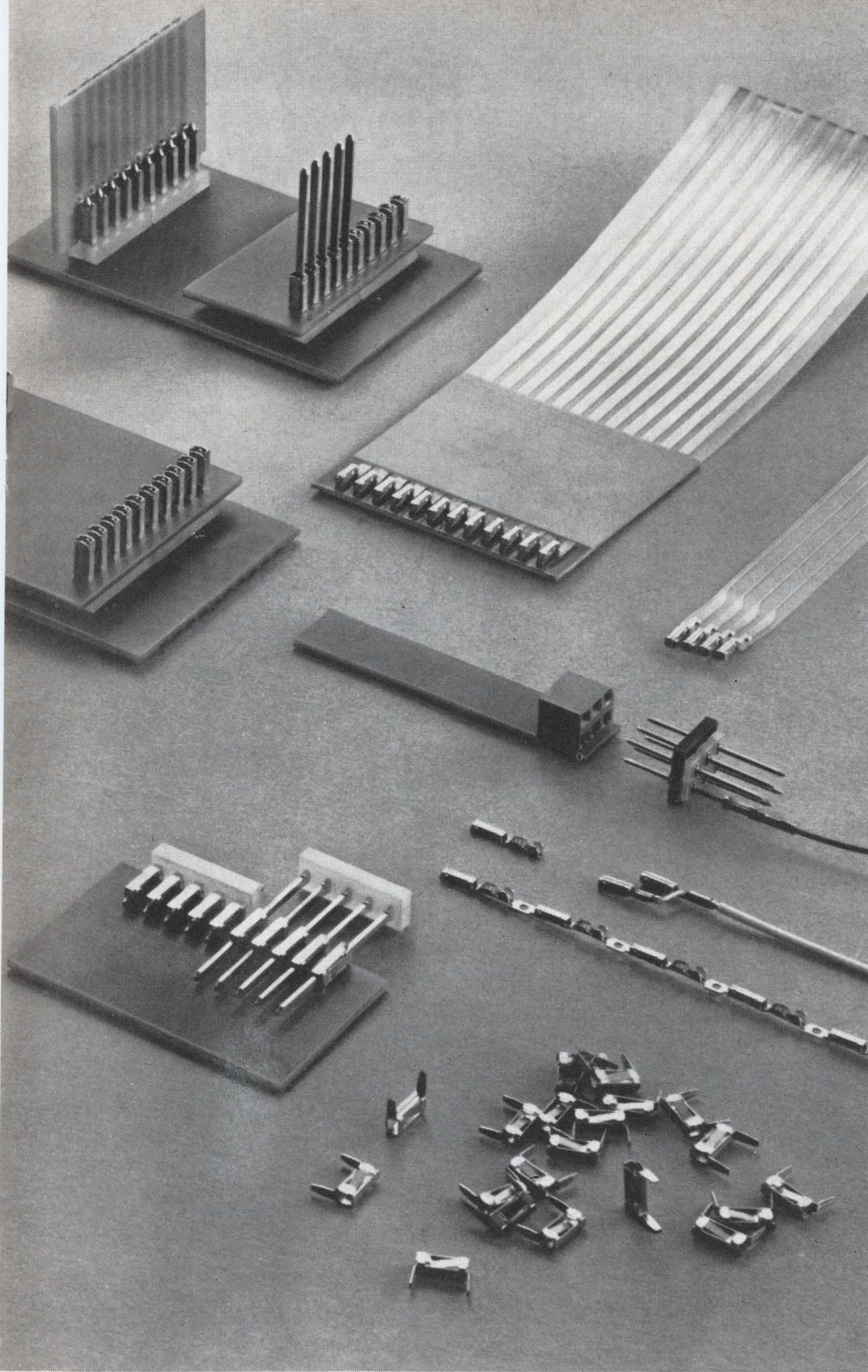
**ELECTRONIC DESIGN** is published biweekly by Hayden Publishing Company, Inc., 850 Third Avenue, New York, N. Y. 10022. James S. Mulholland, Jr., President. Printed at Poole Bros., Inc., Chicago, Ill. Controlled-circulation postage paid at Chicago, Ill., Cleveland, Ohio, and New York, N. Y. Application to mail at controlled postage rates pending at St. Louis, Mo. Copyright © 1967, Hayden Publishing Company, Inc. 61,945 copies this issue.



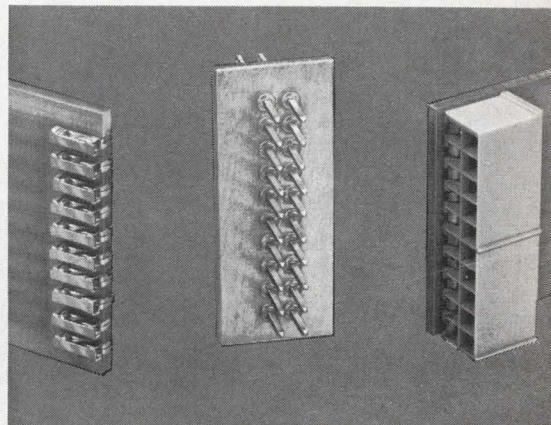
## Go modular the easy way

This entirely new approach to modularization is the AMPMODU\* Interconnection System. It permits almost unlimited design flexibility, high production speed, and economies resulting from automation and low per line cost.

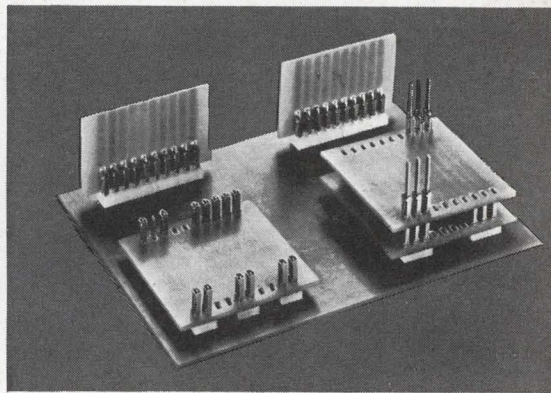
Specifically designed for modular applications using printed circuit boards, it enables mounting module cards at 90° to a mother board, stacking them, or putting them end to end. The female contacts may be staked directly to a printed circuit board or enclosed in molded housings. Male contacts may be staked directly to a printed circuit board, used in nylon incremental connectors, or mounted with nylon bushings in aluminum grid plates. Two sizes of contacts are available: the standard size, which uses .031 x .062" posts for mounting on .156" centers, and the miniature size, which uses .025 x .025" posts for mounting as dense as .100". Electrical and mechanical efficiency are enhanced by the simplicity of the female contact design, which includes dual cantilever-beam springs for redundant contact action and anti-overstress devices to ensure reliability. The long life of the phosphor bronze contacts is a result of AMP's special gold plating. New modular ideas don't have to dead-end at the design stage. For information on how you might use the AMPMODU Interconnection System to modularize your product and lower your costs, write us today.



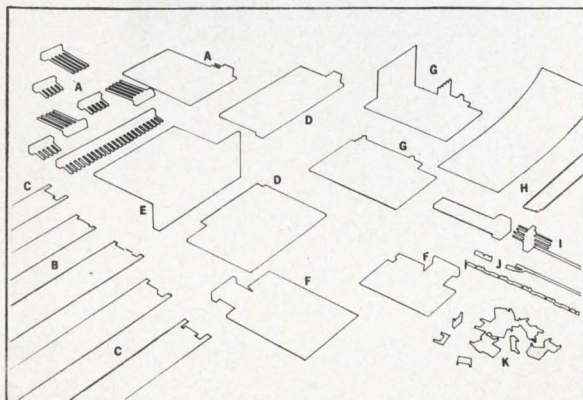
Automatic machines can stake contacts to printed circuit boards at rates of up to 1800 an hour



Miniature AMPMODU contacts may be mounted ten to the inch



The AMPMODU female contacts may be mounted in one of three ways for modular connection versatility



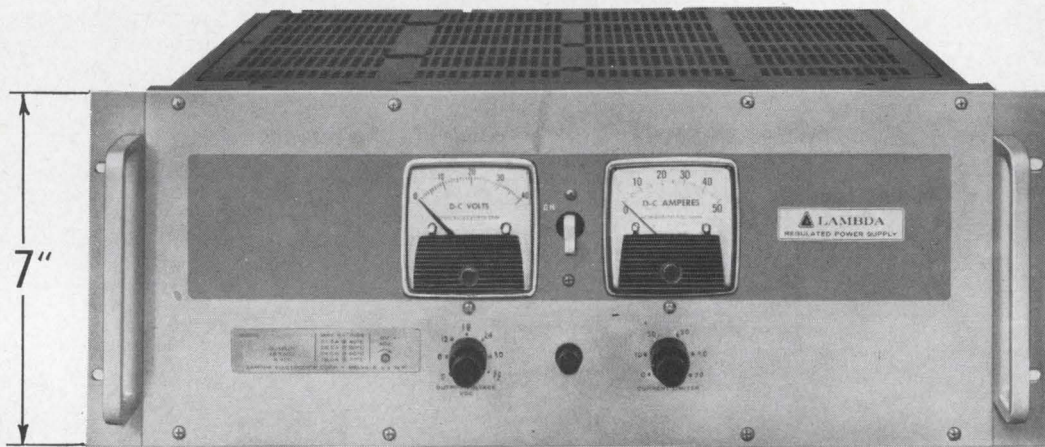
- A. AMPMODU Male Incremental Connectors
- B. Miniature AMPMODU Female Contacts in strip form
- C. Standard AMPMODU Female Contacts in strip form
- D. Miniature contacts in two-row housings
- E. Grid Plate Header
- F. Horizontally staked AMPMODU Contacts with incremental connectors
- G. Vertically staked AMPMODU Contacts
- H. Flexible tape cable AMPMODU Connectors
- I. Molded-in AMPMODU Pin Header and printed circuit board connector
- J. Miniature Crimp-Barrel AMPMODU Female Contacts
- K. Individual Standard AMPMODU Female Contacts

ON READER-SERVICE CARD CIRCLE 4

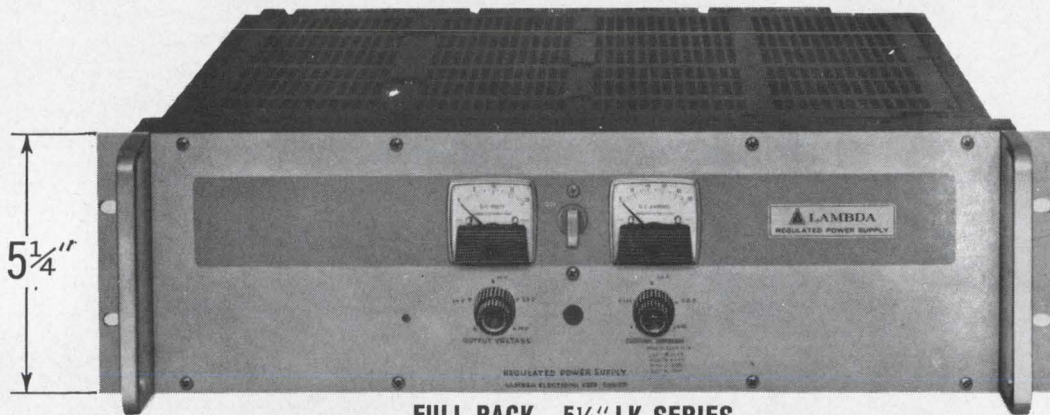
**AMP**  
INCORPORATED  
Harrisburg, Pennsylvania

# Only from Lambda — New 7-inch, broadest line of .015% regulated

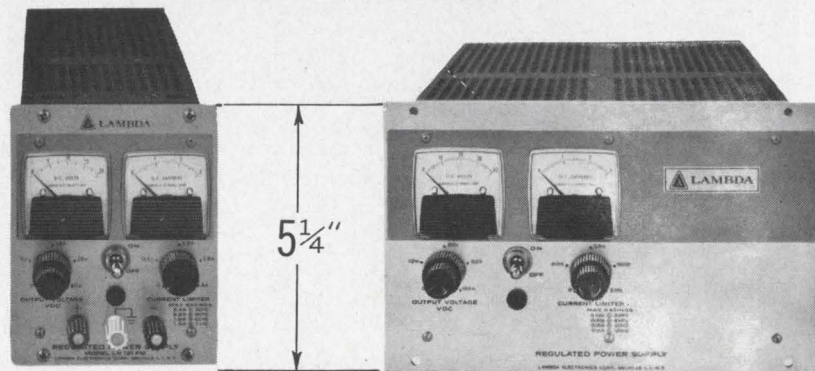
All convection cooled



FULL RACK—7" LK SERIES



FULL RACK—5 1/4" LK SERIES



1/4 RACK—LH SERIES

HALF RACK — LK SERIES  
LH SERIES





# high current models in the all-silicon power supplies

For test equipment and lab use—rack or bench  
 From 1/2 to 66 amps, 0-10, 0-20, 0-40, 0-60, 0-120 VDC  
 Full five year guarantee on materials and labor

## Features and Data

- Convection Cooled
- Remote Programming
- Remote Sensing
- Regulation—.015% or 1 MV (Line or Load)
- Temp. Coef. .015%/°C
- Transformer—designed to MIL-T-27 Grade 6
- Completely Protected—Short circuit proof—Continuously adjustable Automatic current limiting
- Constant I./Constant V. by automatic crossover
- Series/Parallel Operation

- No Voltage Spikes or Overshoot on "turn on", "turn off" or power failure
- Meet Mil. Environment Specs.  
 Vibration: MIL-T-4807A  
 Shock: MIL-E-4907A Proc. 1 & 2  
 Humidity: MIL-STD-810 Meth. 507  
 Temp Shock: MIL-E-5272C (ASG) Proc. 1  
 Altitude: MIL-E-4970A (ASG) Proc. 1  
 Marking: MIL-STD-130  
 Quality: MIL-Q-9858

- Ripple—  
 LK models—500  $\mu$ V RMS  
 LH models—250  $\mu$ V RMS, 1 MV P-P
- Wide Input Voltage and Frequency Range—  
 Models LK360-362FM: 200-250 VAC, 47-63 cps  
 Other LK models: 105-132 VAC, 47-63 cps  
 LH models: 105-135 VAC, 45-480 cps.
- LH models meet RFI Spec.—Mil-I-16910
- Rack Adapters  
 LRA-1—5 $\frac{1}{4}$ " Height x 16 $\frac{1}{2}$ " Depth (For use with chassis slides) Price \$60.00  
 LRA-2—5 $\frac{1}{4}$ " Height Price \$25.00

3 Full-rack Models — Size 7" x 19" x 18 $\frac{1}{2}$ "

Model <sup>2</sup>	Voltage Range	CURRENT RANGE AT AMBIENT OF: <sup>1</sup>				Price <sup>2</sup>
		40°C	50°C	60°C	71°C	
LK 360 FM	0-20VDC	0-66A	0-59A	0-50A	0-40A	\$995
LK 361 FM	0-36VDC	0-48A	0-43A	0-36A	0-30A	950
LK 362 FM	0-60VDC	0-25A	0-24A	0-22A	0-19A	995

3 Full-rack Models — Size 5 $\frac{1}{4}$ " x 19" x 16 $\frac{1}{2}$ "

Model <sup>2</sup>	Voltage Range	CURRENT RANGE AT AMBIENT OF: <sup>1</sup>				Price <sup>2</sup>
		40°C	50°C	60°C	71°C	
LK 350	0-20VDC	0-35A	0-31A	0-26A	0-20A	\$675
LK 351	0-36VDC	0-25A	0-23A	0-20A	0-15A	640
LK 352	0-60VDC	0-15A	0-14A	0-12.5A	0-10A	650

5 Quarter-rack Models — Size 5 $\frac{3}{16}$ " x 4 $\frac{3}{16}$ " x 15 $\frac{1}{2}$ "

Model <sup>2</sup>	Voltage Range	CURRENT RANGE AT AMBIENT OF: <sup>1</sup>				Price <sup>2</sup>
		30°C	50°C	60°C	71°C	
LH 118	0-10VDC	0-4.0A	0-3.5A	0-2.9A	0-2.3A	\$175
LH 121	0-20VDC	0-2.4A	0-2.2A	0-1.8A	0-1.5A	159
LH 124	0-40VDC	0-1.3A	0-1.1A	0-0.9A	0-0.7A	154
LH 127	0-60VDC	0-0.9A	0-0.7A	0-0.6A	0-0.5A	184
LH 130	0-120VDC	0-0.50A	0-0.40A	0-0.35A	0-0.25A	225

11 Half-rack Models — Size 5 $\frac{3}{16}$ " x 8 $\frac{3}{8}$ " x 15 $\frac{1}{2}$ "

Model <sup>2</sup>	Voltage Range	CURRENT RANGE AT AMBIENT OF: <sup>1</sup>				Price <sup>2</sup>
		30°C	50°C	60°C	71°C	
LH 119	0-10VDC	0- 9.0A	0- 8.0A	0- 6.9A	0-5.8A	\$289
LH 122	0-20VDC	0- 5.7A	0- 4.7A	0- 4.0A	0-3.3A	260
LH 125	0-40VDC	0- 3.0A	0- 2.7A	0- 2.3A	0-1.9A	269
LH 128	0-60VDC	0- 2.4A	0- 2.1A	0- 1.8A	0-1.5A	315
LH 131	0-120VDC	0- 1.2A	0- 0.9A	0- 0.8A	0-0.6A	320

Model <sup>2</sup>	Voltage Range	CURRENT RANGE AT AMBIENT OF: <sup>1</sup>				Price <sup>2</sup>
		40°C	50°C	60°C	71°C	
LK 340	0-20VDC	0- 8.0A	0- 7.0A	0- 6.1A	0-4.9A	\$330
LK 341	0-20VDC	0-13.5A	0-11.0A	0-10.0A	0-7.7A	385
LK 342	0-36VDC	0- 5.2A	0- 5.0A	0- 4.5A	0-3.7A	335
LK 343	0-36VDC	0- 9.0A	0- 8.5A	0- 7.6A	0-6.1A	395
LK 344	0-60VDC	0- 4.0A	0- 3.5A	0- 3.0A	0-2.5A	340
LK 345	0-60VDC	0- 6.0A	0- 5.2A	0- 4.5A	0-4.0A	395

<sup>1</sup> Current rating applies over entire voltage range.  
<sup>2</sup> Prices are for non-metered models (except for models LK360FM thru LK362FM which are not available without meters). For metered models, add suffix (FM) and add \$25 to price of LH models; add \$30 to price of LK models.  
<sup>3</sup> Overvoltage Protection: add suffix (OV) to model number and add \$60 to the price of LH models; add \$70 to price of half-rack LK models; add \$90 to price of 5 $\frac{1}{4}$ " full-rack LK models; add \$120 to price of 7" full-rack LK models.  
<sup>4</sup> Chassis Slides for full rack models: Add suffix (CS) to model number and add \$60 to the price.

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# Are you sure you can't afford Heinemann circuit breakers?

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We really are trying to meet you half-way. We've gone to a lot of trouble to produce a breaker which would lower the price barrier without lowering our standards.

The result is our little Series JA breaker. It has all of the advantages inherent in hydraulic-magnetic operation, all of the features of our larger, more expensive models. But it's priced to make new friends out of passing acquaintances.

In quantities of just six to twenty-five, OEM's can buy this breaker for a nickel more than four dollars. And of course, as the quantity goes up, the price goes down even lower.

The JA is our idea of meeting you half-way. If you'd like to learn more about it, or any of our other breakers, drop us a line. We'll be happy to send you more complete information.

Heinemann Electric Co., 2616 Brunswick Pike,  
Trenton, N. J. 08602.



# HEINEMANN



ON READER-SERVICE CARD CIRCLE 6

# THESE LITTLE ERIE EMI FILTERS

ARE RESPONSIBLE FOR FILTERING  
OUT NOISE IN THE GUIDANCE SYSTEM . . .



... ABOARD GRUMMAN'S LUNAR MODULE

## ERIE — GRUMMAN'S CHOICE FOR EMI FILTERS

These superior EMI FILTERS passed Grumman's critical qualification requirements — including random vibration and high transient withstanding capability. Most of these very small filters weigh less than 10 grams, and their inherent reliability make Erie a natural selection as Grumman's filter source.

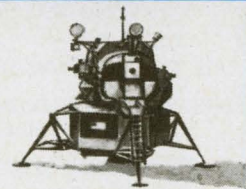
**Bonded Filter Stock** . . . inventories under lock and key in our Quality Control Department . . . is available for LM subcontractors or for other critical programs requiring Established Reliability Filters.

The typical 100 Vdc rated Erie Filter will provide an insertion loss of 67 db @ 150 kHz. A broad line of ERIE FILTERS is available — including MULTIPLE SECTION FILTERS and special configurations for STRIP LINE applications. Custom filters for your applications can be designed. Why not call in an Erie Filter specialist for *your* project?



Write for new catalog 9000 . . . ERIE ELECTRONIC FILTERS

Another Series of Components in Erie's Project "ACTIVE"  
Advanced Components Through Increased Volumetric Efficiency



ERIE

TECHNOLOGICAL

PRODUCTS, INC.



Erie, Pennsylvania

ON READER-SERVICE CARD CIRCLE 7

# Did You Know Sprague Makes 51 Types of Foil and Wet Tantalum Capacitors?

## FOIL-TYPE RECTANGULAR TANTALEX® CAPACITORS



Type 300D polarized plain-foil  
Type 301D non-polarized plain-foil  
Type 302D polarized etched-foil  
Type 303D non-polarized etched-foil

ASK FOR BULLETIN 3650

ON READER-SERVICE CIRCLE 162

## FOIL-TYPE TANTALUM CAPACITORS TO MIL-C-3965C

CL20, CL21 tubular 125 C polarized etched-foil  
CL22, CL23 tubular 125 C non-polar etched-foil  
CL24, CL25 tubular 85 C polarized etched-foil  
CL26, CL27 tubular 85 C non-polar etched-foil  
CL30, CL31 tubular 125 C polarized plain-foil  
CL32, CL33 tubular 125 C non-polar plain-foil  
CL34, CL35 tubular 85 C polarized plain-foil  
CL36, CL37 tubular 85 C non-polar plain-foil  
CL51 rectangular 85 C polarized plain-foil  
CL52 rectangular 85 C non-polar plain-foil  
CL53 rectangular 85 C polarized etched-foil  
CL54 rectangular 85 C non-polar etched-foil

ON READER-SERVICE CIRCLE 163

## 125 C FOIL-TYPE TUBULAR TANTALEX® CAPACITORS

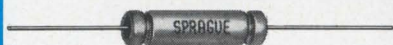


Type 120D polarized plain-foil  
Type 121D non-polarized plain-foil  
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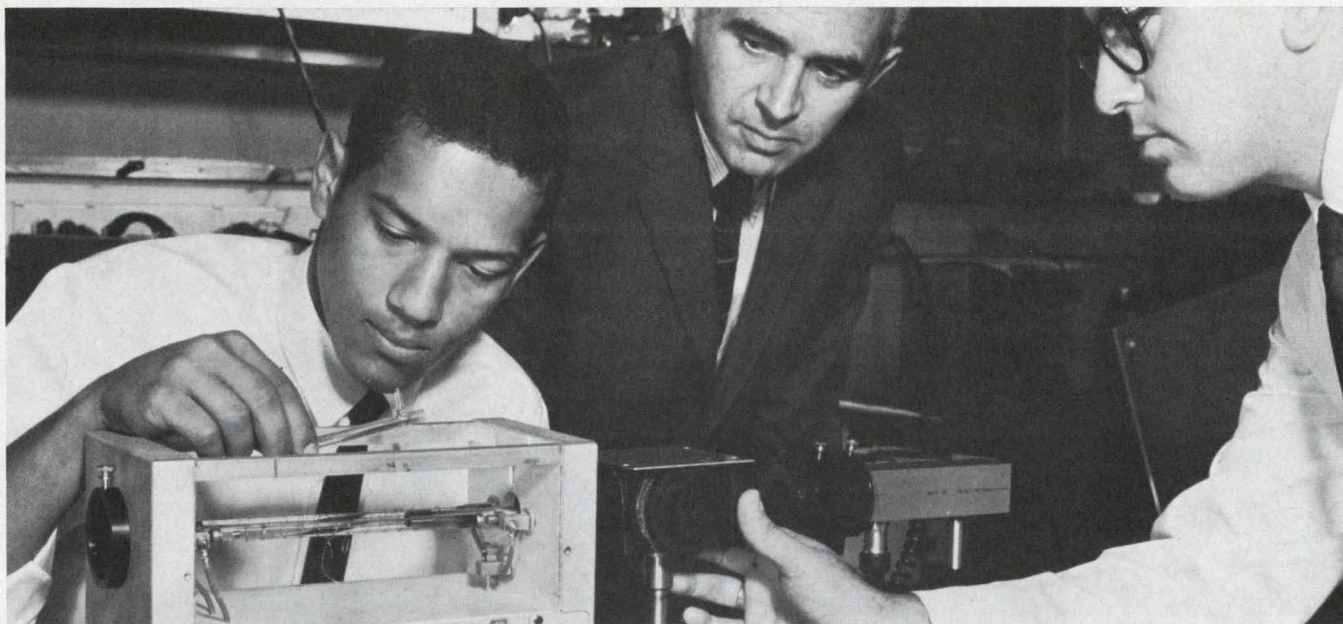
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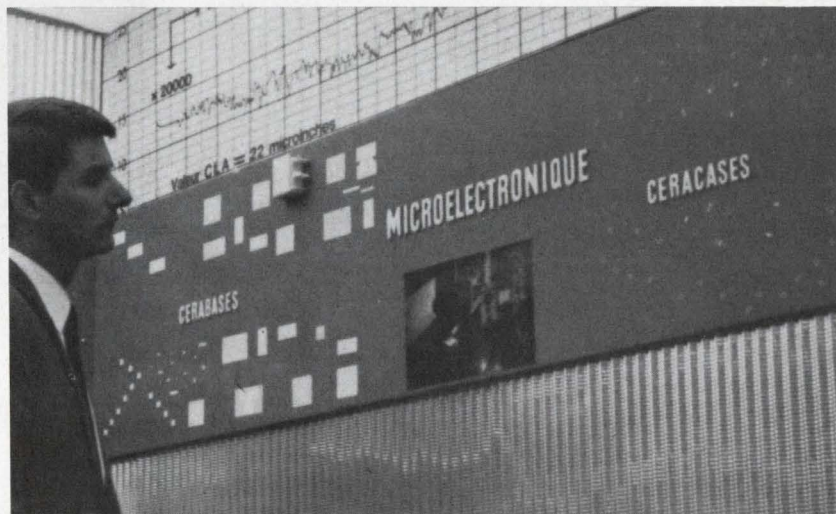
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# News

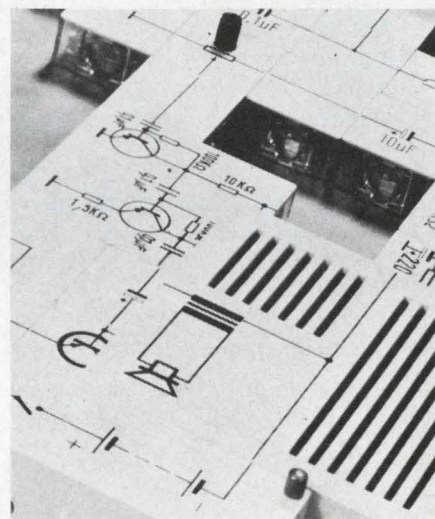


Laboratory liquid lasers open new vistas for communications and biological research.

Here a device is placed in a flash tube that pumps it to a 1-MW energy burst. Page 17



Europe's dependence on U.S. electronics expertise—and its reaction—evident at Paris components show. Page 24



'Domino' modules help the study of electronics. Page 33

## Also in this section:

Electronic robots simulate patients' conditions as medical training aid. Page 38

Complementary MOS arrays about to be marketed. Page 21

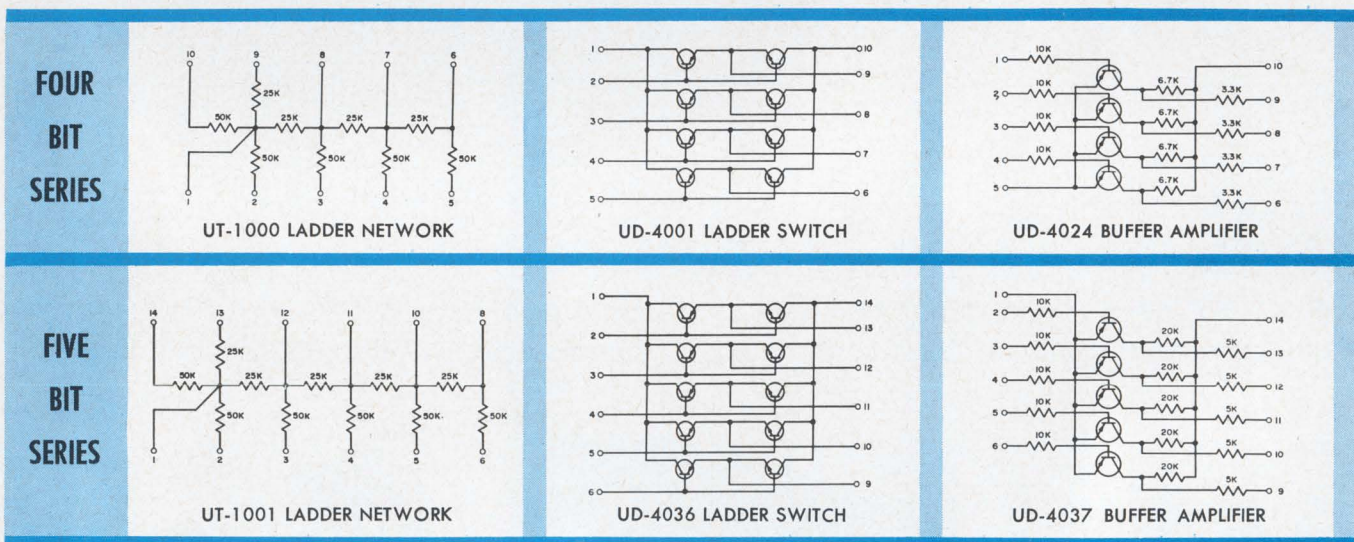
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ON READER-SERVICE CARD CIRCLE 8

# NASA and contractor take blame for Apollo Fire

The massive 3000-page final report issued earlier this month on the tragic Apollo accident appears to have raised more questions than it answered.

Though the specific cause of the tragedy may never be known, the report did reveal many problems of a technical as well as a managerial nature which, many observers feel, could seriously affect the nation's \$23 billion Apollo project.

In their testimonies before Congressional investigating committees, officials of the National Aeronautics and Space Administration and of North American Aviation, Inc., the Apollo spacecraft manufacturer, conceded that they were both blameworthy for the accident and agreed generally with the board's findings.

James E. Webb, NASA Administrator, told sharply critical Congressional investigators that the men of the Apollo project could correct their errors and reach their goal of placing a man on the moon by 1970. He suggested, however, that the review board may have "overstated the case" against Apollo.

North American executives defended their quality control procedures and denied charges that there had been deficiencies in the electrical wiring design, though they admitted that the company had not de-

signed the cockpit to guard against a fire on the ground.

The special eight-man Accident Review Board identified, in their report, the probable cause of the fire as Teflon insulation in a power cable near the environmental control unit. Repeated opening and closing of a compartment door may have worn the wire thin, they said.

Although the board was unable to determine the specific initiator of the Apollo fire, it identified the conditions which it felt led to the disaster. These were:

- A sealed cabin, pressurized with an oxygen atmosphere.
- An extensive distribution of combustible materials in the cabin.
- Vulnerable wiring carrying spacecraft power.
- Vulnerable plumbing carrying a combustible and corrosive coolant.
- Inadequate provisions for the crew to escape.
- Inadequate provisions for rescue or medical assistance.

The board concluded that "in its devotion to the many difficult problems of space travel, the Apollo team failed to give adequate attention to certain mundane but equally vital questions of crew safety."

The investigation revealed "many deficiencies in design and engineering, manufacture and quality control."

The board reported that it found "numerous examples of poor installation, design and workmanship in the wiring." For instance, it cited a wrench socket found among some cabling in the spacecraft.

The report gave a wide sampling of problems and shortcomings with the Apollo program in support of its conclusions. Typical of those cited were these three:

■ A NASA memorandum issued in September 1966 during mating of the command module with the service module which stated: "Many open design change orders were completed and various malfunctions were noted and corrected. . . ."

■ A manned test with flight crew which was initiated soon afterwards but was discontinued after reaching a simulated altitude of 13,000 feet because of failure of a transistor in a spacecraft inverter.

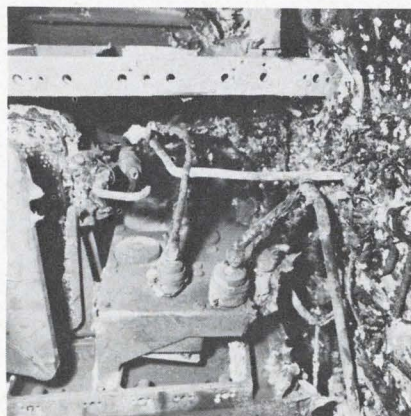
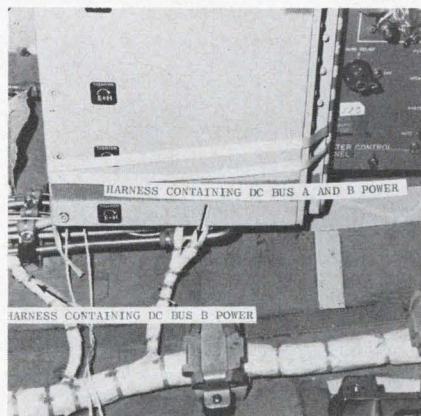
■ A second manned altitude test which was discontinued when a failure occurred in an oxygen system regulator.

The review board concluded its report with a long list of recommendations, some of which the space agency is already reported to be implementing. A new quick-release hatch is on the drawing boards. More fire-resistant materials will be substituted for nylon, where it was used, and they will be located at a safe distance from potential ignition sources.

## French color-TV tube challenges shadow mask

The French are confident that they have come up with a new color-TV tube that will replace the shadow-mask tube in worldwide color set manufacture. It uses a grille of vertical wires and color stripes, rather than dots, to produce color pictures. The wire-grille tube takes one-third the power of the shadow-mask, and thus lends itself well to transistorized design.

The developer of the tube, CFT (Compagnie Française de Télévision)—which also developed SECAM, the French color-TV transmission system—showed a transistorized prototype in operation at its laboratories in Lavellois, near Paris, during the International Components Exhibition, April 5-10. The set produced bright, high-quality pictures



Apollo environmental control unit where fatal fire may have broken out.

# News Scope

CONTINUED

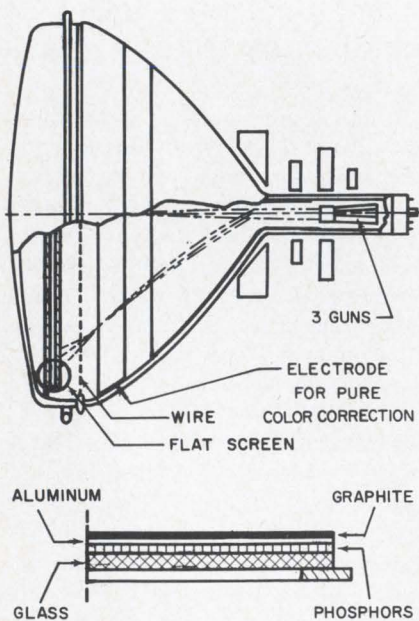
in a well-lighted room.

Several other advantages of the tube were cited during the demonstration by André Fouquier, one of the engineers on the CFT team that developed the tube. These include:

- Simple production.
- Flat screens.
- Brighter pictures.
- Use of the same glass as for black-and-white tubes, rather than special glass as the shadow-mask requires.

Since CFT is only an R&D laboratory, it will license manufacturers to make the tube. Already a pilot plant has been sold to the Soviet Union, although the Russians are using the shadow-mask tube for initial color-set production. The French company hopes to get an American licensee to supply the U.S. market; talks are in progress although the company declines to discuss details.

The tube is a 3-gun type with a series of 550 thin stainless-steel wires strung side by side vertically between the guns and the screen. The wires are 0.1 mm in diameter and are spaced 0.75 mm apart. The phosphors are coated on the screen in vertical stripes. There are 480 groups of three color stripes—in blue-green-red sequence—coated on the screen with no spacing between them. Each of these color stripes is



Color-TV tube contains flat screen and three guns.

0.27 mm wide.

This vertical striping gives the viewer a picture with vertical lines rather than the familiar horizontal pattern. At full brightness no horizontal scan pattern was visible at all, although scanning is done in the normal horizontal manner. At low beam currents, the horizontal pattern begins to be visible, but this would not occur normally.

Voltages for the CFT transistorized set are 25 kV for the screen, 7500 volts for the grid, and 8 kV for the last electrode of each electron gun, according to François Dognin, the engineer who designed the set. He showed that at full brightness the three guns were draining only 100  $\mu$ A. The tube draws a mean value of about 88 watts from the mains, he said, compared with 350-400 watts for a shadow-mask set.

Key to the low power requirements is the high transmissibility of the mesh. It is about 80% transparent to the beams.

In production the grilles and screens can be made separately, and then any mesh used with any screen. In the shadow-mask tube, matching of mask and dot-pattern on the screen is critical. Alignment of the mask and screen is also simpler in the CFT tube, according to Fouquier, because it has to be done in only the vertical plane. The wires are bonded into the tube envelope between two glass surfaces.

One problem the tube does not eliminate is achieving wider deflection angles, and thus a shorter tube. This tube would run into convergence problems just as the shadow-mask would, according to Fouquier.

## GE enters market for linear ICs

General Electric Co. has revealed that this year it will begin selling off-the-shelf, low-cost, plastic linear integrated circuits. This was disclosed in the company's announcement of a multimillion-dollar program to accelerate development and manufacture of integrated circuits. Hitherto the company has manufactured ICs only for internal use and in limited quantities for special orders.

The program includes establishment of an Internal Integrated-Circuit Center to fill the research and

development needs of General Electric's electronic equipment manufacturers. The company will also expand the development and manufacturing capabilities of its Semiconductor Products Dept.

The Internal Integrated-Circuit Center (IICC) will be an organizational part of the company's Research and Development Center, headquartered in Schenectady, N. Y. It will, however, be located at GE's Electronics Park in Syracuse, N. Y. The expanded facilities of the Semiconductor Products Dept. will be added to existing integrated-circuit activities at Electronics Park. The department is responsible for innovations and development in inexpensive electronic devices.

Several GE consumer products paved the way for this expansion, according to a company spokesman. A micro-circuit clock-radio with a built-in battery charger was announced last year. A portable stereo phonograph and a recent stereo tape cartridge player have proved the flexibility of the integrated-circuit approach to entertainment products, he said. A zero-voltage switching IC for application in electric heating has also been announced recently.

## Army moves to adopt computer-aided design

Computer-aided circuit design is likely to become a standard Army engineering tool, according to a Pentagon spokesman. Lt Col. Daniel J. Walsh of the Army Office of the Chief of Research and Development said that the move would probably accompany the Army's adoption of large-scale integration.

He told a NASA seminar at MIT that the Army was already putting computer-aided design to extensive use in a number of applications:

- ECAP, NET-1 and CIRCUS programs are in use at the Redstone Laboratories, Huntsville, Ala., in the analysis of the effects of radiation on electronic circuitry.

- SCEPTRE is being investigated by the Nuclear Engineering Directorate at Picatinny Arsenal, Dover, N. J., for use in the safety analysis of solid-state circuits.

- NET-1 is being applied to synthesizing uhf switching circuits as part of an optimization program at Fort Monmouth, N. J.



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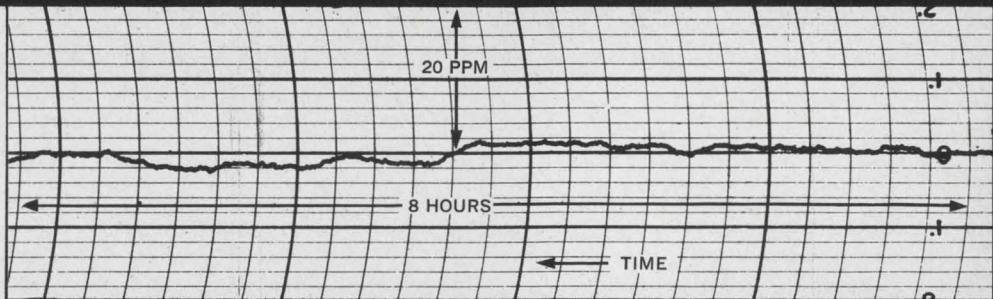
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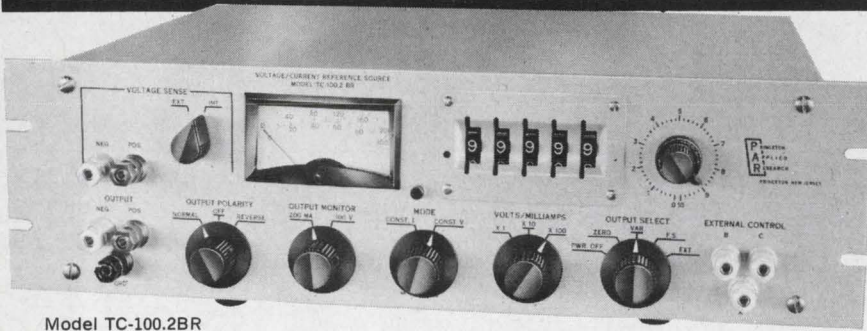
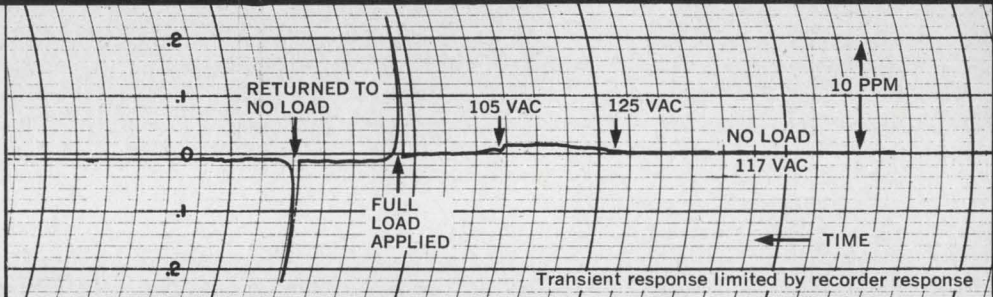
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# Liquid lasers for high-power cw operation sought

## Wider pulsed applications and such laboratory features as 'tunable' colors are also investigated

Richard N. Einhorn  
News Editor

The search for new laser materials has been going on ever since Theodore H. Maiman developed the first working model of a laser in 1960. Solids, gases, plasmas, semiconductors, plastics—all have been tried with varying degrees of success. Liquids, too, have been used, and, in the opinion of some scientists, liquid lasers offer the greatest potential for high-power, continuous operation. But other applications are being studied, too.

Two recent developments in liquid-laser technology have been announced by major companies.

In the first, General Telephone and Electronics Laboratories, New York, unveiled an experimental device using a class of chemicals not previously tried as a lasing medium. Its laser is capable of producing a 1-MW burst that lasts a fraction of a microsecond. Researchers hope ultimately to achieve continuous operation at high power for communications applications.

The second was the disclosure by the Research Div. of the International Business Machines Corp., Yorktown Heights, N. Y., of a rapidly pumped liquid laser that can radiate four colors, one at a time, through the routine substitution of one solution of organic dye for another in the laser cell. The previous color literally goes down the drain. In principle, this offers a useful source of all wavelengths in the visible-infrared spectrum for laboratory work.

### Liquids may best solids

Why the interest in liquids? Well, the energy output of a laser is a function of the volume of the active medium. The larger the lasing medium, the greater the ultimate energy output. Since liquid lasers can be made in lengths far exceeding those of crystalline lasers, the ultimate energy output of the liquid laser is expected to be higher. But there are other advantages as well.

Take solids. To get solid-state

lasers to function, an almost perfect glass is needed, for example. It must be free from strains or distortions, and it must possess a uniform refractive index. Even a slight imperfection might ruin it for laser purposes, because of erratic operation and shortened lifetime.

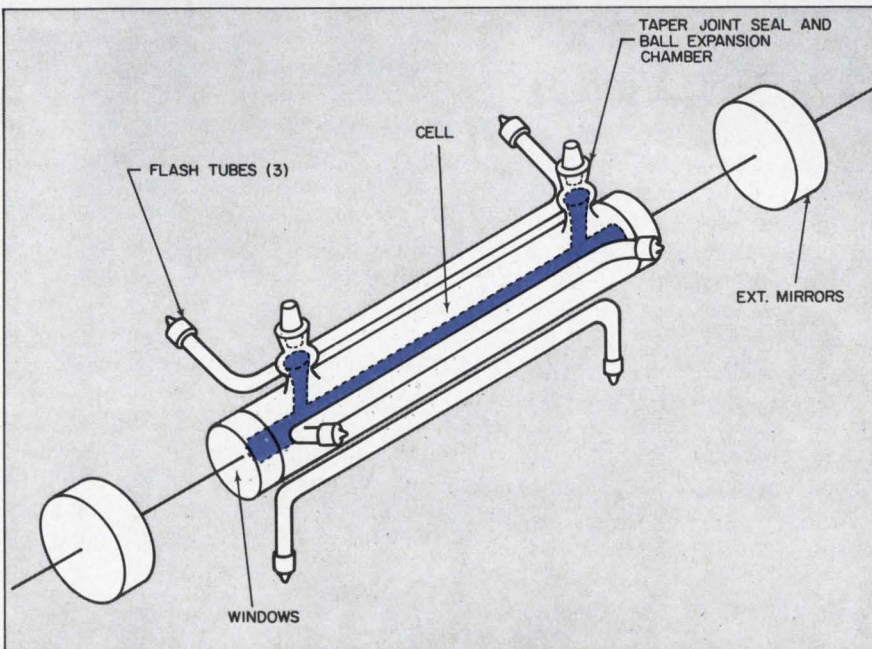
In high-power operation, rubies and other crystals often fail catastrophically when subjected to the massive internal scattering that accompanies laser action. The heat causes cracking and sometimes explosions of the crystal or glass. In liquid lasers, on the other hand, circulation of the liquid could remove heat and thereby permit continuous operation. Even without circulation the liquid can restore itself during pulsed operation.

Liquid lasers have the potential of constant optical character. They are about as good as gas lasers in spatial coherence and beam divergence. They are not readily degraded. Even if the lasing solution decomposes or is contaminated, it can be purified by circulation through a bladder-like device. Or, if a nonlasing peroxide should form because of exposure to air, oxygen can be driven off by heating in the dark.

Still another benefit is the economy of producing liquid lasing materials. Fabricating a perfect glass rod a foot or more in length is a major undertaking that costs thousands of dollars. Solid-state crystal lasers require a laborious, expensive growing process. By way of contrast, liquids can be prepared in a few minutes in the laboratory.

### First liquid laser used chelate

The first successful demonstration of a liquid laser was reported in 1963 by Alexander Lempicki and Harold Samelson of General Telephone and Electronics Research Laboratories. Acting on the 1958 theoretical prediction of Charles H. Townes and Arthur L. Schawlow that it should be possible to build a laser using +3 ions of the rare-earth element europium, Lempicki and Samelson proceeded to do just that. However, they introduced a



1. Energies of 1 MW have been achieved in liquid laser by General Telephone scientists. Three flash tubes activate a lasing solution in a cell only 6 inches long. The medium is a rare earth in a heavy inorganic solvent.

*(liquid lasers, continued)*

new wrinkle: they dissolved europium benzoylacetonate in an alcohol solution. Townes and Schawlow had had a solid in mind.

This material is known as a chelate—a compound of a rare earth in an organic solvent. Unfortunately, chelate lasers were limited in performance because the light atoms of the chelate absorb much of the energy.

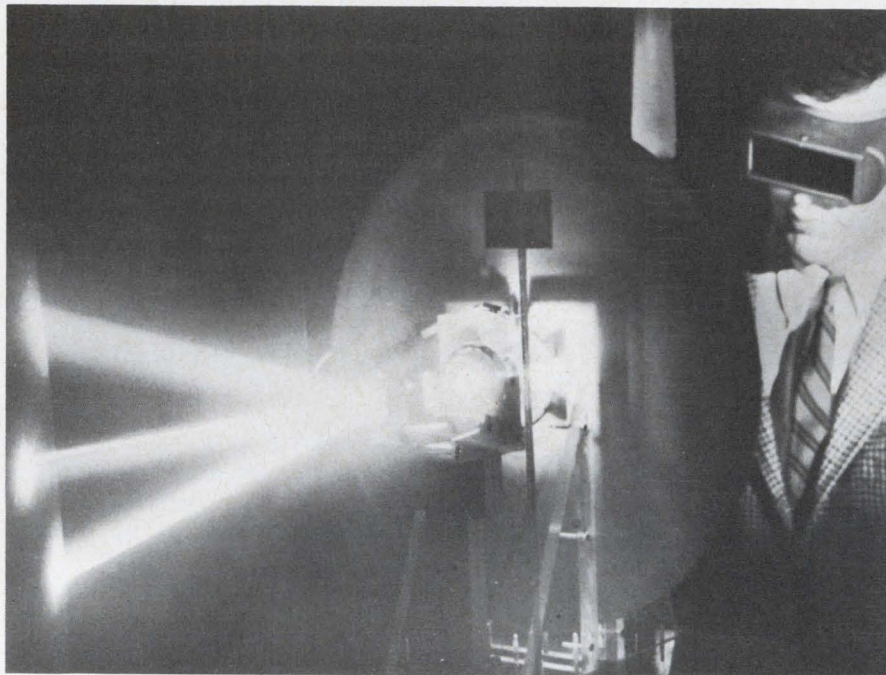
Recently scientists at General Telephone and Electronics Laboratories improved upon their pioneering efforts. Lempicki and Adam Heller evolved a liquid laser in which the active medium is formed by dissolving neodymium, a rare earth, in selenium oxychloride, an inorganic compound. The advantage lies in the absence of atoms of low mass. This greatly increases efficiency, because the neodymium ions are more likely to emit photons, which are discrete quanta of light energy, than to dissipate their energy in heating the solvent. The new approach is not limited to these specific chemicals. Conceivably a whole new family of liquid lasers could arise in which the active medium would be a combination of rare-earth ions and heavy-atomic-weight solvents.

Already Lempicki and Heller have achieved energy bursts of 1 MW peak—approximately 100 times greater than the output of previous liquid lasers—but only for a fraction of a microsecond. Still, they claim to have the first liquid laser that is competitive with solid lasers.

### Engineering problems loom

High-power, continuously operating liquid lasers, however, are not imminent. Says Lempicki: "There are both fundamental and engineering problems to be solved before continuous liquid lasers can be developed. From the point of view of efficiency of the medium itself, it (the neodymium-selenium oxychloride solution) is a completely satisfactory material. But no one has come up with a really good method for handling the liquids.

"There are serious engineering problems in the circulation. The li-



2. High-speed flash lamp is the key to IBM liquid laser that varies color of beam simply by flushing cell and introducing different organic dye solution.

uid is quite corrosive and requires the development of a special pump."

The compound is indeed chemically stable. At the recent IEEE International Convention the laser was flashed more than 500 times for curious engineers, and at the end the liquid was just as good as at the beginning.

The device operates most effectively at room temperature or slightly above it. Its properties are affected only by variations in temperature, not by elevated temperature per se. Circulating the fluid would maintain uniform temperature, but this, of course, would require the special pump that Lempicki mentioned.

"One of our objectives is to build a laser which will pulse 20 times a second," he says, "but for high repetition rate you must have circulation of the lasing liquid." In its present version, with stationary fluid, the laser is flashed once a minute.

### Communications use desired

The application for a continuously operating liquid laser would be obvious: communications. A continuous laser beam is theoretically

capable of accommodating a great many telephone conversations, as well as business data and television data. It is particularly well suited to space communications.

"If we had a continuous laser, we would definitely try to use it for communications," Lempicki says. "However, we are also working on pulsed lasers for special communications, such as for the Air Force."

At present the device works at a wavelength of 1.06 microns, which lies within the infrared region. This is not unlike glass lasers.

When asked whether devices of this type could work in the visible spectrum, Lempicki replied, "We have not done this yet. Offhand, there is no fundamental reason why it shouldn't be possible to do this."

The General Telephone laser (Fig. 1) uses commercially available flash tubes to activate the lasing medium. Input energy required is about the same as that for a solid-state or glass laser of comparable size.

Extensive research would be needed before laser communications links could become a reality. But General Telephone's development is a significant step forward.

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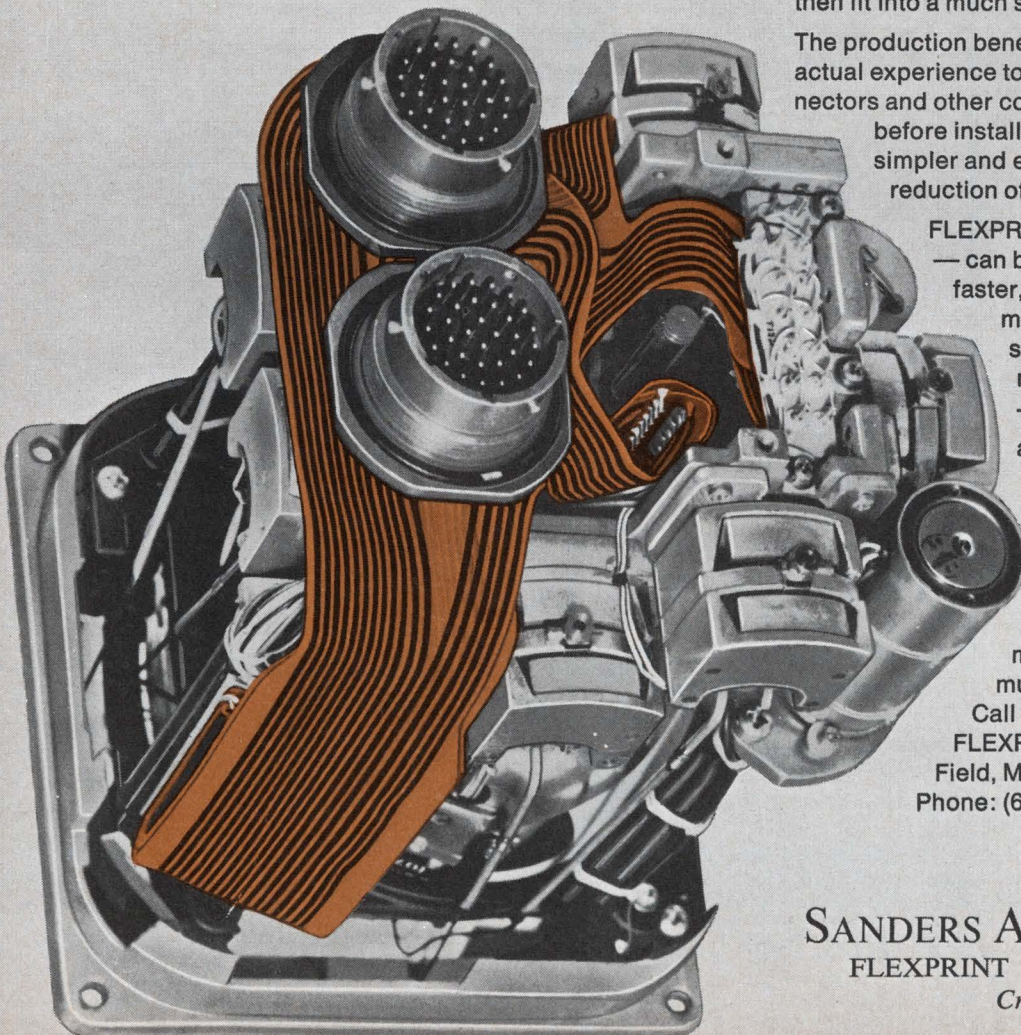
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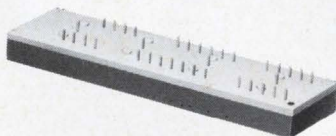


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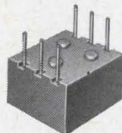
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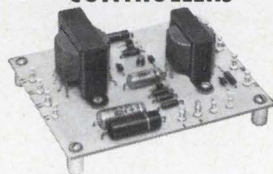
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NEWS

(liquid lasers, *continued*)

liquid lasers, and other configurations as well. For example, Bell Telephone Laboratory scientists make incidental use of liquid media for frequency-mixing experiments.

**Organic dyes change beam color**

A completely different tack has been taken by Peter P. Sorokin and J. R. Lankard of the IBM Research Div. They have developed a compact, conveniently operated device that may well provide energy at almost every wavelength in the visible-infrared spectrum. The basic idea is to substitute organic dyes in a range of colors to fill the spectrum. The color of the beam is changed simply by flushing the cell and refilling it with another dye.

Following the unsuccessful attempts of others, these two men observed lasing action in organic dyes in 1966. In their initial experiments, however, they had to pump the active medium with a giant pulsed-ruby laser. This was expensive and cumbersome, and no wavelengths shorter than the ruby's could be produced without complex frequency-doubling techniques.

Sorokin and Lankard learned to circumvent this by observing the properties of the organic dyes. They came to the conclusion that earlier experiments using flashlamps as laser pumps had failed because there had been no control over occurrence of the giant pulse. Intense flashlamps with slow rise times tended to introduce more loss than gain because of inductance effects. Since flashlamps were rich in energy throughout the infrared and visible spectrum, they would, however, be an ideal source.

Sorokin and Lankard proceeded to develop a flashlamp with a rise time measured in nanoseconds. The new laboratory device consists of an active laser cell, a flashlamp that surrounds the cell and a disk-shaped discharge capacitor (Fig. 2).

The cell that contains the liquid is a quartz tube with polished ends. This is surrounded by a second quartz cylinder. The flashlamp discharges into the space between the two cylinders. The capacitor is a

thin disk mounted coaxially with the two cylinders. A copper conducting sleeve fits over the outer cylinder to form a path to the two end electrodes. This configuration lowers lamp inductance, thereby contributing to a sharper rise time for the pumping pulse.

To date, Sorokin and Lankard have successfully produced lasing in four different fluorescent organic dyes of the xanthene family. They have observed green, yellow, orange and red. Sorokin says that there is no theoretical reason they cannot reproduce all the wavelengths in the visible-infrared spectrum.

### Multicolor for biological research

One use to which the IBM laser may be put is as a laboratory tool for cell biology.

"The different components of a cell, which in turn have different functions, often have the property of being stained with different dyes," Sorokin explains. "When a given component takes up a dye, you can selectively destroy it by pulsing it with a laser frequency that coincides with the dye absorption spectrum. You can study the cell for a few minutes to discover how it functions without the de-

stroyed component."

Microphotographers have already used ruby lasers, but the IBM laser is more widely useful because the experimenter can run through the spectrum until every component has been tested. Sorokin uses the term "tunability" in order to describe the usefulness of the dye-substitution method.

Tunability is not an idly chosen word. In addition to gross changes in color, the emission band of any one dye can be shifted at least 600 Å by changing the concentration of the dye.

Other applications for this laser might be in aircraft, beacons and for satellite-tracking, Sorokin points out. It is compact and inexpensive to make and it can be designed for high repetition rates.

The optical properties of this laser more closely resemble those of a solid laser than of a gas laser. Since alcohol is commonly used in the solvent, the swirling action must be allowed to settle after the flash. There is an initial decrease in power after flashing, but this tends to stabilize.

### IBM laser does not operate cw

Unlike the General Telephone and

Electronics laser, the IBM device is not expected to serve in continuous operation.

"It will not have the brute continuous power or duty cycle of a carbon dioxide laser, but it will give off 1-MW pulses," Sorokin says.

The device is scaled down in power from a ruby laser. With an input energy of 50 joules, the output is 0.2 joule—an efficiency of 0.4%. However, this was achieved with air as the pumping gas. Sorokin sees no difficulty in achieving 1% efficiency with xenon.

By way of comparison, Bell Telephone Laboratories cites 0.1% for helium-neon lasers at 0.2 watts in continuous operation. YAG (yttrium-aluminum-garnet) solid lasers operate at 1% efficiency at 25 watts continuous. But YAG lasers are limited to the kilowatt range for pulsed operation, whereas the liquid devices mentioned have megawatt potentialities.

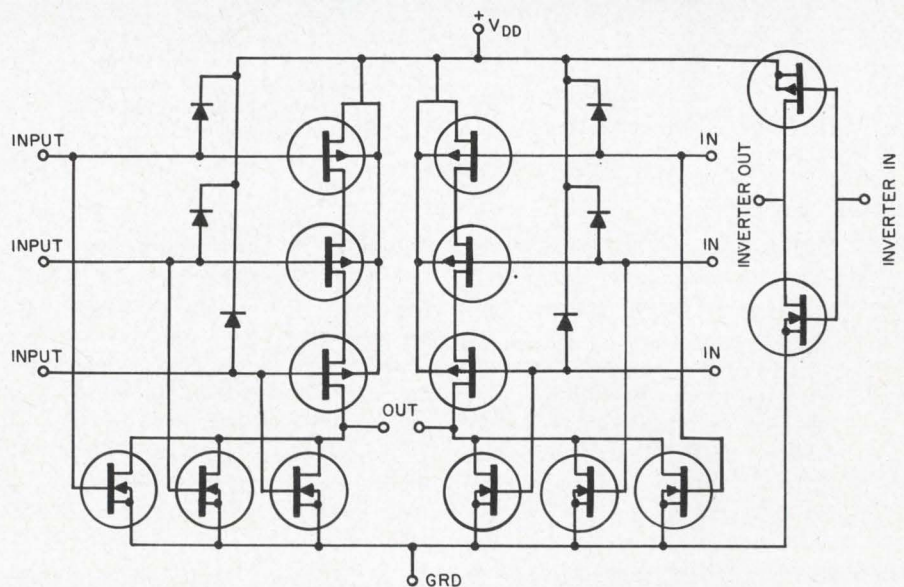
The future of liquid lasers, like that of all other types, is problematical. Sorokin points out that the entire laser technology is less than seven years old.

"Liquid lasers just open one more class. Whether they are any better or any worse than the others remains to be seen," he comments. ■ ■

## Complementary MOS arrays going to market

There are two ways to achieve high-speed switching (above 2 GHz) at extremely low-power dissipation with MOS logic arrays: use either four-phase logic or complementary MOS arrays.

RCA feels that the processing problems associated with the diffusion of complementary MOS transistors are not very serious and that it is easier to overcome them than to put up with the disadvantages of operating four-phase logic. Four-phase, says RCA physicist Dr. Richard Ahrons, is only suitable for ac logic: the clock must be running and data must be moving through the system at all times. Complementary MOS transistors can perform static logic as well as ac logic. RCA will market a complementary MOS dual-input NOR gate in June. ■ ■



Current cannot flow directly to ground in this complementary MOS array.

It dissipates 10 nanowatts when idle and 400 microwatts at 100 kHz.

## Semiconductor sets charges off safely

A detonator that exploits the thermal-runaway characteristics of semiconductors has been developed by the Sandia Corp., Albuquerque, N. M. The device is said to provide an extremely reliable means of detonation.

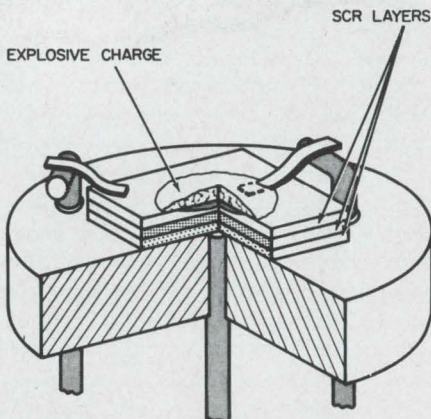
Thermal runaway is obtained by applying the energy signal and the control signal simultaneously. This is ordinarily bad practice in semiconductor design, because resistance decreases, current flows more heavily and the temperature at the main pn junction rises. But in the new detonator the resultant heat is used to set off the explosive charge.

Since this device requires coincidence of two signals, it is far less susceptible to accident than bridge wires or resistance wires, which can be activated by human error, circuit malfunction or radiation fields. An even greater margin of safety can be built in by using three or more signals, Sandia says.

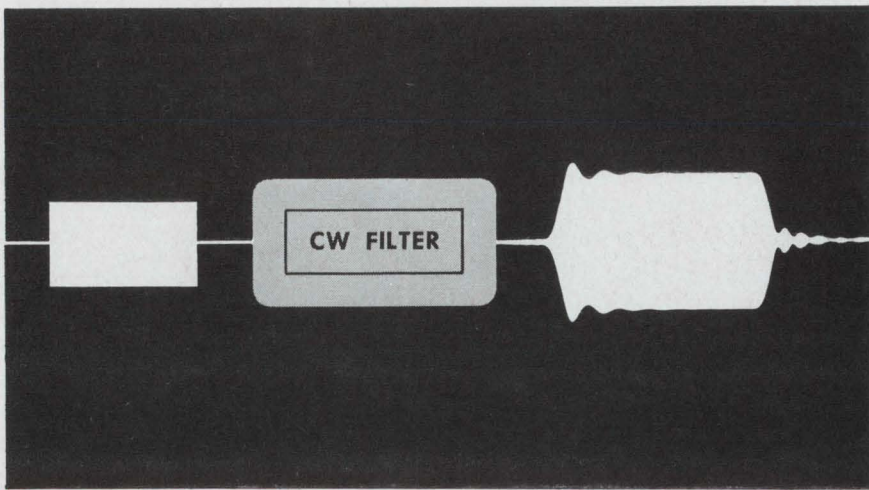
The detonator contains Si layers doped with p- and n-type impurities. The electrodes are mounted axially, like the leads of a transistor.

Several configurations of the multisignal detonator are possible, all of which lead to considerably greater miniaturization than is possible with conventional detonators.

The device was designed and patented by Frank A. Goss, Jr., who is on leave from Bell Telephone Laboratory. ■ ■



**Multisignal detonator** uses thermal-runaway properties of a semiconductor to satisfy a logic function.



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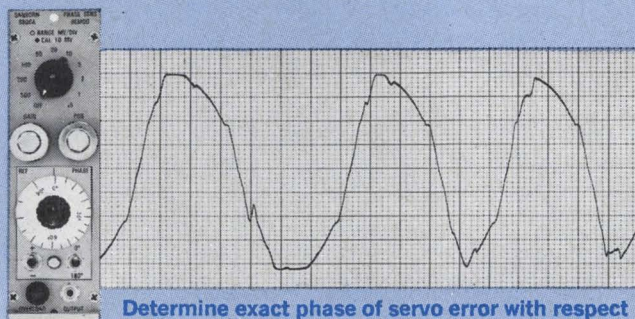
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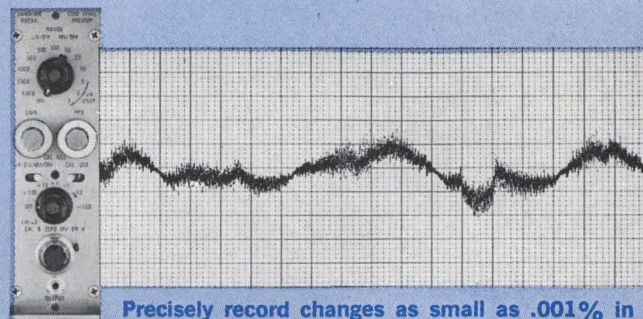


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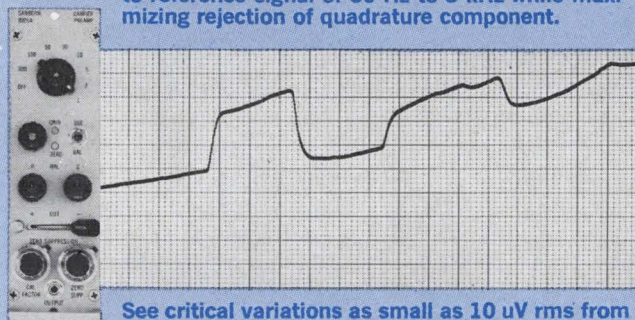
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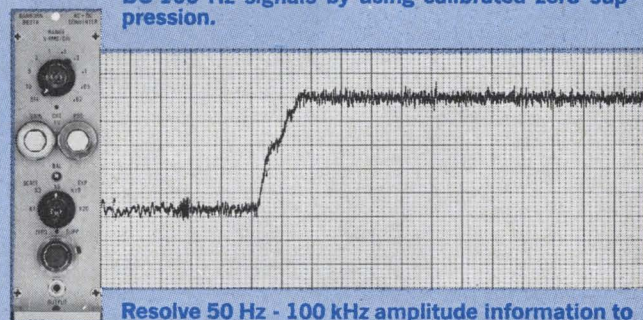
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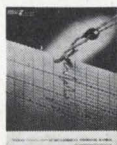


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## At the Paris Electronics Show

## Europe girds for battle with Goliaths of U.S.

## France studying plan that aims to make Europe independent of U.S. microcircuit technology

Robert Haavind  
Managing Editor

PARIS

European dependence on American financing and expertise in electronics has become a major political issue on the Continent, and nationalistic efforts are under way to counteract the trend.

Both the degree of the present dependence and the European reaction against it were much in evidence at the International Components Exhibition here April 5-10.

The French appear to be making the strongest efforts to develop their own electronic industry. Consideration of a Plan Composants by the Government of Charles de Gaulle was revealed at the show by Marc Colonna, who heads the Industry Ministry's Direction des Industries Mécaniques, Electriques et Electroniques. The plan would be similar to Plan Calcul, which was initiated at the beginning of this year to achieve a completely European-based computer industry. The aim of the new program, show exhibitors said, would be to develop independent microcircuit technology, so that Plan Calcul computers would not have to be built with U.S.-sup-

plied chips.

Comparison of the exhibits here with the IEEE Show in New York in March—or even more significantly with discussions at the Solid State Circuits Conference in Philadelphia in February—reveals what an enormous task Europe faces. One engineer from a large British company in the microelectronics business summed up the situation with a colorful twist of phrase:

"We're just a bit of fur on the top of the beast. We could stand here and hop up and down all day long and no one would notice."

The big difference between European and American electronic progress, this engineer and others indicated, is that American research is almost entirely subsidized by the Government.

"We can't keep up with outfits like TI or Fairchild with all that Government support," the British engineer commented. "In our case the Government market is peanuts. We're going it for the industrial and consumer business."

Microcircuitry on display at the show was primarily based on silicon planar technology. A little MOS developmental work by CSF-Compag-

nie Générale de Télégraphie Sans Fil was in evidence, while the General Instrument Corp. and Philco-Ford's Microelectronics Div. showed they were ready to market MOS arrays—GI through a Milan subsidiary and Philco-Ford with a master decal approach. The latter approach, to be introduced in May, allows the user to design and fabricate his own circuit configuration.

The promise of electronics for raising the entire economic status of a nation appears to be behind the French urgency to curtail dependency on the U.S. Plan Calcul was initiated to offset investments by the General Electric Co. in Compagnie des Machines Bull in 1964, when Bull was on the verge of going bankrupt.

Appointed to head the European venture in computer design and programming training was Robert Galley, fresh from a major post in the development of a French nuclear capability. As an official in atomic energy, Galley was responsible for organizing French industry to construct a \$1-billion enriched-uranium plant. Independent companies have been formed to develop computers (Compagnie Internationale pour l'Informatique) and peripheral gear (Société Sperac).

## 1968 marketing goal

Galley is expected to have about \$130 million over the next four years for computer development and programming training. He will also have a say in all Government computer purchases. Since the French endeavor doesn't expect to have a machine on the market until late '68, IBM and Bull-GE, the largest suppliers here, expect to get a continuing share of the market for some time.

Bad feeling engendered by the Bull-GE maneuver—layoffs were necessary before the company regained its equilibrium—is being felt in the components and semiconductor areas here, according to some French representatives. Other American manufacturers are proceeding much more warily than in



E. Schafer of Depex, N.V., Holland, inspects an amplifier chain for collective antennas, being shown by M. Portenseigne of France.



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(Paris show, continued)

the past, after watching the GE experience.

An exchange of views at a reception given by the American Electronic Industries Association on the second day of the exhibition reflected this wariness.

William T. Ellis of the EIA's international department, reading some remarks in French with a somewhat Americanized pronunciation, expressed the hope that the French electronic industry had benefited by the investments and technical assistance of American companies.

The reply by Charles Legorju, president of the Components Exhibition, was quite pointed:

"You have made allusion to the importance of American investments in France. This concerns a delicate matter, because our country lacks the enormous absorption possibilities that your national marketplace offers, and it's important that competition between companies respects the scale of the differences."

Although some fresh European ideas were apparent at the show, many merely reflected the domi-

nance of U.S. technology. Following is a run-down of some of the more significant products of both types:

A 140-MHz quartz-crystal oscillator shown by the Marconi Co., Ltd., Chelmsford, England, was mounted on a TO-5 header. The oscillator will put out 15 mW at frequencies from 60 to 140 MHz, depending on the crystal chosen. In airborne equipment several oscillators might be kept in an oven to get higher stability, according to Dr. S. S. Fortes, manager of applications engineering for Marconi's Microelectronics Div. The price is \$30 to \$50, depending on quantity. Multiple standard chips were used rather than a single monolithic circuit, Dr. Fortes explained, because volume did not warrant the expense of making special masks.

A 150-MHz transistor of unique design that has already produced 25-W outputs and is expected to reach 50 W soon was a highlight of the CSF-Compagnie Générale de Télégraphie Sans Fil display. Cosem, the CSF semiconductor subsidiary, is developing the device and expects to market it in 1968.

In structure the device resembles RCA's interdigitated transistor. The unique aspect is the doping profile (shown in the diagram), according

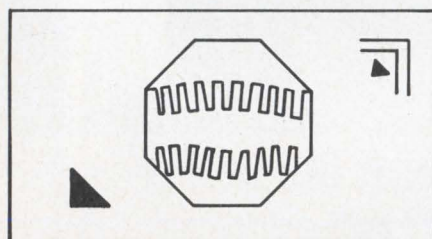
to a CSF spokesman.

CSF was also showing ferrite waffle-iron memories, based on work at Bell Telephone Laboratories that was reported to the Solid State Circuits Conference three years ago.

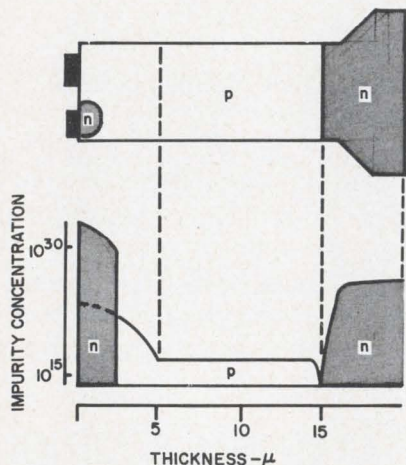
Nondestructive readout may be possible with a new technique developed by CSF. In this type of memory a flat ferrite plate has grooves cut in rows and columns. Nickel-iron films are deposited over the resulting checkerboard pattern. The films are isotropic, but the grooves beneath them give an anisotropic effect (preferred directions of magnetization), needed for storage. In the normal destructive type of memory, bits are stored diagonally across an intersection. In the nondestructive mode being studied by CSF, the bits are stored in fields linking vertically adjacent corners.

Cofélec, CSF's magnetics subsidiary, will be marketing a destructive readout memory featuring a 200-ns read-write cycle time. This type of memory operates on small currents; yet it is insensitive to exterior magnetic fields, in contrast with thin-film types. It should be easier to manufacture than core memories, CSF believes.

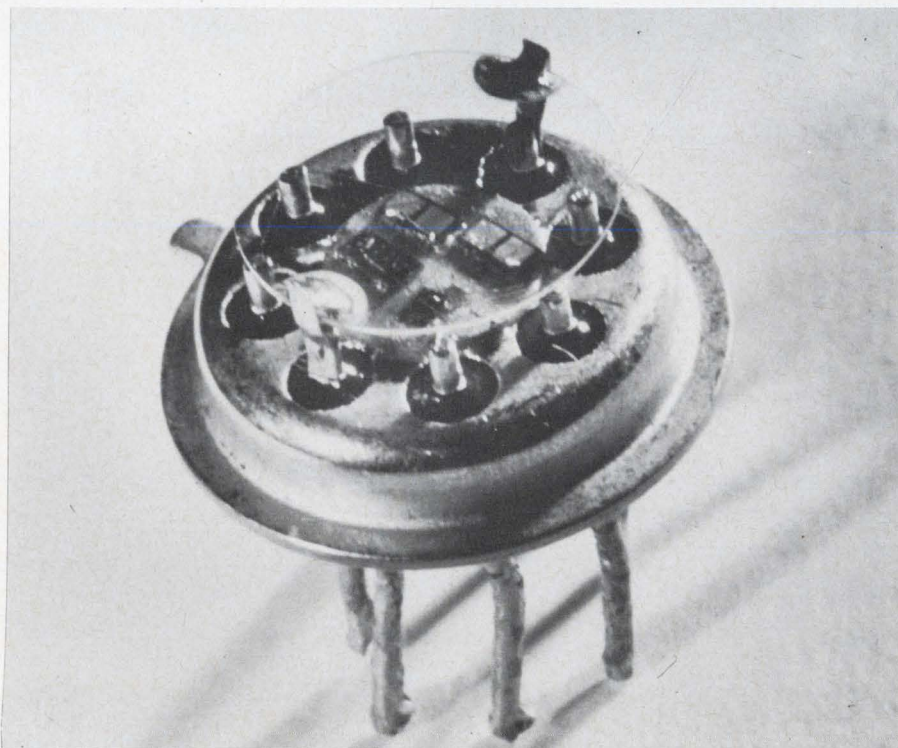
The company expects applications  
(continued on p. 32)



TOP



French-made 150-MHz transistor has reached 50 watts output at 150 MHz. It has an interdigitated emitter (top).

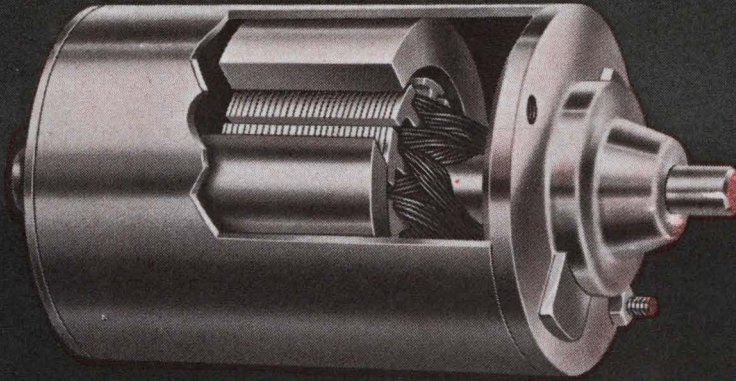


Oscillator in a TO-5 can has a quartz crystal (top) mounted over a multichip circuit. The smallest chip in the center is a transistor. The one to the left of it is a resistor network and the two above it are capacitors.

# American Bosch

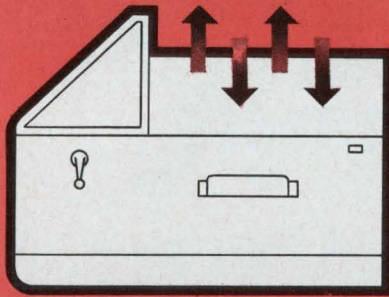
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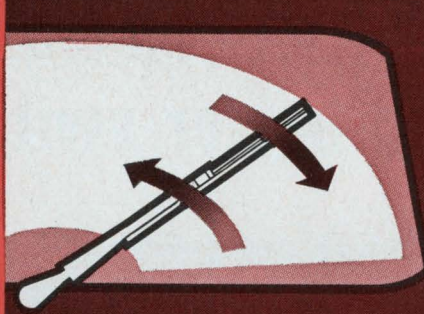


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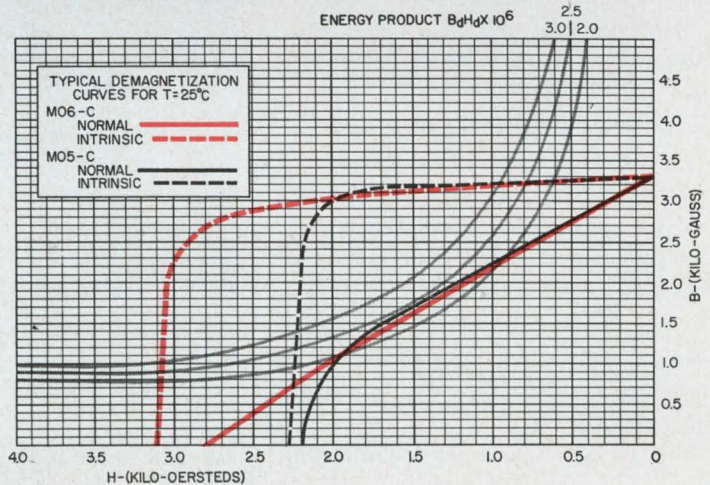
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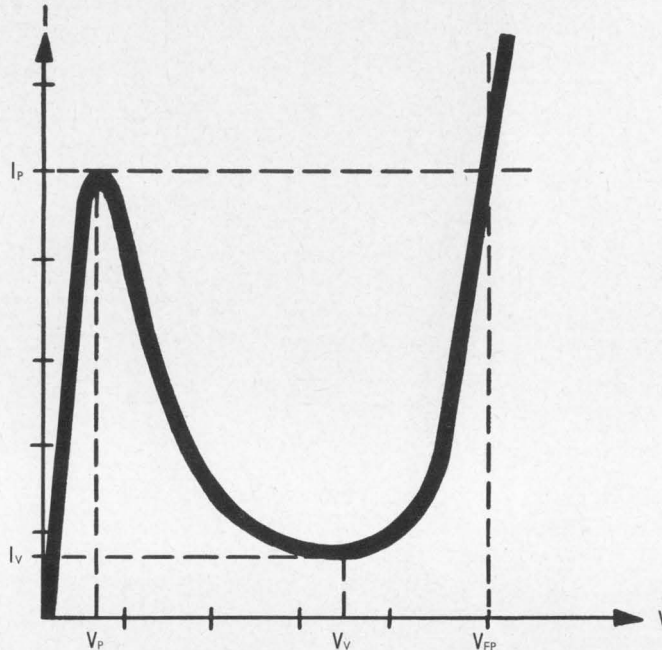
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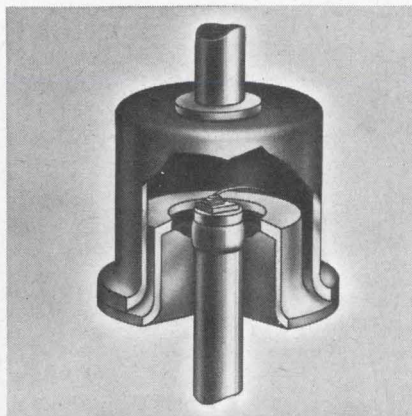
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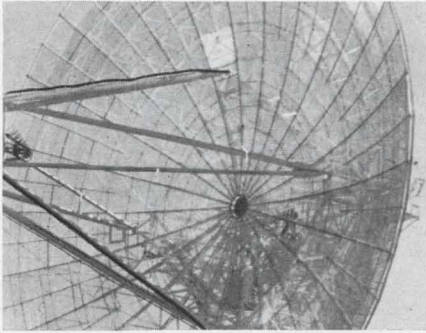
For further details call your nearest GE engineer/salesman, or semiconductor distributor. Or write to Section 220-50, General Electric Company, Schenectady, N.Y. In Canada: Canadian General Electric, 189 Dufferin St., Toronto, Ont. Export: Electronic Components Sales, IGE Export Division, 159 Madison Ave., New York, N.Y.

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### Billion-dollar radio link sought

Over a billion dollars may be involved in developing a common radio communications system to link United States and allied forces on the battlefield. That is the figure used by Defense Dept. officials who are discussing the plan. It will link battle units of the United States, Canada and Australia, and, perhaps later, most NATO countries. The proposal, which may include communication satellites, involves so much money that the U. K. has withdrawn for financial reasons. Pentagon officials are trying to persuade the British to rejoin. Observers believe that any such success may rest on granting the British a large measure of the development and production contracts.

Project Mallard, as the planning phase is called, has received approval from the Director of Defense Research and Engineering, John S. Foster, the No. 3 man in the Pentagon, and has now been sanctioned by Defense Secretary Robert S. McNamara (see News Scope, p. 14).

The system will permit not only allied battlefield commanders to talk to one another, it will also allow communications between the troops of one nation and those of another. Thus an Australian infantry patrol leader could direct U.S. fighter-bombers to tactical targets, or a U.S. company commander could call for support from Canadian tanks previously designated as his back-up.

The hope at the Pentagon is that Mallard will so completely standardize radio equipment and communications practices among the cooperating nations that lower-echelon commanders will be able to talk directly to one another without going through a high-echelon switchboard. The Pentagon has selected Canada and Australia—and hopes to regain Britain—for the early phases of the program because of the common language. Wherever possible, voice communications will be used. Messages between small battle units attached to the same large element will be relayed by portable

# Washington Report

S. DAVID PURSGLOVE,  
WASHINGTON EDITOR

ground stations, according to present plans. Messages between more widely separated units would be handled by communications satellites.

According to McNamara's announcements, the project will be operated from Fort Monmouth, N. J., under the direction of Brig. Gen. Paul A. Feyereisen. A staff member of the Canada-U.S. Military Cooperation Committee said Canada would be represented in the project by Lt. Col. D. C. Coughtry, and Australia by Lt. Col. L. G. Moore.

The U.S. Defense Dept. hopes to have the system operational by 1975-77. About three and a half years would be allowed for development of working designs. This project-definition phase would cost \$40 million, of which the U.S. would provide 60 per cent. The U. K. was to have put up 32 per cent and Canada and Australia 4 per cent each. If Britain cannot be persuaded to rejoin the effort, the U.S. would likely pick up her share.

If the project definition works out on schedule, Pentagon sources say, then a \$1-billion production program would follow.

### U.S. aid for school computers urged

A Presidential committee has urged that the Federal Government give computer programs in colleges the same degree of financial support that it now gives the schools' libraries—about \$60 a student. If the recommendation is followed, the advanced computer facilities now available at a few pioneering colleges and universities would be commonplace by 1971 at nearly all institutions of higher learning in the country.

The suggestion for aid has come from a panel on computers within the President's Science Advisory Committee. The panel contends that computers have become such important learning tools that the Government should support a program to give every college student access to one.

*(continued on p. 30)*

# Washington Report

CONTINUED

The committee is headed by Dr. Donald Hornig, the Presidential Science Adviser, and the chairman of the computer panel was Dr. John R. Pierce of Bell Telephone Laboratories, Inc., Murray Hill, N. J. Once a program for Federal aid is under way, the panel suggested, it could be extended to computer programs in high schools.

## Post Office R&D gains momentum

A year ago a staff member of the House Science and Astronautics Committee, noting the growing postal research and engineering program, commented that the Post Office R&D budget might easily exceed \$100 million a year in about five years. Now he says his estimate was too conservative. That budget was \$12 million in fiscal 1966, \$16.2 million in 1967, and the request for 1968 is over \$23 million.

The biggest part of the budget is given over to electronics. Here are projects in the works:

The Post Office Bureau of Research and Engineering is looking for digital recording equipment that might be applied to "off-line" letter-sorting systems. It would provide a system for "canceling" without touching the envelope or defacing it. Presumably the mail—of a special type—would be numbered, and the digital system would record the numbers as the envelopes passed by. A number used twice would be subject to the same penalty as an attempt to use a canceled stamp.

Companies with experience are being sought to develop a presorting technique that would separate mail addressed in an ordinary way from mail carrying addresses that could be scanned by optical-reading machines. The general concepts have already been laid out by postal R&D specialists; the electronics companies would reduce the concept to hardware and refine it. The system must be better than 95 per cent accurate.

## Train controls report published

The long-awaited report is in on the first Government-sponsored study of automatic train controls envisioned for high-speed transportation systems. The Department of Housing and Urban Development, through

three urban mass-transportation demonstration grants, supported a test of controls in the San Francisco Bay Area Rapid Transit District.

In a nutshell: All four control systems under evaluation successfully met the "general functional requirements," but no single system was outstanding.

The systems were tested on three laboratory cars over three miles of double track. They were under evaluation for their capabilities in train protection, speed and running-time regulation, and programmed precision stopping at stations. The test may have to be repeated on a larger scale, because the propulsion and braking systems of the test cars were themselves developmental and under evaluation, and this may have clouded some of the detailed performance data. Nevertheless the Government believes that the test was valid enough to prove the reliability of fully automatic controls.

## World weather forecasting spurred

The U.S. plans to contribute approximately \$20 million over four years to help poorer nations develop their weather forecasting services. This has been indicated by Robert M. White, head of the U. S. delegation to the Fifth Congress of the World Meteorological Organization in Geneva.

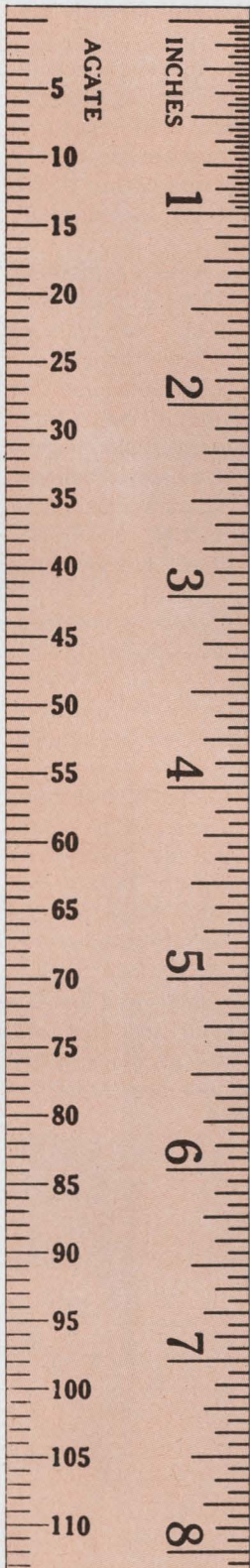
The funds would help the poorer nations participate in the worldwide forecasting network that utilizes satellites, high-speed communications systems and computers.

## Electronic patent reform suggested

Two representatives of the National Association of Manufacturers have called the U.S. Patent Office the most efficient in the world—"but even so," they add, "it takes them at least two to three years to issue a patent." Writing in *Challenge*, the *Magazine of Economic Affairs*, Frederic O. Hess and Reynold Bennett of the NAM's Patent Committee say the situation is worse elsewhere in the world. For the inventor who wants international protection, they assert, it is near chaos: he must deal with over 80 different national patent systems. Their remedy: an international patent office, with "high-capacity satellites synchronized with large patent-data-processing and information storage systems." Patent applications could be processed in days, the authors contend.



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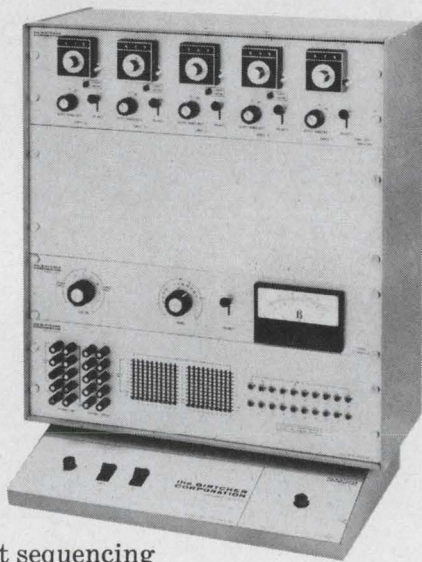
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## NEWS

(Paris show, continued from p. 26)

in  $10^4$ -to- $10^5$ -bit memories. For smaller memories, it believes semiconductor types will be preferred, because the peripheral circuits can be built in.

Cofélec will also market a permanent type of memory using Permalloy films. Meanwhile CSF expects to spend a year or more studying the nondestructive version before it will know whether it is commercially producible.

Although there were no displays of working color TVs at the show this year—the show management having decided to rule them out—there was one big announcement in this area: a wire-grid color tube, which the manufacturer, Compagnie Française de Télévision, believes will replace the shadow-mask tube (see News Scope, p. 13).

Among the other developments were these:

- Fluid logic devices by the Plessey Co., Ltd., Ilford, England, were shown in four devices: an OR/NOR gate, a memory device, an amplifier, and a flip-flop based on the Coanda effect.

- A photo of an 800-W molecular  $\text{CO}_2$  laser was displayed by Compagnie Industrielle des Lasers, a French laser company. It expected to demonstrate the laser at the French Physics Society's show here last week.

The show was sponsored by five French professional societies and was held under the auspices of the Fédération Nationale des Industries Electroniques. ■ ■



Miss D. de Saint of Pile Wonder, a French battery manufacturer, shows a battery with an O-ring seal that has resisted leakage despite 15 days in a short circuit.

# IDEAS

from SYLVANIA Electronic Components Group

## PHOTOCONDUCTORS

### Now, highly reliable UV detection ... even in IR ambients

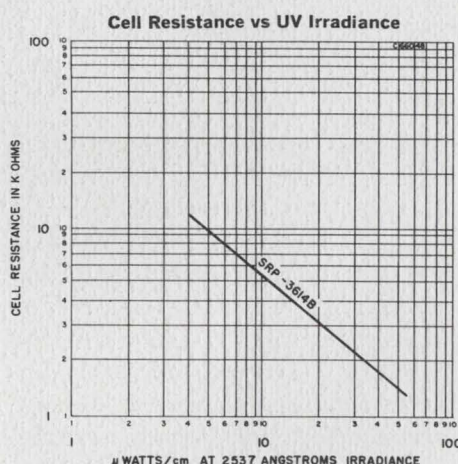


A shortcoming of many ultraviolet detectors is that they're also sensitive to infrared radiation. Thus it's often difficult, if not impossible, to use them to detect just UV in an ambient containing both infrared and ultraviolet radiation. Last year, Sylvania introduced a UV cell with attenuated infrared characteristics. Now, an improved version of this device has greater sensitivity and shows even better infrared attenuation.

Sylvania's new Type SRP-3614B ultraviolet photoconductor improves further the detection and measure-

ment of UV radiation. Like previous designs, the new device requires only simple low voltage circuits to provide an inexpensive, highly reliable UV detection system. The SRP-3614B does differ from earlier types in two important characteristics: it is less sensitive to IR radiation and uses a more sensitive photocell.

Key electrical ratings for the new unit are a power dissipation rating of 300 mW, an ON resistance of 1,300 ohms at 64  $\mu\text{W}/\text{cm}^2$  irradiance, and a dark resistance of 100,000 ohms. Ascent time is 130 msec (at 64  $\mu\text{W}/$



$\text{cm}^2$ ) while descent time is 40 msec at the same radiation level.

The SRP-3614B has the proven high reliability of Sylvania's hermetically sealed cadmium-sulfide photoconductors, but with the spectral response characteristic shifted into the ultraviolet region in the range of 2500 to 4000 angstroms.

The excellent electrical character-

(continued)

## This issue in capsule

**Integrated Circuits** — How to prevent unused inputs from degrading IC performance.

**CRTs** — Eliminate unnecessary trade-offs when choosing computer displays.

**Microwave Diodes** — Punch-through varactors, new route to improved harmonic efficiency.

**Photoconductors** — How photoconductor-lamp assemblies are making music sound better.

**Diodes** — With whiskerless diodes, you can get more components on a board.

#### ELECTRICAL DATA RATINGS (Absol. Max.)

	SRP-3614	SRP-3614A	SRP-3614B
Dissipation at 40°C	300mW	300mW	300mW
at 70°C	25mW	25mW	25mW
Temp. Rge.	-40 to +70°C	-40 to +70°C	-40 to +70°C
<b>CHARACTERISTICS</b>			
Cell (Light) Res. (ohms)	2500	5500	1300
Dark Res. (ohms)	1,000,000	1,000,000	100,000
Ascent Time			
at 64 $\mu\text{W}/\text{cm}^2$			130 ms
4 $\mu\text{W}/\text{cm}^2$			720 ms
Descent Time			
at 64 $\mu\text{W}/\text{cm}^2$			40 ms
4 $\mu\text{W}/\text{cm}^2$			260 ms

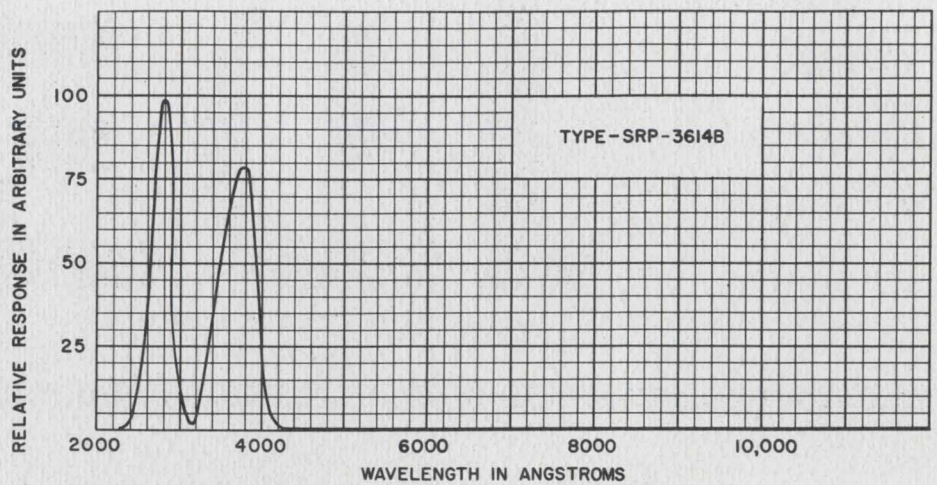
## PHOTOCONDUCTORS (continued)

istics of this improved photoconductor are protected by a small, rugged package with a maximum diameter of 0.70" and a length of 1.625".

Coupling the small size, long life, analog response characteristic with the simple associated circuit requirements makes the SRP-3164B ideal for applications where UV detection, measurement, control or regulation are needed, such as intrusion and fire alarm systems. The new photoconductor can effectively and economically replace many avalanche or continuous monitoring devices.

CIRCLE NUMBER 300

Spectral Response



## MARKETING MANAGER'S CORNER

# Circuit Designer—IC Manufacturer... Conflict or Complement?

The rapid growth of the integrated circuit industry has given rise to a pertinent question: whether or not there is a functional conflict between the IC manufacturer and the manufacturer of electronic equipments and/or systems. In other words, are we, as IC manufacturers who produce complete functional circuits, overstepping our bounds and infringing on the functions of circuit designers? What about circuit design engineers? Will they become high priced order clerks, purchasing all the circuits they need to build an equipment out of an IC catalogue?

To aggravate the picture, the trend in the IC industry appears to be headed for even greater density. LSI (large scale integration) is now in the horizon, cramming many more and larger circuits into a single package. It may be possible to eventually encapsulate an entire automated operation or computer function into a single IC package. Will this development turn the computer manufacturers into automated factories, whose purpose it will be to merely assemble various combinations of IC packages?

Not at all! On the contrary, as the electronics industry expands, all its constituent components will expand along with it. With standard circuits such as flip-flops, gates, registers, and counters available as packaged items, the design engineer can concentrate on larger and more complex circuit configuration. Furthermore, many cir-

cuits required for equipment design have a unique configuration, in one aspect or another, and, therefore, must be designed by the equipment manufacturer; the IC manufacturer only fabricating these "customized" circuits.

With reference to this last point, it should be remembered that in order to work effectively with the integrated circuit manufacturer, the circuit designer must familiarize himself with integrated circuit technology, its advantages, its applications, and its limitations. He should know the IC circuits that are available as "off-the-shelf items." He should also be knowledgeable of the manufacturing process of integrated circuits so that he can design new circuits which are most applicable to the present state of the art. This will result in a reduction of IC costs, a functionally superior IC, and a better working relationship between circuit designers and integrated circuit manufacturers.

The same situation exists with regard to system designers. No matter how complex and dense ICs become, they will only serve as building blocks for large systems. Furthermore, the systems of today will become the subsystems of tomorrow's larger, more complex and sophisticated systems. Therefore, with the availability of larger and more efficient "building blocks," system design engineers will be able to concentrate on solving the design problems associated with cre-

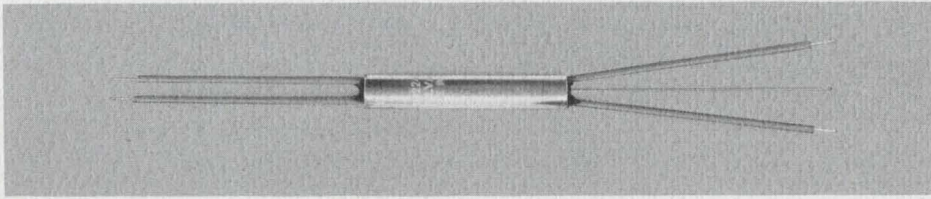
ating larger and more efficient systems.

Finally, it must be noted that the trend toward LSI is not a self-generating movement. IC manufacturers are not simply producing denser ICs just for the sake of cramming more circuitry into a package. This trend, to a great extent, is the result of certain design requirements dictated by military and industrial contractors. The great need for space and weight savings, and the requirement for extended operation reliability within the space program has had a significant effect on IC design. The noise immunity requirements of high frequency circuitry and high speed computers also have dictated the direction which IC manufacturers have had to take. However, when one looks at the total picture, he finds the word that describes the relationship of equipment and systems manufacturers, and IC manufacturers, is "complementary"; each has its own function which complements the other. And the very evident direction of motion is upward. The electronics industry continues to grow; equipment and systems are becoming more complex and sophisticated. Keeping up with this growth in complexity and sophistication is the IC manufacturer.

*Roger A. Swanson*

R. A. SWANSON

# How PL assemblies are making music sound better



*Photoconductor-lamp (PL) assemblies are being used to produce special musical effects such as tremolo, vibrato and percussion. What makes these units ideal for these applications is the intrinsic characteristics of the photoconductor-lamp combination. It provides noise-free operation because of electrical isolation between control and signal circuitry. This, of course, eliminates the introduction of hum from the control circuit. Result is an effect pleasing to the listener. Here's how a tremolo circuit using a Sylvania PL assembly makes an electric guitar sound more pleasing.*

Tremolo effects—subsonic modulation of an audio signal—can be produced easily and reliably by an electric guitar amplifier which uses Sylvania's PL assembly. The circuit shown uses a PL-8224C assembly and a phase shift oscillator to get the tremolo effect. The oscillator output frequency of 40 to 8 Hz is controlled by a 1-megohm potentiometer in one

arm of the phase shift network. Output of the oscillator is decoupled by a 330 K resistor into another 1-megohm potentiometer which varies the level of the control signal voltage fed into the PL driver stage.

The on/off switch can ground the arm of the 'Depth' potentiometer to remove modulation from the light source portion of the PL assembly. The dc operating current of the light source is determined by the setting of cathode resistor in the PL driver stage. The ac output of the 'Depth' control is superimposed on this dc level, providing an ac variation in the resistance of the PL. Shunting this ac varying resistance divider across the volume control gives the desired modulation of the audio signal. Depth of modulation depends on the setting of the 'Depth' control and may approach 100 percent.

Basic action of this circuit is that of a volume control being varied around its operating point at a sinusoidal rate

with the rate controlled by a low frequency oscillator.

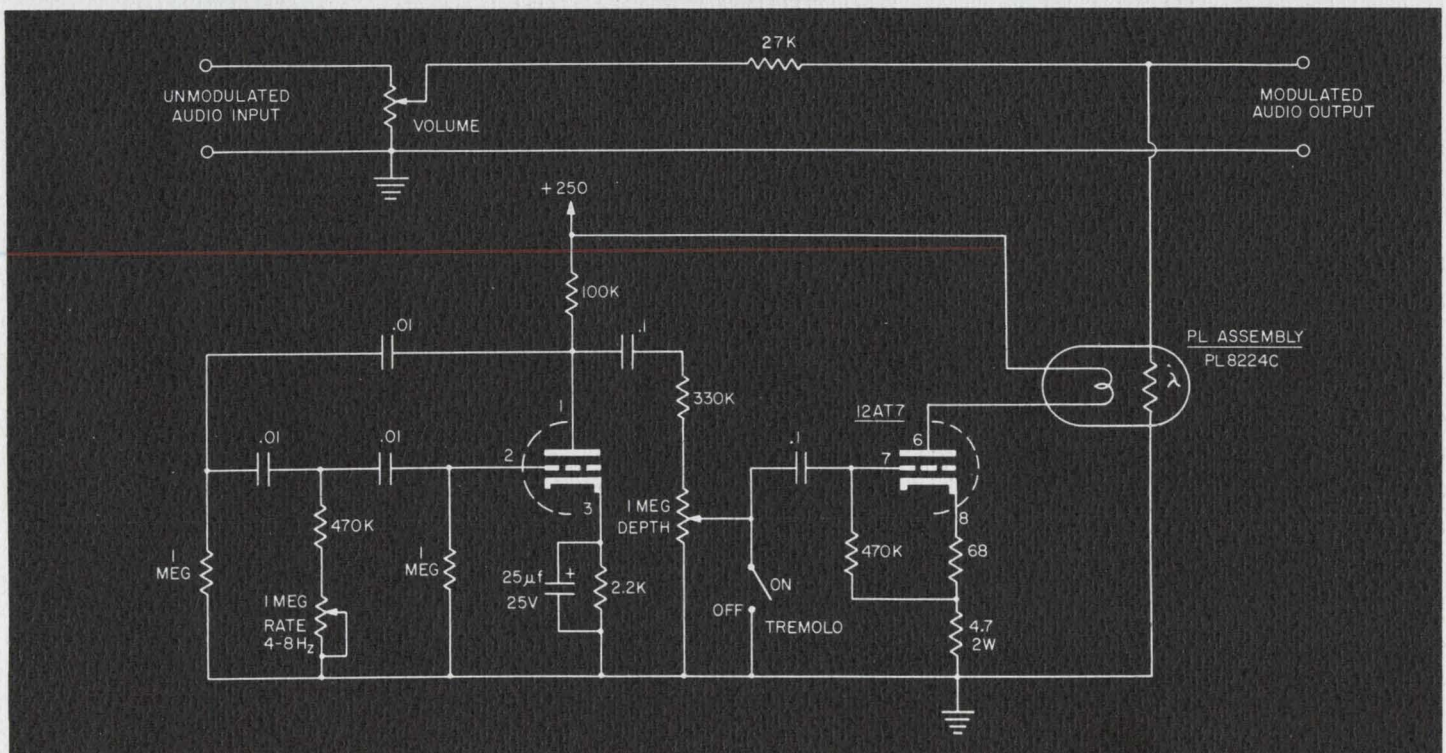
The type PL-8224C assembly used in this application consists of a hermetically sealed cadmium sulfide photoconductor and an incandescent lamp potted in a metal cylinder 1.75 inches long and 0.31 inches in diameter. Its cell voltage is rated at 300 V max and can handle up to 50 mW at 25°C. Cell resistance varies from below 60 K (ON) to above 10 megohms (OFF).

The PL-8224C is just one of many standard and custom PL Assemblies available from Sylvania. These PL assemblies, because they have the characteristics of both a switch and a potentiometer, have many other circuit applications in addition to generating musical effects.

Such applications as: On-Off Switch, Sequential Switch, Logic Functions, Gain/Volume Controls, Electrically Controlled Circuit Functions (Delays, Oscillators, Filters), Linear Amplifiers, Voltage and Current Regulators, Motor Speed Regulators and Modulators.

In all these applications the PL assemblies provide moderate power handling capability, noise-free operation, and high circuit isolation.

CIRCLE NUMBER 301



# Preventing unused inputs from degrading IC performance

Frequently, all inputs of an integrated circuit are not required in a particular application. What does the circuit designer do with these unused inputs? They may be left open, but this could degrade circuit operation; or additional components can be added to insure top performance. SUHL™ devices by Sylvania require only simple wiring and no extra components to obtain optimum performance characteristics. Here's the how and why for gates and flip-flops.

The high drive capability of SUHL I and II output networks allows unused gate inputs of these ICs to be tied directly to signal inputs with insignificant sacrifice in speed or static characteristics. In the same way, unused inputs of these SUHL flip-flops can be tied to active inputs or outputs to maintain propagation delay time, clock width, and amplitude. With SUHL gates and flip-flops it's basically a matter of eliminating the effect of the capacitance associated with each of the unused inputs.

In SUHL gates, each input has a capacitance to ground of about 1.2 pF (package and chip). If wiring is also connected to the emitter, then additional capacitance is added. How the capacitance of unused inputs influences circuit operation can be explained by Figure 1. Here, if input A goes to logic "0" and input B is float-

ing, the voltage at B tries to follow the voltage at A. In time, B falls to logic "0." When A rises to logic "1," B is held down until its capacitance charges through the base resistor. This action slows down the recognition of the logic "1" data at A.

To prevent this, unused emitters should be terminated with a voltage greater than the logic "1" threshold voltage. In this way, stray capacitance on the inactive inputs will always be at logic "1" and won't slow circuit operation. There are a number of ways to insure that these gate inputs remain at logic "1."

The unused inputs can be connected to a dc voltage as shown in Figure 2A. For SUHL units, the voltage should never be higher than 5.5 V, the breakdown rating of the inputs. A 5.0 V supply is satisfactory if it never goes above 5.5 V, even during power turn on. Should the supply go above 5.5 V, then a resistor (ranging from 500 to 5000 ohms) is placed between the emitters and the supply as indicated in Figure 2B.

Many emitters can be tied together. One convenient method of supplying the required voltage is to use one NAND gate with its inputs grounded to hold all unused emitters at Logic "1."

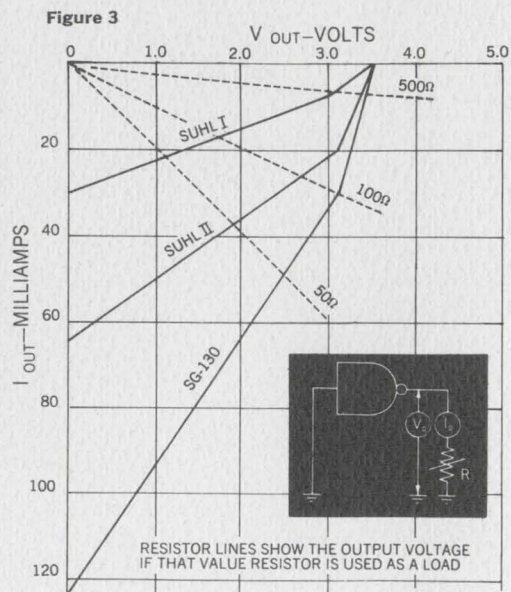
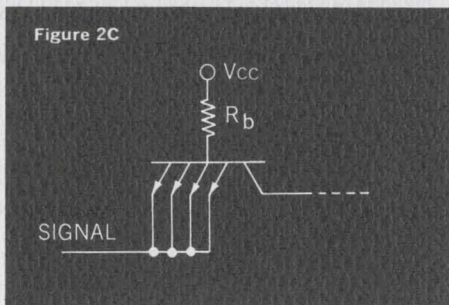
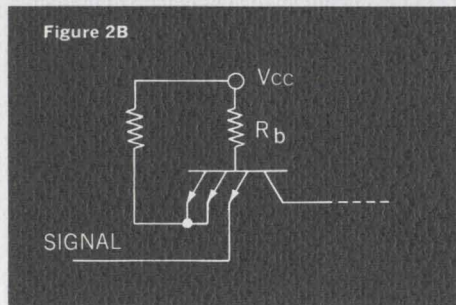
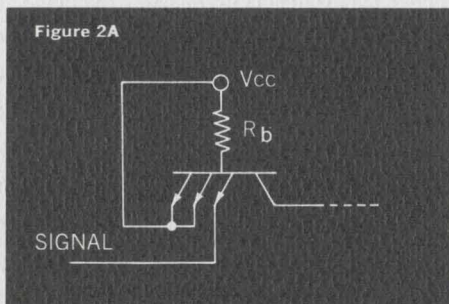
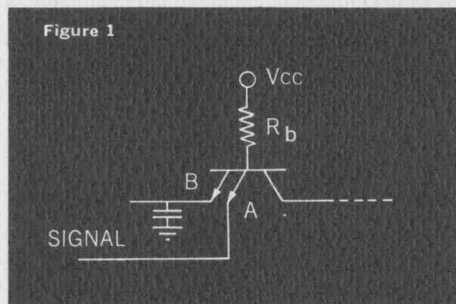
A more convenient neutralization technique is to tie unused emitters to

one of the signal emitters as shown in Figure 2C. This requires no extra components. Only simple wiring is needed and performance of the system is not degraded. In this approach, when the data signed goes to "0," all capacitance is directly discharged to "0" through the driver. Since this capacitance is small and the drive capability of SUHL is high, there is a negligible effect on speed (about 0.03 nsec/pF). In this configuration, input current is the same as if only one input were used, because the base resistor limits current flow.

In Figure 2C, when the driver rises to logic "1," each input and its capacitance is pulled to a positive voltage. Again, because of the high drive capability of SUHL output networks, pull-up speed is negligibly affected by the small capacitance increase (about 0.4 nsec/pF). The high current capability of the output network of all SUHL elements also means that static characteristics remain constant.

These SUHL output characteristics are shown in Figure 3. Even with many milliamps of loading, logic levels are still high and well above threshold.

In flip-flops, it is extremely important that all inactive inputs be terminated. Not only is propagation delay time effected, but so is clock width, amplitude and the waveform required



for triggering.

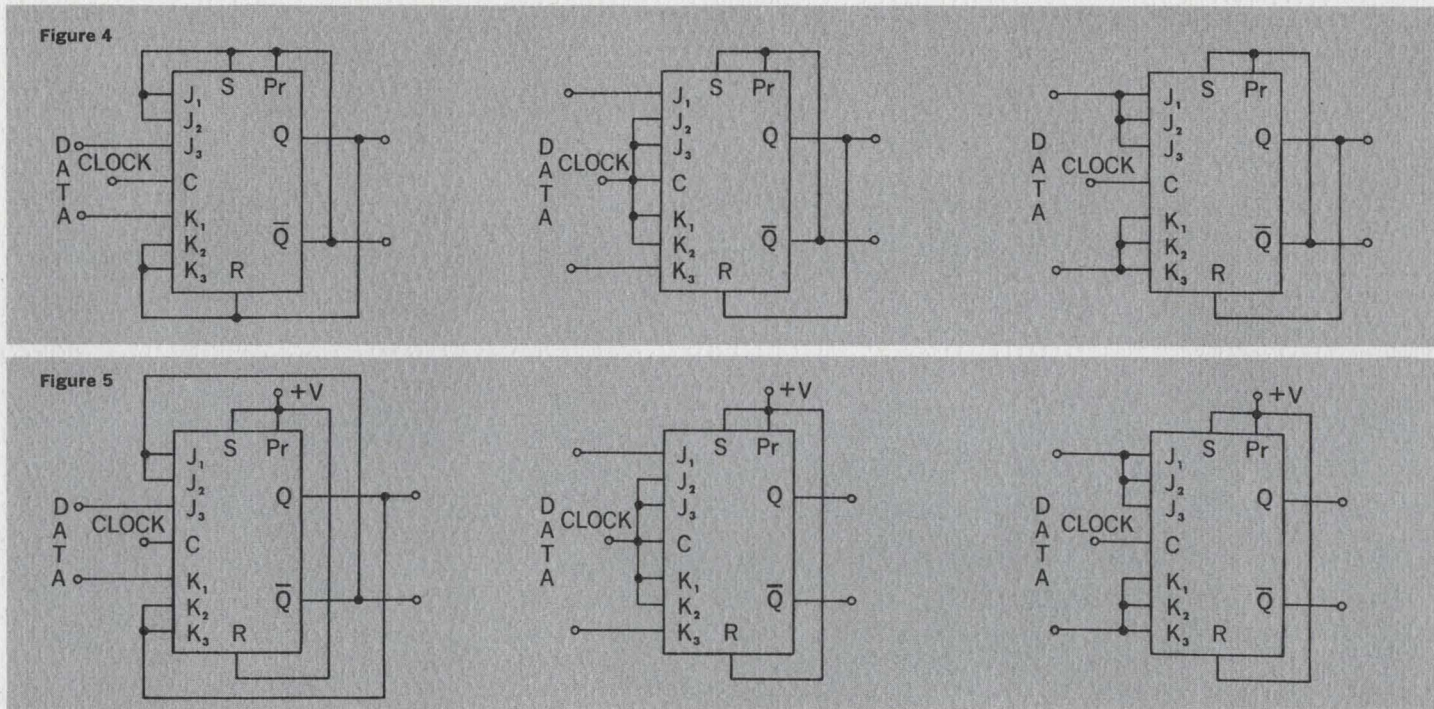
Synchronous or data inputs of flip-flops can be terminated with dc in the same manner as a gate, but for each flip-flop there are signal carrying inputs or outputs to which unused inputs can be connected. Examples are

shown in Figures 4 and 5.

Unused asynchronous input terminals (DC Set, Preset, Reset) can also have a degrading effect on performance, particularly if they are connected to wiring or board metalizing which increase capacitance. Even at

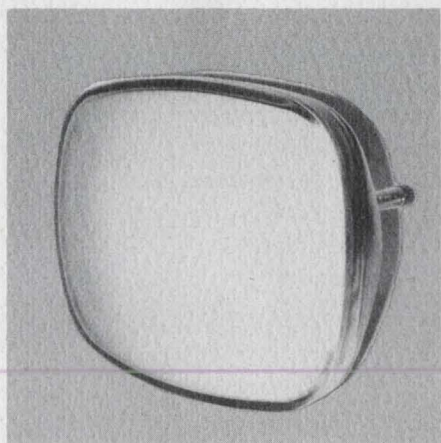
low frequencies it is important that asynchronous inputs be connected to a positive voltage or terminated in some other way. The same techniques used for gates or those shown in Figures 4 and 5 can be employed.

CIRCLE NUMBER 302



CRTs

## Eliminate unnecessary trade-offs when choosing computer displays



*The value of a computer often is directly related to how fast the information output can be obtained by the people who need the information. CRTs provide an effective and very fast graphic display of such information. But picking the right tube (and the right tube manufacturer) for computer display applications is not simple. Many factors must be evaluated. A good way to start is to look at the manufacturer's present capability in CRTs for computers.*

Years of leadership in CRT technology and display design give Sylvania the full capability needed to meet demands for computer CRTs. This capability is based on a solid background of providing CRTs for the computers of several manufacturers.

These CRT displays offer many advantages. Display of alphanumeric information on a tube face is much faster than waiting for a typed output. A dynamic display also permits on-line program debugging, text editing and revision, and rapid scanning of stored material. Coupled with a camera, these displays can give a hard-copy output. The growing interest in using displays to permit on-line, two-way conversation with the com-

puter opens up a host of applications. For instance, results of calculations can be plotted, and the user can select regions where he wants calculations to be carried out in more detail.

Selecting the optimum tube for such applications can be a difficult chore. Many factors must be considered; such factors as size of display, deflection, focusing method, sensitivity, resolution, brightness, power requirements, and phosphor characteristics. Trade-offs may be necessary. But, at Sylvania these trade-offs are kept at a minimum; because the designer isn't limited to a few off-the-shelf items. Sylvania's wide range of standard and custom tubes permit a better match of tube to application.

TYPICAL COMPUTER TYPES				
Basic Type	Deflection Angle	Screen Size	Useful Scan	Overall Length
SC-4649	70°	7"	5-3/4" x 4-3/8"	10"
8QP-	90°	8"	7-3/16" x 5-3/8"	9-15/16"
8KP-	90°	8"	7-3/16" x 5-3/8"	11-15/16"
17DWP-	70°	17"	11-1/8" x 14-5/16"	19-3/16"
21EYP-	72°	21"	19-1/16" x 15-1/16"	23-1/32"

CIRCLE NUMBER 303

# Punch-through varactors: new route to improved harmonic efficiency

There's a great deal of confusion in the microwave industry regarding high-order multiplier diodes. Names such as step diodes, step recovery varactors, snap diodes, snap-off varactors, etc. are being used to describe diffused diodes having a varying capacitance-voltage relationship. Sylvania uses the term PTV, or Punch-Through Varactor, to better describe a diode which was developed to have a sharp decrease in junction capacitance, as well as a series resistance at a reverse bias 15 to 20% of the rated breakdown voltage. This deflection point occurs when the depletion width "punches-through" the thin epitaxial layer of high-resistivity silicon.

The Sylvania D-4410 PTV exhibits little capacitive nonlinearity in the reverse bias region, but shows a marked nonlinearity in the forward bias region because of charge storage. The relatively flat capacitance change over a large reverse bias range offers several advantages, such as minimal detuning over the temperature range,

simplified tuning procedure, and improved dynamic range. Simplified matching techniques can be employed, and under broad band operating conditions improved operating efficiencies can be realized.

If PTVs are driven into the forward bias region, high conversion efficiencies can be obtained as a result of the marked non-linear capacitance curve. The lower average  $R_s$  value over the drive cycle also contributes to better efficiency by reducing the power dissipation. Harmonic generators operating with multiplication ratios as high as 27:1 or as low as 2:1 will yield highly efficient performance at frequencies from VHF to Ku-band. These diodes, made from epitaxial silicon, have diffused junctions tailored for punch-through at a reverse bias voltage which is low relative to the breakdown voltage.

Electrical specifications and typical operation in a multiplier circuit for a Sylvania PTV are given in the table.

Carefully controlled fabrication techniques give Sylvania's PTVs

these additional advantages: uniformity of performance characteristics, higher power handling capability, improved circuit stability, higher power, and frequency operating range.

All units are baked at a minimum temperature of 200°C for at least 16 hours prior to final hermetic sealing. Finished devices see these test procedures: centrifugal acceleration of 20,000 G, temperature cycling from -65°C to +150°C; breakdown checking at 150°C; 48 hour burn in at 200°C; and gross and fine leak (Radioflo) testing.

Units in the new PTV series are available in four packages: the 017, 023, 075, and 099.

ELECTRICAL SPECIFICATIONS (Type D-4440)	PERFORMANCE IN MULTIPLIER (Type D-4440)
$V_B = 45$ Volts	$F_{in} = 1$ GHz
$C_j (-6V) = 1 - 1.5$ pF	$F_{out} = 10$ GHz
$T_s = 250$ picosec	$P_{in} = 1$ watt
$T_L = 60$ nanosec	Efficiency = 13%
$R_s = 0.8$ ohms	
$I_F = 100$ milliamps	
$R_T = 45^\circ\text{C}/\text{watt max}$	

CIRCLE NUMBER 304

## PTV DIODES

In a varactor multiplier, power handling capability and conversion efficiency are determined by the breakdown voltage, junction capacitance, junction conductance, and series resistance. Breakdown voltage is determined primarily by the resistivity of the N-type semiconductor material used in the P-N junction. The other parameters are shown in the simplified equivalent circuit of Figure 1.

The nonlinearity of the voltage-variable junction capacitance is the dominant factor in the frequency multiplication process. Junction conductance and series resistance dissipate power, limiting output power and conversion efficiency. The frequency conversion process also depends on the quality factor  $Q$  or cut-off frequency  $\omega_{co}$ . These are given by the equations  $Q = 1/\omega R_s C_j$  and  $\omega_{co} = 1/R_s C_j$ .

Specifically, frequency conversion depends on the average values of

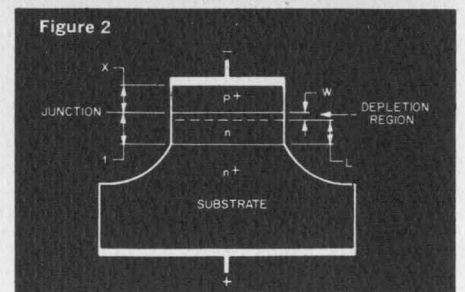
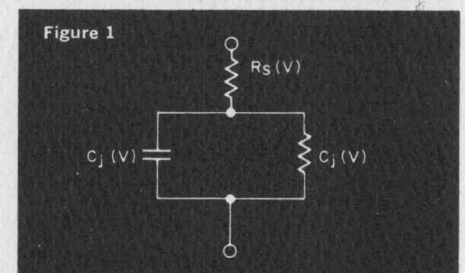
these factors over the drive cycle of the multiplier. Since both  $R_s$  and  $C_j$  vary with reverse voltage, their values should be kept at a minimum over most of the drive cycle. The nature of these nonlinear parameters can be examined with the aid of the simplified P-N junction of Figure 2. Here, a thin layer of lightly doped, n-type semiconductor of thickness  $t$  is grown epitaxially on a substrate of heavily doped, n-type material, and p-type dopant is diffused to a depth  $X$  into the n-type layer.

A reverse bias voltage applied to the varactor sweeps mobile carriers out of the lightly doped n-region. These carriers recombine in the p region, forming a depletion region of width  $W$  in the n layer. Width of this region varies with applied voltage as;  $W = K_1 (\phi - V)^\gamma$ . Where  $\phi$  is the built-in voltage of the junction,  $K_1$  is a constant, and  $V$  is the applied reverse bias. The term  $\gamma$  varies from 1/3 to 1/2 depending on the type of junction. The depletion region boundaries

act as a parallel plate capacitor with capacitance of:

$C_j = EA/w = k_2 (\phi - V)^{-\gamma}$ ,  
where  $E$  is the dielectric constant of the n-type material,  $A$  is the junction area and  $k_2$  is a constant. Increasing the applied reverse voltage  $V$  increases  $w$  and decreases  $C_j$ .

Two additional factors determine





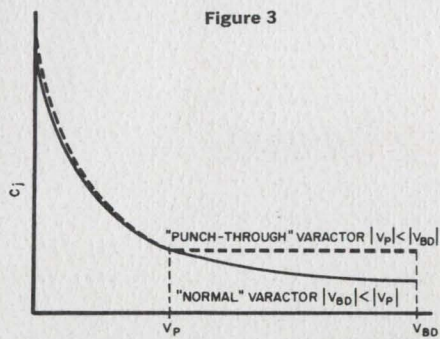


Figure 3

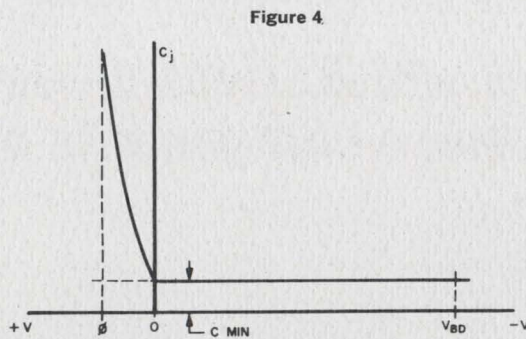


Figure 4

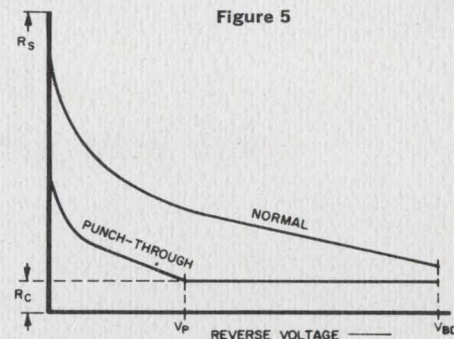


Figure 5

the variation of  $C_j$  as  $V$  increases. One is the maximum allowable applied reverse voltage, with the reverse breakdown voltage  $V_{bc}$ . At  $V_{bd}$ , avalanche multiplication takes place and a large current flows through the diode.

The second factor is the thickness  $t$  of the n-type layer. Depletion width,  $w$ , increases continuously with applied voltage, but it cannot exceed thickness  $t$ , because at that point the depletion region boundary is in contact with the heavily doped  $n^+$  substrate. When  $w = t$ , no further decrease in junction capacitance can occur.

Depending upon thickness and resistivity of the n-layer, avalanche breakdown may occur at a reverse voltage either lower or higher than that at which  $w = t$ . The voltage at which  $w = t$  is the punch-through voltage,  $V_p$ . Figure 3 shows the junction capacitance and applied reverse voltage relationship for the punch-through and conventional (or "normal") varactors.

If the punch-through voltage occurs at a voltage which is low with respect to the breakdown voltage, then the overall capacitance-voltage relationship approaches the case where  $\gamma = 0$  and  $C_j$  is constant for any applied reverse voltage beyond

the punch-through point.

While the PTV exhibits little capacitive nonlinearity with a reverse bias, a marked nonlinearity occurs with a forward bias. This is due to charge storage. This charge storage capacitance, sometimes called the diffusion capacitance, is an exponential function of forward voltage, and also depends upon the recombination lifetime of the semiconductor material. For effective charge storage, the recombination lifetime should be large compared to a period of the drive frequency. Figure 4 shows an idealized capacitance-voltage plot ( $\gamma = 0$ ) of a punch-through varactor.

The series resistance,  $R_s$ , of an epitaxial varactor consists of a sum of four terms:  $R_s = R_p + R_n + R_{n+} + R_c$ . Resistance  $R_p$  is that of the p-layer;  $R_n$  that of the n-layer;  $R_{n+}$  that of the substrate; and  $R_c$  that of the ohmic contacts.

In practice,  $R_c$  is usually a few tenths of an ohm at uhf frequencies, but may be higher at high microwave frequencies because of skin effect in the connecting leads. For surface concentrations normally used in epitaxial varactors,  $R_p$  is usually negligible compared to  $R_c$  and  $R_n$ .

Likewise,  $R_{n+}$  is negligible for a highly doped substrate. Thus, the re-

sistance of the epitaxial layer,  $R_n$ , is the dominant component of  $R_s$ , and is given by  $R_n = P_n L / A = P_n (t-w) / A$ .  $P_n$  is the resistivity of the epitaxial n-layer, and  $L$  is as shown in Figure 2.

Since  $w$  varies with reverse voltage,  $R_n$  and  $R_s$  also vary with  $V$ . As with  $C_j$ , if  $|V_{bd}| < |V_p|$ , then  $R_s$  decreases continuously as voltages from zero to  $V_{bd}$  are applied. If  $|V_p| < |V_{bd}|$ , then  $R_n$  vanishes at  $V_p$ . This is because  $w = t$ ,  $L = 0$  and the total series resistance is  $R_s \approx R_c (|-V| \geq |V_p|)$ . Figure 5 shows the variation of  $R_s$ , for the normal and punch-through cases. The change in series resistance with reverse voltage may be quite appreciable. For epitaxial varactors with breakdown voltages of 50 to 100V, the ratio of series resistance at zero bias to that at the breakdown voltage may be greater than 2:1 and up to 10:1 for higher-voltage varactors.

Varactors with the same value of  $R_s$  at breakdown may have quite different values of  $R_s$  at lower reverse voltages. In the PTV, the  $R_s$  is lower at zero bias than in a conventional varactor and reaches its minimum value at the punch-through voltage. The result is a lower average  $R_s$  over the drive cycle and higher conversion efficiency than in the normal varactor.

CIRCLE NUMBER 304

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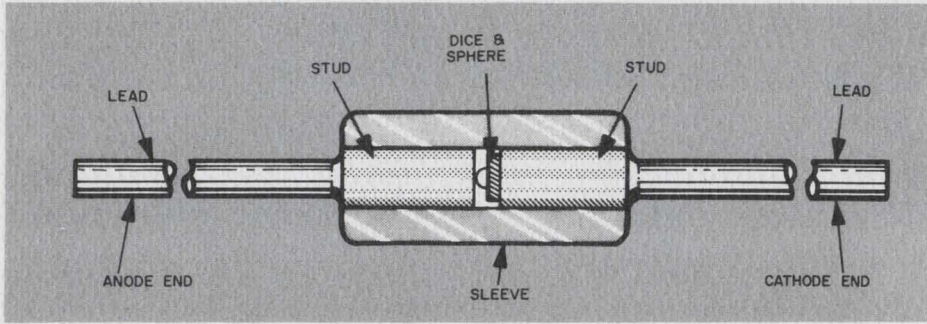
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# How whiskerless diodes let you get more components on a board



Designing computers or other equipment which requires fast logic circuits or small signal switching? Here's your chance to get more money for your diode dollar. Use Sylvania's miniature whiskerless diodes to replace DO-7 types, to get significant savings in mounting space, and improve reliability without any increase in cost.

Because Sylvania's miniature dual stud whiskerless diodes are much smaller than DO-7 types, they allow designers to decrease circuit board requirements significantly. Costing no more than their electrical equivalents in DO-7 packages, the rugged whiskerless units have a package volume which is 68 percent smaller. But smaller size is not the only advantage of these newer diodes. The single unit construction makes for higher reli-

ability and for devices able to take shock and vibration environments.

With these 0.075" dia. by 0.160" long Sylvania units you get top electrical performance. Typical reverse leakage currents of units in the whiskerless line are a low 15 na. Switching speeds are in the order of 4-10 nsec. Ratings for these silicon epitaxial diodes include average rectified currents of up to 150 mA (with surges of 500 mA) and a power dissipation of 500 mW.

Key construction features of the whiskerless devices are: use of a plated silver sphere to make contact to the junction, dumet studs for good heat conduction away from the junction, and protection of the active area with a soft glass sleeve. What results is a rugged single-piece device capa-

ble of taking high-g shocks.

Reliability of this simple structure is enhanced further by the pains taken during the manufacturing process. Sylvania has developed special production techniques to make sure the silicon dice used is more symmetrical and is free from any jagged edges, cracks, or out-of-tolerance parameters.

Sylvania's whiskerless diodes can be used with standard automatic insertion equipment.

CIRCLE NUMBER 305

### SILICON EPITAXIAL DIODES

Type	Outline	DO-7 Electrical Equivalent
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1N4149	DO-35	IN916
1N4151	DO-35	IN3604
1N4152	DO-35	IN3605
1N4153	DO-35	60V IN4152
1N4154	DO-35	IN4009
1N4446	DO-35	IN914A
1N4447	DO-35	IN916A
1N4448	DO-35	IN914B
1N4449	DO-35	IN916B

#### ABSOLUTE MAXIMUM RATINGS:

Average Rectified Current, $I_o$	75 mA
Peak Forward Current, $I_{pk}$	225 mA
Forward Surge Current, (1 sec)	500 mA
Power Dissipation, $P_T$	500 mW
Junction Temperature, $T_J$	-65 C to +175°C

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## Electronics taught with domino module

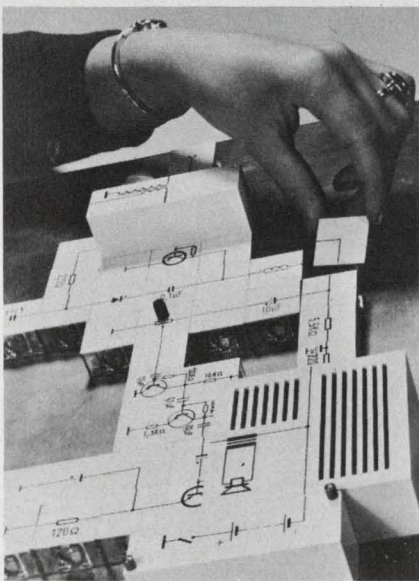
Electronic "domino" modules are helping students learn about electronics without the bother of wiring and soldering components. The modules are quickly snapped together to form a variety of circuits—and just as quickly, they can be taken apart.

More than 90 different electronic experiments are possible with each set, according to the Macalaster Scientific Corp. of Watertown, Mass., distributor of the teaching aids.

Among the circuits that can be formed, Macalaster says, are radio receivers, a fire alarm, a tone generator, a rectifier, and amplifier, a sound-level meter and even an electronic flash unit.

The modules are held together by built-in magnets, which also make an effective electrical contact. This is said to permit the assembly of a transistorized radio receiver in about 10 minutes.

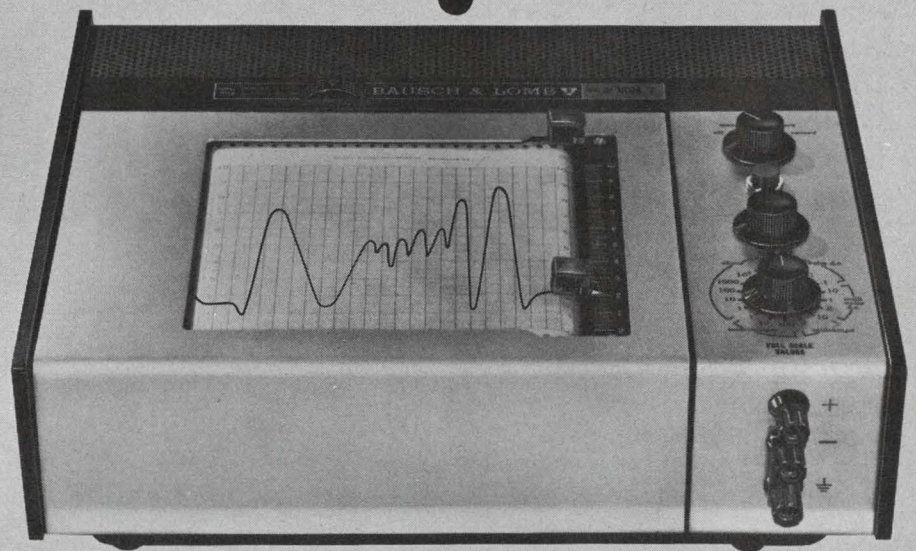
The circuit elements are packaged in transparent plastic boxes, with schematic symbols imprinted on opaque covers. When put together, a complete schematic is formed. The student is able to view both the component and its representation while assembling and checking his experiments. ■ ■



A radio receiver is assembled in an electronic theory class the easy way, by snapping together components packaged as "dominoes."

ON READER-SERVICE CARD CIRCLE 19 ➤

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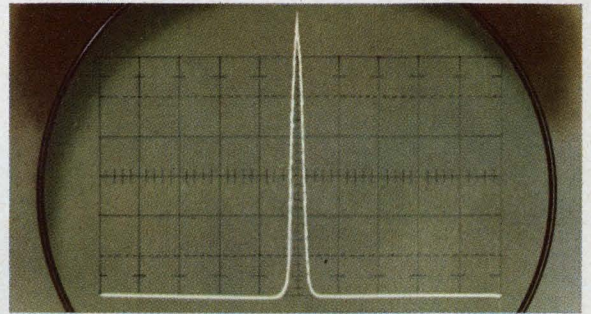
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ON READER-SERVICE CARD CIRCLE 21

# Chapter II.

# *The Word from GENISCO.*

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And that means no step function voltage to generate high-frequency components. And that means that the switch is *free* from radio frequency interference. *Quod est demonstrandum.*

The second reason we call it "free" is we thought that if you thought you could get a \$50 switch for nothing you'd probably be greedy enough to read this ad. There appears to be some justification for this assumption.

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## OUR TELEMTRY GEAR WILL NEVER GET OFF THE GROUND

Because we manufacture only equipment associated with checking out telemetry transmission while the transmitter is still nice and accessible.

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## HOW WE INVENTED THE SANDWICH

To make the ruggedest possible field portable tape recorder we suspended the entire tape transport mechanism between two parallel flat plates. This gives double support to all members, and as the tape contacts only the primary drive mechanism, reel hubs, two turn rollers and the head surfaces, its oxide coating gets maximum protection.

As you know, the flanges on tape reels are cantilevered members which can be supported against extreme shock and vibration only at the cost of a substantial increase in the rotational inertia of a system. So we got rid of them. The tape can't slip off the reel because hoop tension

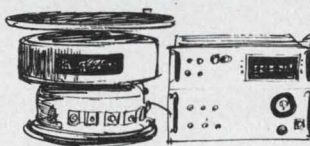


forces resulting from normal pulling of the tape provide great compressive forces within the reel stack. It would take in excess of 300 g's for slippage to occur.

The result of our Sandwich and Flangeless design approaches (plus a few other neat ideas): a rugged, high performance field portable tape system. Request full information.

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## OUR RATE-OF-TURN TABLE LAUGHS AT ABUSE



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The Model 1147's compactness makes it ideal for field or bench checking. Its ruggedness makes it ideal in case you just happen to feel like kicking hell out of a fine piece of equipment.

**Circle reader service #124**

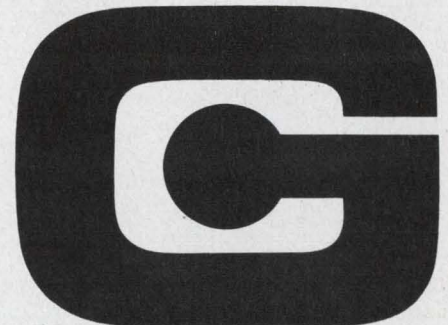
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Out of the hundred or so companies in the industry only two or three use computers. We're better at it than they are, and besides our salesmen know good jokes. Come on, give us a break.

**Circle reader service #125**



GENISCO TECHNOLOGY CORPORATION  
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# Electronic robot speeds training of doctors

## Breathing, heartbeat, even reaction to drugs are simulated in 'patient' and recorded for analysis

The modern Frankensteinian scientist doesn't slink covertly in an eerily lighted laboratory; he works at a modern industrial plant with the help of university professors and a U.S. grant. His robot doesn't look or act like Boris Karloff; it looks like a hospital patient and acts very much like one. And no bolt of lightning is needed to get the robot moving; electronic circuitry and a computer do the job nicely.

Such a robot has been developed to train doctors in operating-room procedures. It is called Sim One by its creators—engineers of the Aerojet-General von Karman Center in Azusa, Calif., and researchers of the University of Southern California in Los Angeles.

Working under a \$272,130 grant from the U.S. Office of Education, the research team devised a "patient" that has soft, plastic skin; a jaw that opens on a full set of teeth, a tongue, vocal cords, a windpipe

and other vital structures; eyes that open and close; carotid and temporal pulse beats; blood pressure; a moving diaphragm and chest, paced by the breathing apparatus; and such physiological reactions as muscles that can freeze in paralysis, a brow that can wrinkle and eye pupils that dilate and constrict when different drugs are administered.

Dr. J. S. Denson of the University of Southern California School of Medicine, co-director of the project with Dr. Stephen Abrahamson, says that Sim One is sufficiently lifelike to be truly representative of a human on an operating table awaiting surgery.

The school hopes the simulator will cut drastically the time needed to teach anesthesia procedures to students (see ED 4, Feb. 15, 1967, p. 68). For example, it now takes about two months to teach a student to insert an air tube delicately

into the windpipe without damaging tissue. With Sim One, it is hoped this time can be slashed to two days.

To develop Sim One, Aerojet engineers reduced all of the physiological responses desired to mathematical equations.

A general-purpose computer with 4000 24-bit words of memory and a 10- $\mu$ s add time is used to control the electropneumatic system that activates the manikin's physical reactions.

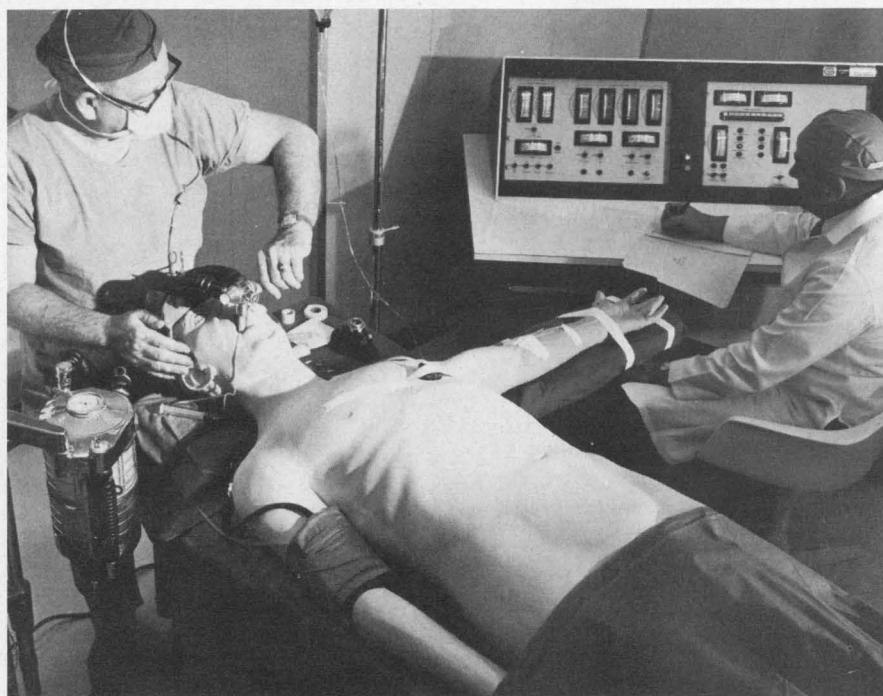
A computer-controlled typewriter printout makes a permanent record of everything the student doctor does to the "patient" and the time it takes the doctor to respond. A strip chart records the action of all vital physical signs as they occur.

### Monitored by instructor

The instructor, seated at a control and display console, monitors the student's actions and the simulated physiological data. The instructor can insert emergency situations, such as severe spasm and closing of the larynx, a block in either the right or left bronchial tube or bucking—an attempt to cough the air tube out of the throat. Heart arrest and even vomiting can be induced.

The robot was manufactured by the Sierra Engineering Co., of Sierra Madre, Calif.

One of Aerojet's biggest problems was to devise a simple way to detect the quantity and kind of drugs administered. This was eventually solved by magnetically coding the needle on each syringe used for injections. In normal surgical procedures, a needle and cup device is inserted into the patient's arm before the surgery begins, and all drugs are administered through this cup. In Sim One a magnetic sensing coil has been placed in the cup to detect which magnetically coded needle is inserted. A piston in the patient's arm is displaced by the drug (which is actually water). The piston operates a potentiometer to indicate the quantity injected. ■ ■



**Electronically controlled manikin** exhibits all the physical properties of a real patient. Student anesthesiologist is adjusting the oxygen flow while the instructor monitors the procedure from the control console.



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TRANSITRON ELECTRONIC CORPORATION, 168 ALBION STREET, WAKEFIELD, MASSACHUSETTS 01880

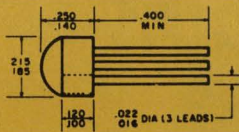
Transitron plastic-packaged silicon planar transistors offer an excellent combination of performance, reliability and low, low price.

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	NPN	2N3710	2N930
	PNP	2N4288	2N2604
	PNP	2N4289	2N2605
General purpose high frequency amplifier and driver	NPN	2N4140	2N2221
	NPN	2N4141	2N2222
	PNP	2N4142	2N2906
	PNP	2N4143	2N2907
High frequency logic	NPN	2N4274	2N744
	NPN	2N4275	2N2369
	PNP	2N4121	2N3248
	PNP	2N4122	2N3249
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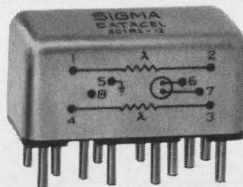
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ON READER-SERVICE CARD CIRCLE 24

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An opto-electronic  
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Solid-state and opto-electronic switching benefits are combined in low-cost Sigma Series 301 Databcels.

**Electrically Isolated Input-Output Circuits:** Light-beam coupling to 1, 2 or 4 photocells provides isolation resistance on the order of  $10^9$  ohms and smooth turn-on, turn-off.

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**Compact Construction:** 1, 2 and 4 pole versions

all designed for high-density printed-circuit packaging. Also socket conversion to solder terminal mounting. In addition each unit visually indicates its on-off state to aid system trouble-shooting.

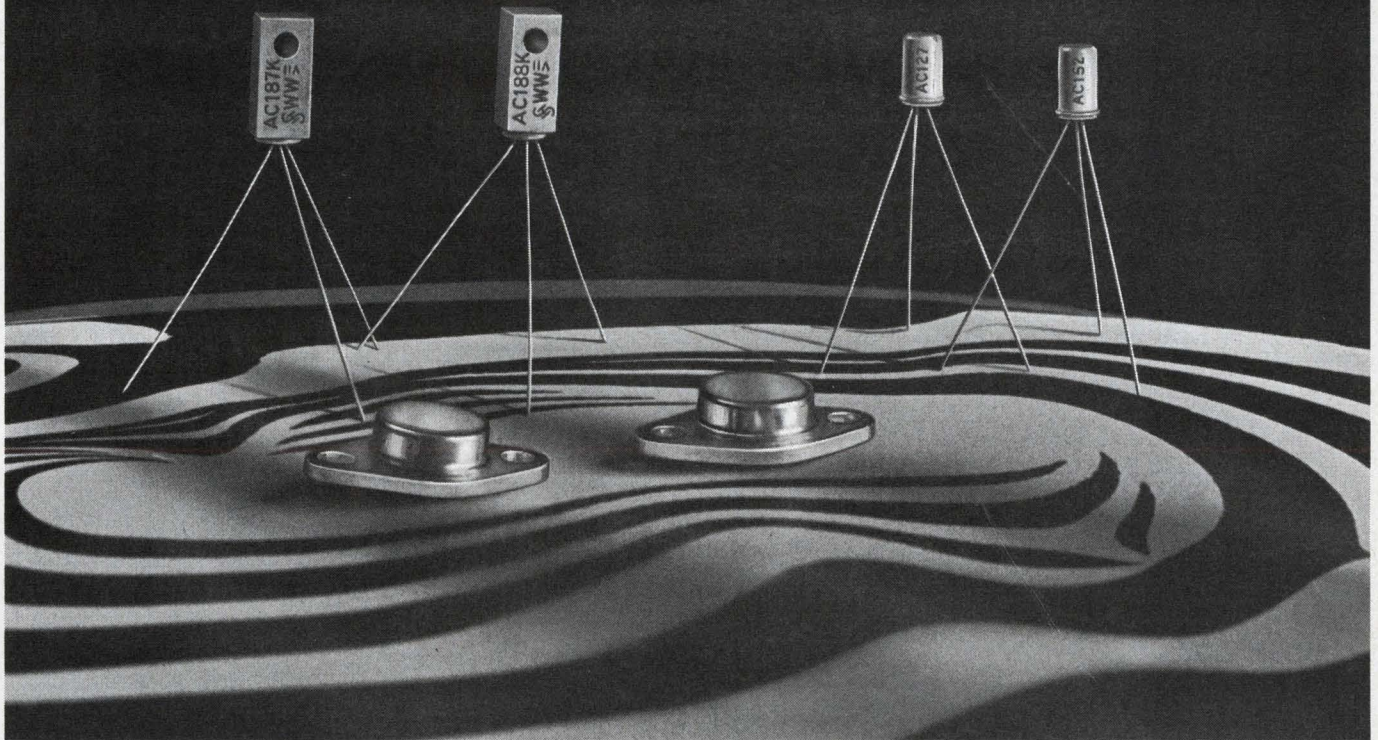
**We'd like to give you a new solid-state Sigma Databcel**—or any of our standard relays. It's the best way we know to prove what we say about Sigma performance. Just circle our reader service number on the reader service card. We'll send you the new Sigma catalog and a "free" request form. Return the form to us and your Sigma representative will see that you get the sample you need.

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ELECTRONIC DESIGN 9, April 26, 1967



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ON READER-SERVICE CARD CIRCLE 26

## Scanner converts maps for EDP storage

An automatic scanner that converts maps into binary data for computer processing is helping the Canadian government manage land resources.

Surveys of natural resources covering vast expanses of terrain are being stored in computer memories or on tape for convenient reference when needed. More than 30,000 such maps have been made in Canada in the last 40 years, according to government sources.

The maps contain information on such points as these: land being used for farming that is unsuitable for this purpose; land unsuitable for farming that is desirable for forestry; land suitable for forestry that should be protected for its wildlife and recreation potential.

Until the introduction of the computer technique, there was no way of bringing all this information together conveniently.

The cartographic scanning system being used by the Canadian Agricultural Rehabilitation and Development Administration was built by the International Business Machines Systems Development Div. at Kingston, N. Y. It consists of a motor-driven drum, a lens-fiber optic array, an amplifier and register, magnetic-tape and control logic units and a clock.

Specially prepared maps up to 50 inches by 50 inches are rolled around the 16-inch drum and held by vacuum. When the drum is rotated, the eight-channel optical head is set to travel down the length of the

drum. This action forms a spiral scan over the map. Each fiber optic channel views a four-mil-square area and is pulsed to eliminate overlap. If at least half the area seen by each channel is black when the pulse is received, a "one" bit is generated. If not, a "zero" bit is formed. The "ones" and "zeros" from each pulse are recorded in groups of eight bits—called bytes—on magnetic tape.

IBM spokesmen say the eight-channel, parallel-to-serial method of scanning simplifies the data transfer to magnetic tape and decreases scanning time. Bytes are produced at tape speed, they say; so a 16-square-foot map (of 18 million bytes) can be scanned in less than 11 minutes.

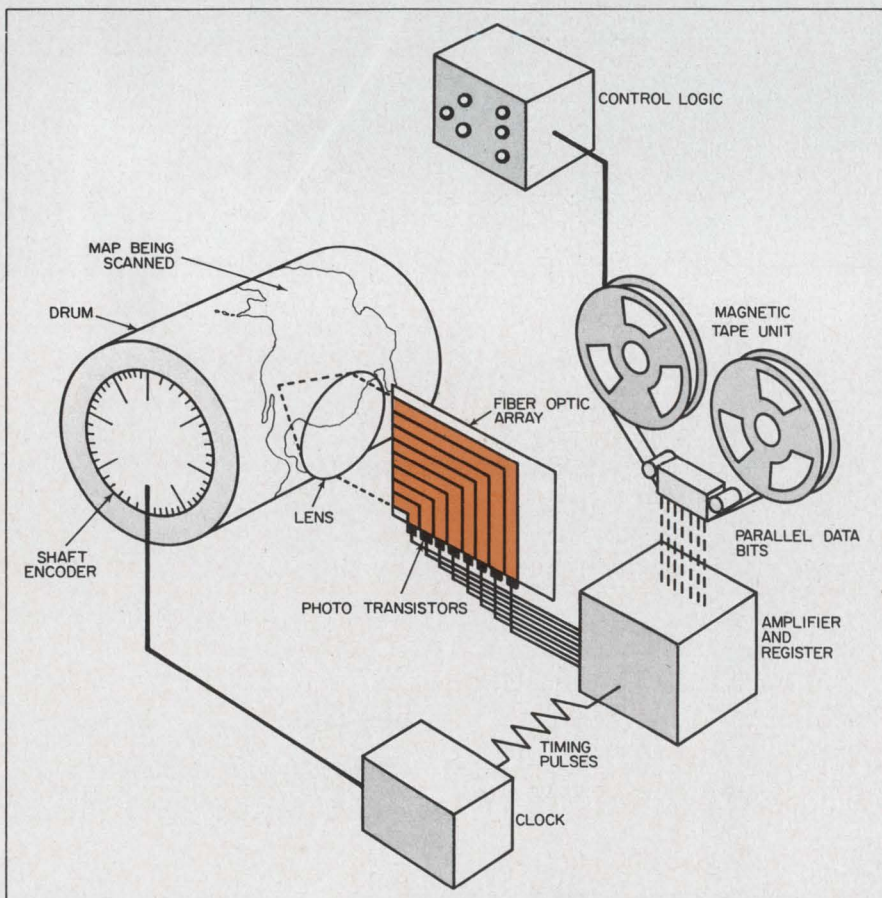
The scanner is used "off line" with an IBM 2401 magnetic tape unit.

Maps to be scanned must be specially prepared to meet minimum standards for contrast, line width and line separation. One way, IBM engineers suggest, is to place a white-coated sheet of transparent plastic over the source map. A stylus is then used to trace the boundaries of the map onto the plastic sheet. As it traces, the stylus removes an eight-thousandths-inch-wide strip of the white coating. When the traced map is placed over the black drum surface, the boundaries appear as high-contrast lines.

After a map has been completely scanned, the tape unit shuts off and the scan head is returned automatically to the starting position. The map can then be removed. IBM says that it takes less than a minute to mount a new map.

The complete geographic information system, which includes the scanner, will use an IBM 360 computer model 65 to create the "data bank."

Information obtained from the Canada Land Inventory program could, according to IBM, be extremely valuable to pulp and paper companies seeking the best possible sites for locating their mills. ■ ■



An IBM cartographic scanner uses an eight-channel fiberoptic array to scan eight 4-by-4-mil spots for parallel-to-serial conversion. Phototransistors convert optical signals from maps into bits for recording on magnetic tape.

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*"Remember, you're never more than a few feet away from a product of ITW®"*



A McDonnell Phantom photo

ON READER-SERVICE CARD CIRCLE 27

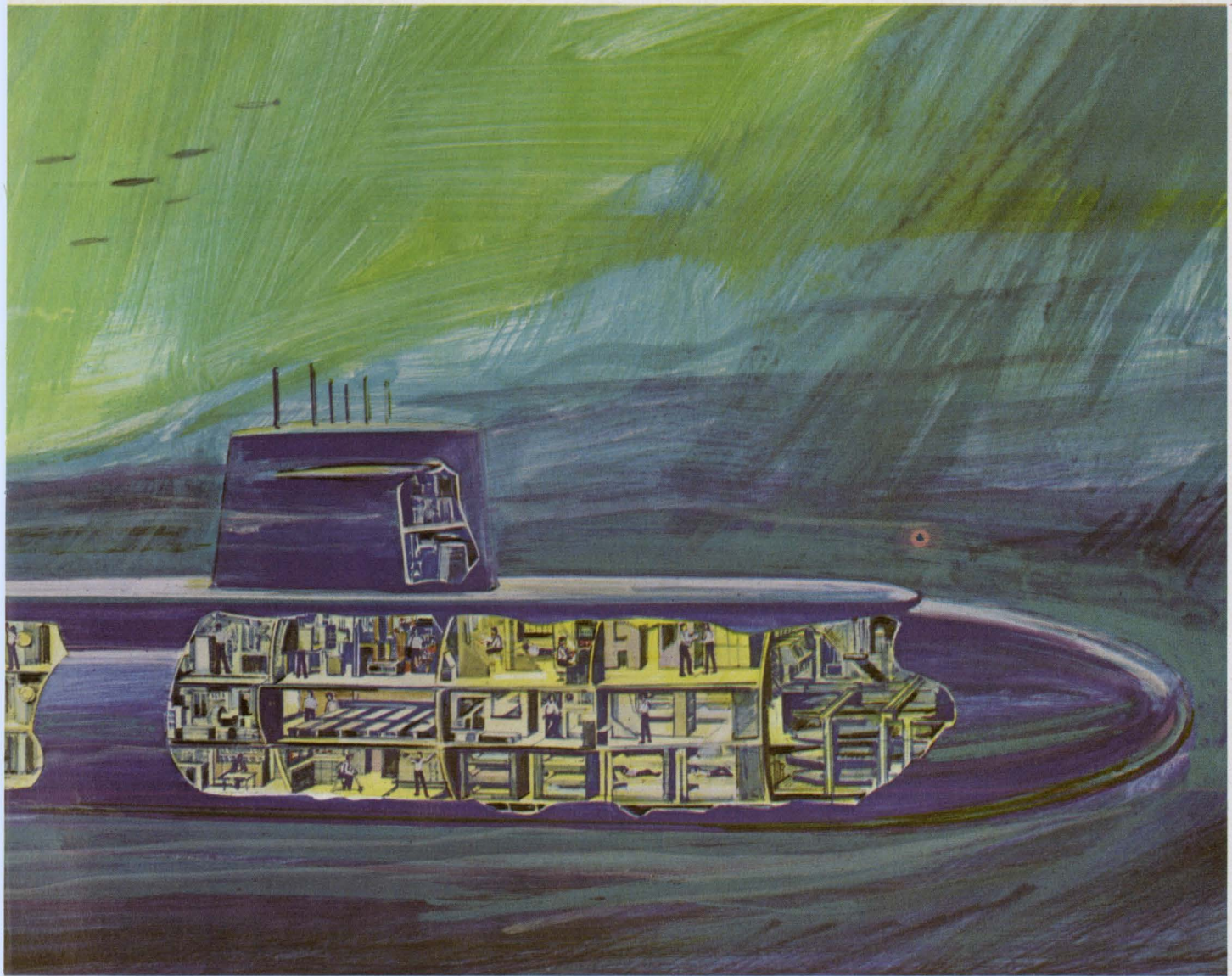


## The Kind of Knowledge that makes progress possible...

During the 1890's, a Paterson, N. J. schoolteacher named John P. Holland was busy perfecting a submarine. It was the ninth underwater vessel he had built in over thirty years, and his eight previous attempts had taught him well. This ship was motor-driven and carried torpedos within its hull. It could travel submerged for fifty miles. In 1900, the U.S. Navy not only commissioned the vessel, but honored its inventor by naming it after him.

Since the *Holland*, men have piled fact upon fact in an unending scientific quest to improve the materials, the propulsion, the range, the striking power, the defenses and the livability of submarines. Today's nuclear-powered submarines are marvels of engineering, controlled by a maze of intricate electronic





## IS THE KIND OF KNOWLEDGE YOU GET FROM KESTER

systems. They can launch missiles while submerged. They can roam the seas for months without resurfacing, while their crews live in a cleaner atmosphere than do most city dwellers. The modern submarine is an amazing example of man's application of accumulated knowledge.

This knowledge of experience is the kind of knowledge you get from Kester. Even before the Holland sub was commissioned, Kester Solder products and soldering knowledge were serving industry. And as technology accelerated, Kester kept pace.

Today, after 67 years of working with development engineers in the technology of solders, fluxes and their applications, Kester stands ready to serve you. Write, phone or wire for specific information.



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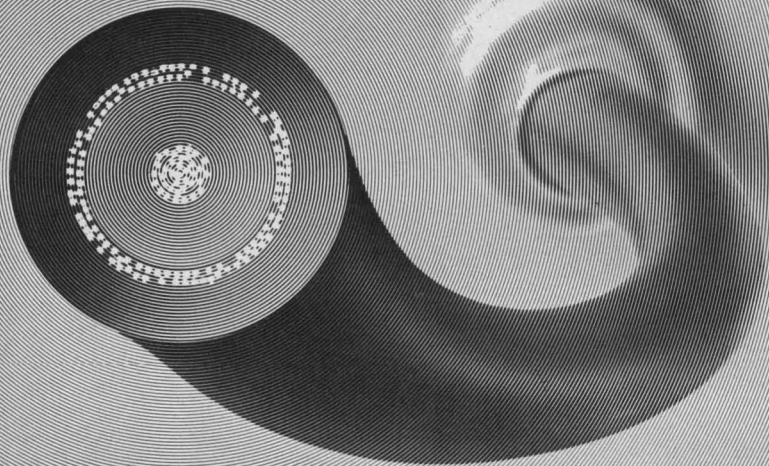
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ON READER-SERVICE CARD CIRCLE 28

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(From 20 MHz to 1000 MHz)

If you're checking frequency response of a high power circuit you just can't get along without it! Now, with one of Telonic's four PD Sweep Signal Generators you can test response at power conditions that simulate actual operation of the circuit.

The PD instruments provide a full 4 watts of swept RF or 2 watts CW covering frequencies from 20 to 1000 MHz. Sweep width is continuously variable from 0.2% to 15% and a 1 db stepping attenuator provides a wide 59 db of attenuation range.

Call your local Telonic representative for a demonstration or write for Catalog 70 covering the entire line of Telonic Sweep Generators and "How To Use Them."



General Specifications

Models	Range (MHz)	Function
PD-2	20-100	Sweep—14 volts RMS into 50 (4 watts)
PD-3	100-250	
PD-7	200-375	CW—2 watts into 50 ohms
PD-8	375-1000*	

\*Up to 2000 MHz (with 2 watts output) using Telonic Frequency Multiplier.

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Represented throughout the U.S. and overseas. Factory offices in Maidenhead, England, and Frankfurt, Germany.

ON READER-SERVICE CARD CIRCLE 29

NEWS

Device measures minute distance

An ultrasensitive instrument that accurately measures extremely short distances— $10^{-3}$  to  $10^{-6}$  cm—with an accuracy of about 10 parts per million has been developed by a National Bureau of Standards scientist.

The accuracy of the instrument, according to its developer, Dr. Russell Young, is limited only by available calibration techniques.

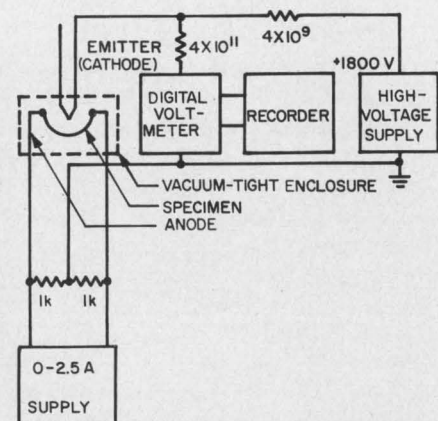
Called a field-emission ultramicroscope, the instrument is basically an arrangement of field-emission electrodes enclosed in a vacuum chamber.

The electrodes are connected to a constant-current electrical circuit (see diagram) such that a precise digital voltmeter indicates a voltage directly related to the spacing between the electrodes. The current source ensures a constant electron flow through the emitter to the anode.

Available devices of limited use

Devices for precise measurement of short distances have been available, Young noted, but are limited in two important respects:

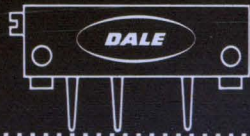
- They involve delicately balanced bridges and mechanical or optical



Field-emission ultramicroscope can measure distances in the  $10^{-3}$ -to- $10^{-6}$ -cm range with a reproducibility said to be within 1 part in  $10^5$ . In the experimental setup above, the tantalum strip serves as the anode. The recorded voltage is directly related to the spacing between the emitter and anode.

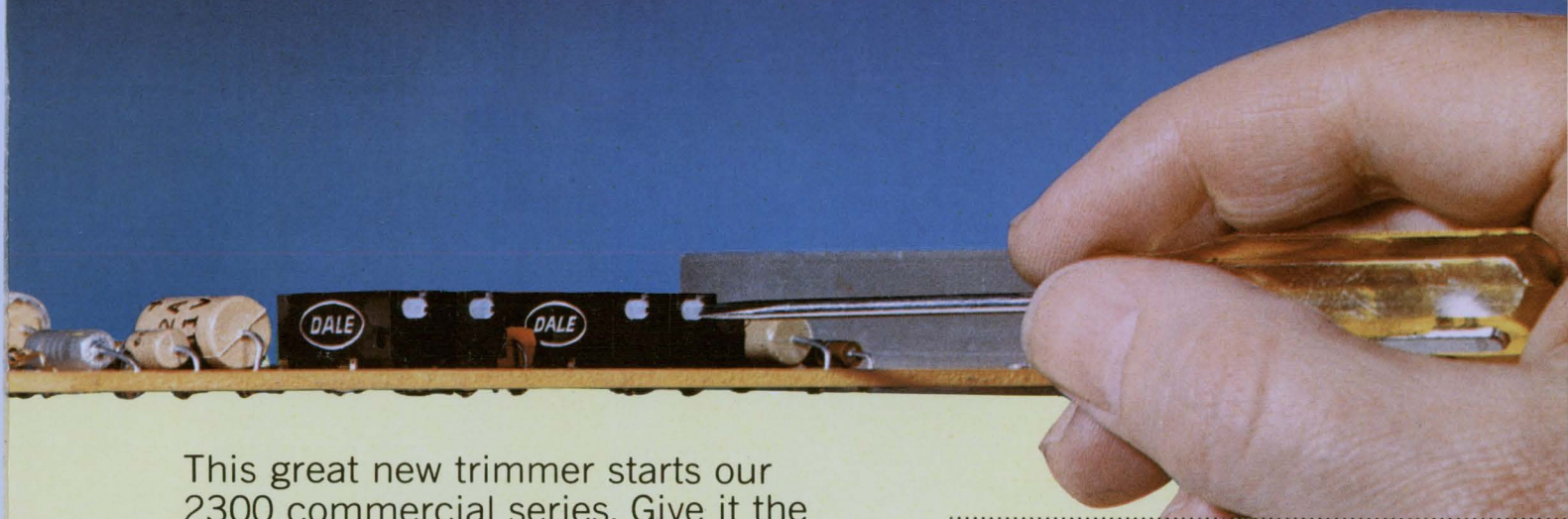
ON READER-SERVICE CARD CIRCLE 135 ➤

# You name it.



Dale's new 1/2 watt trimmer — costs less than \$1.00

## Win \$500.



This great new trimmer starts our 2300 commercial series. Give it the right trade name and you'll win \$500.

Remember these 3 important tips:

1. It costs less than \$1.00\*.
2. It is interchangeable with other one inch commercial models.
3. It has excellent setting stability.

One thing more, it's a direct descendant of Dale's Mil-Style trimmer line and uses many similar design and production techniques. Go ahead. Send us the name you like best on the reply card. It could earn you an easy \$500. There's nothing to buy — unless you're looking for a better source for 1/2 watt commercial wirewounds — for less than \$1.00\*.

\*In 1,000 quantities

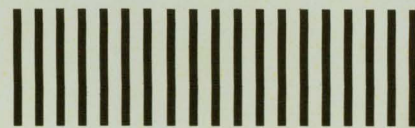
**Send this postpaid entry card today.**

*Complete contest details on reverse side.*



**DALE ELECTRONICS, INC.**  
1300 28th Avenue, Columbus, Nebraska 68601  
In Canada: Dale Electronics Canada, Ltd.

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PERMIT NO. 503  
Columbus, Nebr.



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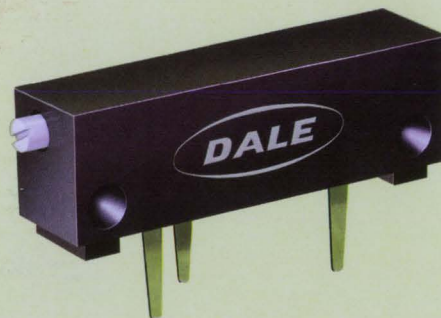
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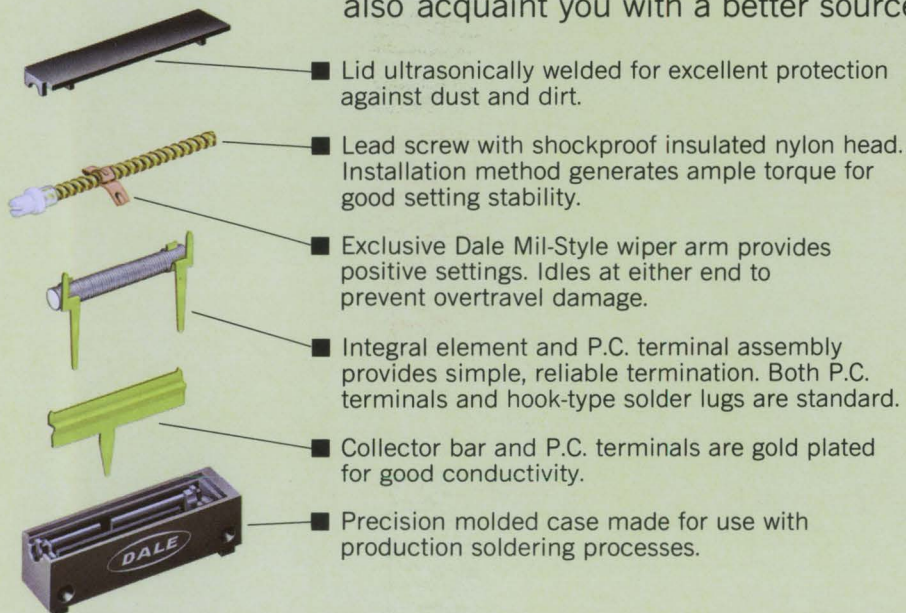
**DALE ELECTRONICS, INC.**  
Dept. 88600, P.O. Box 609  
Columbus, Nebraska 68601

# Win \$500.

Name Dale's new 1/2 watt commercial trimmer - costs less than one dollar



**Read before entering.** These details can help you choose a good trade name for Dale's 2300 Series. They can also acquaint you with a better source for low cost trimmers.



- Lid ultrasonically welded for excellent protection against dust and dirt.
- Lead screw with shockproof insulated nylon head. Installation method generates ample torque for good setting stability.
- Exclusive Dale Mil-Style wiper arm provides positive settings. Idles at either end to prevent overtravel damage.
- Integral element and P.C. terminal assembly provides simple, reliable termination. Both P.C. terminals and hook-type solder lugs are standard.
- Collector bar and P.C. terminals are gold plated for good conductivity.
- Precision molded case made for use with production soldering processes.

## SPECIFICATIONS

**Standard Resistance Range:** 10 ohms to 50K ohms

**Resistance Tolerance:** ±10% standard

**Resolution:** .18% to 1.82%

**Power Rating:** 0.5 watt at room temperature to 0 watt at 85° C

**Operating Temperature Range:** -55° C to 85° C

**Mechanical Adjustment:** 15 turns nominal

**Mechanical Stops:** None. Clutch mechanism permits overtravel without damage

**Dimensions:**  
1.0" L x .36" H x .28" W

**Terminals:**  
P.C. terminals (Model 2387)  
Hook-type solder lugs (Model 2389)

*I think Dale's 2300 Series Trimmers should be trade named:*

- \_\_\_\_\_
- Send me additional information on the 2300 Series

*My job function:*

- Design Engineering  
 Specification  
 Procurement

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TITLE \_\_\_\_\_

COMPANY \_\_\_\_\_

ADDRESS \_\_\_\_\_

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Card must contain all requested information in order to qualify for contest.

# Enter today!

**It's easy - just fill out & mail this postcard.**

Make it short! Something that quickly describes 2300 advantages. Examples are "Cost-Trim" or "PC-Pot".

Nothing to buy - but if you want to call for a price on the 2300 Series, our number is 402-564-3131.

## CONTEST RULES

Send the return postcard at left or a similar form containing identical details to Dale Electronics, Dept. 88600, Box 609, Columbus, Nebraska 68601. Submit only one name per card. Entry must be postmarked by midnight, June 15, 1967, and must be received by Dale by June 22, 1967. Anyone living in the United States or its possessions is eligible except employees of Dale Electronics, affiliated companies, advertising agencies and their families. All entries become the property of Dale Electronics and entrant relinquishes all claims for use of proposed trade name submitted. Entries will be judged solely on the basis of their usefulness as a trade name describing Dale 2300 Series Trimmer Potentiometer. Judges decision is final. In case of duplication, winner will be determined by earliest postmark. Winner will be notified by mail approximately 30 days after contest closes. No other correspondence will be entered into. Winner assumes all tax responsibility for prize. Contest void where prohibited by law.

For complete information circle 181



**DALE ELECTRONICS, INC.**

1300 28th Avenue, Columbus, Nebraska 68601  
In Canada: Dale Electronics Canada, Ltd.



Printed in U.S.A.

levers that are sensitive to high temperatures.

■ They have to be in physical contact with the object that is to be measured.

The field-emission ultramicro-  
meter overcomes these limitations. It  
is particularly suited to measuring  
curved surfaces where errors may  
be introduced by depressions or  
scratches, the scientist said. The  
simplicity and small size of the sen-  
sor is another advantage cited by  
Young.

The ultramicrometer is expected  
to have a variety of applications.  
These include uses as a strain gauge  
to measure the deformation of struc-  
tural materials, as a differential  
thermal expansion cell, as a con-  
tact-free delineator of surface pro-  
files and contours, and as a means  
for measuring the diameters of balls  
and holes.

#### Operation similar however used

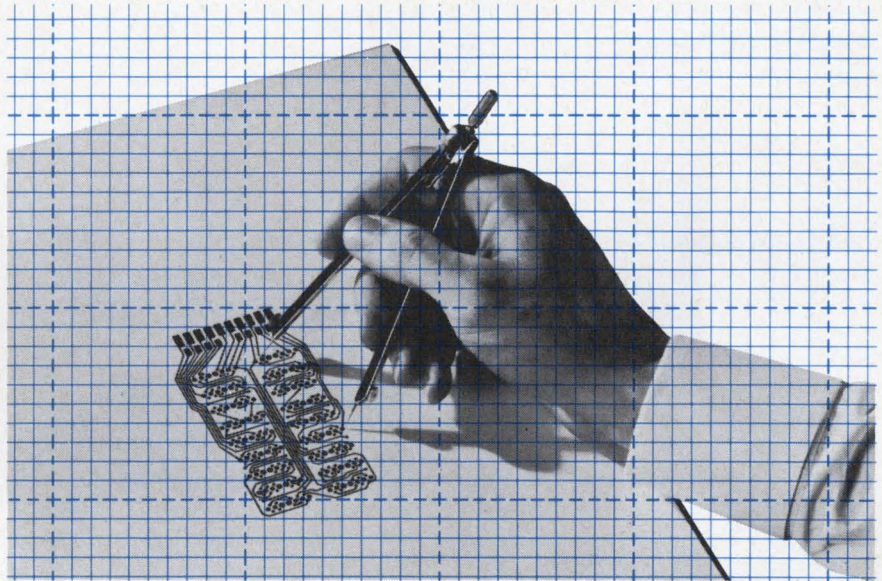
The operation of the instrument  
for the various applications is essen-  
tially the same. For example, as a  
delineator of surface profile, a field-  
emission tip serves as one electrode  
(at a high negative voltage) and the  
surface to be measured as the other.  
As the field emitter moves across  
the surface, recorded changes in  
voltage indicate changes in profile.  
Equations fix the relationship be-  
tween the voltage and the distance  
from the emitter to the surface.

The accuracy of the minimum de-  
tectable displacement, Young said,  
depends on solutions of Laplace's  
equation, the precision of the volt-  
meter, the stability of the constant-  
current source, and the mechanical  
stability of the components. These  
factors, Young said, can all be eval-  
uated without recourse to any form  
of experimentation.

The field-emission ultramicro-  
meter has already been used in sev-  
eral applications at the NBS In-  
stitute for Basic Standards (U.S.  
Dept. of Commerce). NBS has de-  
cided not to patent the device but  
has put it in the public domain.  
Consequently, a number of outside  
manufacturers have expressed great  
interest in it.

One company, according to Young,  
plans to use it to detect the surface  
roughness of steel balls. Another  
foresees uses in measuring the cur-  
vature of optical surfaces. ■ ■

# Shortest accurate distance between two points ...



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\*ACCURATE, STABLE, NON-REPRODUCIBLE

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pensate for inaccurate graphs and grids. Adapting. Redesigning. Erasing  
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extremely high accuracy. Either the fifth or the tenth line on \*ASN  
grids is broken to permit easier interpretation of dimensions. And the  
CAPITOL grid will not smear or erase.

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ON READER-SERVICE CARD CIRCLE 30

# IBM Circuit Design and Packaging Topics

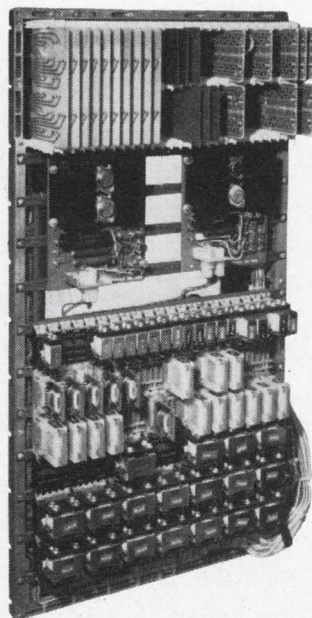
- packaging cost reductions
- high-speed switching
- reed switch application data

## packaging cost reductions

Performance Measurements Co., Detroit, Michigan, reports significant savings in packaging their new electronic recording system. The packaging method previously employed required two gates to mount the components in the main console. Now, with IBM's modular packaging as pictured below, only one gate is needed. That's because the IBM technique makes the most efficient use of console space with compactly mounted and connected circuit boards, relays and hardware.

Mounting time has been saved too. Pluggable components, low-cost card receptacles and interlocking card guides have so simplified the packaging job, that Performance Measurements now saves 70% on the cost of mounting hardware. Fewer and shorter wires are needed in the compact console—eliminating three feet of 1½-inch cable and shortening a second cable by eight inches. The modular chassis gave designers freedom to experiment freely with various mounting configurations. It also permits easy access for servicing and diagnostic analysis.

The same design freedom, plus significant hardware and labor savings are available in many applications.



IBM components and packaging can help you in timing control, digital logic testing, telemetering, process or numerical control.

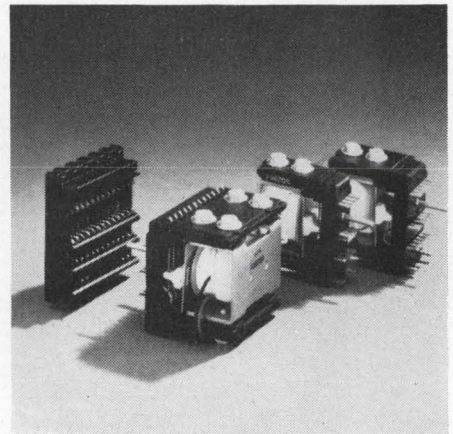
## high-speed switching

IBM wire contact relays were originally designed for data processing use. Now they are being used extensively in machine tool and assembly applications. One of these assembly applications is a numerically-controlled component insertion machine. It sequentially inserts random combinations of up to 24 different types of axial lead resistors and diodes into printed circuit boards. Such machines have been widely used, often on a round-the-clock, three-shift basis, in IBM's electronic assembly operations.

Insertion rates range from 3,000 to 4,500 components per hour, depending upon the type of components being inserted.

Instructions from an 8-channel punched paper tape provide the logic input to the relay gate. The gate employs three rows of 6- and 12-pole IBM wire contact relays. These relays control the movement of each printed circuit

board through the X and Y axis positioning of the board for each component insertion. They also control the component feed, component insert, and cut-and-clinch cycles for each insertion operation.



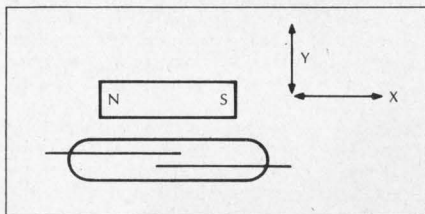
IBM wire contact relays can perform in excess of 200 million operations with an operate speed as fast as 4.5 ms, a release time of 5 ms maximum. The product line includes 4-, 6-, and 12-pole Form C relays, 4- and 6-pole latch models, all with compact, solderless, pluggable mountings—with coil-voltages up to 100 VDC.

## reed switch application data

Data on the magnetic switching characteristics of miniature dry reed switches is available to design engineers on request. The data was compiled from ex-

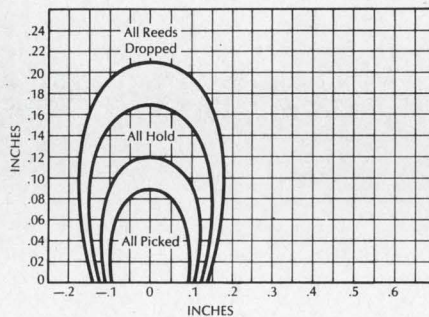
tensive tests conducted by IBM to help the design engineer use these switches most effectively. It can also help him determine the motion and position of the magnet required.

Simply described, a miniature dry reed switch operates under the influence of a permanent magnet. When the magnet is adjacent to the reed switch,



the flux of the magnet flows through the cantilever beams, as illustrated. While this magnetic flux is being carried by the beams, a polarity exists across the beams. Look at the overlap area of the beams. The north pole of one beam and south pole of the other beam are in proximity. Since unlike poles of a magnet attract each other, when the magnetic force becomes great enough to overcome the physical mass of the beams, they "snap" together, thus switching.

On the graph the X axis represents the displacement (in degrees for rotary motion, inches for lateral motion) of a magnet's center with reference to the center of the reed switch. The Y axis represents displacement (in inches) of the magnet from the outer edge of the



dry reed switch glass envelope. Dimensions shown along both axes represent displacement from the center of the magnet in alignment with the center of the reed switch.

There are some "gray areas" where performance varies due to minor differ-

ences in the characteristics of each switch. In these areas the status of each switch is not completely predictable.

Assume the zero point on the X axis is the magnetic center of an IBM reed switch. The magnet is positioned with its center at +.5 on the X axis, and .04 inches above the glass envelope. If the magnet is set in motion along the X axis toward the center of the switch, some reeds will pick when the center of the magnet reaches the point +.12 on the X axis. (The magnet has then reached the "gray area"). If motion is continued toward the center of the switch, all reeds will pick when the center of the magnet reaches the point +.09 on the X axis.

**IBM Industrial Products Marketing Dept. T1**  
**1000 Westchester Avenue**  
**White Plains, New York 10604**

- packaging cost reductions
- high-speed switching
- reed switch application data

name \_\_\_\_\_

position \_\_\_\_\_

company \_\_\_\_\_

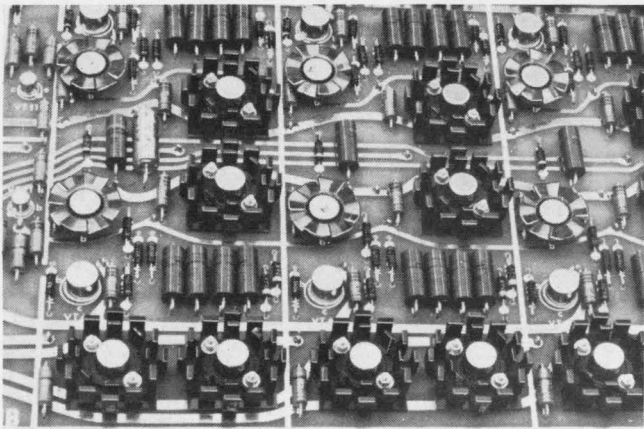
address \_\_\_\_\_

city \_\_\_\_\_ state \_\_\_\_\_ zip \_\_\_\_\_

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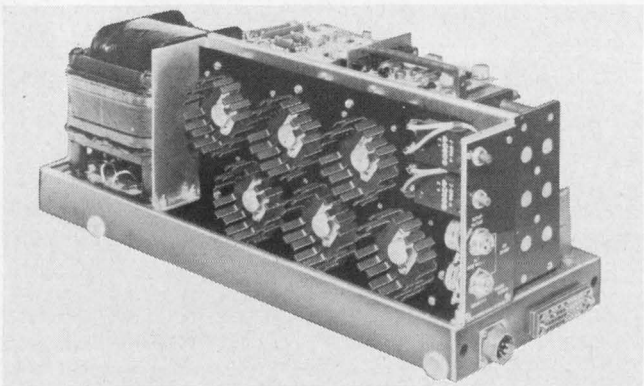
# Tips on cooling off hot transistors

See how circuit designers use IERC heat dissipators to protect semiconductors... improve circuit performance and life.

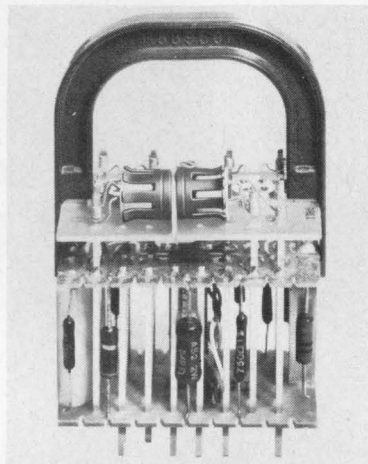


A 2N1837 transistor mounted only to a p-c board with IERC's unique LP dissipator can be operated at 5 watts with a junction temperature of only 153°C. The LP's clamping method makes good thermal contact on both surfaces of the transistor flange, minimizing thermal resistance from transistor to dissipator.

Heat from power transistors or diodes is quickly dissipated with IERC's HP dissipators. Large finger area maximizes efficiency in natural convection or forced air environments. Staggered-finger design which prevents finger surfaces from "looking at each other," radiates heat to the ambient, not back to the dissipator.

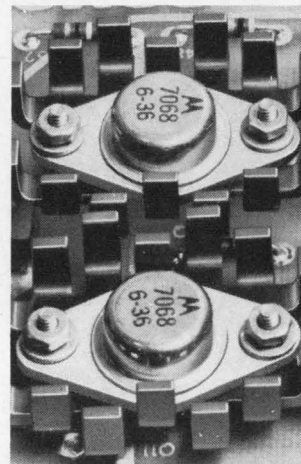
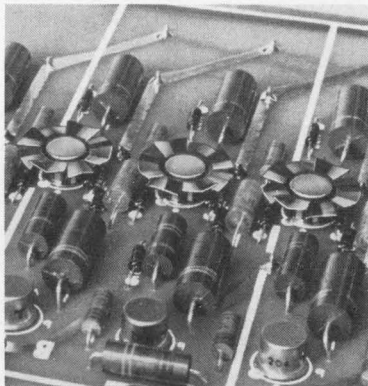


**Send for test reports.** The most thorough test reports in the industry are available on IERC Heat Dissipators. These are multi-page reports complete with graphs showing case and junction temperatures vs. power dissipation for transistors in several mounting conditions. Please indicate which test reports you wish—LP, UP, HP or Therma-Link. On your company letterhead, please.



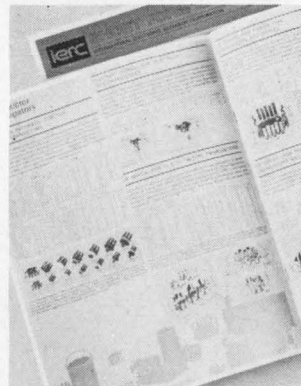
**Mounting matched transistors** for thermal stability so electrical characteristics stay identical is simple with back-to-back Therma-Link dissipators/retainers. Also used as heat sinks.

**Fan-top dissipators** increase transistor performance levels, permit use of cheaper transistors. Note how design needs no board space, permits other components to be positioned close by.



**New dissipator** for TO-66 transistor uses only 1.7 sq. in. of board space. IERC's unique, staggered-finger design dissipates 9 watts with case temperature of less than 150°C.

**Free 8-page catalog** gives complete pictorial and ordering data on IERC dissipators, retainers and tube shields, also prices. Send for a copy.

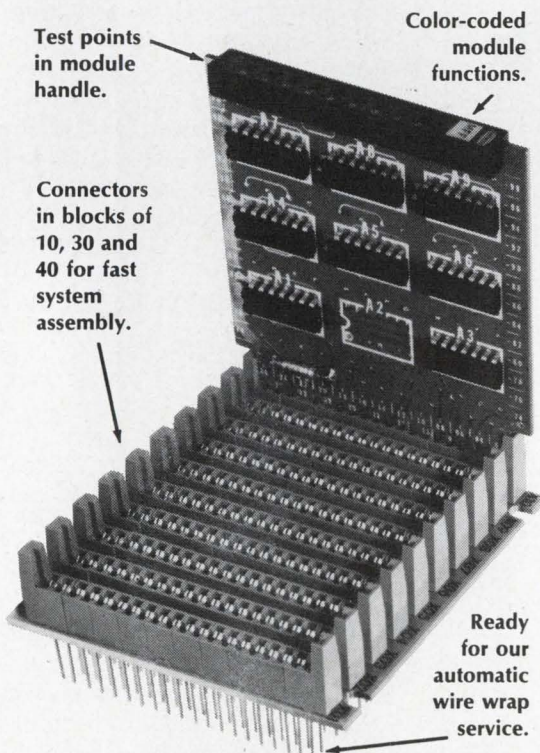


**ierc**  
SEMICONDUCTOR  
HEAT DISSIPATORS

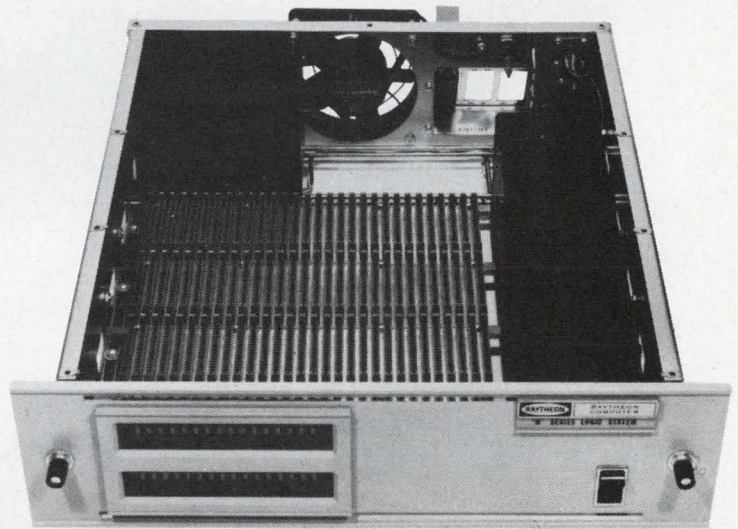


# The Unbeatable IC System:

**Your logic design and Raytheon Computer modules and hardware.**



Laminated power bus bars installed and wired in each module case. Reduces noise, eliminates power inter-connections, cuts hours from assembly and test time.



Indicator lights display system operation.

This case holds 120 modules. There's also one for 40; another for 400.

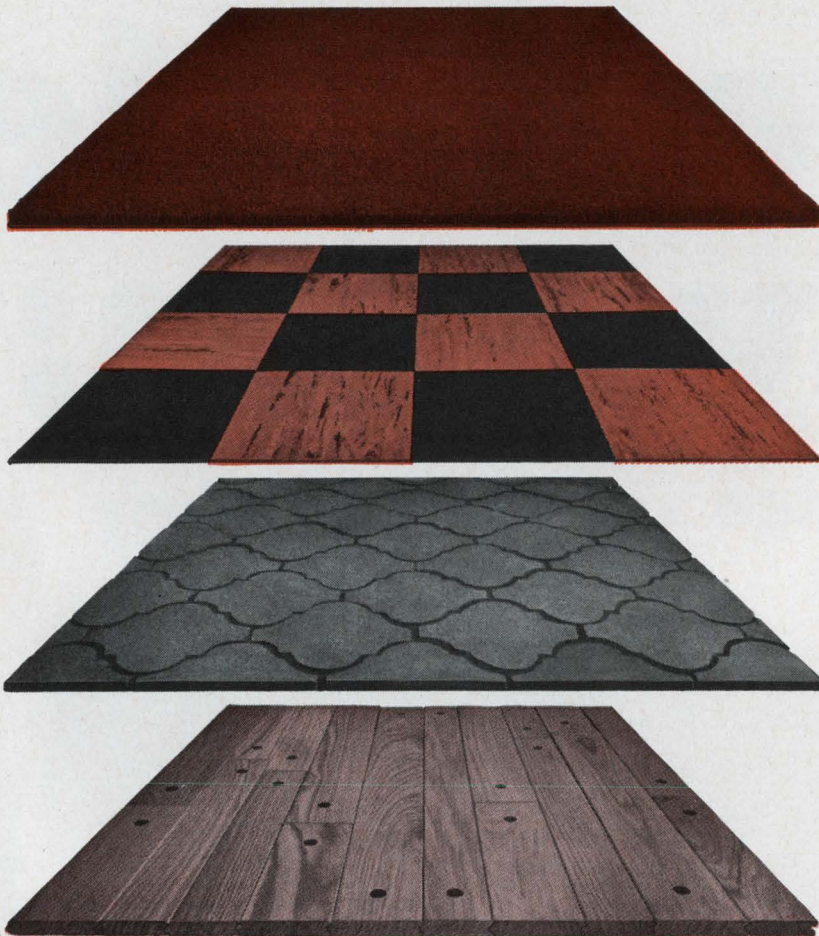
**Raytheon Computer's M-Series** — more than 30 modules—connectors, cases, power supplies and power distribution are so thoroughly engineered you can concentrate on logic and electronic design, not mechanical details. Every step—design, assembly, test, check-out, troubleshooting—is easier than you thought it could be.

**We'll even help you design your logic.** Call or write today for a visit from a helpful applications engineer or for the whole story in print. Ask for Data File M-136. Raytheon Computer, 2700 S. Fairview St., Santa Ana, Calif., 92705, Phone: (714) 546-7160.



ON READER-SERVICE CARD CIRCLE 33

## Lamb Electric engineering turns your product on.



### Example: the whole world of floor care

If your product has got to vacuum, scrub or polish, you need Lamb engineering. Lamb products turn on the whole range of equipment that cares for floors.

For example, you might be interested in our gear motors customized from standard Lamb parts . . . or one of our many vacuum motors that assure you of the right combination of performance, life and cost. Whatever floor care product you manufacture, Lamb Electric has the motor that will do the job for you.

Let Lamb engineers turn your product on. Write for motor details and performance curves. Put us to the test. We'll turn your product on . . . with exactly the motor that you need. Ametek, Inc., Lamb Electric Division, Kent, Ohio 44240.

**AMETEK / Lamb Electric**

# AMETEK

ON READER-SERVICE CARD CIRCLE 34

## Letters

### FBI affirms interest in computer fingerprinting

Sir:

I am concerned about the misinformation appearing in the "Washington Report" by S. David Pursglove published in the March 1, 1967, issue of *ELECTRONIC DESIGN* [ED 5, p. 31]. His inaccurate comments regarding the study undertaken to develop a computer program for FBI fingerprint files tend to discredit the efforts of our own and the automatic-data-processing industry personnel.

The facts are that a request for a quotation was submitted to the industry on Dec. 16, 1966. The closing date for proposals in response to this request was set at Feb. 20, 1967. As an indication of the industry's interest, it is noted that representatives of more than 30 companies attended a preproposal conference held on Jan. 12, 1967, at FBI Headquarters. A number of proposals have been received and are currently being studied.

The entire law enforcement community is eagerly awaiting this milestone development in the war on crime. In view of the widespread importance of the study and in the interest of fairness and accuracy, I want to bring these facts to the attention of your readers.

J. Edgar Hoover

Director  
Federal Bureau of Investigation  
Washington, D. C.

### Correspondent's reply

*Much misinformation in reportorial coverage of the FBI stems from that agency's unhealthy compulsion toward secrecy extending even to its purchases of office stationery and supplies.*

*When we heard of the request for proposals to which Mr. Hoover refers, our Washington Office telephoned a public-relations official at the FBI for details. He replied that*

*(continued on p. 60)*

ON READER-SERVICE CARD CIRCLE 35 ➤



## With a little ingenuity...

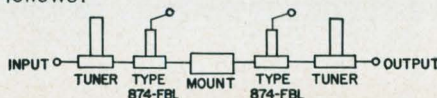
you can interconnect GR874-equipped coaxial elements to form countless unique "instruments" or special-purpose circuits that are both practical and inexpensive. Experimentation with various setups is greatly simplified by the sexless design of the GR874 connector; any two connectors mate, whether they are locking or non-locking types.

The GR874 connector is the keystone of a versatile coaxial system that includes a wide variety of elements and components . . . power dividers, air lines, trombones, tees, elbows, pads, terminations, adaptors, etc. Typical VSWR of a pair of locking-type, rigid-air-line connectors is less than 1.02 to 6 GHz and about 1.06 at 9 GHz. Pulses are passed faithfully by the connector without ringing or deterioration of rise/fall times.

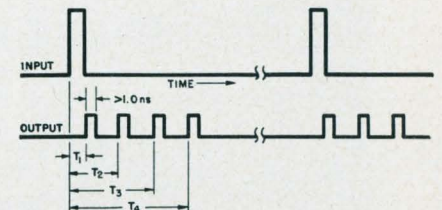
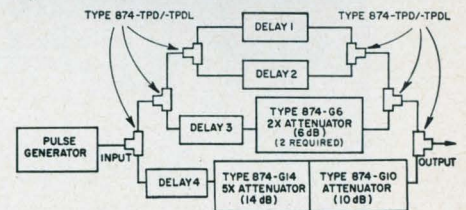
You can build a simple one-transistor amplifier operable to 5 GHz with two tuners (each comprising a GR874 tee and a GR874 adjustable stub), two bias insertion units (Type 874-FBL), and a transistor mount (one of eight types available) arranged as follows:



Type 874-BBL Basic Connector (locking) for use on  $\frac{1}{16}$ -inch-ID, rigid, 50-ohm air lines.



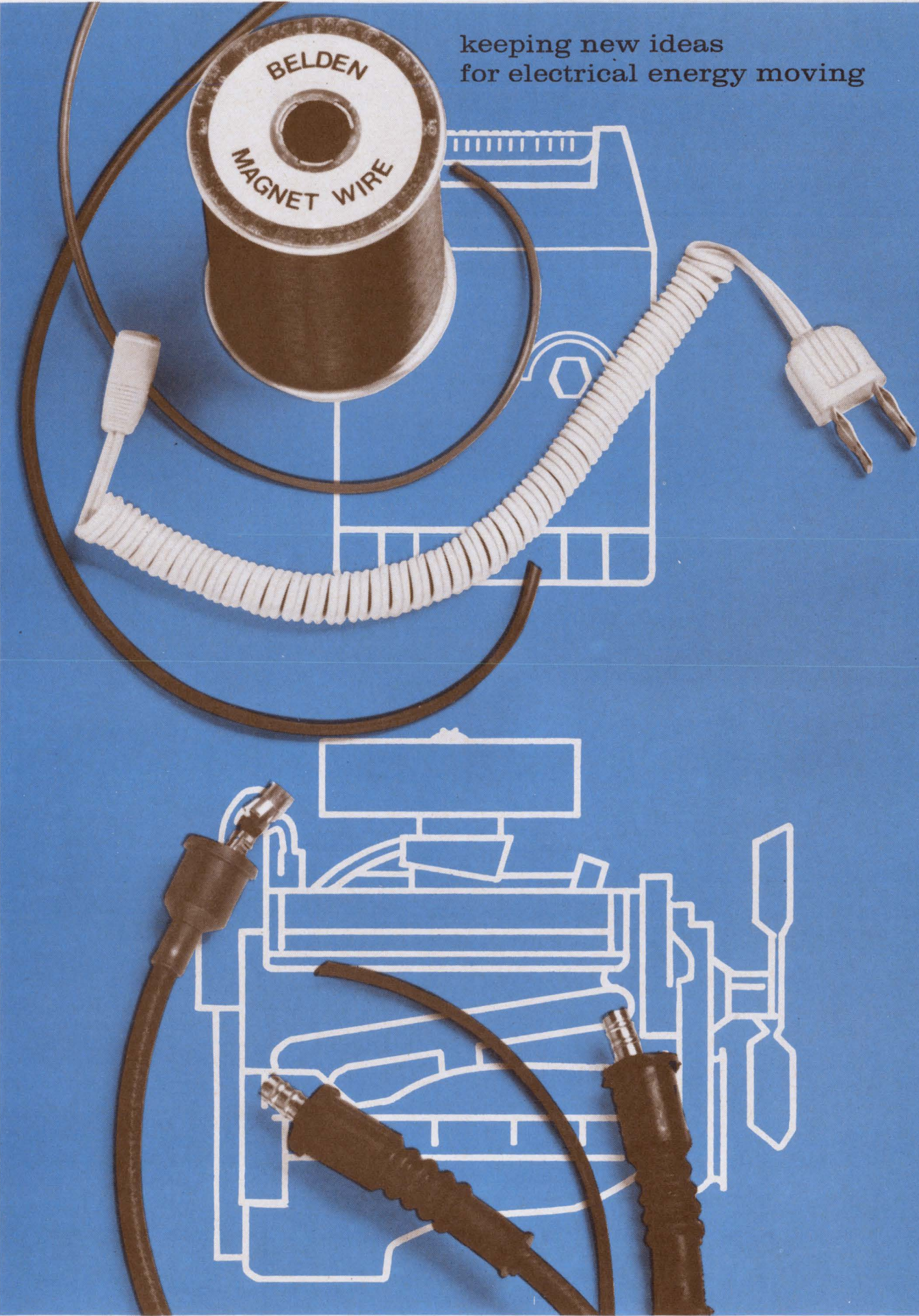
As another example of GR874 versatility, the components shown below can be used to produce bursts of high-rep-rate pulses from the output of a low-frequency, sub-nanosecond-rise-time pulse generator. The delays (up to 1 ns per section) are provided by GR874 air lines.

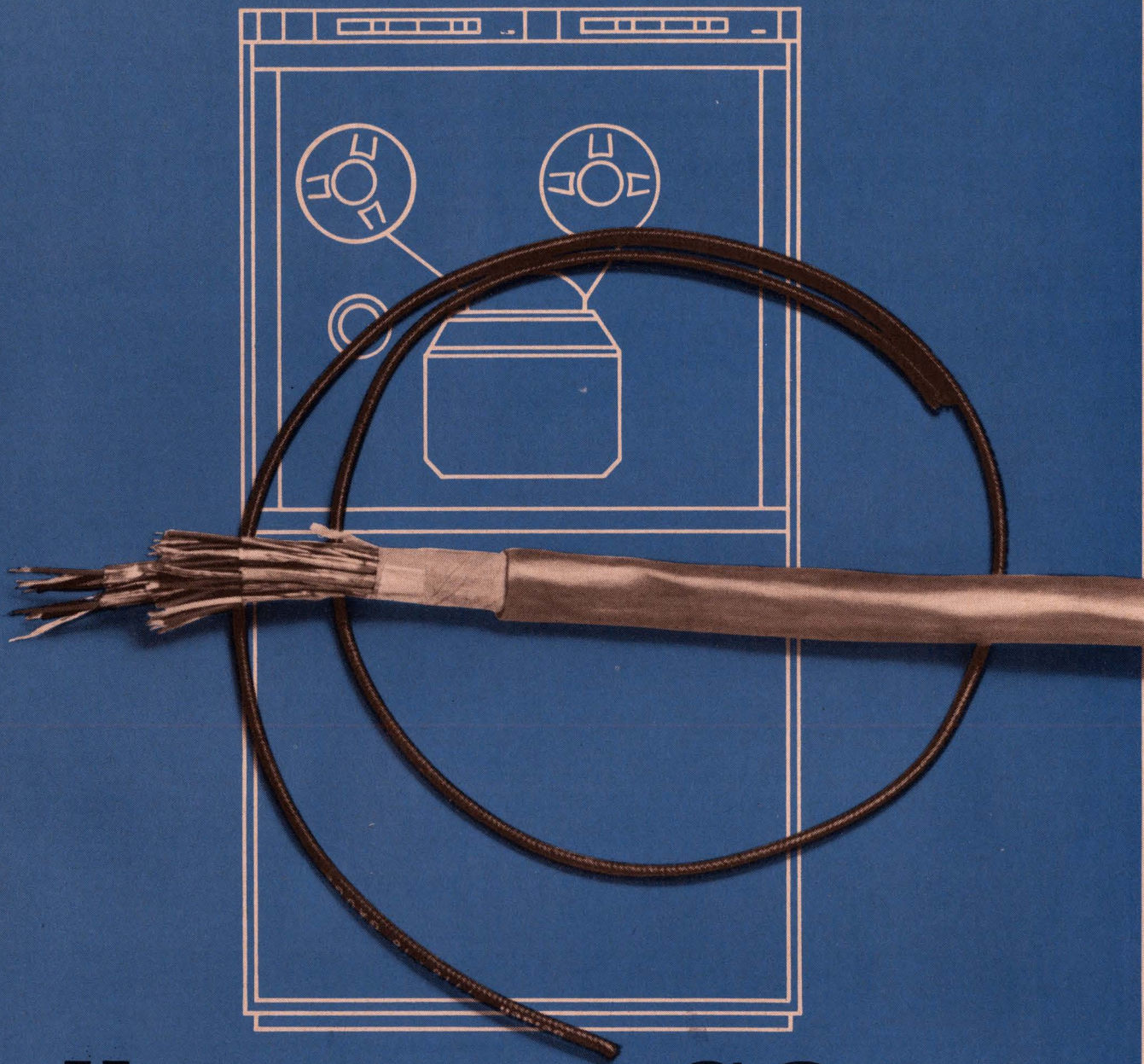


For complete information on the GR874 line, write General Radio, W. Concord, Massachusetts 01781; telephone (617) 369-4400; TWX 710 347-1051.

**GENERAL RADIO**

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for electrical energy moving





# all systems GO

...when a Belden team of wire specialists shows you their dozen or so ways to wring out hidden values and costs. For example you can delve into design..maneuver with materials..analyze assembly..pry into processing..pick different packaging..or a host of others. But success takes a supplier who is really perceptive—one who makes all kinds of wire for all kinds of systems. Want to join us in wringing out values and costs? Just call us in...Belden Manufacturing Company, P.O. Box 5070-A, Chicago, Illinois 60680.

**Belden**

ON READER-SERVICE CARD CIRCLE 36

## COULD YOU SLICE THIS ANGLE INTO 300 EQUAL PARTS?

### MCCOY DOES EVERY DAY!

That's the final step in cutting crystal blanks at McCoy. Prior to this several cuts are made with diamond saws...and after each cut, blanks are X-rayed to assure proper angle.

X-ray inspection equipment is accurate to 1/300 of 1° of angle. Angle accuracy is vital because it influences crystal behavior under varying temperatures.

Blanks are then lapped—a few millionths of an inch at a time—to the desired thickness, accurate within 10

millionths of an inch. Crystals are then coated with metal films (in high vacuum evaporation platers) only a few millionths of an inch thick to provide the exact frequency required.

These are but a few of the precision operations that assure you of the highest quality available when you specify McCoy crystals, oscillators and filters.

For full details on these precision components, write for our new product catalog.



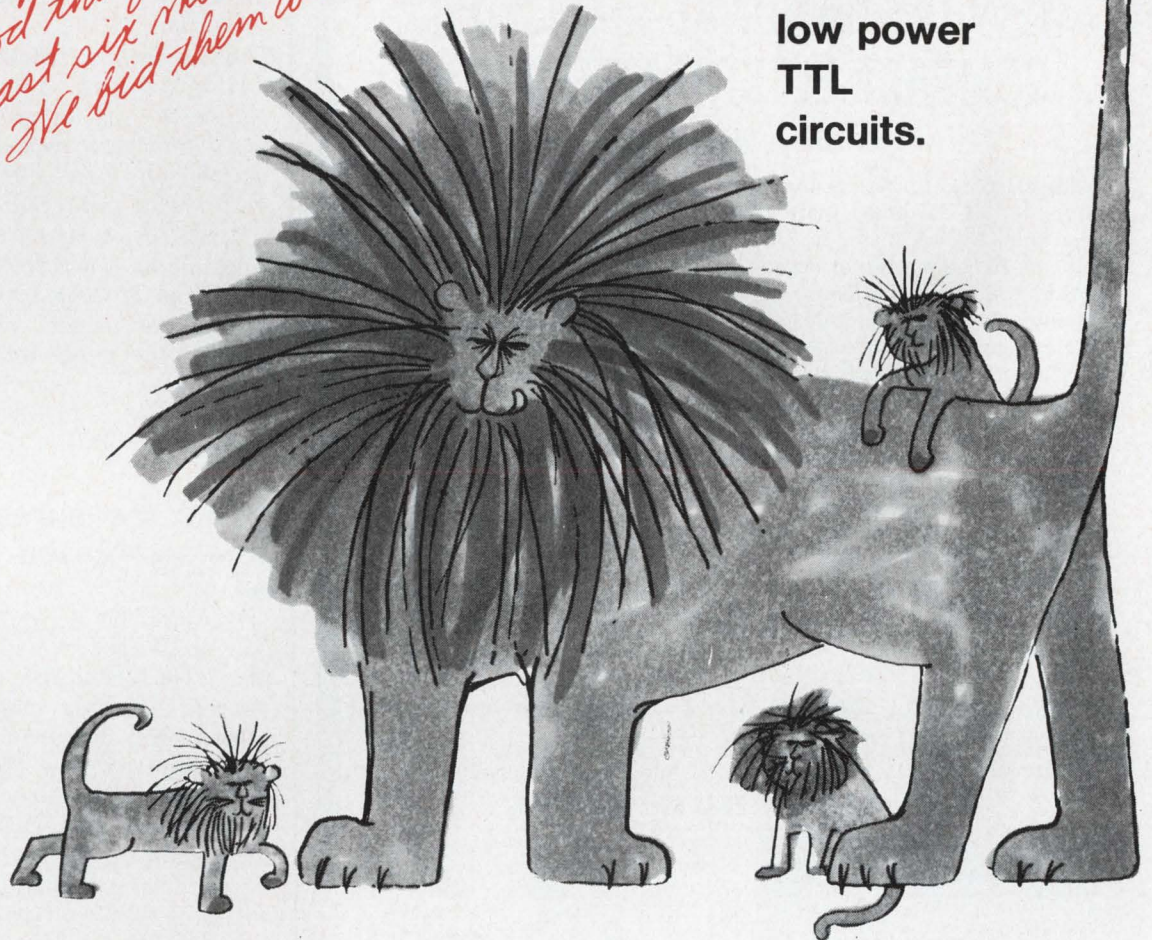
#### MCCOY ELECTRONICS COMPANY

A Subsidiary of OAK ELECTRO/NETICS CORP  
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ON READER-SERVICE CARD CIRCLE 37

*\*...until one of our smartest competitors recognized "a good thing" in the 8000 series for the past six months. We bid them "welcome aboard!"*

~~We have~~ *had\**  
 the only fully compatible family of high speed and low power TTL circuits.



You can go wild with Signetics new Designer's Choice 8000 Series: it gives you the widest selection of design trade-offs in speed, power, noise immunity and price ever offered in a TTL family. The family consists of a very high speed set (the 8800's) and a fully compatible but slower low power set which offers very high AC noise immunity. Now TTL system designs can be optimized without laborious calculations, unusually expensive and time-consuming special ground-plane designs, or extensive use of outboard discrete components in areas where the highest possible speed is not required. All you do is follow the published S8000-series usage rules. All circuits are compatible over the full MIL temperature range of  $-55^{\circ}\text{C}$  to  $+125^{\circ}\text{C}$  and are available off-the-shelf in Signetics 14-lead glass-Kovar flat pack. Hunt up your local Signetics distributor. For further information on the Designer's Choice 8000 Series, write Signetics, at 811 E. Arques Avenue, Sunnyvale, California 94086. ■ At the IEEE Show, be sure to check into Rooms 3000A & B at the New York Coliseum, for latest Signetics news.

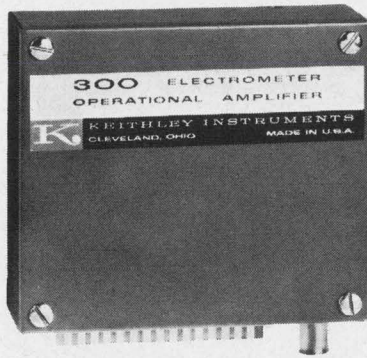
TYPE	DESCRIPTION	TYPE	DESCRIPTION
S8416	Dual 4-Input Nand Gate	S8816	Dual 4-Input Nand Gate
S8417	Dual 3-Input Nand Gate	S8825	DC Clocked J-K Binary Element
S8424	Dual AC Binary Element	S8826	Dual J-K Binary Element
S8440	Dual Exclusive-Or Gate	S8840	Dual 4-Input Exclusive-Or Gate
S8455	Dual 4-Input Buffer/Drive	S8855	Dual 4-Input Power Gate
S8480	Quadruple 4-Input Expander	S8870	Triple 3-Input Nand Gate
S8806	Dual 4-Input Expander	S8880	Quadruple 2-Input Nand Gate
S8808	8-Input Nand Gate		

**SIGNETICS  
 INTEGRATED  
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A SUBSIDIARY OF CORNING GLASS WORKS

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## NEW OPERATIONAL AMPLIFIER ...COMPACT ELECTROMETER, TOO!

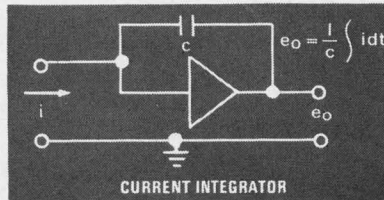
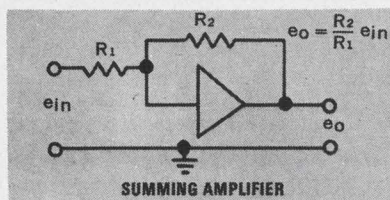
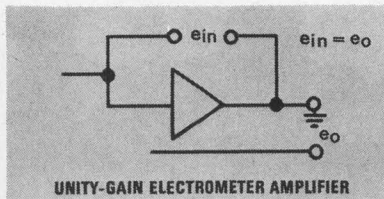
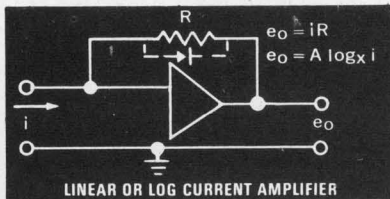
### Keithley Model 300

This economical little package is a true electrometer operational amplifier. It combines more than  $10^{14}$  ohms input resistance, less than  $5 \times 10^{-14}$  ampere offset current and ultra-low current drift of  $10^{-15}$  ampere per day into a precise single-ended output design that meets demands in conditioning signals as low as  $10^{-14}$  ampere.  Completely shielded, the 300 is a simple-to-use, easy mounting plug-in module. An output voltage of 11 volts at 11 ma is provided. Works to specs on unregulated supplies from  $\pm 16$  to  $\pm 25$  volts, at +25 ma or -8 ma.  For experiments or systems requiring extraordinary conditioning of small current signals, the Model 300 is the finest operational amplifier on the commercial market. Particularly for researchers in automated R & D, designers and producers of process or production control equipment.  Ask your Keithley engineer for a demonstration. But read our technical engineering note first. It's yours by dropping us a line.

#### CHARACTERISTICS

Voltage Gain dc open loop: >20,000	Voltage Offset adjustable to zero	
Input Resistance: > $10^{14}$ ohms	Voltage Drift <500 uv/hr.	
Capacitance: <10 pf	Overload Limit $\pm 400V$	
Current Offset: < $5 \times 10^{-14}$ amp	Output Voltage: $\pm 11V$	
Current Drift: < $10^{-15}$ amp/day	Current: $\pm 11ma$	

**SINGLE UNIT \$200... LESS IN QUANTITIES**



**KEITHLEY  
INSTRUMENTS**

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ON READER-SERVICE CARD CIRCLE 39

## LETTERS

(continued from p. 54)

details would be forthcoming as soon as he could contact the technical authorities. Later in the day, however, he informed us that no information would be made available. Following a discussion—sometimes heated on both sides—he said that the internal activities of the FBI including procurement plans extending even to office supplies were privileged matters, not public information.

We therefore followed time-honored journalistic practice and bypassed the official spokesman. The story that was published was the outcome of talks with officials involved with the technical problems.

Mr. Hoover could ensure accurate coverage of the FBI by the simple expedient of cooperation with the information media, making available to the public facts from his office.

S. David Pursglove  
Washington, D.C.

## Meter measures forward-biased diodes

Sir:

George L. Snider's article, "Measure capacitance and resistance" [in ED 4, Feb. 15, 1967, pp. 92-95], certainly offers one approach to forward-biased diode measurements. The Hewlett Packard 4815A vector impedance meter, however, will eliminate all the tedium of building the suggested bridge circuit. After biasing the diode with a dc supply or battery, the vector impedance is measured simply by placing the probe across the diode. Thus the vector impedance is found at any frequency from 500 kHz to 110 MHz with a meter type of instrument. The 4815A injects a constant signal of  $4 \mu A$  rms and measures the voltage, which is directly proportional to impedance.

James A. Brockmeier  
Sales Engineer  
Hewlett Packard Co.  
Rockaway, N. J.

## The author replies

Sir:

James Brockmeier indicated in his letter that measurements could

(continued on p. 66)



**OHMICONE®**  
**SILICONE-CERAMIC**  
**COATED AXIAL LEAD**  
**RESISTORS**

# two Choices from OHMITE



# 1

MOLDED



## SERIES 88 • MOLDED OHMICONE®

Coating is uniformly thick, dense and smooth. Meets 1000 VAC insulation test. Consistent form and size make these resistors highly suitable for rapid automated assembly techniques and also permit firm mounting in clips for significant heat-sink advantages. Available in commercial, military, precision, and non-inductive types. Can be provided to meet new Char. U of MIL-R-26. Solderable or weldable leads. **(Bulletin 101)**

**Wattages (Commercial):** 1.5, 2.25, 3.25, 6.5, 9, 11 watts at 25°C.

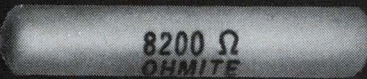
**Resistances:** 0.1 to 226K ohms.

**Tolerances:** To 0.05%; standard commercial, 3%.

**Low Temperature Coefficient of Resistance:**  $0 \pm 20$  ppm/°C, 10 ohms and above.

# 2

CONFORMAL



## SERIES 44 • CONFORMAL OHMICONE®

Same basic high quality wire-wound resistor as above, but with a conformal coating (1000 VAC rating). While it does not have the uniform shape and dimensions of the molded Series 88, the Series 44 is available with the same close, standard tolerance and low TC. It is supplied in commercial and high precision types. Can also be furnished to meet MIL-R-26 requirements. **(Bulletin 109)**

**Wattages (Commercial):** 1.5, 3.25, 6.5, 11 watts at 25°C.

**Resistances:** 0.1 to 442K ohms.

**Tolerances:** To 0.05%; commercial, 3% for values above 1 ohm.

**Low Temperature Coefficient of Resistance:** Standard is  $0 \pm 20$  ppm/°C for 10 ohms or more.

**OHMICONE Silicone-Ceramic**—Not just a conventional silicone coating, but rather silicone combined with a ceramic compound. Blending the two materials provides a coating which has the best characteristics of each. Developed and patented by Ohmite, *Ohmicone* envelopes a wire-wound resistor in an unusually tough, resilient jacket that has high moisture resistance and excellent dielectric properties, plus good stability and low temperature coefficients. Choose either the molded or conformal coating in accordance with your requirements.

**RHEOSTATS • POWER RESISTORS • PRECISION RESISTORS • VARIABLE TRANSFORMERS • RELAYS  
TAP SWITCHES • TANTALUM CAPACITORS • SEMICONDUCTOR CONTROLS • R.F. CHOKES**

# OHMITE

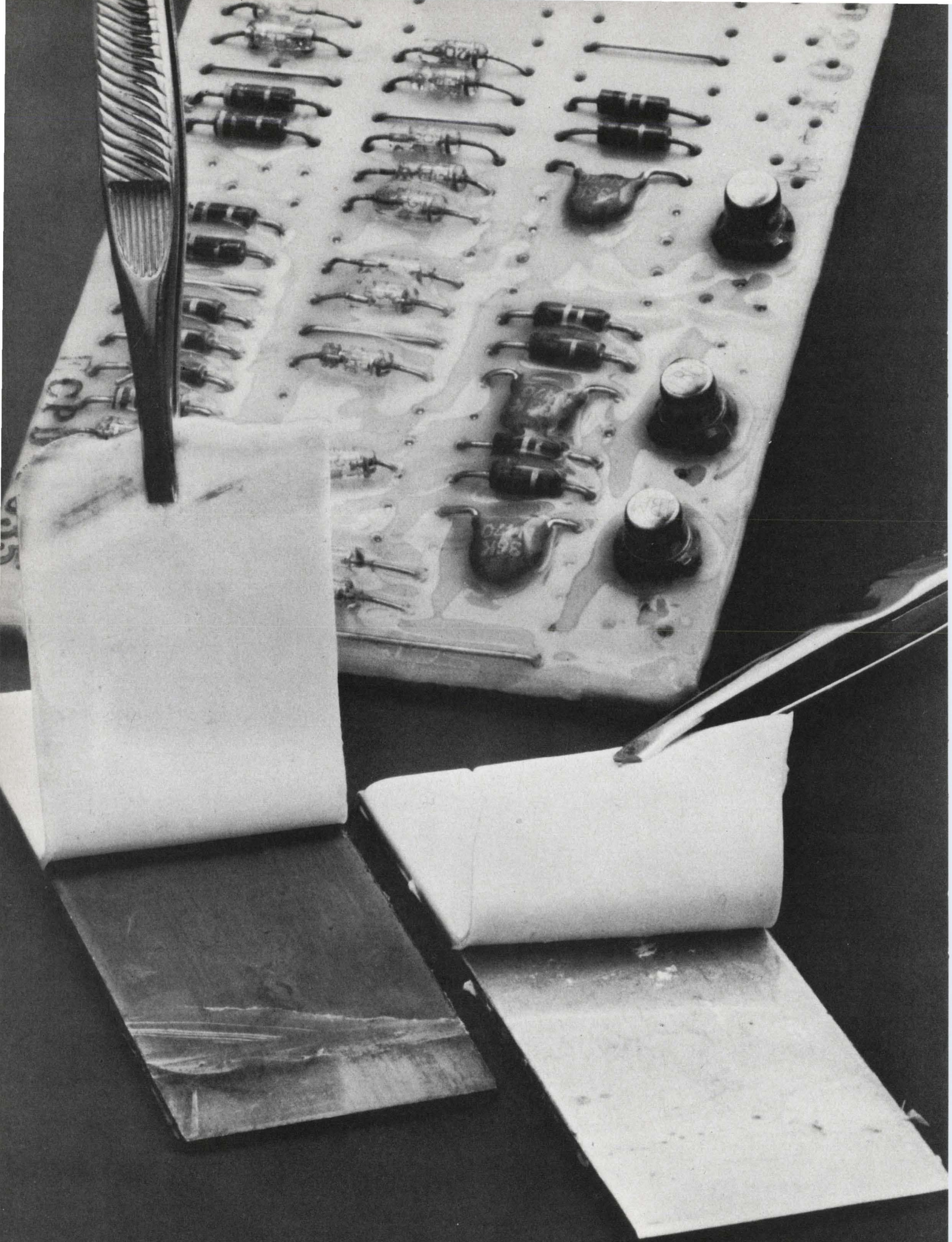
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ON READER-SERVICE CARD CIRCLE 40





# **N**ew, noncorrosive one-part RTV... tough silicone protection

Dow Corning® 3140 RTV coating and 3145 RTV adhesive/sealant are designed to be used in corrosion-sensitive equipment without harm to delicate electronic circuits and components.

Both are products of new silicone technology.

Dow Corning 3140 RTV coating is ideal for conformal protection of printed circuits . . . encapsulation of circuits, components and connectors. It is tough, translucent, self-leveling. Clarity of the coating allows easy visual inspection, identification, and faulty component removal. Repairs in the coating are easily made without loss of dielectric integrity.

Dow Corning 3145 RTV adhesive/sealant has high cured strength . . . is opaque, nonflowing . . . withstands long term exposure to temperature of 250 C — to 300 C for short periods. This *tough* material is excellent for bonding wires and terminals, mounting resistors, sealing electronic enclosures and providing a flexible adhesive for glass, ceramics, plastics and silicone rubber.

Dow Corning leads the way in making materials for the job you have at hand. For complete information on Dow Corning 3140 RTV coating and Dow Corning 3145 RTV adhesive/sealant, write Dept. 3916, Electronic Products Division, Dow Corning Corporation, Midland, Michigan 48640.

**DOW CORNING**

*We're a materials producer exclusively. Let us tailor a material to your need.*

# WIRE HARNESS LACING, like most manual jobs—costs money!

- Saving by using low cost lacing material seems good economy...

- ...until production lags and rejects pile up!

- For real economy you need the uniformity, the high quality of GUDEBROD LACING TAPE.

- That's why this guarantee can help you cut costs in cable harnessing!



You owe it to your zero defects program to investigate Gudebrod lacing tape. Its guaranteed quality and its constant uniformity are important to you—and to your harnessing operation. Why? Because Gudebrod smooths and speeds the hand operation of lacing and knot tying. There's no need for readjusting or retying. Rejects are minimal. The result? You save time—and that saves money and hastens delivery. Gudebrod sets its manufacturing standards high and adheres to them. When you use Gudebrod tapes you can set production goals and achieve them. This is the combination that saves you money in your harness department. Ask for the Gudebrod Product Data Book.

#### GUDEBROD CABLE-LACER

The first hand tool engineered for wire harnessing. Handle holds bobbins, feeds tape as needed, grips tape for knotting. Speeds, eases harnessing. Pays for itself in time saving.



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**GUDEBROD BROS. SILK CO., INC.**

FOUNDED IN 1870

*Electronics Division*

12 SOUTH 12th STREET, PHILADELPHIA, PENNSYLVANIA 19107

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# Something new in a thin film ion-pumped system

## ... Sputtering!

Here's the only system specially designed to deposit thin films by sputtering in an ion-pumped chamber. The new CVI-18 combines with CVC's PlasmaVac® sputtering unit to give you the first and finest ion-pumped sputtering system capable of electronic and optical thin-film deposition.

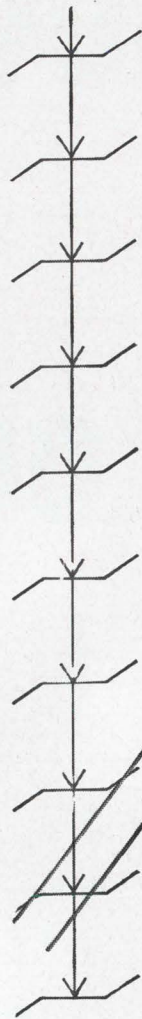
With the CVI-18 you get faster, more efficient coating cycles for pilot plant or production line operation: An automatic pre-bake saves up to two hours every working day. The high efficiency Quick-Start ion pump and gettering system give you

faster pumpdown, high throughput that allows starting in the 50 micron range, and ultimates to the  $10^{-10}$  range.

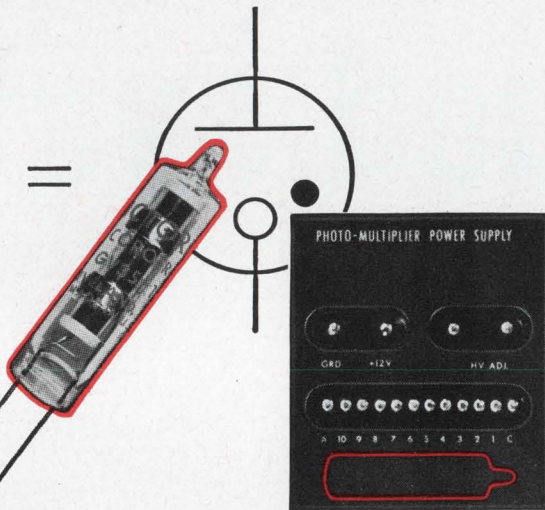
You get more consistent performance, too—with a new titanium sublimation unit. System pressure may be automatically held below a preset process pressure over a wide range of gas loads.

Typical CVI-18 applications include electronic, optical, and optoelectronic coating as well as environmental studies. The CVI-18 is something new, something better in an ion-pumped coater. Just write for full details. Consolidated Vacuum Corporation, Rochester, N.Y. 14603. A subsidiary of Bell & Howell.





# NEED A 3000 VOLT ZENER DIODE?



Corotron actual size: Photo-multiplier power supply, showing Corotron location, 1/3 size.

You could string together several hundred zeners. Or you could specify *one* Victoreen Corotron. It is the gaseous equivalent of the zener with all the advantages of an *ideal* HV zener diode.

For space research and other rugged applications requiring absolute power supply stability, GV3S Series, shown, provide the ideal reference voltage anywhere in the range of 400 to 3000 volts. They enable circuitry to maintain constant high voltage regardless of battery source voltage or load current variations. Cubage and weight (GV3S Corotron weighs only 4 gm.) are important considerations. So is temperature variation (Corotrons operate from 200°C down to -65°C). Ruggedized versions withstand shock to 2000 G, vibration 10 to 2000 cps.

If you're trying to simplify circuits . . . to cut cost, size and weight . . . to upgrade performance—you need Corotron high voltage regulators. Models are available now from 400 to 30,000 volts. A consultation with our Applications Engineering Dept. will speed up the countdown.

8501-A



**Components Division**

**THE VICTOREEN INSTRUMENT COMPANY**

**10101 WOODLAND AVENUE • CLEVELAND, OHIO 44104**

EUROPEAN SALES OFFICE: GROVE HOUSE, LONDON RD., ISLEWORTH, MIDDLESEX, ENGLAND

ON READER-SERVICE CARD CIRCLE 44

## LETTERS

(continued from p. 60)

easily be made with the Hewlett Packard 4815A meter. The measurement procedure apparently involved only biasing the diode with a dc supply or battery, and measuring the impedance by placing the instrument probe across the diode. In making the measurement by this method, there are several questions that occur:

- What is the effect of stray capacitance and inductance due to the wiring necessary to connect the diode to the voltage source?
- If there is no isolation between the dc supply and the diode, will not the impedance reading include the effects of power supply impedance?
- What is the effect of probe residual impedance on measuring low-capacitance diodes (<2 pF)?

I have attempted measuring forward-biased diode parameters with the Model 8405A vector voltmeter in the manner suggested in an article by Fritz K. Weinert of Hewlett Packard. The arrangement used was that suggested for measurement of a complex impedance. I found, however, that the meter was extremely sensitive to stray capacitance and inductance, and above 15 MHz it was impossible to obtain repeatable results. I concluded that it was impossible to get repeatable measurements without the need to resort to carefully fabricated "plumbing" fixtures.

The method that I suggested in my article in *ELECTRONIC DESIGN* does have certain advantages:

- The circuitry is inexpensive to build—\$150 for parts and labor. This is far less than the cost of the RF vector impedance meter—\$2650.
- The accessory equipment required is available in any electronics laboratory.
- The readout is direct. No computation is required to obtain the resistance and capacitance values.

The method has also been used to measure transistor junction impedance under forward-bias conditions and the source-drain impedance of field-effect transistors as a function of gate voltage.

Moreover I have been able to extend the range of the method to resistance values of 200 kΩ and ca-

(continued on p. 72)

VARIABLE  
BANDWIDTH  
MARKERS  
PINPOINT THE  
FREQUENCY



## ***Sweep Oscillator gives top performance in the 100 kHz to 110 MHz range***

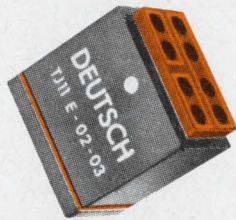
All solid-state Hewlett-Packard 3211A Sweep Oscillators with RF and marker plug-ins meet virtually all of your swept frequency testing requirements. Variable bandwidth markers permit accurate, well defined marking under a variety of test conditions.

The main frame of the 3211A contains everything you could hope to find in a sweeper. RF plug-ins operate at fundamental frequencies with good linearity and spurious mixing products are eliminated. Plug-in markers offer not only variable bandwidth, but also Z-axis or pulse-type marking. An accurate 59-db attenuator makes the unit a valuable tool for testing both high- and low-gain circuits.

The 3211A is ideal for general testing in the video to VHF range where flat, linear output and an accurate marking system is required. Typical applications are: alignment, calibration and design of FM tuners and receivers and testing filters, amplifiers, transformers, resonant circuits and IF sections of TV receivers, radar and communications systems. For complete specifications, contact your local Hewlett-Packard field engineer or write Hewlett-Packard, Green Pond Road, Rockaway, N.J. 07866.

HEWLETT  PACKARD  
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for science and industry

# NEW DEUTSCH SYSTEM OBSOLETES




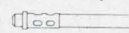
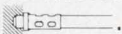

## THE TERMINAL JUNCTION

A new system for point to point wire connection and integration

This newest, most flexible system releases today's engineer from the limitations usually associated with interconnection. One wire or thousands of wires may be connected by this simple, reliable method that:

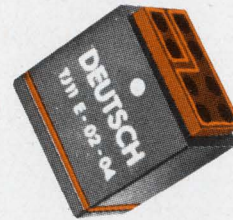
- Replaces terminal strips and binding posts
- Does away with contact damage
- Eliminates splices and solder
- Uses standard crimp tools
- Uses **one** fail-safe, expendable assembly tool
- Uses **one** fool-proof assembly procedure
- Is self-locking
- Is modular
- Saves weight and space
- Connects and disconnects instantly
- Protects connections without potting
- Meets or exceeds MIL-C-26482 where applicable, and exceeds most user specifications

The Terminal Junction system is the ultimate in simplicity.

- The wire termination is ruggedized so that it can't bend, break, bind or gall .
- Crimping the terminal to any wire is done with standard tools, and provides strong, reliable termination . When inserted in the modular block, the terminations are interconnected instantly in a variety of hook-up patterns .
- The low-resistance connections are secured by self-locking retainers that defy vibration, shock and high pulling loads .

System build-up, breadboarding and all processes where one must patch, bus, splice or feedthru can be vastly simplified with this flexible, "people oriented" system. Its simplicity, combined with total reliability, makes possible immediate conversion without special training of assembly personnel... and, with the move to Terminal Junctions come the benefits of efficiency and upgraded connections.

The following columns describe how you can save time, space and circuits. Read on... let your own ingenuity dictate how you can benefit by using this revolutionary system.

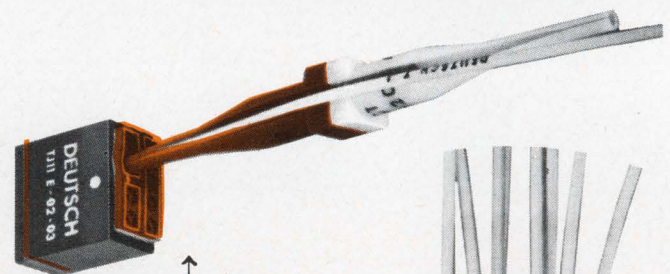


## TIME SAVER


The Terminal Junction system eliminates wasted time and motion in all phases of equipment design, breadboard, prototype, assembly, checkout and maintenance.

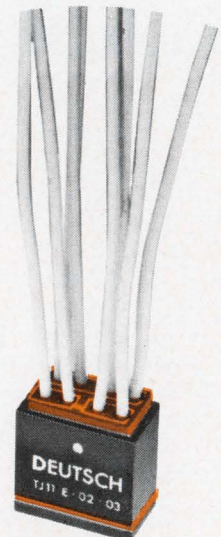


Quick, reliable crimp termination of wires with standard tools.



Instant connection (or disconnection) requires one, fail-safe, expendable tool which is small enough to be stored with wire harnesses.

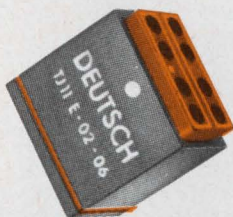
One Terminal Junction module, with eight wires that have been connected in a fraction of the time required by other methods. 



\*Terminal Junction modules shown are model TJ11E-02\*\* which connect wire sizes AWG 20 through AWG 24.

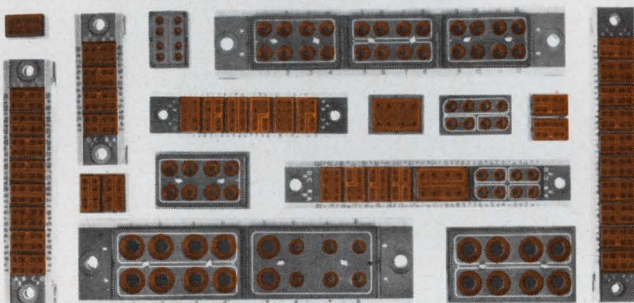


# EXISTING CONNECTION METHODS

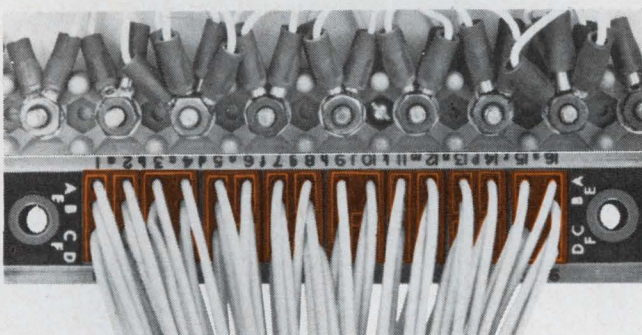


## SPACE SAVER

Terminal Junctions occupy a fraction of the space formerly needed for an equal connection capacity. And, there is no limit to the number of modules and multi-module assemblies that may be used to form high density interconnection panels and systems.



Typical module and multi-module assemblies for space-saving connection and integration. Standard units shown will handle wire sizes AWG 24 through AWG 4. White lines on each module outline points of common connection.



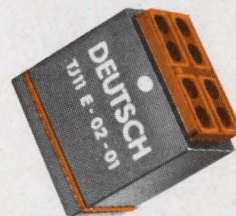
Sixty four size AWG 20 wires perfectly connected and fully protected in a fraction of the space previously needed. Compare the amount of space saved in this case...the terminal strip handles only 28 wires, and affords them no protection.



Use Feedthru Terminal Junctions for all through-connection applications; use them as high density, lightweight, fully environmental connectors; or, use multi-module assemblies for patchboard and through-panel applications.

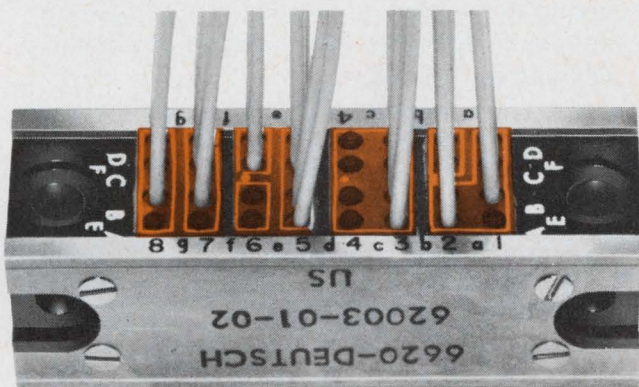


The **JIFFY JUNCTION**® is a fully environmental single conductor connector. Use it as a replacement for splices or any one-wire connection problem.



## CIRCUIT SAVER

Circuit and equipment failures due to the breakdown of exposed or poorly protected junctions and splices are eliminated by Terminal Junctions. All connections in each module are protected from mechanical damage by solid dielectric material; shorting caused by moisture and contaminants is prevented by resilient silicone rubber sealing glands at each wire entry point; the positive locking retention system resists shock, vibration and high pulling loads to assure perfect continuity in each circuit. Dielectric separation between circuits exceeds military specifications, and because the tool used for connection and disconnection is of dielectric material the shorting possibility normally associated with checkout and maintenance is reduced to a minimum.



Actual size modules are shown in a multi-module assembly; typical busing layouts are included (white lines outline common connection points). Those entry points not occupied by wires are sealed by plugs to assure complete environmental immunity.

The Terminal Junction is the newest member of the performance proven Rear Release Family of Deutsch connectors and interconnection devices. Using **one** type of crimp tooling, **one** assembly procedure, and **one** fail-safe insertion/removal tool, any interconnection system may be upgraded to modern levels of efficiency and reliability. For more information about Terminal Junctions contact your local Deutschman, or write today; ask for Data File TJ-3.

# DEUTSCH

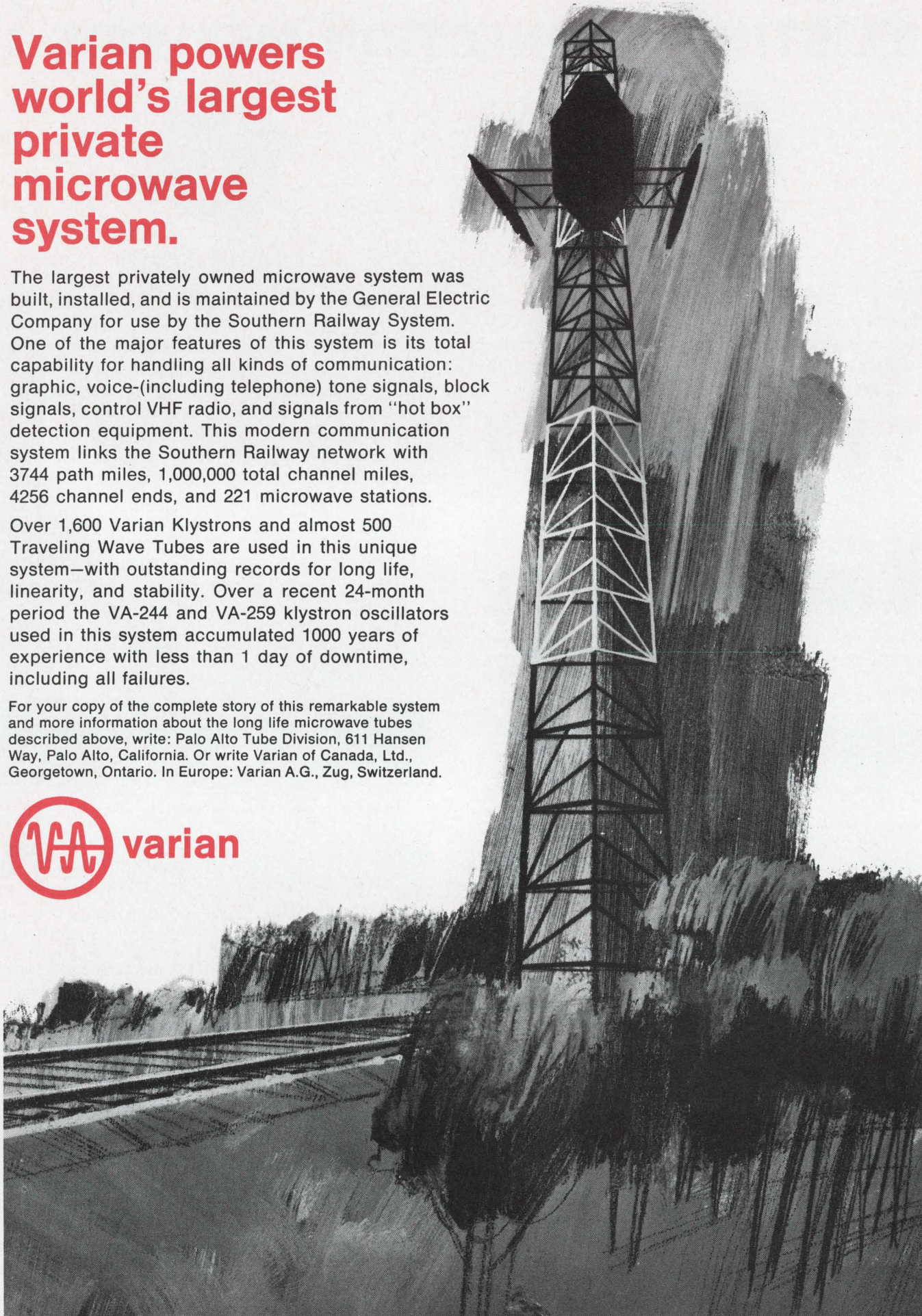
ELECTRONIC COMPONENTS DIVISION • Municipal Airport • Banning, California

# Varian powers world's largest private microwave system.

The largest privately owned microwave system was built, installed, and is maintained by the General Electric Company for use by the Southern Railway System. One of the major features of this system is its total capability for handling all kinds of communication: graphic, voice-(including telephone) tone signals, block signals, control VHF radio, and signals from "hot box" detection equipment. This modern communication system links the Southern Railway network with 3744 path miles, 1,000,000 total channel miles, 4256 channel ends, and 221 microwave stations.

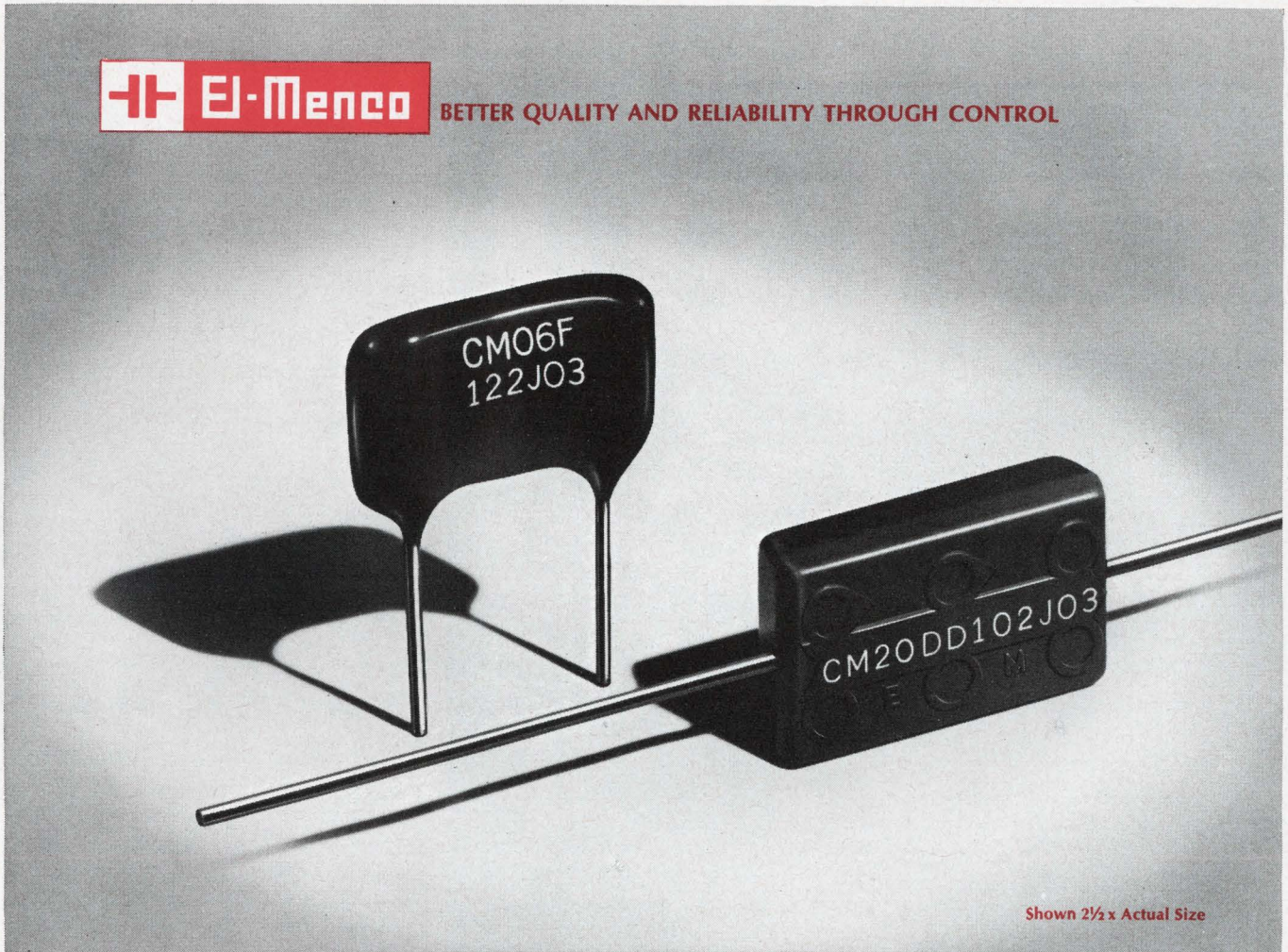
Over 1,600 Varian Klystrons and almost 500 Traveling Wave Tubes are used in this unique system—with outstanding records for long life, linearity, and stability. Over a recent 24-month period the VA-244 and VA-259 klystron oscillators used in this system accumulated 1000 years of experience with less than 1 day of downtime, including all failures.

For your copy of the complete story of this remarkable system and more information about the long life microwave tubes described above, write: Palo Alto Tube Division, 611 Hansen Way, Palo Alto, California. Or write Varian of Canada, Ltd., Georgetown, Ontario. In Europe: Varian A.G., Zug, Switzerland.





BETTER QUALITY AND RELIABILITY THROUGH CONTROL



Shown 2 1/2 x Actual Size

## Capacitor Problems That Require A Lot Of Self-Control...Chemically Speaking

**Problem 1:** How to make sure the silver paste composition used for electrodes provides the best results for each electrical parameter in a given capacitor design?

**Problem 2:** How to improve the recognized moisture reliability of our dipped mica capacitors without adversely affecting life reliability?

**Problem 3:** How to upgrade the reliability of molded mica capacitors to equal that of dipped mica capacitors so designers can take advantage of body uniformity and axial lead design?

**Solution: Chemical self-control!** To do this we operate our own chemical manufacturing plant where we formulate silver pastes, phenolic dipping compounds, and epoxy molding compounds — all under strict controls.

**Result:** Dipped mica capacitors and molded mica capacitors of equally high reliability that operate up to 150°C. Send for technical literature and always insist on El-Menco brand capacitors . . . your assurance of better quality and reliability through control.

### THE ELECTRO MOTIVE MFG. CO., INC.

WILLIMANTIC, CONNECTICUT 06226

Dipped Mica • Molded Mica • Silvered Mica Films • Mica Trimmers & Padders  
Mylar-Paper Dipped • Paper Dipped • Mylar Dipped • Tubular Paper

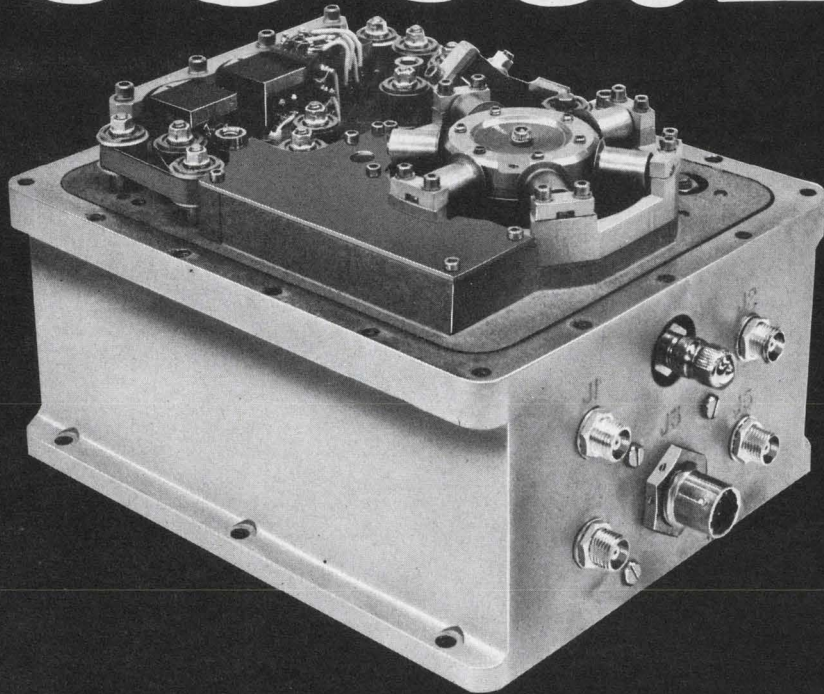
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ON READER-SERVICE CARD CIRCLE 48

everyone here works for . . .

# total



# reliability

Ingenuity and reliability merge in Borg-Warner Instrumentation Recorders. For example, the Model R-305 is a continuous-loop tape recorder for space vehicle reentry. Extremes in temperature, strain, vibration and g forces were overcome in this application.

Borg-Warner recorders are in use right now, successfully fulfilling their missions of collecting data for transmittal to earth. This is not surprising though, because BWC has 14 flight proven magnetic tape recorder models.

Whatever your recorder requirement: Continuous-loop, reel-to-reel, or random bin. Whatever your use: Orbiting space station, reentry, geological or ocean survey and other hazardous environments, or ground station applications—Borg-Warner Controls probably has an instrumentation recorder design ready for you. If modification to existing design is necessary, or if you need a recorder beyond the state-of-the-art, Borg-Warner Controls can solve your problem with ingenuity and reliability.

**BORG-WARNER CONTROLS** 3300 South Halladay Street, Santa Ana, California 92702



ON READER-SERVICE CARD CIRCLE 49

## LETTERS

(continued from p. 66)

capacitance values as low as 1 pF through modification of the circuit and test procedure.

Since I have an RF vector voltmeter at hand, any advice on its possible use in this area of measurement would be appreciated. Of particular value would be suggestions about methods of fabricating test fixtures and about means to eliminate or compensate for stray capacitance and inductance.

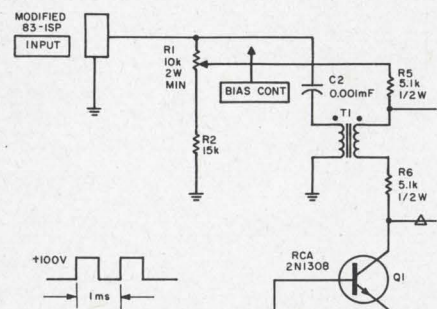
George L. Snider

Senior Engineer  
Arinc Research Corp.  
Santa Ana, Calif.

## Accuracy is our policy

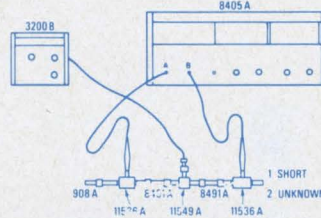
In "New technology keys Solid-State Circuits show," ED 5, March 1, 1967, pp. 17-20, John Copeland of Bell Telephone Laboratories, Inc., calls attention to a typographical error. On p. 18, column 1, para. 2 should read: "Copeland reported that he has achieved 0.7 watts with 0.7% efficiency at 51 GHz . . ." omitting the words ". . . 33 watts of pulsed power at 10 GHz . . ." which were interpolated by mistake.

In the Idea for Design, "Generate pulses by varying length of the termination line," published in ED 3, Feb. 1, 1967, on p. 94, there were three errors in the accompanying schematic. The upper left-hand portion of that schematic is reproduced below with the three errors corrected. The errors were: resistor  $R_2$  was unlabeled; capacitor  $C_2$  was omitted; and the polarity dots for  $T_1$  were left out.



# Measurement of Complex Impedance with the HP 8405A Vector Voltmeter

The measurement of complex impedance in the 1 to 1000 MHz range using slotted line or bridges has always been a time-consuming and cumbersome process, particularly when determining phase angle. Now, with the HP 8405A Vector Voltmeter, faster and simpler techniques are possible.



Below 100 MHz, the method illustrated above is especially convenient. Signal power is equally split, and the voltage drop across the unknown impedance is compared against the drop across the known. Results are easily entered on the Smith Chart for rapid determination of impedance.

From 100 MHz to 1 GHz, impedance is measured in the form of Reflection Coefficient, using a new, extremely wideband dual directional coupler as in the set-up shown below. The 8405A Vector Voltmeter measures incident and reflected voltage and their phase

angle, allowing quick entry into the Smith Chart.

### Free Application Data

Application Note 77-3 discusses "Measurement of Complex Impedance". For your copy write Hewlett-Packard, 1501 Page Mill Road, Palo Alto, Calif. 94304; Europe: 54 Route des Acacias, Geneva.

You can appreciate the wide-range of the 8405A from these brief specifications; match them to your measurement requirements. And call your HP field engineer for complete information on this wideband, 2-channel RF millivoltmeter-phasermeter.

### Major Specifications, HP 8405A Vector Voltmeter

**Frequency Range** is 1 to 1000 MHz in 21 overlapping octave bands; automatic tuning within each band.

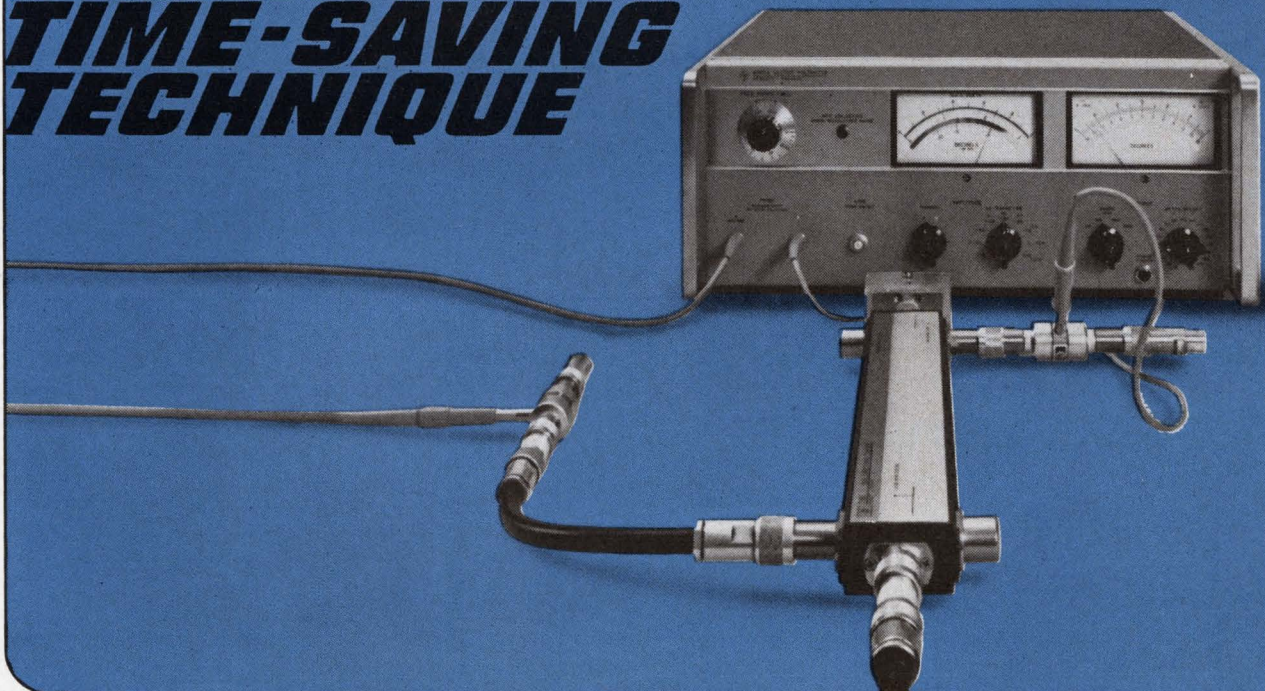
**Voltage Range for Channel A** (synchronizing channel), 300  $\mu$ V to 1 V rms (5-500 MHz), 500  $\mu$ V to 1 V rms (500-1000 MHz), 1.5 mV to 1 V rms (1-5 MHz).

**Voltage Range for Channel B** (input to Channel A required), 100  $\mu$ V to 1 V rms, full scale. Full-scale meter ranges from 100  $\mu$ V to 1 V in 10 dB steps. Both channels can be extended to 10 V rms with 11576A 10:1 Divider.

**Phase Range** of 360° indicated on zero-center meter with end-scale ranges of  $\pm 180^\circ$ ,  $\pm 60^\circ$ ,  $\pm 18^\circ$ ,  $\pm 6^\circ$ . Phase meter OFFSET of  $\pm 180^\circ$  in 10° steps permits use of  $\pm 6^\circ$  range for 0.1° phase resolution at any phase angle.

**Price:** \$2750.

**A NEW  
TIME-SAVING  
TECHNIQUE**



HEWLETT **hp** PACKARD

ON READER-SERVICE CARD CIRCLE 50



## PG-13 . . . Big, Fast Pulses

With our new PG-13 you can get  $\pm 100V$  or, as a current source,  $\pm 2A$  pulses. And 10 ns rise and fall times; repetition rate 1 Hz to 25 MHz; duty cycle 50% at 1A out with a pulse width to 5 ms. No hedging. The specs are real specs: when we say  $\pm 100$  volts we mean  $\pm 100$  volts; 10 ns rise time means 10 ns rise time, worst case, at 100 volts. So if you need a truly fast high-output pulser for, say, magnetic core testing, radar pulse simulation or similar applications you would do very well to consider the PG-13.

This is why, in brief part:

The PG-13 is all solid-state (rack height  $3\frac{1}{2}$ ""). Operates in either voltage or current modes; in the voltage mode the range is  $\pm 100$  mV to  $\pm 100V$  from a 50 ohm source; in the current mode it is  $\pm 50$  mA to  $\pm 2A$  from a 1K, min,

source. PRF, 1 Hz to 25 MHz. Single or double pulses plus sync. Instantaneous overload protection and a front panel warning light. Can be gated or triggered up to the max rep rate. Manual one-shot. DC-offsets either direction to 100 mA. Independently variable rise and fall times, 10 ns to 50 ms. PRF, rise, fall, amplitude, width (of either pulse independently), offset and delay are all variable continuously.

The PG-13 is one of the 3-I/Chronetics new generation pulse generators.

We'll be glad to whisk a PG-13 to your lab for a demonstration. And there's a new catalog on the new generation pulse generators. Please write or 'phone for either or both.

Intercontinental Instruments Inc, an affiliate of CHRONETICS

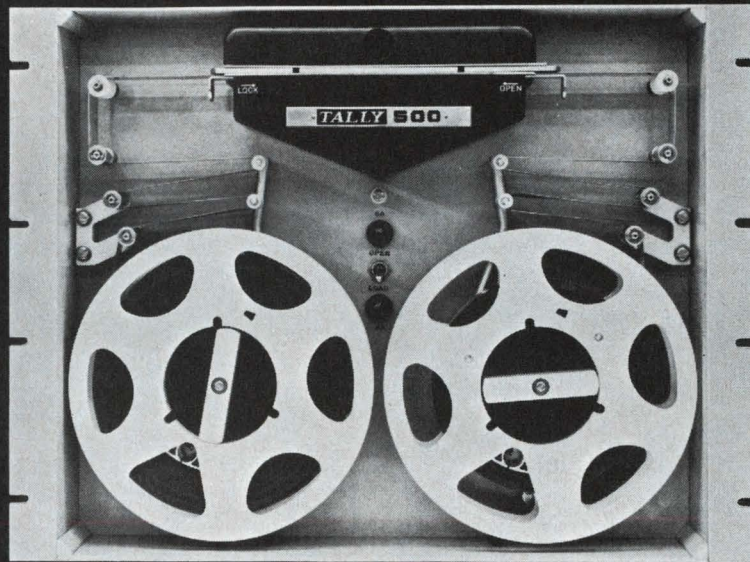


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ON READER-SERVICE CARD CIRCLE 51

# New Tally 500 series photoelectric tape readers work up to 1000 characters per second.

That's not unique.



**But working without pinch rollers, friction brakes, clutches, or solenoids – that is!**

There's no point in Number 1 introducing just another "me too" product. Just to give you an idea of how good the new line is, in a recent life test, one photoelectric reader ran for 15,000 hours at maximum speed without a failure. You can see why we say these new readers represent genuine "state of the art" achievement. Adding them to the Tally line rounds out the broadest line of perforated tape equipment on the market today.

#### **The 500R, 500RF, and 500T.**

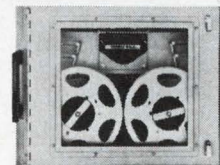
These three readers operate at up to 200 characters per second asynchronously (stop on character), up to 500 char/sec in the synchronous or free running mode (stop before next character), and 1000 char/sec in the wind/search mode. All feature printed motor direct capstan drive, and bi-directional reading and winding. The Model 500R (recess mounted) and the Model 500RF (flush mounted) are reader and spooler com-

binations, while the Model 500T comes without the reel servo system. For tape handling only, two spoolers using printed circuit motors and proportional reel servo are offered, one with 8 inch reels, the other with 10½ inch reels.

#### **MIL-SPEC reader, Model 500RM and "ruggedized" reader, Model 500RF/10**

Fully militarized, the Model 500RM is the first high speed reader that meets all applicable military specifications without exception. Featuring the same basic design as other Series 500 photoelectric readers, this unit will work in environments of -40°F to +145°F, in humidities of 100%, and take more than 15 g's shock. Pertinent RFI specs are met. MTBF is 5,000 hours. Expected life is 10,000 hours minimum.

Where severe environmental conditions are not encountered, the Model 500 RF/10 will perform with the same accuracy and life for about half the cost. Reading speeds for both readers are

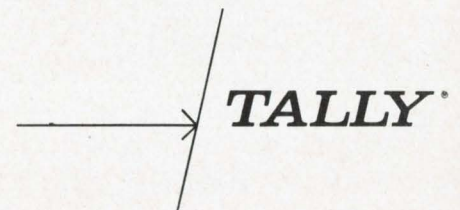


*Model 500 RM*

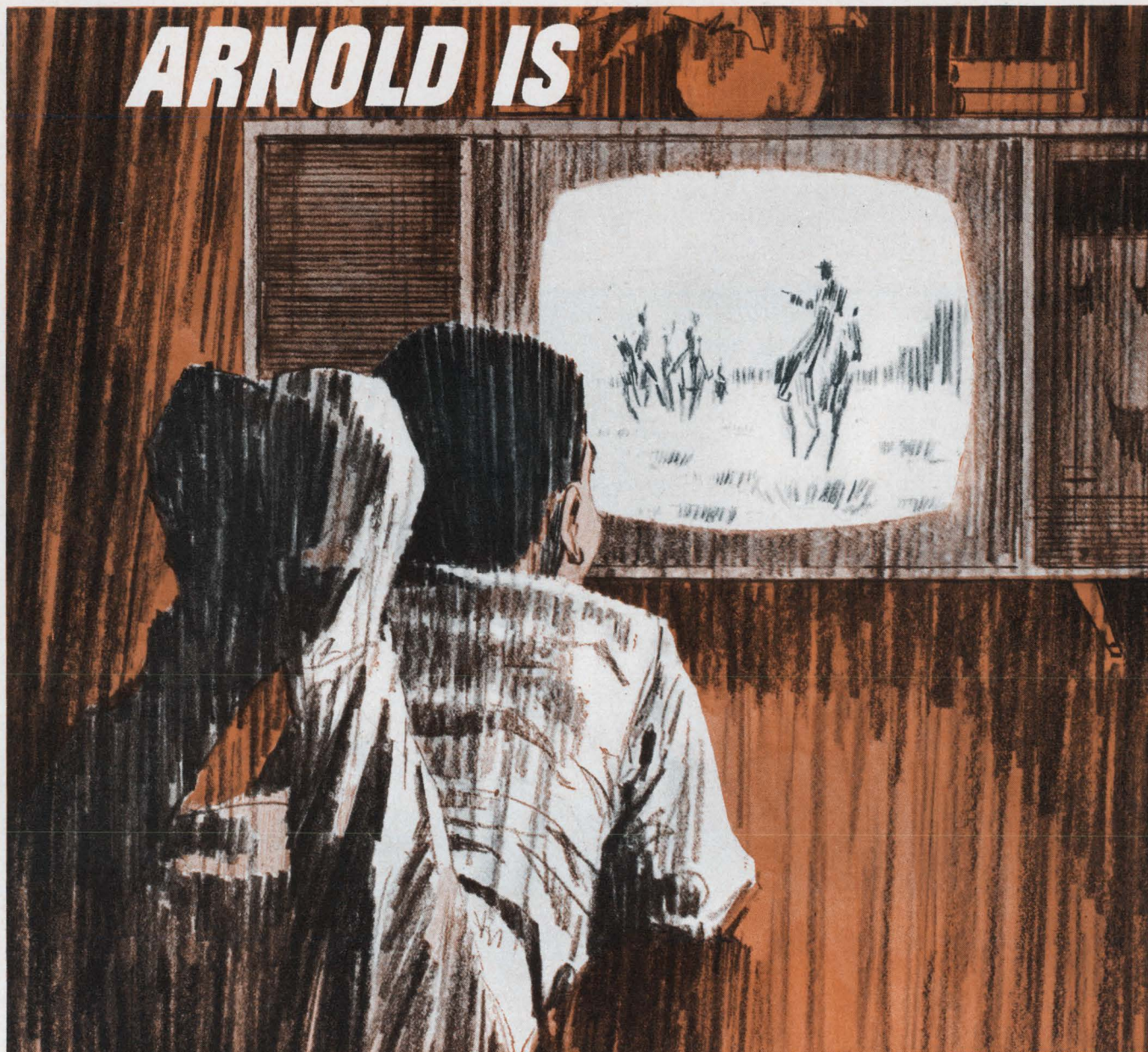
150 char/sec asynchronously, 500 char/sec synchronously, and 1000 char/sec wind/search.

#### **Full disclosure.**

For all the facts, call your full service Tally sales engineer (see EEM), or write Ken Crawford, Tally Corporation, 1310 Mercer Street, Seattle, Washington 98109. In the U.K. and Europe, address Tally Europe, Ltd., Radnor House, 1272 London Road, London, S.W. 16, England.

 **TALLY**

# ARNOLD IS



## IRON POWDER CORES

From 5" dia. to Subminiature Toroids

Arnold has total capability across all design configurations—toroids, insert cores, threaded cores, plain cores, bobbin cores, sleeve and hollow cores, cup cores and subminiature toroids. All the necessary raw materials are carried in stock to provide optimum performance over the specified frequency spectrum. Our facilities include the most modern powder processing, pressing, quality control and final test equipment available in the industry.

Call us, write us, TWX us, we can handle any problem.

Arnold is also ■ Permanent Magnets ■ Tape Wound Cores ■ MPP Cores  
■ Magnetic Shielding ■ Electrical Alloy Transformer Laminations ■ Trans-  
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**EDITORIAL**

## They just keep rolling along . . .

Eight years ago, after careful investigation of the diode market, we became alarmed at the rising numbers of devices being produced and the difficulty facing the design engineer who has to choose the right diode for his application. And so, in the June 10, 1959, issue of *ELECTRONIC DESIGN* we published an editorial. In it we warned that diode types had increased from 2500 to 4000 in one year; we urged the industry to take steps toward meaningful standardization of diodes.

Today there are more than 30,000 diode types on the market!

Of the many lessons that may be drawn from this development, these seem at least fairly reasonable: nobody cares what is said in an editorial; industry doesn't care about the problems of design engineers; engineers don't care that industry doesn't care—they welcome punishment on the job.

We keep wondering how much time the design engineer spends to keep track of all these devices, their latest specs, exact test-method descriptions, sources of supply and other pertinent facts. We doubt that any designer patiently searches for just the right device; we suspect he settles for the types he's used before.

A comparable situation is shaping up for transistors. *ELECTRONIC DESIGN* has just completed its fifteenth annual Semiconductor Directory. It's fatter than last year's. Close to 3200 JEDEC-registered transistor types are listed, compared with 2600 in 1966. There are now almost 1900 IC types, against 1100 a year ago.

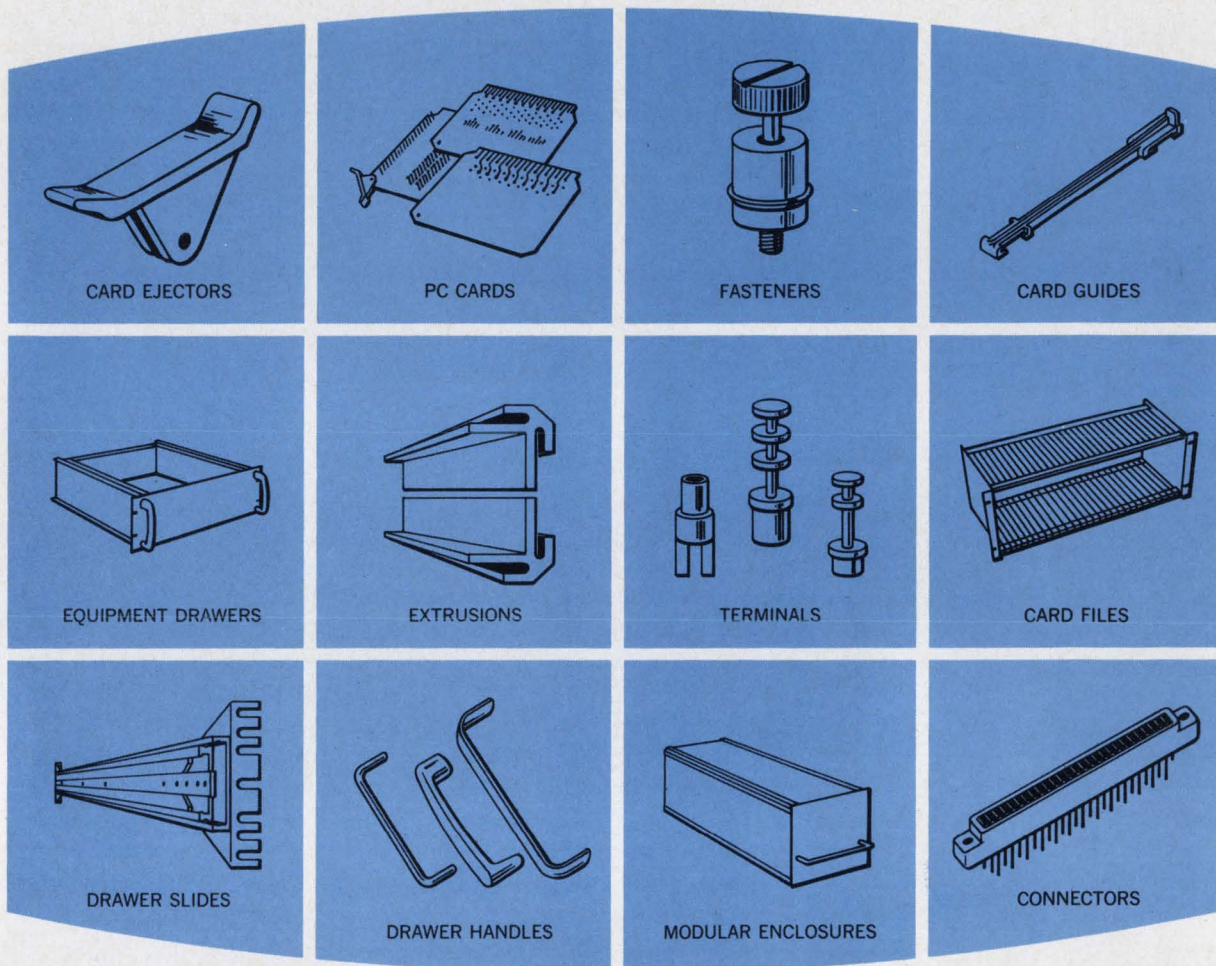
We have never criticized the introduction of new types that offer improvements in equipment performance; they're needed and welcome. But we continue to oppose "new" devices that offer slight parameter improvements at the cost of almost hopeless confusion for the designer who attempts to evaluate the selection.

Roger Field and Peter Budzilovich, the editors responsible for *ELECTRONIC DESIGN*'s applications-oriented Semiconductor Directory, join us in urging semiconductor manufacturers to increase their efforts to standardize device packages, test methods and specification data formats. Let's work to bring ICs under control before the list gets out of hand.

In the meantime, if you're a designer, you'd better check the Semiconductor Directory, which starts on page 81. It's the best aspirin around to ease your headache.

HOWARD BIERMAN

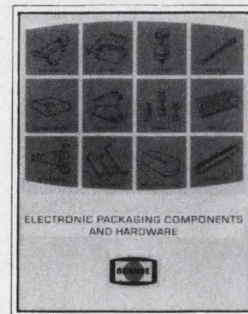
# Who makes a **complete line** of **electronic packaging hardware**?...**Scanbe does!**



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- SINGLE SOURCE SERVICE ■ COMPLETE AND WIDEST SELECTION OF HARDWARE ■ OFF-THE-SHELF AVAILABILITY
- EXPERIENCED DESIGN ASSISTANCE ■ PRECISION MANUFACTURING ■ RIGID QUALITY CONTROL

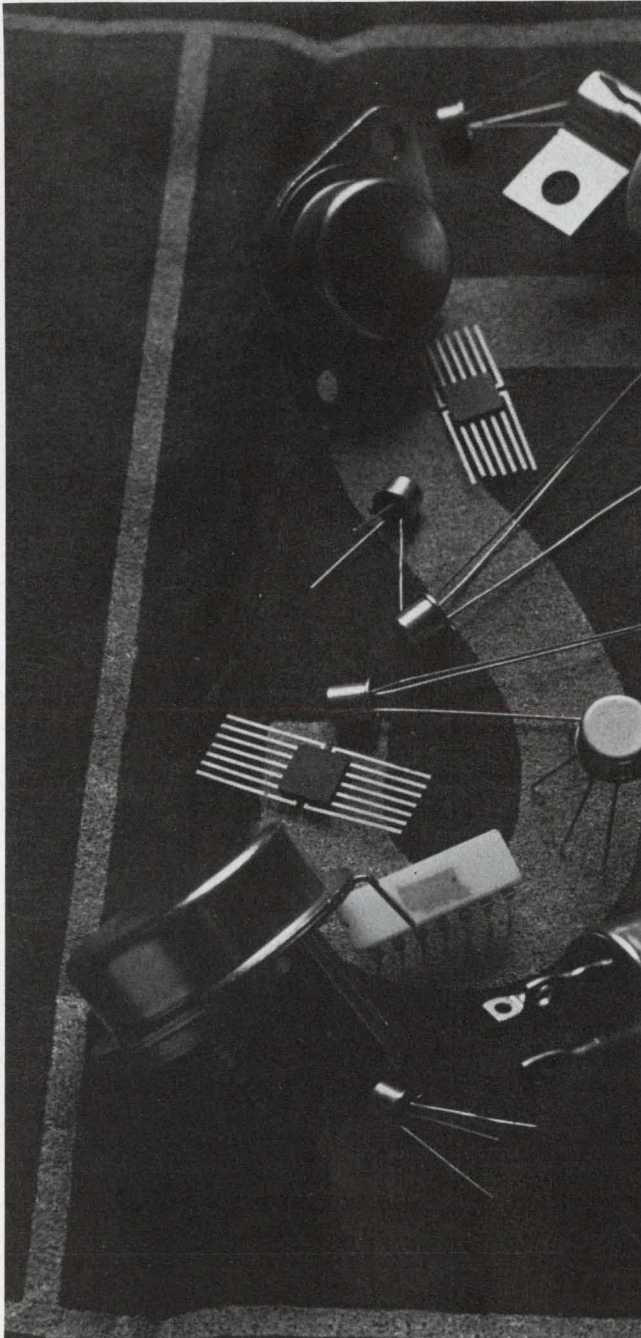
Save money and time without sacrificing performance—contact Scanbe, the specialist in electronic packaging hardware. Write for Scanbe's new electronic packaging hardware guide.



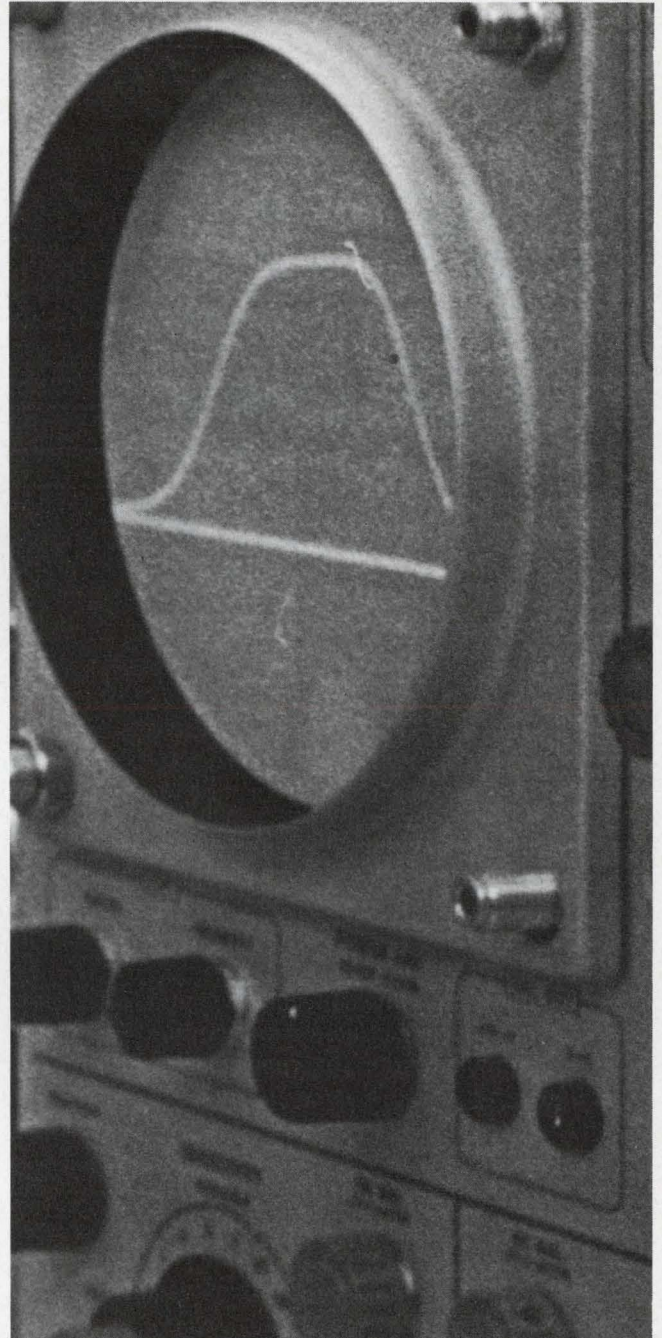
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# Technology



**Semiconductor reference directory** lists over 5000 devices by major parameters. Page 81



**Stagger-tuning of IC amplifier stages** gives the right gain and selectivity curve. Page 236

## Also in this Section:

**Measure the 0-TC point of FETs:** theoretical values may be inaccurate. Page 230  
**Ideas for Design.** Pages 241 to 245

# While other major semiconductor manufacturers are eagerly trying...

## One company has already mastered the practical production of Large Scale Integration...

Only General Instrument's exclusive **MTOS (Metal-Thick-Oxide-Silicon)** process provides Large Scale Integration without the need for high-cost discretionary wiring.

Before **MTOS**, there existed no practical Large Scale Integration of any real significance. LSI, much discussed, widely experimented with, and heralded throughout the industry as the microcircuitry of the future, was just that... the microcircuitry of the future. While MOS represented an important step on the road to LSI, what was required to make LSI a present-day reality was a major technical breakthrough. General Instrument's exclusive **MTOS** process provided that breakthrough. For the first time, yield, cost, reliability and performance parameters are being effected that make LSI a dramatic and meaningful reality... today.

### The **MTOS** process—second generation MOS

In the **MTOS** process a thick oxide is grown over the entire silicon chip except for the gate regions. The thin oxide over the gate regions is retained to keep the threshold voltages low. The thick-oxide layer produced by the **MTOS** process is ten times as thick over the P-regions as any other known process employed in the manufacture of MOS devices. This strengthened thick-oxide layer over the P-regions, and the sequence of steps used in the **MTOS** process, which limits the etching time before metallization, eliminate the problems caused by pinholes that could occur at crossover points,

a major cause of failure in integrated circuits. Further, the thick oxide over the P-regions also minimizes the possibility of electrical short-circuits caused by the breakdown of the oxide resulting either from a flaw in the oxide layer or an accidental overvoltage.

### Speed and **MTOS**

Because crossovers occur over the thick oxide, stray capacitance is reduced, thereby increasing frequency and switching speeds by a factor approaching 10 for the more complex circuits. The **MTOS** process, in providing higher yields, permits the production of larger, more complex chips. This increased complexity makes possible the utilization of highly sophisticated circuitry to further improve speed capabilities. One example of such a circuit now in use is a multi-phase dynamic system which not only enhances operating speeds, but reduces still further the low power dissipation inherent in **MTOS** circuits. **MTOS** arrays are now being delivered with rated operating frequencies of 5MHz. (Pilot production devices are operating at still higher frequencies.)

### LSI means Large Scale Benefits, too...

The unprecedented packaging density and high yields made possible with the **MTOS** process provide cost and reliability advantages never before attainable in integrated circuits. In addition to the resulting lower initial costs per function, costs are further reduced by the elimination of most external wiring, printed circuit boards and assembly labor. Moreover, by

minimizing the need for external interconnections, a higher order of reliability, improved performance and product yield are obtained, making available the most complex functions so far achievable on a single monolithic chip.

### What **MTOS** can do for you

- It can lower the cost of your equipment
- It can shrink the size of your equipment
- It can upgrade the reliability of your equipment
- It can improve the performance of your equipment
- It can put you ahead of your less innovative competitors...and at least abreast of your more aware ones!

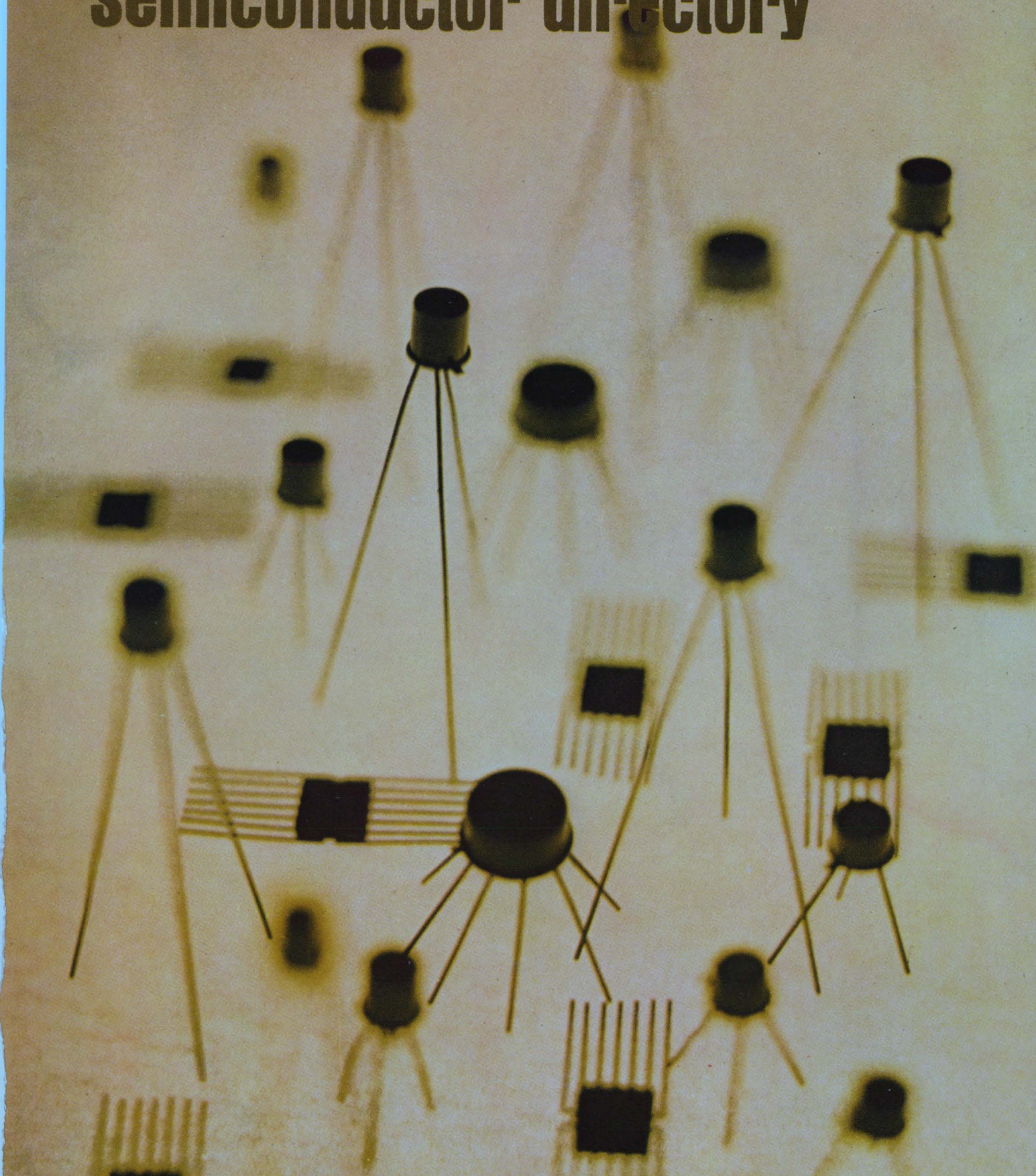
General Instrument's exclusive **MTOS** has made Large Scale Integration a practical reality. There is no longer any need to await the possible future developments of LSI... It is ready now for utilization in your equipment designs—whether you want to choose from the only broad line available, or in order to meet your special requirements—at General Instrument.

Write for full information and the "**MTOS** Circuit Digest."

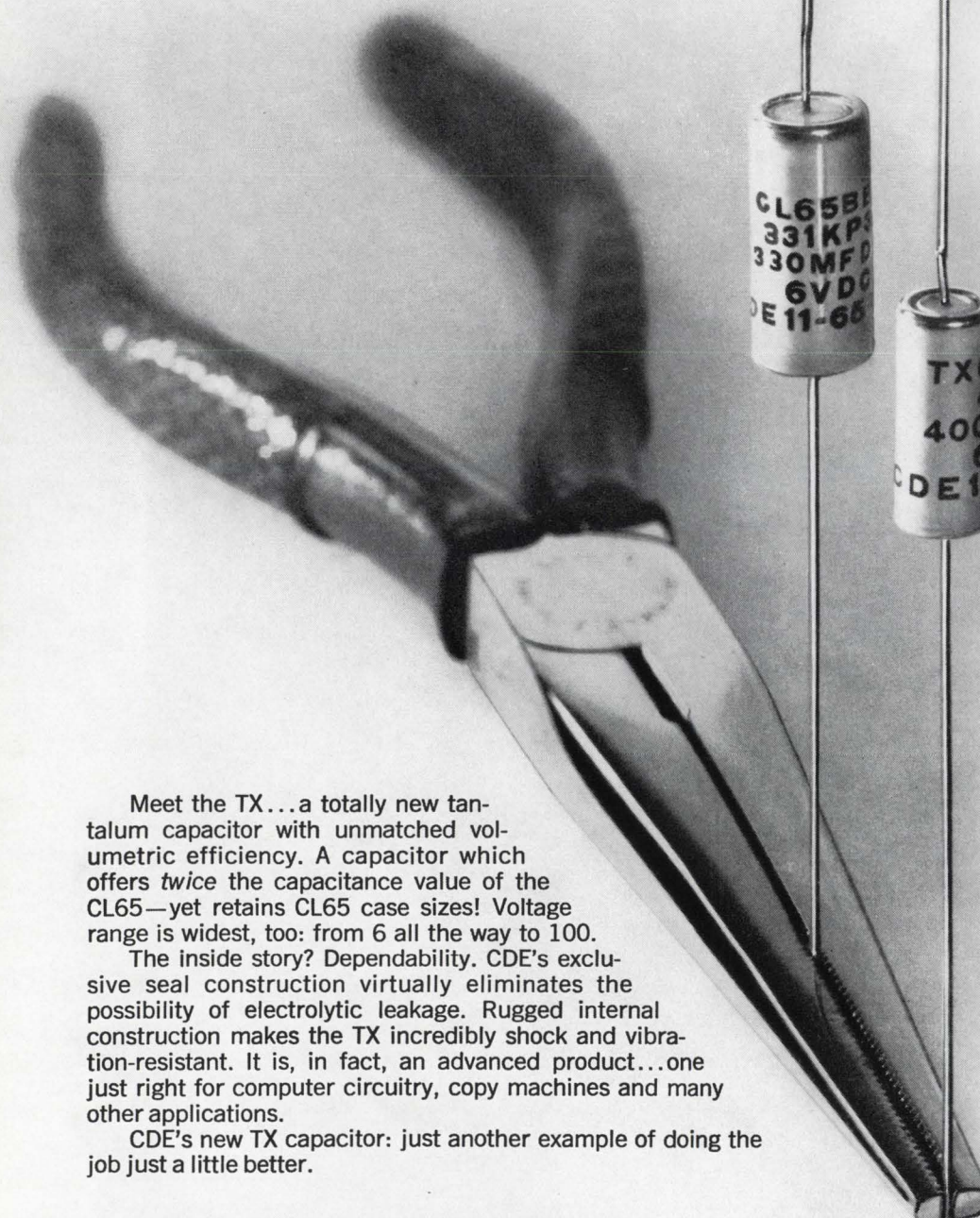


# Electronic Design

## semiconductor directory



# Looks are deceiving...



**CDE's  
new TX  
capacitor  
packs T3  
capacitance  
in a T2  
case!**

Meet the TX... a totally new tantalum capacitor with unmatched volumetric efficiency. A capacitor which offers *twice* the capacitance value of the CL65—yet retains CL65 case sizes! Voltage range is widest, too: from 6 all the way to 100.

The inside story? Dependability. CDE's exclusive seal construction virtually eliminates the possibility of electrolytic leakage. Rugged internal construction makes the TX incredibly shock and vibration-resistant. It is, in fact, an advanced product...one just right for computer circuitry, copy machines and many other applications.

CDE's new TX capacitor: just another example of doing the job just a little better.

**CDE** CORNELL-  
DUBILIER

# Addenda to ELECTRONIC DESIGN 1967 Semiconductor Directory (ED 9, April 26, 1967)

The following integrated circuits manufactured by Sprague Electric Co. were omitted from our 1967 Semiconductor Directory. Included are their operating temperature ranges and package descriptions. For full specifications, circle **388** on the Reader-Service Card in this issue.

**Operating temperature ranges**

-55 C to +125 C Series SE, US      +10 C to +55 C Series LU  
 -20 C to +85 C Series SU      +15 C to +70 C Series SP  
 0 C to +70 C Series NE, ST

**Packages** (letter following the type number)

A 14-lead plastic dual in-line      E TO-91  
 B 10-lead flat pack      G TO-91  
 C TO-85      J TO-88  
 D TO-78      K TO-100

			Fan-out	Propagation delay (nsec)	Average power (mW)	
DTL	NE106A, NE106J, SE106J	Dual 5-input gate expander	—	—	—	
	SE111J	Dual 4-input high fan-out gate	19	20	34	
	NE112A, NE112J, SE112J	Dual 3-input high fan-out gate	19	20	34	
	NE116A, NE116J, SE116J	Dual 4-input NAND gate	6	25	15	
	NE124A, NE124J, SE124J	RST binary element	7	18 MHz	28	
	NE125A, NE125J, SE125J	J-K binary element	8	12 MHz	40	
	SE155J	Dual 4-input clock/cap. line driver	19	20	34	
	NE156A, NE156J, SE156J	Dual 4-input clock/cap. line driver	19	20	34	
	NE161A, NE161J, SE161J	Monostable multivibrator	4	—	51	
	NE170A, NE170J, SE170J	Triple 3-input NAND gate	6	25	15	
	NE180A, NE180J, SE180J	Quadruple 2-input NAND gate	6	25	15	
	SP616A, ST616A	Dual 4-input expandable NAND gate	5	30	34	
	SP620A, ST620A	J-K binary element	5	5 MHz	28	
	SP629A, ST629A	RST binary element	5	10 MHz	40	
	SP631A, ST631A	Quadruple 2-input gate expander	—	—	—	
	SP659A, ST659A	Dual 3-input buffer/driver	12	25	34	
	SP670A, ST670A	Triple 3-input NAND gate	5	30	15	
	SP680A, ST680A	Quadruple 2-input NAND gate	5	30	15	
	US-720J	Quadruple 2-input NAND gate	6	25	14	
	US-721J	Triple 3-input NAND gate	6	25	14	
	US-727J	Triple 2-input NAND gate	6	25	15	
	US-729J	RST binary element	7	18 MHz	28	
	US-730J	Dual 5-input NAND gate	6	25	15	
	US-731J	Quadruple 2-input gate expander	—	—	—	
	US-732J	12-input gate expander	—	—	—	
	mWRTL	US-0908D, US-0908E	adder	—	120	10
		US-0909D, US-0909E	buffer	—	80	10
US-0910D, US-0910E		dual gate	—	40	4	
US-0911D, US-0911E		gate	—	80	4	
US-0912D, US-0912E		half adder	—	120	8	
US-0913D, US-0913E		register	—	120	15	
US-0921D, US-0921E		gate expander	—	40	0	
TTL		NE416A, NE416J, SE416J	Dual 4-input expandable NAND gate	7	32	9
	NE417A, NE417J, SE417J	Dual 3-input expandable NAND gate	7	35	8	
	NE424A, NE424J, SE424J	Dual AC binary element	7	9 MHz	14	
	NE440A, NE440J, SE440J	Dual exclusive OR gate	7	25	10	
	NE455A, NE455J, SE455J	Dual 4-input power/driver	24	29	12	
	NE480A, NE480J, SE480J	Quad 2-input NAND gate	7	25	9	
	NE806A, NE806J, SE806J	Dual 4-input expander	—	—	—	
	NE808A, NE808J, SE808J	Single 8-input NAND gate	10	13	20	
	NE816A, NE816J, SE816J	Dual 4-input NAND gate	10	13	20	
	NE825A, NE825J, SE825J	Dc clocked J-K binary element	10	20 MHz	70	
	NE826A, NE826J, SE826J	Dual J-K binary element	5	30 MHz	35	
	NE840A, NE840J, SE840J	Dual 4-input exclusive OR gate	10	13	35	
	NE855A, NE855J, SE855J	Dual 4-input power gate	30	13	25	
	NE870A, NE870J, SE870J	Triple 3-input NAND gate	10	13	20	
	NE880A, NE880J, SE880J	Quad 2-input NAND gate	10	13	20	
	SE8416J	Dual 4-input expandable NAND gate	7	35	4.5	

**Operating temperature ranges**

-55 C to +125 C Series SE, US  
 -20 C to +85 C Series SU  
 0 C to +70 C Series NE, ST

+10 C to +55 C Series LU  
 +15 C to +70 C Series SP

**Packages** (letter following the type number)

A 14-lead plastic dual in-line E TO-91  
 B 10-lead flat pack G TO-91  
 C TO-85 J TO-88  
 D TO-78 K TO-100

			Fan-out	Propagation delay (nsec)	Average power (mW)	
TTL	SE8417J	Dual 3-input expandable NAND gate	7	50	4.5	
	SE8424J	Dual AC binary element	7	9 MHz	9.0	
	SE8440J	Dual exclusive OR gate	7	25	4.5	
	SE8455J	Dual 4-input buffer/driver	20	28	7.0	
	SE8480J	Quad 4-input NAND gate	7	25	3.5	
	SE8806J	Dual 4-input expander	-	-	-	
	SE8808J	Single 8-input NAND gate	10	12	20	
	SE8816J	Dual 4-input NAND gate	10	12	20	
	SE8825J	Dc clocked J-K binary element	10	20 MHz	70	
	SE8826J	Dual J-K binary element	10	30 MHz	35	
	SE8840J	Dual 4-input exclusive OR gate	10	12	25	
	SE8855J	Dual 4-input power gate	26	12	25	
	SE8870J	Triple 3-input NAND gate	10	12	20	
	SE8880J	Quad 2-input NAND gate	10	12	20	
	SP416A, ST416A	Dual 4-input expandable NAND gate	7	40	12	
	SP417A, ST417A	Dual 3-input expandable NAND gate	7	40	12	
	SP424A, ST424A	Dual AC binary element	7	9 MHz	22	
	SP440A, ST440A	Dual exclusive OR gate	7	45	18	
	SP455A, ST455A	Dual 4-input power/driver	24	45	16	
	SP480A, ST480A	Quad 2-input NAND gate	7	40	9.0	
	SP806A, ST806A	Dual 4-input expander	-	-	-	
	SP808A, ST808A	Single 8-input	8	20	25	
	SP816A, ST816A	Dual 4-input NAND gate	8	20	25	
	SP825A, ST825A	Dc clocked J-K binary element	8	20 MHz	135	
	SP826A, ST826A	Dual J-K binary element	4	30 MHz	60	
	SP840A, ST840A	Dual 4-input exclusive OR gate	8	20	30	
	SP855A, ST855A	Dual 4-input power gate	24	20	45	
	SP870A, ST870A	Triple 3-input NAND gate	8	20	25	
	SP880A, ST880A	Quad 2-input NAND gate	8	20	25	
	RCTL	US-0100B	R-S flip-flop/counter/shift reg.	4	-	2
		US-0101B	R-S flip-flop/counter/shift reg.	20	-	3
		US-0102B	6-input NOR/NAND gate	5	-	2
		US-0103B	6-input NOR/NAND gate	25	-	2
US-0104B		Dual 3-input NOR/NAND gate	5	-	2	
US-0104B		Exclusive OR circuit	5	-	3	
US-0106B		Dual 2-input NOR/NAND gate and inv.	25	-	2	
US-0107B		Clock driver circuit	20	-	3	
US-0108B		Single shot multivibrator	5	-	4	
US-0109B		Pulse exclusive OR gate	5	-	6	
US-0110C		R-S flip-flop with dual resets	4	-	2	
US-0111C		R-S flip-flop with dual resets	20	-	3	
US-0112C		Triple 2-input NOR/NAND gate	5	-	2	
US-0113C		Triple 2-input NOR/NAND gate	5	-	2	
US-0114B		4x1x1 input NOR/NAND gate	5	-	2	
US-0115B	4x1x1 input NOR/NAND gate	25	-	2		
Linear Circuits	NE501, SE501	RF/video/pulse amplifier	-	4-40 MHz	25	
	NE505, SE505	Small signal diff. amplifier	-	1 MHz	100	
	NE506, SE506	Operational amplifier	-	500 kHz	180	
	NE518, SE518	Voltage comparator	-	5 MHz	170	
Utilogic	LU300K, SU300K	Dual 3-input gate expander	-	-	-	
	LU305K, SU305K	6-input AND gate	10	25	5	
	LU306K, SU306K	Dual 3-input AND gate	10	25	5	
	LU314K, SU314K	7-input NOR gate	17	30	18	
	LU315K, SU315K	Dual 3-input NOR gate	17	30	18	
	LU316K, SU316K	Dual 2-input NOR gate	17	30	18	
	LU320K, SU320K	J-K binary element	17	4 MHz	90	
	LU331K, SU331K	Dual 2-input OR gate	17	30	36	
	LU332K, SU332K	Dual 3-input OR gate	17	30	36	

The following companies should be added to the diode chart:

Company	Products	Company	Products	Company	Products
Parametric Industries, Inc. 63 Swanson Street Winchester, Mass. 01890 Tel.: (617) 729-7333	Varactors PIN diodes	Monsanto Electronics 800 N. Lindbergh Blvd. St. Louis, Mo. 63166 Tel.: (314) 694-2136	Lasers Visible and invisible light emitting diodes and arrays	Victory Engineering P.O. Box 187 Springfield, N.J. Tel.: (201) 379-5900	Varistors



# 1967

## Semiconductor Directory

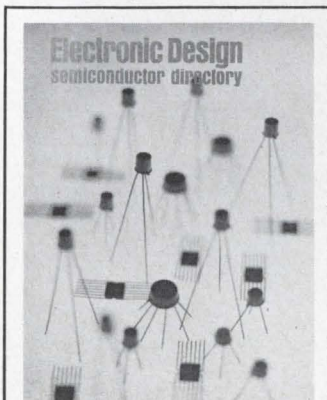
### Reference Issue

**Roger Kenneth Field**     **Peter N. Budzilovich**  
*Technical Editors*

ELECTRONIC DESIGN's Fifteenth Annual Semiconductor Data Charts once again are tailored to the specific needs of the design engineer.

Unlike other existing lists, which group devices by manufacturer or numerical sequence (and are fine for salesmen but of limited use to engineers), the devices in ELECTRONIC DESIGN's directory are listed both by application categories and numerically with cross-indexes. Within each application category (see table of contents below) the devices are arranged in order of the corresponding key parameter.

<b>List of semiconductor manufacturers</b>			86
<b>How to use the charts and glossary of symbols</b>			85
<b>Bipolars:</b>			
Audio and General-Purpose	95	Low-level switching	138
High-frequency	102	High-level switching	146
Power	120		
<b>Field-Effect transistors:</b>			
Analog switching	156	Differential dc amplifiers	162
Digital switching	158	General-purpose ac amplifiers	162
Low-drift single-ended dc amplifiers	160	Low-noise ac amplifiers	166
		High-frequency ac amplifiers	167
<b>Unijunction</b>			
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<b>Transistors cross index</b> (bipolars, FETs, UJTs)			170
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<b>Microelectronics cross-index</b>			218



The cover, photographed by Barry Ashley, shows a group of devices that were put at the disposal of Electronic Design by Fairchild Semiconductors.

# Update Your Semiconductor File

...in two easy steps (at no charge)



## Step 1

Discard obsolete data sheets and catalogs.

## Step 2

Circle appropriate numbers on the Reader-Service card and receive the latest data sheets, application notes and catalogs from semiconductor manufacturers. Full test details, recommended applications, price lists and other specific data will be sent to you.

## Result

... a completely updated semiconductor file.

# How to use the charts

There are two ways to locate the devices—by the application on hand or by the device number (only JEDEC numbers for bipolars are listed).

If you are looking for a device to do some specific job, follow these steps:

1. Locate the proper chart as defined in the table of contents, page 83.
2. Locate the device in accordance with the required value of the key parameter (shaded column in all charts).

If you know the device number, go through these steps:

1. Locate the device in the proper Cross Index.
2. The Cross Index will tell you exactly where the device is listed in the data charts.

The manufacturer whose data is used for each device is listed under "Mfr." in coded form. Manufacturers full names and addresses appear in the manufacturers list, page 86.

Other suppliers of the same device are found under "Remarks". There is no implication that the company listed under "Mfr." is a prime supplier or a cheaper source. The final choice of supplier is obviously up to the designer.

Values of only major device parameters are listed in the charts. Detailed specifications in all cases may be obtained by circling appropriate numbers as called out on the Reader-Service card (which is valid for one year). Circle as many numbers as you please.

## Key to Symbols

$f_{ae}$	= small signal short-circuit forward current transfer ratio cutoff frequency (common-emitter)
$f_{ab}$	= small-signal short-circuit forward current transfer ratio cutoff frequency (common-base)
$f_T$	= gain-bandwidth product
$P_c$	= collector power dissipation (average)
$T_j$	= junction temperature °C
$mW/°C$	= derating factor
$V_{CEO}$	= max collector voltage, collector to emitter base open
$V_{CBO}$	= max collector voltage, collector to base, emitter open
$I_c$	= max collector current
$I_p$	= max collector current (peak)
$h_{fe}$	= small-signal short-circuit forward current transfer ratio (common-emitter)
$h_{FE}$	= dc short-circuit forward current transfer ratio (common-emitter)
$I_{CO}$	= collector cutoff current (dc) emitter open
$C_{oe}$	= output capacitance (common-emitter)
$C_{ob}$	= output capacitance (common base)
$t_r$	= rise time
$t_s$	= storage time
$V_{CE(sat)}$	= collector-to-emitter saturation voltage

$g_m$	= transconductance
$V_p$	= pinch-off voltage
$I_{DSS}$	= zero-bias drain current
$BV_{DGO}$	= drain-gate breakdown voltage with gate-source open-circuited
$BV_{DGS}$	= breakdown voltage from drain to gate with drain shorted to source
$C_{is}$	= common source short-circuit input capacitance
N.F.	= noise figure
$\eta$	= intrinsic standoff ratio
$I_{EO}$	= max emitter reverse current
$I_p$	= max peak point emitter current
$V_{E(sat)}$	= max emitter saturation voltage
$V_{EB2}$	= min emitter reverse voltage
$V_{OB1}$	= min base one peak pulse voltage

## Construction

AE	= Annular epitaxial
AJ	= Alloy junction
AD	= Alloy diffused
DD	= Double diffused
DG	= Grown diffused
DJ	= Diffused junction
DM	= Diffused mesa
DDM	= Double diffused mesa
DP	= Diffused planar
DR	= Drift
ED	= Electro-chemical diffused-collector
EM	= Epitaxial mesa
EP	= Epitaxial

FA	= Fused alloy
FJ	= Fused junction
GD	= Grown diffused
GJ	= Grown junction
GR	= Rate grown
MB	= Meltback
MD	= Micro-alloy diffused base
MS	= Mesa
PE	= Planar epitaxial
PL	= Planar
SBT	= Surface barrier
SP	= Surface precision alloy
TDP	= Triple-diffused planar
PADT	= Past alloy diffused technique

## Materials

ge	= germanium
si	= silicon

## FET Symbols

n	= n-type channel
p	= p-type channel
F	= junction FET
M	= MOS FET

## Microelectronic package types

A	= TO-5 type packages.
B	= TO-47
C	= 1/4 in. sq. flat-pack (TO-86, TO-91)
D	= 1/4 x 1/8 in. flat-pack (TO-84, TO-85, TO-89, TO-90)
E	= 3/8 in. sq. flat-pack
F	= 1/4 x 3/8 in. flat-pack (TO-87, TO-88, TO-95)
G	= Special packages
DIP	= Dual in-line package (14 lead)

# List of Semiconductor Manufacturers and their literature offerings

Bring your semiconductor data file up to date. Use the Reader-Service card to obtain data sheets, catalogs, application notes and other useful information. Letter codes in the first column are used to identify transistor and microelectronics manufacturers in the data charts. Consult dot charts for Diodes and Rectifiers (p. 186) to learn who makes what.

Code	Company	Type of Information Offered	Transistor	Diode	Micro-electronics
	<b>Airtron Div., Litton Industries</b> 200 East Hanover Avenue Morris Plains, N.J. 07950 (201) 539-5500 TWX: 201-538-6744	Data sheets. Article reprints.		250	
	<b>Alpha Industries</b> 381 Elliot St. Newton Upper Falls, Mass. 02164	Data sheets. Short form catalog.		251	
	<b>Alpha Microelectronics Co., Inc.</b> 10501 Rhode Island Avenue Beltsville, Maryland 20705 (301) 474-1222	Application notes.			252
AL	<b>Amelco Semiconductor</b> 1300 Terra Bella Avenue Mountain View, California 94042 (415) 986-9241 TWX: 415-969-9112	Short form catalog. Application notes. Data sheets. Complete catalog. Article reprints. Customer applications service.	253		254
	<b>American Electronic Laboratories, Inc.</b> P.O. Box 552 Lansdale, Pa. (215) 822-2929 TWX: 510-661-4976	Data sheets. Catalogs. Article reprints. Customer applications service.		255	
	<b>American Semiconductor</b> 4 N. Hickory Ave. Arlington Heights, Ill. 60004	Data sheets. Catalogs.		256	
AMP	<b>Amperex Electronics Corp.</b> Providence Pike Slatersville, Rhode Island 02876 (401) 762-9000 TWX: 710-387-1591	Data sheets. Complete catalog. Customer applications service. Design aids. Short form catalog. Article reprints.	257	258	259
	<b>Atlantic Instrument &amp; Elect. Inc.</b> 50 Hunt Street Newton, Massachusetts 02158 (617) 926-2400		260		

Code	Company	Type of Information Offered	Transistor	Diode	Micro-electronics
	<b>Atlantic Semiconductor Inc.</b> 905 Mattison Ave. Asbury Park, New Jersey 07712 (201) 775-1827	Data sheets.		261	
	<b>Bell, F. W., Inc.</b> 1356 Norton Avenue Columbus, Ohio 43212 (614) 294-4906 TWX: 810-482-1716	Data sheets.		262	
BE	<b>Bendix Semiconductor Div.</b> South Street Holmdel, New Jersey 07733 (201) 747-5400 TWX: 201-946-9400	Application notes. Short form catalog.	263	263	
	<b>Bradley Semiconductor Corp.</b> 275 Welton St. New Haven, Connecticut 06506 (203) 787-7181 TWX: 203-772-0676	Short form catalog.		264	
	<b>Bunker-Ramo Corporation</b> 8433 Fallbrook Avenue Canoga Park, California 91304 (213) 346-6000 TWX: 213-348-2361				265
BU	<b>Burroughs Corp. Electronic Components Div.</b> Mt. Bethel Road Plainfield, New Jersey 07061 (201) 757-5000 TWX: 710-981-7907		266	267	
	<b>CTS Corporation</b> 1142 W. Beardsley Avenue Elkhart, Indiana (219) 523-0210 TWX: 810-294-2256				268

Code	Company	Type of Information Offered	Transistor	Diode	Micro-electronics
	<b>Centralab</b> Div. <b>Globe-Union Inc.</b> 5757 N. Green Bay Ave. Milwaukee, Wisconsin 53201 (414) 228-2616 TWX: 910-262-3084	Data sheets.			269
	<b>Columbia Components Corp.</b> 24-30 Brooklyn-Queens Expressway Woodside, New York 11377 (212) 932-0800	Catalog. Application notes on hybrid circuits.			270
	<b>Computer Diode Corp.</b> Pollitt Drive Fairlawn, N.J. 07410 (201) 797-3900 TWX: 201-796-0660	Data sheets.		271	
	<b>Conant Laboratories</b> 6500 O St. Lincoln, Nebraska 68501 (402) 488-0432	Catalogs.		272	
CDC	<b>Continental Device Corp.</b> 12515 Chadron Street Hawthorne, California 90252 (213) 772-4551 TWX: 910-325-6217	Data sheets. Catalogs. Article reprints. Short form catalog.	273	274	
CT	<b>Crystalonics Inc.</b> 147 Sherman Street Cambridge, Mass. 02140 (617) 491-1670 TWX: 617-499-9156	Application notes. Data sheets. Short form catalog. Complete catalog. Article reprints.	275	276	
DE	<b>Delco Radio Div.</b> <b>General Motors Corp.</b> 700 East Firmin Street Kokomo, Indiana 46901 (317) 457-8461 TWX: 317-452-5747	Short form catalog.	277	278	
	<b>Delta Semiconductors Inc.</b> 879 W. 16th St. Newport Beach, California 92660 (714) 540-4160 TWX: 714-642-1335	Data sheets. Catalogs.		279	
DIC	<b>Dickson Electronics Corp.</b> Gains Guaranty Building 20 West Main Street Scottsdale, Arizona 85252 (602) 947-5751 TWX: 602-949-0146	Data sheets. Application notes.	280	281	
	<b>Diodes Incorporated</b> 9261 Independence Avenue Chatsworth, California 91311 (213) 341-4850 TWX: 213-341-2912			282	
	<b>Eastern Delta Corporation</b> 2909 Broadway Fairlawn, New Jersey 07411 (201) 797-4200	Data sheets.		283	
	<b>Eastron Corporation</b> 25 Locust Street Haverhill, Massachusetts 01830 (617) 373-3824	Data sheets. Application notes.		284	
	<b>Edal Industries</b> 4 Short Beach Road East Haven, Connecticut 06512 (203) 467-2591	Data sheets. Complete catalog. Short form catalog. Application notes.		285	
	<b>Egerton, Germeshausen &amp; Grier, Inc.</b> 160 Brookline Ave. Boston, Massachusetts 02215 (617) 267-9700 TWX: 617-262-9317	Data sheets. Application notes.		286	
	<b>Electro-Optical Systems, Inc.</b> 300 North Halstead Pasadena, California 91107 (213) 449-1230 TWX: 213-577-0060			287	

Code	Company	Type of Information Offered	Transistor	Diode	Micro-electronics
	<b>Electronic Control Corp.</b> 1010 Pamela Drive P.O. Box J Euleless, Texas (817) 283-1596			288	
	<b>Electronic Devices Inc.</b> 21 Gray Oaks Avenue Yonkers, New York 10710 (914) 965-4400 TWX: 914-476-3110	Application notes. Complete catalog.		289	
ETC	<b>Electronic Transistors Corp.</b> 153-13 Northern Boulevard Flushing, New York 11354 (212) 539-6700	Data sheets. Catalogs.	290		
	<b>Erie Technological Products, Inc.</b> 644 West 12th St. Erie, Pennsylvania 16512 (814) 456-8592 TWX: 814-453-6816	Complete catalog.		291	
	<b>Espey Mfg. &amp; Electronics Corp.</b> Box 422 Saratoga Spring, N.Y. 12866 (518) 584-4100	Data sheets.		292	
FA	<b>Fairchild Semiconductor</b> 545 Whisman Rd. Mountain View, California 94040 (415) 962-5011 TWX: 910-379-6435	Data sheets. Application notes. Short form catalog.	293	294	295
	<b>Gemini Semiconductors, Inc.</b> 482 Ridgedale Ave. Hanover, N.J. 07936 (203) 887-8181	Catalogs with application notes.		296	
GE	<b>General Electric Co.</b> <b>Semiconductor Products Dept.</b> Bldg. 7, Electronics Park Syracuse, N.Y. (315) 456-2798 TWX: 710-541-0498	Data sheets. Catalogs. Application notes. Article reprints.	297	298	299
GI	<b>General Instrument Corp.</b> 100 Andrews Rd. Hicksville, N.Y. 11802 (516) 681-4042	Application notes. Data sheets. Complete catalog. Short form catalog. Technical bulletin.	311	312	313
	<b>General Semiconductors, Inc.</b> 230 West 5th Street Tempe, Arizona 85280 (682) 966-7263 TWX: 910-950-1942	Data sheets. Catalogs. Data manuals. Customer applications service.		314	
	<b>Green Rectifier Corp.</b> 1-10 30 Street Fairlawn, N.J. 07411 (201) 797-8100			315	
	<b>HP Associates</b> 2900 Park Boulevard Palo Alto, Calif. 94304 (415) 321-8510	Data sheets. Application notes. Catalogs.		316	
	<b>Halex, Inc.</b> 139 Maryland Street El Segundo, Calif. (213) 772-2545 TWX: 213-322-1608	Data sheets.			317
	<b>Heliotek Div.</b> <b>Textron Electronics Inc.</b> 12500 Gladstone Ave. Sylmar, Calif. 91734 (213) 365-6301 TWX: 213-764-5923			318	
HOF	<b>Hoffman Electronics Corp.</b> <b>Semiconductor Division</b> 4501 North Arden Drive El Monte, Calif. 91734 (213) 686-0123 TWX: 910-587-3429	Data sheets. Catalogs. Application notes. Article reprints.		319	

Code	Company	Type of Information Offered	Transistor	Diode	Micro-electronics
HU	<b>Hughes Aircraft Co.</b> Microelectronics Division 500 Superior Ave. Newport Beach, Calif. 92663 (714) 548-0671 TWX: 714-548-0671	Data sheets. Application notes.	320	321	322
	<b>Hunt Electronics Co.</b> 2617 Andjon Dallas, Texas 75220 (214) 352-8421			323	
ITT	<b>ITT Semiconductors</b> 3301 Electronics Way West Palm Beach, Fla. 33402 (305) 842-2411 TWX: 510-952-6667	Catalogs.	324	324	324
IND	<b>Industro Transistor Corp.</b> 35-10 36th Avenue Long Island City, N.Y. (212) 392-8000		325		
	<b>Instrument Systems Corp.</b> 770 Park Avenue Huntington, N.Y. (516) 423-6200 TWX: 516-421-4042	Data sheets.		326	
IN	<b>Intellux, Inc.</b> 26 Coromar Dr. Goleta, Calif. 93017 (805) 968-3541 TWX: 805-449-7223	Data sheets. Catalogs. Application notes. Article reprints. Data manuals. Customer applications service. Design aids.			327
	<b>International Diode Corp.</b> 90 Forrest St. Jersey City, N.J. 07304 (201) 432-7151	Data sheets. Short form catalog.		328	
IEC	<b>International Electronics Corp.</b> 316 South Service Rd. Melville, L.I., N.Y. 11749 (516) 694-7700 TWX: 212-479-9410	Data sheets. Application notes. Complete catalog.	329	329	
	<b>International Rectifier Corp.</b> 233 Kansas Street El Segundo, Calif. 90245 (213) 678-6281 TWX: 213-322-2623	Data sheets. Complete catalogs. Application notes.		330	
	<b>IRC, Inc.</b> Semiconductor Div. 71 Linden Street West Lynn, Mass. 01905 (617) 598-4800 TWX: 617-599-4391	Data sheets. Complete catalog. Short form catalog.		331	
KMC	<b>KMC Semiconductor Corp.</b> Parker Road Long Valley, N.J. 07853 (201) 876-3811	Data sheets. Complete catalogs. Application notes. Article reprints. Short form catalog.	332	332	
KSC	<b>KSC Semiconductor Corp.</b> 437 Cherry St. West Newton, Mass. (617) 969-8451	Data sheets. Complete catalog. Short form catalog.	333		
	<b>Kemtron Electron Products</b> 14 Price Place Newburyport, Massachusetts 01950 (617) 462-4464			334	
	<b>Korad Corporation</b> 2520 Colorado Avenue Santa Monica, Calif. 90404 (213) 393-6737 TWX: 213-879-0556			335	
LAN	<b>Lansdale Transistor &amp; Electronics Inc.</b> 1111 North Broad Street Lansdale, Pa. 19446 (215) 885-9004 TWX: 510-661-7532		336		

Code	Company	Type of Information Offered	Transistor	Diode	Micro-electronics
	<b>Ledex, Inc.</b> 123 Webster Street Dayton, Ohio (513) 224-9891 TWX: 513-944-0286	Catalogs.		337	
	<b>M. S. Transistor Sub. of Silicon Transistor Corp.</b> 80-02 51st Ave. Elmhurst, N.Y. 11373 (212) 478-3134	Short form catalogs.	338		
	<b>MSI Electronics Corporation</b> 116-06 Myrtle Avenue Richmond Hill, N.Y. (212) 441-6420			339	
	<b>Mallory Semiconductor Co.</b> 424 South Madison Street DuQuoin, Ill. 62832 (618) 542-2154 TWX: 618-542-4120			340	
MEP	<b>Mepco, Inc.</b> 35 Abbett Morristown, New Jersey 07960 (201) 539-2000 TWX: 710-986-7437	Data sheets.			341
	<b>MicroSemiconductor Corp.</b> 11250 Playa Court Culver City, Calif. 90230 (213) 391-8271	Data sheets. Catalogs. Application notes. Article reprints. Short form catalog.		342	343
	<b>Micro State Electronics Corp.</b> Subsidiary of Raytheon Co. 152 Floral Avenue Murray Hill, N.J. 07971 (201) 464-3000 TWX: 710-984-7966	Data sheets. Catalogs. Application notes. Article reprints. Short form catalog.		344	
	<b>Microwave Associates</b> South Street Northwest Industrial Park Burlington, Mass. 01803 (617) 272-3000 TWX: 272-1492	Data sheets. Application notes. Complete catalogs.		345	
MO	<b>Motorola Semiconductor Products, Inc.</b> P.O. Box 955 Phoenix, Ariz. 85001 (602) 273-6900 TWX: 602-255-0590	Data sheets. Catalogs. Short form catalogs. Application notes.	346	347	348
	<b>National Electronics Inc.</b> 628 North Geneva, Ill. 60134 (312) 232-4300 TWX: 910-237-1685	Data sheets.		349	
NA	<b>National Semiconductor Corp.</b> Commerce Rd. Danbury, Conn. 06810 (203) 744-0060 TWX: 203-456-1142	Data sheets. Short form catalog.	350		351
NOR	<b>Norden Div., United Aircraft Corp.</b> Commerce Road Norwalk, Conn. 06856 (203) 838-4471 TWX: 710-468-0888	Data sheets. Catalogs. Application notes. Article reprints. Customer applications service.			352
NUC	<b>Nucleonic Products Co., Inc.</b> 3133 East 12th Street Los Angeles, Calif. 90023 (213) 968-3464 TWX: 910-321-3077	Data sheets.	353	354	
	<b>Ohmite Manufacturing Co.</b> 3601 Howard Street Skokie, Ill. 60076 (312) 675-2600 TWX: 312-677-6704			355	

Code	Company	Type of Information Offered	Transistor	Diode	Micro-electronics
PR	<b>Philbrick Researches, Inc.</b> Allied Drive at Route 128 Dedham, Mass. 02026 (617) 329-1600 TWX: 617-326-5754				356
PH	<b>Philco-Ford Corporation</b> <b>Microelectronic Div.</b> 2920-San Ysidro Way Santa Clara, Calif. 95051 (408) 245-2966	Data sheets. Short form catalog.	357	358	359
	<b>Power Components, Inc.</b> P.O. Box 421 Scottsdale, Pa. 15683 (412) 887-6600 TWX: 412-887-5152	Catalogs. Application notes.		360	
RAD	<b>Radiation Inc.</b> P.O. Box 37 Melbourne, Florida 32901 (305) 723-1511 TWX: 305-723-7865	Data sheets.		361	361
RCA	<b>Radio Corp. of America</b> <b>Electronic Components &amp; Devices</b> 415 S. Fifth Street Harrison, N.J. 07029 (201) 485-3900 TWX: 201-621-7846	Catalogs.	362	362	362
RA	<b>Raytheon Co.</b> <b>Semiconductor Operation</b> 350 Ellis St. Mountain View, Calif. 94041 (415) 968-9211 TWX: 910-379-6445	Data sheets. Catalogs.	363	364	365
	<b>Rectico Inc.</b> 20 Village Park Road Cedar Grove, N.J. 07009 (201) 239-6464			366	
	<b>Sanford Miller Corp.</b> 89 Throop Avenue Brooklyn 6, N.Y. (212) 387-0600	Complete catalog.		367	
	<b>Sarkes Tarzian, Inc.</b> 415 N. College Avenue Bloomington, Indiana 47401 (812) 332-1435 TWX: 810-351-1384	Data sheets. Catalogs. Application notes. Data manuals. Short form catalog.		368	
	<b>Schauer Mfg. Corp.</b> 4500 Alpine Avenue Cincinnati, Ohio 45242 (513) 791-3030			369	
	<b>Semcor Div., Components Inc.</b> 3540 W. Osborn Road Phoenix, Arizona 85019 (602) 272-1341 TWX: 602-255-0479			370	
	<b>Semicon Inc.</b> Sweetwater Avenue Bedford, Mass. 01730 (617) 275-8542 TWX: 617-862-3302			371	
	<b>Semiconductor Devices Inc.</b> 875 W. 15th St. Newport Beach, Calif. 92663 (714) 642-5100			372	
	<b>Semiconductor Specialists Inc.</b> 5700 W. North Avenue Chicago, Ill. 60639 (312) 622-8860 TWX: 910-221-1333			373	
	<b>Semi-Elements Inc.</b> Saxonburg Boulevard Saxonburg, Pa. 16056 (412) 352-1548	Catalogs. Data sheets.		374	

Code	Company	Type of Information Offered	Transistor	Diode	Micro-electronics
	<b>Semtech Corp.</b> 652 Mitchell Rd. Newbury Park, Calif. 91320 (213) 628-5392 TWX: 805-499-7137	Data sheets. Catalogs. Short form catalog.		375	
SA	<b>Siemens America Inc.</b> 230 Ferris Ave. White Plains, N.Y. 10603 (914) 948-3434 TWX: 914-997-0725	Data sheets. Complete catalog. Short form catalog.	376	377	378
SIG	<b>Signetics Corp.</b> 811 E. Arques Ave. Sunnyvale, Calif. 94086 (408) 739-7700 TWX: 910-339-9220	Data sheets. Application notes. Article reprints.			379
STC	<b>Silicon Transistor Corp.</b> E. Gate Blvd. Garden City, N.Y. (516) 742-4100 TWX: 510-222-8258	Data sheets. Catalogs. Application notes. Customer applications service.	380	380	
SI	<b>Siliconix Inc.</b> 1140 W. Evelyn Ave. Sunnyvale, Calif. 94086 (408) 245-1000 TWX: 408-737-9948	Application notes. Data sheets. Article reprints.	381		382
	<b>Slater Electric, Inc.</b> 45 Sea Cliff Ave. Glen Cove, N.Y. (516) 671-7000 TWX: 516-671-3815	Data sheets. Catalogs. Application notes.		383	
	<b>Solar Systems Inc.</b> 8241 N. Kimball Ave. Skokie, Ill. 60076 (312) 676-2040 TWX: 910-233-3642			384	
SSP	<b>Solid State Products Inc.</b> One Pingree St. Salem, Mass. 01970 (617) 745-2900 TWX: 710-347-0226	Data sheets. Catalogs. Application notes. Customer applications service.	385	385	
SOL	<b>Solitron Devices Inc.</b> 1177 Blue Heron Blvd. Riviera Beach, Fla. 33404 (301) 848-4311 TWX: 510-952-6676	Data sheets. Catalogs. Short form catalogs. Application notes.	386		
SSD	<b>Sperry Semiconductor</b> 380 Main Ave. Norwalk, Conn. 06852 (203) 847-3851 TWX: 710-468-0591	Data sheets. Application notes. Short form catalog.	387		387
SPR	<b>Sprague Electric Co.</b> 491 Marshall St. North Adams, Mass. 01247 (413) 664-4411 TWX: 413-663-3581	Data sheets. Application notes. Short form catalog.	388		388
SW	<b>Stewart-Warner Microcircuits Inc.</b> 730 W. Evelyn Ave. Sunnyvale, Calif. 94086 (408) 245-9200				389
SY	<b>Sylvania Electric Prods.</b> 100 Sylvan Road Woburn, Mass. 01801 (617) 933-3500	Data sheets. Catalogs. Application notes. Customer applications service. Design aids.	390	391	392
	<b>Syntron Co.</b> 283 Lexington Ave. Homer City, Pa. 15748 (412) 479-9477			393	
TRWS	<b>TRW Semiconductors Inc.</b> 14520 Aviation Blvd. Lawndale, Calif. 90260 (213) 679-4561 TWX: 910-325-6206	Data sheets. Article reprints. Short form catalog.	394	395	

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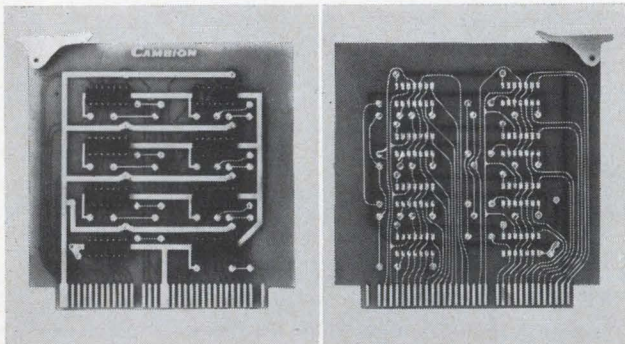
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TI	Texas Instruments Inc. Semiconductor Components Div. P.O. Box 5012 Dallas, Texas 75222 (214) 238-2011 TWX: 214-231-1492	Data sheets. Catalogs. Application notes. Customer applications service.	396	397	398
TR	Transitron Electronic Corp. 168 Albion St. Wakefield, Mass. 01881 (617) 245-4500 TWX: 617-245-7823		399	399	399
TRI	Trio Laboratories 80 DuPont St. Plainview, N.Y. 11803 (516) 681-0400 TWX: 516-433-9573	Data sheets. Application notes.		400	401
UC	Union Carbide Electronics 365 Middlefield Rd. Mountain View, Calif. 94040 (415) 961-3300		402		403
	Unitrode Corp. 580 Pleasant St. Watertown, Mass. 02172 (617) 926-0404 TWX: 710-327-1297	Data sheets. Catalogs. Data manuals. Customer applications service. Design aids.		404	
	Vactec Inc. 2423 Northline Industrial Blvd. Maryland Heights, Mo. 63045 (314) 432-4200			405	
	Varian/Bomac Div. Salem Road Beverly, Mass. 01915 (617) 922-6000 TWX: 617-922-1978			406	
VAR	Varo Inc., Special Products Div. 2201 Walnut St. Garland, Texas 75040 (214) 276-6141 TWX: 214-276-8577			407	408
VEC	Vector Solid State Labs. Southampton, Pa. 18966 (215) 357-7600		409		
	Wagner Electric Corp. 1 Summer Ave. Newark, N.J. 07104 (201) 484-8500 TWX: 710-995-4607	Data sheets. Catalogs.		410	
	Western Semiconductors Inc. 2200 Fairview St. Santa Ana, Calif. 92704 (714) 546-5717 TWX: 714-546-2245	Data sheets. Catalogs. Customer applications service.		411	
	Western Transistor Corp. 11581 Federal Drive El Monte, Calif.		412		
WH	Westinghouse Electric Corp. Molecular Electronics Division Box 7377 Elkridge, Maryland 21227 (301) 796-3666 TWX: 301-761-4340	Data sheets. Short form catalog. Complete catalog. Application notes. Article reprints.			413
WH	Westinghouse Electric Corp. Semiconductor Div. Youngwood, Pa. 15697 (412) 925-7272 TWX: 412-679-2783	Data sheets. Catalogs. Application notes. Article reprints. Design aids. Short form catalog.	414	415	



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The Editors of Electronic Design

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Part No.	Noise Figure @ Given Frequency	Power Output as Oscillator at Given Frequency (typ.)	ft in GHz		Price Quantity 1 to 9
			Min.	Typ.	
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K5201C	3 db @ 1 GHz		1.5	2.0	\$100 ea.
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K2121	2.5 db @ 450 MHz		1.0	1.4	\$ 25 ea.
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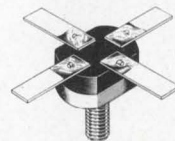
Performance—the industry's lowest emitter and base inductances (0.1 nH and 0.2 nH respectively) result in optimum gain and power capability right up to 700 MHz... efficient for broadband and narrowband transmitters.

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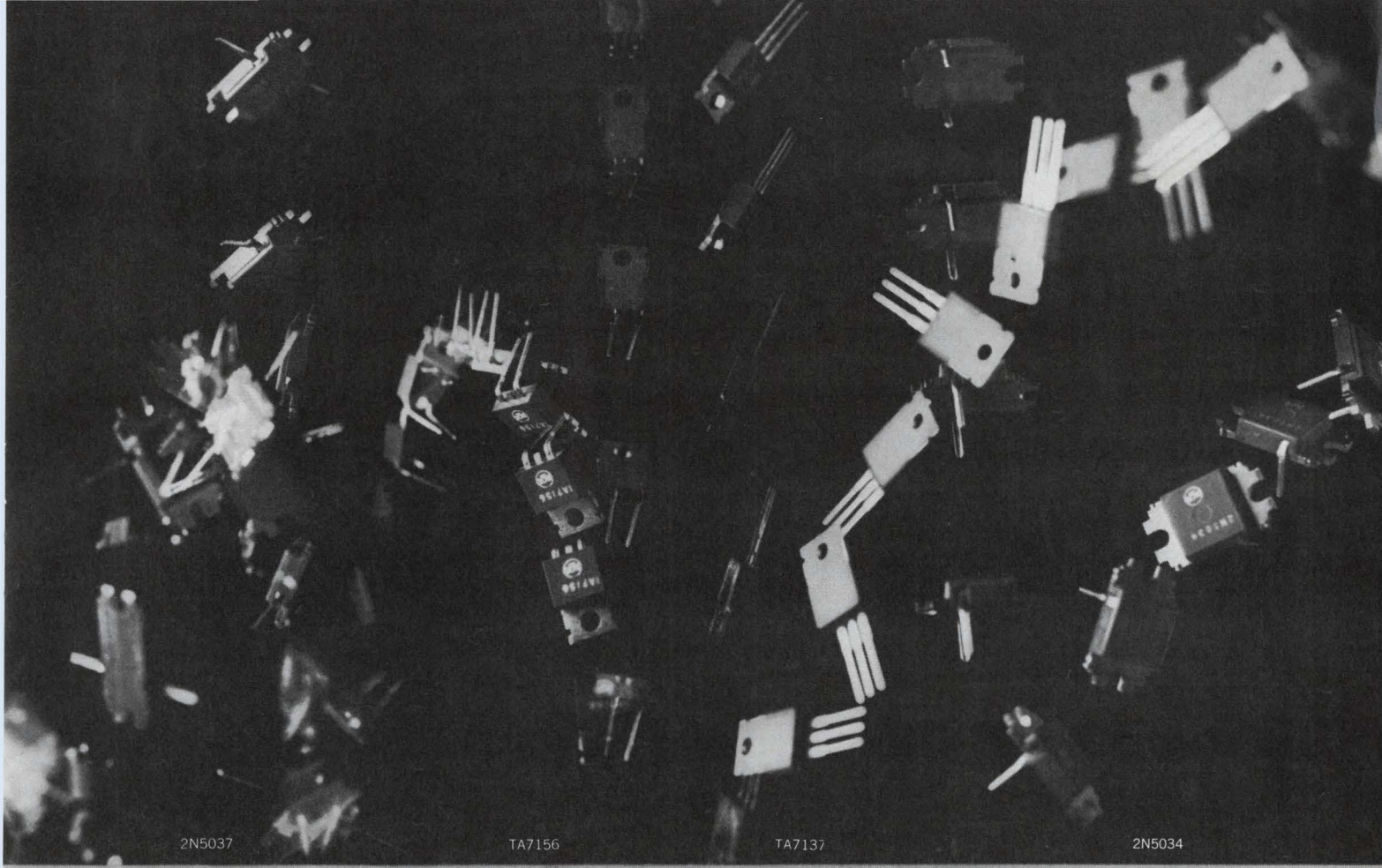
Versatility—"terminal block" structure permits choice of stripline, printed

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2N5036	TO-3 equivalent	60 V @	8A	20-70 @	1.5	83 W
2N5037	P.C. type	R <sub>BE</sub> = 100 ohms		3A	°C/W	
2N5034	TO-3 equivalent	45 V @	6A	20-70 @	1.5	83 W
2N5035	P.C. type	R <sub>BE</sub> = 100 ohms		2.5A	°C/W	
TA7155	TO-66 equivalent	60 V @	4A	25-100 @	3.5	36 W
TA2911	P.C. type	R <sub>BE</sub> = 100 ohms		0.5A	°C/W	
TA7156	TO-66 equivalent	50 V @	4A	20-120 @	3.5	36 W
TA7137	P.C. type	R <sub>BE</sub> = -500 ohms		0.1A	°C/W	



RCA Electronic Components and Devices

The Most Trusted Name in Electronics

ON READER-SERVICE CARD CIRCLE 60



# Audio (continued)

Cross Index Key	Type No.	Mfr.	Type	h <sub>fe</sub> *h <sub>FE</sub>	MAX. RATINGS						CHARACTERISTICS			Package Outline (TO-)	Remarks
					P <sub>c</sub> (mW)	T <sub>j</sub> (°C)	mW/°C	V <sub>CEO</sub> *V <sub>CBO</sub> (V)	I <sub>c</sub> (mA)	I <sub>co</sub> (μA)	f <sub>αe</sub> *f <sub>T</sub> (MHz)				
A 9	2N1383	TI	npn,ge	20	200	85	3.3	*25	200	14	-	5	TRWS, TR, NA TR TI		
	2N1445	TI	npn,si	*20	800	200	4.57	*120	750	10	-	5			
	2N1564	TI	npn,si	20	600	175	4	60	50	1	-	5			
	2N1572	TI	npn,si	20	600	175	4	80	50	1	-	5			
	2N1672	GI	npn,AJ,ge	*20	120	85	2	*40	-	25	2	5			
A 10	2N2371	NA	npn,A,si	*20	200	200	1.0	15	100	.005	-	5	Low Level, Low Noise, AMP, CT, SPR Low Level, Low Noise, CT, SPR		
	2N2373	NA	npn,A,si	*20	150	200	1	15	100	.005	-	18			
	2N3579	SSD	npn,EP	*20	400	200	2.28	60	30	0.05	80	46			
	2N4292	NA	npn,EP,si	*20	200	150	1.60	*30	-	0.5	*600	-			
	2N4293	NA	npn,EP,si	*20	200	150	1.6	*30	-	0.5	*600	-			
	2N3877	GE	npn,PL,si	*20 min.	200	100	2.67	70	50	0.5	135	98			
	2N3877A	GE	npn,PEP,si	*20 min	200	100	2.67	85	50	0.5	135	98			
A 11	2N530	GI	-	-	100	85	2	*15	-	5	3	5	TI		
	2N2042	MO	npn,AJ,ge	*20-50	200	100	*2.67	105	200	10	-	5			
	2N2042A	MO	npn,AJ,ge	*20-50	200	100	2.67	105	200	10	-	5			
	2N926	NA	npn,A,si	20-55	150	200	.85	40	100	.025	-	18			
	2N339A	TR	npn,PL,si	*20-80	250	175	3	60	150	1	10	11			
	2N340A	TR	npn,PL,si	*20-80	250	175	3	85	150	1	10	11			
	2N341A	TR	npn,PL,si	*20-80	250	175	3	125	150	1	10	11			
A 12	2N3793	NA	npn,DD,EP,si	*20-105	250	150	2.0	*40	500	0.5	*1.0	-	TR GE, TR, NA TR SSD		
	2N118	TI	npn,si	24	150	175	1	*45	25	2	-	-			
	2N333	TI	npn,si	24	150	175	1	*45	25	2	-	5			
	2N1150	TI	npn,si	24	150	175	1	*45	25	2	-	5			
	2N924	NA	npn,A,si	24-60	150	200	.85	25	10	.025	-	18			
	2N330A	RA	npn,si	25	380	160	2.9	30	50	0.1	0.05	5			
	2N563	GI	npn,AJ,ge	25	150	85	2.5	*30	300	5	0.8	-			
A 13	2N564	GI	npn,AJ,ge	25	120	85	2	*30	300	5	0.8	5	SSD, AMP, CT TI, SSD IND, TI TR TR TR CT, SPR STC TRWS		
	2N1589	TI	npn,si	25	125	87.5	2	10	25	1	-	-			
	2N1590	TI	npn,si	25	125	87.5	2	20	25	1	-	-			
	2N1591	TI	npn,si	25	125	87.5	2	40	25	1	-	-			
	2N1623	RA	npn,si	*25	250	160	1.85	20	50	1.0	0.05	5			
	2N2304	RA	npn,PL,si	*25	600	300	3-4	30	250	.010	10	5			
	2N2617	AMP	npn,si	*25	350	150	2	*25	50	.001	3	-			
A 14	2N2831	SY	npn,PE,si	*25	360	175	-	*40	200	.30	250	18	2N531 2N4298 2N658 2N306 2N2860 2N279 2N662 2N727 2N1477 2N1654		
	2N531	GI	-	25-30	100	85	2	*15	-	5.0	3.5	5			
	2N4298	RCA	npn,TDP,si	*25-75	20,000	175	133	350	1000	100	*60	66			
	2N658	TI	npn,AJ,ge	*25-80	250	100	6.66	12	1000	6	-	5			
	2N306	SY	npn,AL,ge	*25-125	180	85	-	*20	-	20	.600	22			
	2N2860	SY	npn,PE,si	*25-125	200	175	-	*30	-	1	*1000	18			
	2N279	AMP	npn,AJ,si	30	125	75	2.5	30	10	110	0.15	1			
A 15	2N650A	MO	npn,AJ,ge	30-70	200	100	2.67	*45	500	10	-	5	TI TI TI TI,IEC NUC,CDC, IEC		
	2N653	MO	npn,AJ,ge	30-70	200	100	2.67	*30	250	15	1	5			
	2N1186	MO	npn,AJ,ge	30-70	200	100	2.67	*60	500	10	-	5			
	2N1191	MO	npn,AJ,ge	30-70	200	100	2.67	*40	200	15	-	5			
	2N2711	GE	npn,PL,si	30-90	200	100	2.67	18	100	.5	-	98			
	2N2713	GE	npn,PEP,si	*30-90	200	100	2.67	18	200	0.5	-	98			
	2N1051	GE	npn,DD,si	30-100	500	150	4	40	100	.1	4	5			
A 16	2N1707	MO	npn,AJ,ge	30-150	200	100	2.66	*30	400	15	†4	5	Full line spread CDC,IEC NA † fab, TI TR, NA		
	2N244	TI	npn,si	32	750	150	6	*60	60	1	-	-			
	2N405	RCA	npn,AJ,ge	35	150	71	-	*20	35	14	0.65	40			
	2N406	RCA	npn,AJ,ge	35	150	71	-	*20	35	14	0.65	1			
	2N780	TI	npn,si	*35	300	175	2	45	50	0.01	-	18			
	2N1010	LAN	npn,AJ,ge	35	20	55	-	*10	2	10	2	1			
	2N2389	TI	npn,si	35	450	200	2.57	*75	500	0.01	-	50			
A 16	2N533	GI	-	35-40	100	85	2.0	*15	-	5	4.5	5	LAN AL LAN AL NUC, † Full line spread, GME, CDC, IEC CT, SPR		
	2N4284	NA	npn,EP,si	*35-150	250	150	2.0	*25	100	0.10	*7.0	-			
	2N4285	NA	npn,EP,si	*35-150	250	150	2.0	*35	100	0.01	*7.0	-			
	2N2926	GE	npn,PL,si	†35-470	200	100	2.67	18	100	0.5	-	98			
	2N937	SSD	AJ	*36	385	160	2.85	30	50	0.1	-	18			









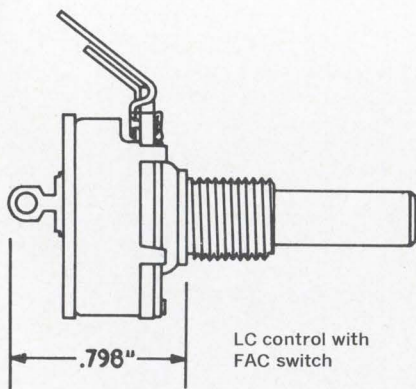
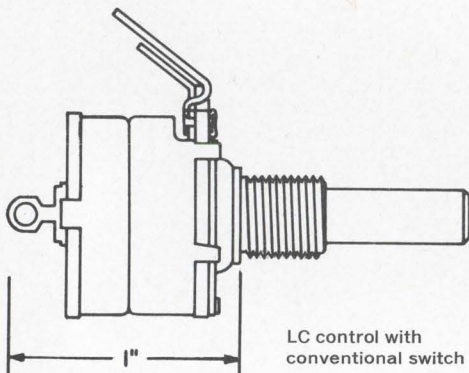


# DESIGNER'S

P. R. MALLORY & CO. INC., INDIANAPOLIS, INDIANA 46206

## New space-saving switch now available on Mallory carbon controls

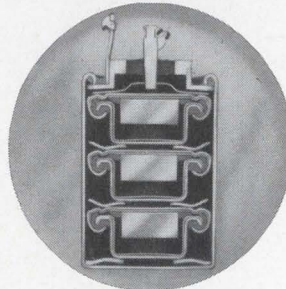
A new kind of rotary switch, with flat configuration, can now be supplied on Mallory carbon controls for applications where back of panel space is limited. From front face of the mounting bushing to tip of the terminals, the total back-of-panel depth of a Mallory LC single control with the new switch measures only 0.798"—compared with 1.00" for the usual single LC control-switch combination.



The new switch is rated 3 amperes at 125 VAC, and is presently available in the SPST design. It has UL approval. Price is slightly lower than that of the standard Mallory "O" ring switch. The FAC switch can be supplied on all standard Mallory LC series controls.

CIRCLE 106 ON READER SERVICE CARD

## Reliability Report on Mallory Wet Slug Tantalum Capacitors



Cutaway view of 3-cell Type XT capacitor  
U.S. Patent 3,275,902

Ever since we started making wet slug tantalum capacitors 17 years ago, we have been accumulating data on their reliability. At latest count, we had over 22 million piece-

hours of testing for this product line on which to base evaluation of reliability.

The incidence of catastrophic failure has been exceptionally low. This quality is an inherent property of the wet slug construction, which provides a self-healing capability.

The data shown on the chart represents a summary of test programs to date on several Mallory wet slug types. We will be glad to supply detailed test records on specific capacitor models. And we welcome your personal inspection of our manufacturing, quality control and life test facilities.

CIRCLE 105 ON READER SERVICE CARD

### SUMMARY OF RELIABILITY DATA MALLORY WET SLUG TANTALUM CAPACITORS

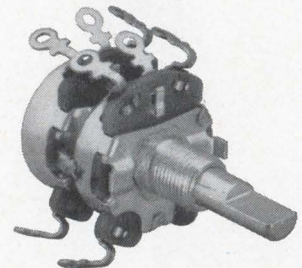
Capacitor Type	Test Conditions Temp.	Volts	Total Unit test hrs.	Failures (catast.)	Failure rate: % per 1000 hrs.*	Mean time between failures: hours*
MTPH	85°C	Rated	6,214,300	1	0.032	3 x 10 <sup>6</sup>
TLS	85°C	Rated	832,750	0	0.11	0.9 x 10 <sup>6</sup>
	125°C	67% Rated	697,650	1	0.29	0.32 x 10 <sup>6</sup>
All XT Series	85°C	Rated	8,291,100	6	0.09	1.1 x 10 <sup>6</sup>
	175°C	67% Rated	7,361,200	7	0.11	0.9 x 10 <sup>6</sup>

\*60% confidence level

## Matched dual controls for stereo systems

For the leading manufacturers of stereo equipment, we have been producing dual volume controls whose resistance tapers are closely matched throughout the audible range of the control. Single-knob control of both stereo channels simultaneously becomes practical, with perfect tracking of both amplifiers without need for adjustment of a clutch coupling the control sections.

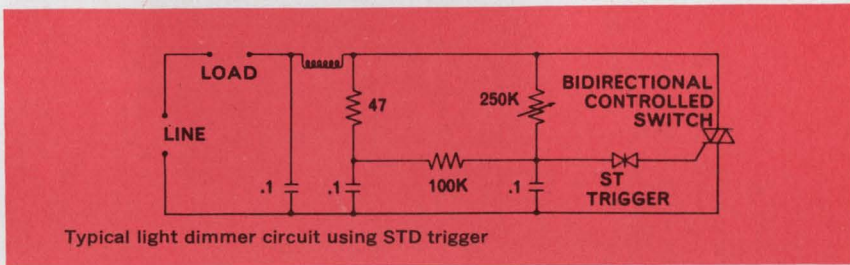
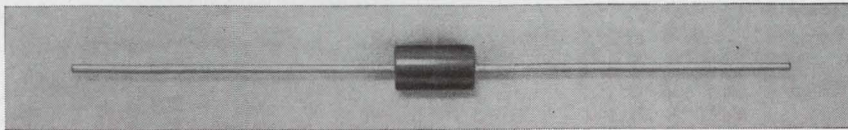
This simplification of stereo adjustment is made possible by the refined production control procedures which



Mallory applies to the manufacture of carbon control elements. We were the first to make dual controls which tracked within 2 db, from 0 to -50 db, and are now producing matched controls in a variety of tapers for audio equipment—including the lower resistance values used in solid-state circuitry.

CIRCLE 107 ON READER SERVICE CARD

## Dual trigger diode generates voltage peaks for SCR circuits



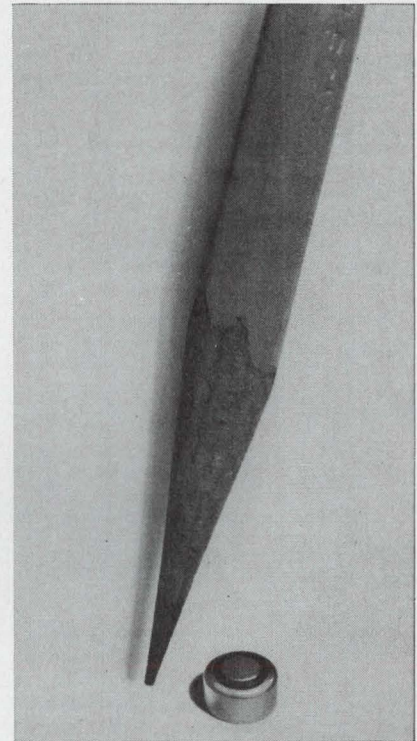
Typical light dimmer circuit using STD trigger

The Mallory STD dual trigger diode is a symmetrical three-layer avalanche diode which has many applications in activating SCR's and bi-switches. It's somewhat like two zener diodes connected back to back. When you apply AC to it, it allows current to pass only during that part of each half cycle when applied voltage exceeds its firing voltage. Thus it produces impulses, whose phase can be readily controlled, to switch the SCR on at different points in the cycle.

The STD has a symmetrical switching mode, as shown by the typical

characteristic curve. At voltages beyond the breakover point, its resistance decreases rapidly; this "snap back" characteristic affords improved stability of control in the SCR circuit.

The STD comes in molded case only .375" long by .200" in diameter. It is rated 1 watt average at 50°C ambient. It can handle 1.0 ampere peaks of 20 microseconds duration on a 0.5% duty cycle. Standard breakover voltage ratings go from 24 to 120 volts, in standard tolerance of ±10%. Symmetry of break-over voltage is within 5%.



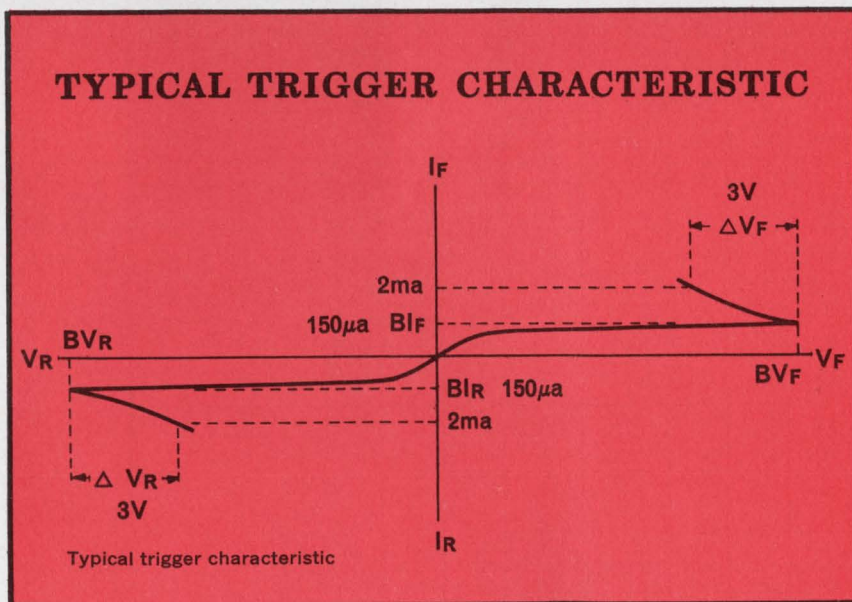
## Miniature cells for Microcircuits

Circuits have shrunk and now so have batteries—but that doesn't mean that efficiency suffers in the least. The new Mallory mercury batteries in sizes to complement integrated circuits retain their extraordinary high energy density. Performance, if anything, is improved.

Miniature Mallory mercury cells are now available to power everything from hearing aids to ordnance devices. Capacities range from 16 MAH to 160 MAH, sizes from 0.225" to 0.450" diameter.

(See Table below.)

	RM-212	RM-312	RM-575	RM-675
CAPACITY MAH	16	36	100	160
RATED DRAIN MA	.75	2	3	5
DIA. (IN.)	.225	.305	.450	.450
HT. (IN.)	.130	.135	.130	.200
WT. (OZ.)	.01	.02	.05	.09



Typical trigger characteristic

CIRCLE 108 ON READER SERVICE CARD

CIRCLE 109 ON READER SERVICE CARD







# 4 NEW MINIATURE HIGH POWER DIODES

Which of these new Unitrode developments is going to help you build a smaller, lighter, more reliable circuit this year?

## RADIATION-RESISTANT HIGH CURRENT RECTIFIERS

 Actual Size

- 2 Amp Continuous Rating
- 25 Amp Surge Rating
- PIV's to 250 Volts

These high current, controlled avalanche diodes are capable of withstanding substantial dosages of various types of radiation with negligible change in specified parameters. They may be operated at their full 2 Amp rating after withstanding a cumulative neutron dose in excess of  $10^{16}$  N.V.T. Both gamma and electron radiation have negligible effect.

CIRCLE 131 ON INQUIRY CARD

## HIGH POWER THYRISTOR DIODES

 Actual Size

- 1.5 Amp Continuous Rating
- Firing Voltages to 300 Volts
- High Surge Ratings

Four-layer diodes have been available for some years, but this is the first miniature high power and high voltage controlled avalanche version to be offered. Firing voltages are available from 40 to 300 volts. Continuous current is 1.5 amp and short duration surges as high as 500 amps can be withstood, with an 8.3 msec surge rating of 15 amps.

CIRCLE 132 ON INQUIRY CARD

## ULTRA-FAST RECOVERY RECTIFIER


 Actual Size

- Typical Recovery under 50 Nanoseconds
- 25 Amp Surge Rating
- PIV's to 250 Volts

These ultra-fast recovery, controlled avalanche rectifiers can operate at frequencies of 100 KC square wave, or 350 KC sine wave. These 2 amp rated devices have typical recovery times of 50 nanoseconds; they can withstand surges up to 25 amps, and have leakages under 1 microamp at 25°C.

CIRCLE 133 ON INQUIRY CARD

## 9 AMP FAST-RECOVERY RECTIFIER (Stud Mount)

 Actual Size

- Controlled Avalanche
- 150 Amp Surge Rating
- 40 KC Square Wave Operation

Recovery times as low as 250 nanoseconds permit full power operation at frequencies as high as 40 KC square wave, or even higher frequencies sine wave. These miniature stud mount rectifiers provide a 9 amp continuous and 150 amp surge rating in a package that, at less than 1.5 grams, is only one-fifth the weight and one-quarter the volume of conventional types.

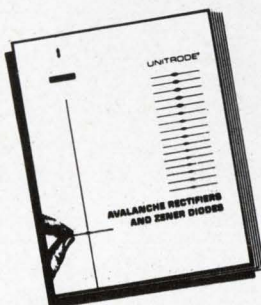
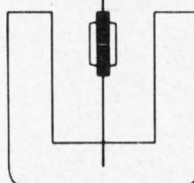
THE SAME PACKAGE IS ALSO AVAILABLE IN REGULAR RECOVERY WITH A 12 AMP RATING

CIRCLE 134 ON INQUIRY CARD

## THE UNIQUE UNITRODE CONSTRUCTION



The silicon wafer is metallurgically bonded between two terminal pins of the same thermal coefficient as the silicon. A sleeve of hard glass is then fused to the pins and all the exposed silicon surface, resulting in a voidless, monolithic, whiskerless structure.



NEW 32 PAGE DIODE CATALOG  
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- Technical Specifications
- Mounting Data
- Applications Information
- Physical Drawings
- Derating Information
- Multiple Surge Ratings

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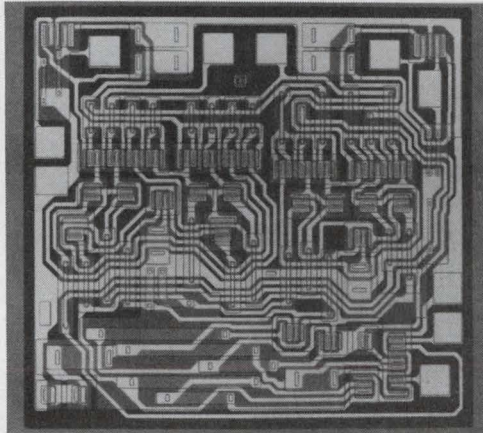
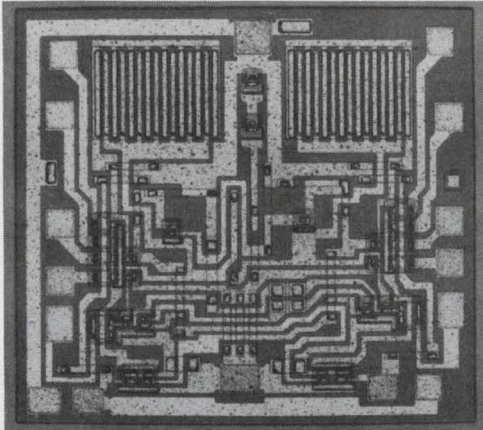








85 MHz J-K FLIP-FLOP



8 ns FULL ADDER

...you're in  
fast company  
with MECL II  
Integrated Circuits!

The impressive speed credentials of Motorola's new MECL II\* integrated circuit logic are well represented by the ultra-fast 85 MHz (typ) J-K Flip-Flop and the complex 12-gate-array Full Adder (and Subtractor, too) with 8 nanosecond typical propagation delay.

These circuits command the attention of any designer who needs *speed* in his design. And, you can count on the entire line of multifunction MECL

II circuits to deliver state-of-the-art performance for fastest overall system operation.

And, if you're already designing with MECL I\* circuits, you'll find these new MECL II types fit right in your present designs — with identical logic levels and power supply requirements. (They are compatible with the 1.0 ns MECL III\* gates we're presently developing, too.)

If your design doesn't require highest speed, ask your Motorola representative about our other digital integrated logic families . . . MTTL\*, MDTL\*, MRTL\*, MVTL\*, MHTL\* (high threshold), mWRTL\*. We make them all.

See your nearest Motorola distributor for evaluation quantities of new MECL II circuits for prototyping. For complete details, write Motorola Semiconductor Products Inc., Box 955, Phoenix, Arizona 85001.

\*Trademark of Motorola, Inc.

	Min.	Max.	Unit
J-K FLIP-FLOP (MC1013P <sup>†</sup> , MC1213F <sup>†</sup> )			
Toggle Frequency (50% duty cycle)	70	—	MHz
AC Fan-out	15	—	—
FULL ADDER (MC1019P, MC1219F)			
FULL SUBTRACTOR (MC1021P, MC1221F)			
Propagation Delay (Carry-in to sum)	—	8	ns
AC Fan-out	15	—	—

<sup>†</sup>"P" suffix for plastic package (0 to +75°C temp. range)

"F" suffix for flat package (-55°C to +125°C temp. range)

— where the priceless ingredient is care!



**MOTOROLA**  
**Semiconductors**

ON READER-SERVICE CARD CIRCLE 62







# Solitron's low cost ISOLTAXIAL<sup>T.M.</sup>

## NPN SILICON TRANSISTORS

PAT. PENDING

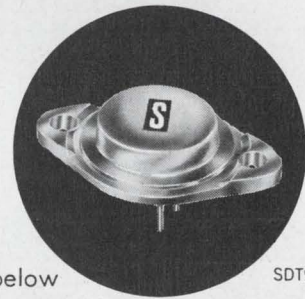
### GUARANTEE RELIABILITY

with...

- All aluminum metalization-die and leads
- Molybdenum pedestal mounting for matching thermal coefficients
- Alloy mounting to eliminate thermal fatigue
- Copper base assembly providing low thermal resistance



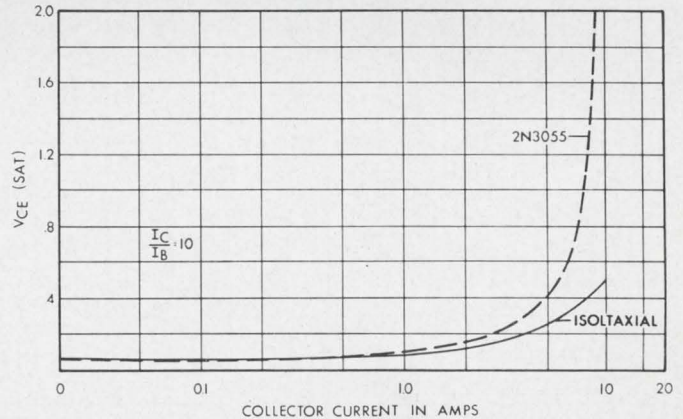
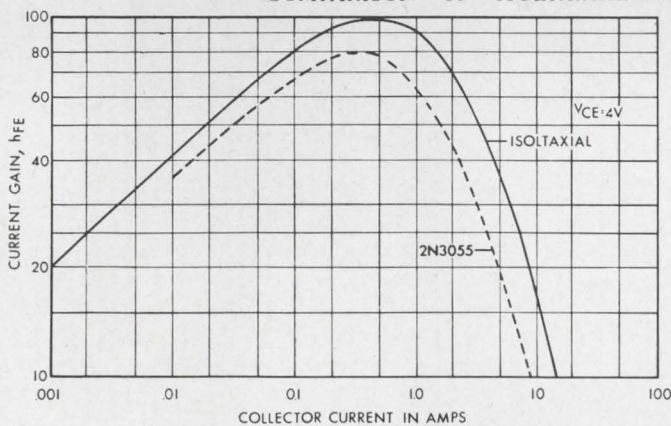
SDT9901-4



SDT9801-4

The gain and  $V_{CE}$  (sat) comparison curves shown below warrant your inspection. They illustrate Solitron's new ISOLTAXIAL NPN Silicon Power Transistors which have characteristics of low-leakage planar units, combined with resistance to secondary breakdown offered by homogeneous devices. Developed with the high reliability standards associated with Solitron, these ISOLTAXIAL devices may be used in power supplies, audio amplifiers, inverters, converters, relay drivers and series regulators. Available in TO-3 and TO-61 cases, the ISOLTAXIAL transistors are priced lower than epitaxial or triple-diffused planar devices.

COMPARISON OF ISOLTAXIAL DEVICE TO COMPETITIVE 2N3055



CONTACT US TODAY FOR COMPLETE INFORMATION

TRANSISTOR DIVISION

# Solitron DEVICES, INC.

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Leader in Germanium and Silicon Power Transistors, Cryogenic Thermometers, High Voltage Rectifiers, Hot Carrier Diodes, Temperature Compensated Zeners, Voltage Variable Capacitors, Random/White Noise Components, Microelectronic Circuits, and Power-Sink Interconnection Systems.

ON READER-SERVICE CARD CIRCLE 63











# Selected devices from the Amperex Total Capability...

## SEMICONDUCTORS

### for RF Applications:

Low Power to 1500 MHz with Low Noise (3db) and Low Intermodulation Distortion:

Use the Amperex 2N5054 and A210 families.

High Gain, Extremely Low Feedback IF Amplifiers for frequencies through 60 MHz:

Use the Amperex A467 and A473 families.

General purpose RF and IF Amplifiers for AM/FM and TV Applications: Use the Amperex A415, A484 and A494 families.

High Power to 36 watts at 175 MHz at 12.0V and 28.0V:

Use the Amperex A202 and 2N3632 families.

To 22 watts at 450 MHz or 8 watts at 1 GHz:

Use the Amperex 1N4885 Varactor family.

### for Drive Applications:

In Video Circuitry:  
Use the Amperex A779 family.

In Indicator and Memory Circuits:  
Use the Amperex A983 SCS family.

In Control Circuitry:  
Use the Amperex A903 SCR family.

In Audio/Power Circuitry:  
Use the Amperex A523 family.

### for Small Signal and Logic Applications:

To amplify low level signals to output levels between 1  $\mu$ A and 500 mA:  
Use the Amperex 2N2484, 2N2222 and 2N2920 families.

Chopping or switching low level signals to output levels of up to 100 mA:  
Use the Amperex 2N2569 and 2N2369 families.

To amplify at impedance levels of 10,000 megohms with low noise and high gain.

Use the Amperex A190 and A192 families of FET's.

### for Diode and Rectifier Applications:

In High Speed Switching:  
Use the Amperex A23 diode.

In Controlled Avalanche (12.5KV) CRT Focus Rectifier Circuits:  
Use the Amperex A74.

In High Voltage Power Supplies up to 800V DC Output.  
Use the Amperex BY127 Rectifier family.

In Bridge Rectifiers up to 400V DC Output:  
Use the Amperex BY123 Bridge Rectifier Assembly.

### for Audio Applications:

Small Signal Silicon:  
Use the Amperex A104 series in TO-18 and the A747 series in the plastic autosert package.

Silicon Power:  
Use the Amperex A515 in high voltage applications and the A522, A523 and A572 for high power.

Complementary Germanium Pairs:  
Use the Amperex 2N4136 pair for 2-watt systems and the 2N4107 or 2N4079 pairs for higher power.

# ...for all your solid state design requirements

## MICROELECTRONICS

### **Linear Monolithic Integrated Circuits for:**

Small Signal Amplifiers up to 600 KHz:

Use the *Amperex TAA103, TAA263, TAA293.*

High Gain Audio Preamplifiers for Playback/Record:

Use the *Amperex TAA310.*

High Input Impedance, High Gain, Preamplifiers:

Use the *Amperex TAA320 BiFET.*

(A bipolar transistor and MOS/FET on a single chip.)

### **Hybrid Integrated Circuits for:**

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TOMORROW'S THINKING IN TODAY'S PRODUCTS

ON READER SERVICE CARD CIRCLE 44





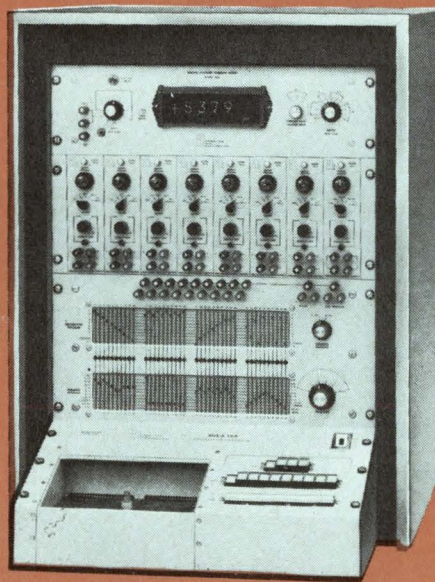




# NEW

## semi-automatic integrated circuit analyzer

# MICA 150



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Now the integrated circuit user can get all the flexibility and performance of an expensive, large scale IC test system in an accurate and reliable DC bench top analyzer.

**The new MICA-150 Modular Integrated Circuit Analyzer tests all IC configurations of up to 40 pins with unique programming, fast pushbutton sequencing and built-in DVM readout.**

**Fast, Versatile Programming** Two independent 10x40 crossbar switches and rapid pushbutton sequencing provide up to 40 tests on a single device without re-programming. For example, it's now quick and easy to check a 10 pin device using four completely different test programs without resetting any switches to advance the test from pin-to-pin or program-to-program. Additional flexibility allows the built-in DVM to measure current on one pin of the device and voltage on another—all pre-programmed.

**Universal Test Adapters** Through use of universal test adapters, the MICA-150 is designed to check ICs according to the number of pins of a particular package, not device or circuit type. Adapters are available for diode, transistor, TO-5, flat-pack, dual in-line and other package configurations, and can also be provided for Kelvin connections.

**Accurate Digital Readout** Specifically designed for the MICA-150 analyzer, the built-in Digital Volt/Ammeter has a conservatively rated readout accuracy of 0.1% with a four digit display. Other features include automatic ranging and polarity selection, self-calibration, automatic voltage or current readout selection. Measures currents as low as 1 nanoamp, voltages to 1 mv.

**Modular Design** Modular construction allows users to select an economical, customized tester without obsolescence problems. Maximum capacity of eight function generators permits later expansion, including modules for AC and pulse testing, without additional modifications.

**Variable Soak Time** Marginal device operation can be easily detected through use of an adjustable test time control which provides a period for thermal stabilization prior to measurement. A continuous position on the control allows parameters to be varied while observing results.

**Precision, Wide Range Power Supplies** Highly precise supplies utilize multi-turn calibrated potentiometer controls with high resolution and repeatability. Constant current supplies are continuously variable from 0-100 ma with voltage compliance adjustable to 100v. Constant voltage supplies are variable from 0-100v with automatic current limiting to 100 ma to provide device protection.

### QUICK ACTION REPLY

Detailed technical literature on the MICA-150 will be mailed immediately upon receipt of this request.

Attn.: A. Norman Into, Marketing Manager  
Computer Test Corporation, Three Computer Drive  
Cherry Hill, N.J. 08034 • Phone: (609) 424-2400

Name \_\_\_\_\_

Company \_\_\_\_\_

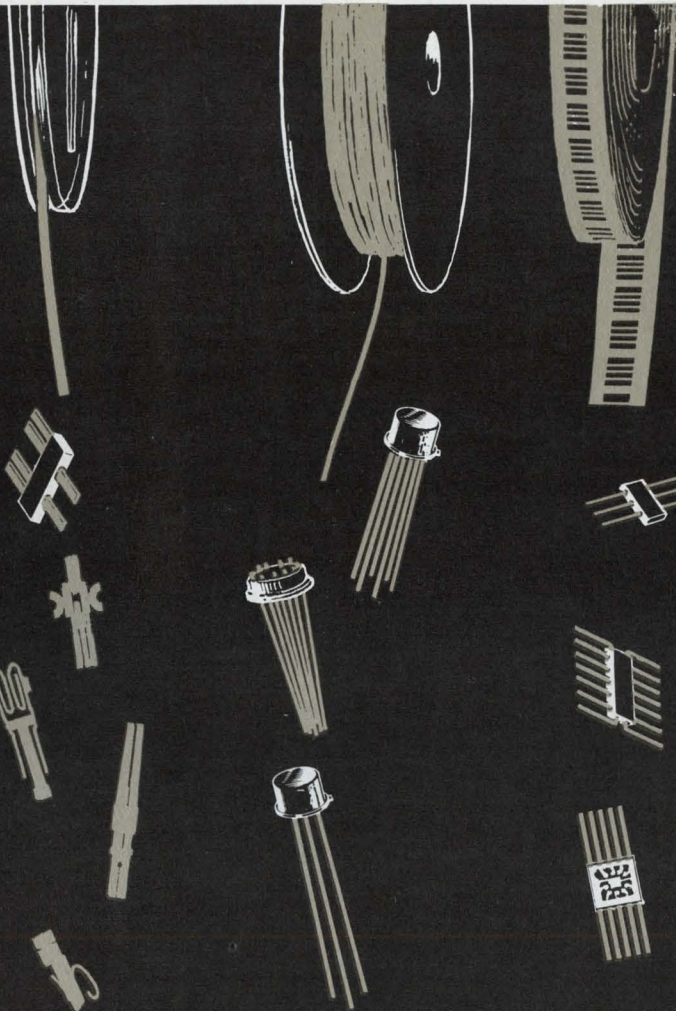
Address \_\_\_\_\_

City \_\_\_\_\_ State \_\_\_\_\_ Zip \_\_\_\_\_







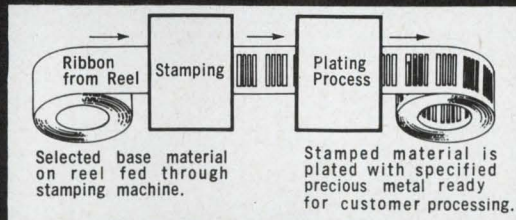


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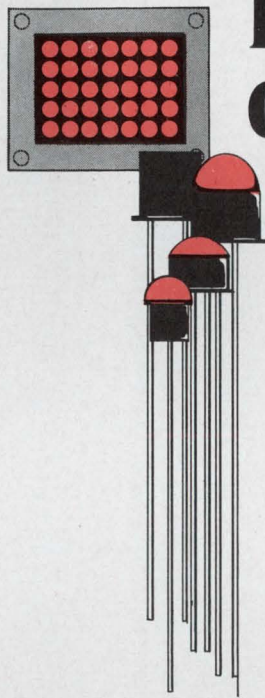








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- Miniature size
- Rugged

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- Low power consumption
- Fast switching (10 nsec)
- Linear output
- Forward bias operation

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**ELECTRONICS**

ON READER-SERVICE CARD CIRCLE 87





# Power (continued)

Cross Index Key	Type No.	Mfr.	Type	MAX. RATINGS					CHARACTERISTICS			Package Outline (TO-)	Remarks
				P <sub>c</sub> (W)	W/°C	T <sub>j</sub> (°C)	V <sub>CEO</sub> *V <sub>CBO</sub> (V)	I <sub>c</sub> (A)	h <sub>FE</sub> *h <sub>FE</sub>	I <sub>CO</sub> *I <sub>CEO</sub> †I <sub>CEX</sub> (mA)	f <sub>αE</sub> *f <sub>T</sub> (kHz)		
P 105	2N1817	WH	npn, AJ, si	250	2.22	175	100	30	*10	15	14.5	†	†MT 14
	2N1818	WH	npn, AJ, si	250	2.22	175	150	30	*10	15	14.5	†	†MT 14
	2N1819	WH	npn, AJ, si	250	2.22	175	200	30	*10	15	14.5	†	†MT 14
	2N1823	WH	npn, AJ, si	250	2.33	175	50	30	*10	15	16	†	†MT 14
	2N1824	WH	npn, AJ, si	250	2.22	175	100	30	*10	15	16	†	†MT 14
P 106	2N1825	WH	npn, AJ, si	250	2.22	175	150	30	*10	15	16	†	†MT 14
	2N1826	WH	npn, AJ, si	250	2.22	175	200	30	*10	15	16	†	†MT 14
	2N1830	WH	npn, AJ, si	250	2.22	175	50	30	*10	15	14	†	†MT 14
	2N1831	WH	npn, AJ, si	250	2.22	175	100	30	*10	15	14	†	†MT 14
	2N1832	WH	npn, AJ, si	250	2.22	175	150	30	*10	15	14	†	†MT 14
	2N1833	WH	npn, AJ, si	250	2.22	175	200	30	*10	15	14	†	†MT 14
	2N2109	WH	npn, AJ, si	250	2.22	175	50	30	*10	15	14	†	†MT 17
	2N2110	WH	npn, AJ, si	250	2.22	175	100	30	*10	15	14	†	†MT 17
	2N2111	WH	npn, AJ, si	250	2.22	175	150	30	*10	15	14	†	†MT 17
	2N2112	WH	npn, AJ, si	250	2.22	175	200	30	*10	15	14	†	†MT 17
P 107	2N2113	WH	npn, AJ, si	250	2.22	175	250	30	*10	15	14	†	†MT 17
	2N2114	WH	npn, AJ, si	250	2.22	175	300	30	*10	15	14	†	†MT 17
	2N2116	WH	npn, AJ, si	250	2.22	175	50	30	*10	15	14.5	†	†MT 17
	2N2117	WH	npn, AJ, si	250	2.22	175	100	30	*10	15	14.5	†	†MT 17
	2N2118	WH	npn, AJ, si	250	2.22	175	150	30	*10	15	14.5	†	†MT 17
	2N2119	WH	npn, AJ, si	250	2.22	175	200	30	*10	15	14.5	†	†MT 17
	2N2123	WH	npn, AJ, si	250	2.22	175	50	30	*10	15	16	†	†MT 17
	2N2124	WH	npn, AJ, si	250	2.22	175	100	30	*10	15	16	†	†MT 17
P 108	2N2125	WH	npn, AJ, si	250	2.22	175	100	30	*10	15	16	†	†MT 17
	2N2126	WH	npn, AJ, si	250	2.22	175	150	30	*10	15	16	†	†MT 17
	2N2130	WH	npn, AJ, si	250	2.22	175	50	30	*10	15	14	†	†MT 17
	2N2131	WH	npn, AJ, si	250	2.22	175	100	30	*10	15	14	†	†MT 17
	2N2132	WH	npn, AJ, si	250	2.22	175	150	30	*10	15	14	†	†MT 17
	2N2133	WH	npn, AJ, si	250	2.22	175	200	30	*10	15	14	†	†MT 17
	2N3149	STC	npn	300	2	200	80	70	*10	-	-	*	*1 1/16" Hex
	2N3150	STC	npn	300	2	200	100	70	*10	-	-	*	*1 1/16" Hex
P 109	2N3151	STC	-	300	2	200	150	70	*10	-	-	*	*1 1/16" Hex
	2N4865	SOL	npn, PL, si	350	0.5	200	80	100	10-40	0.1	20,000	-	-
	2N4866	SOL	npn, PL, si	350	0.5	200	120	100	10-40	0.1	20,000	-	-
	2N4079	AMP	2N4077 & 2N4078 combined to form matched complementary pair										
	2N4107 & 2N4136	AMP	2N4105 & 2N4106 combined to form matched complementary pair										

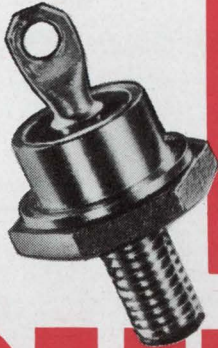
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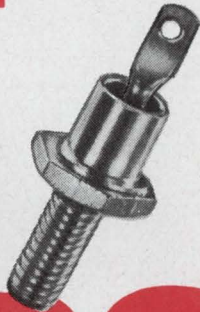
Complete listing of semiconductor manufacturers starts on page 86.

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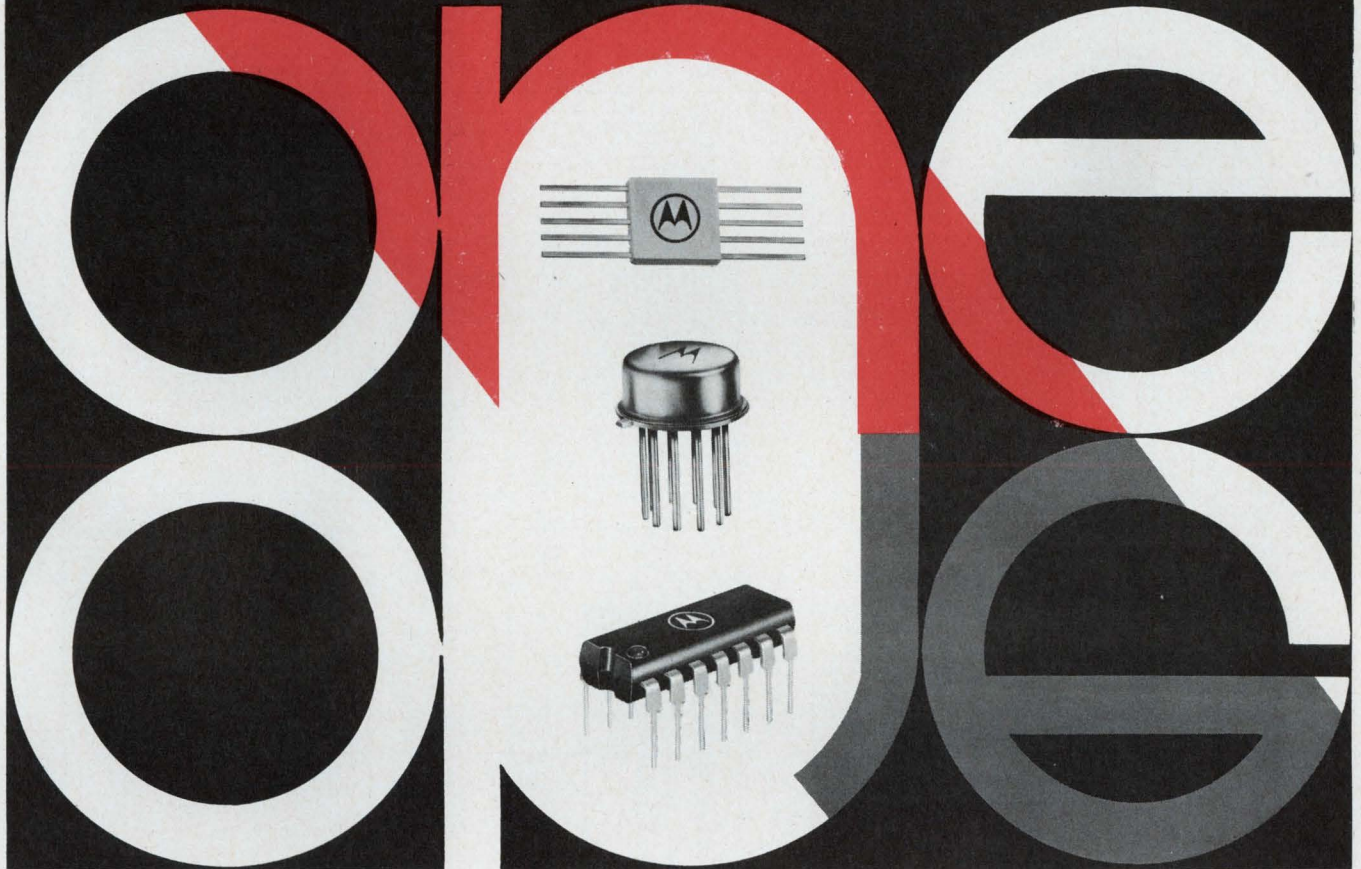








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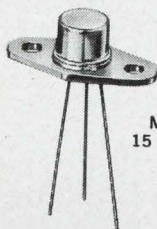
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$H_{FE}$ @ $V_{CE} = 10\text{V}$ $I_C = 20\text{mA}$	30 min	$H_{FE}$ @ $V_{CE} = 4\text{V}$ $I_C = 50\text{mA}$	30 min
GBW @ $V_{CE} = 20\text{V}$ $f = 5\text{MC}; I_C = 10\text{mA}$	6 min	GBW @ $V_{CE} = 10\text{V}$ $f = 20\text{MC}; I_C = 50\text{mA}$	2.5 min

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200-500V

TO-5 and MD-14

**NPN**  
200-700V

PNP	
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$V_{CER}$ @ $I_C = 200\mu\text{A}$	200-500V
$H_{FE}$ @ $V_{CE} = 10\text{V}$ $I_C = .25\text{A}$	25 min
$H_{FE}$ @ $V_{CE} = 10\text{V}$ $I_C = .1\text{A}$	40 min
GBW @ $V_{CE} = 10\text{V}$ $I_C = 50\text{mA}$ $f = 5\text{MC}$	4 min

NPN	
$V_{CEO}$ @ $I_C = 25\text{mA}$	200-500V
$V_{CER}$ @ $I_C = 200\mu\text{A}$	200-700V
$H_{FE}$ @ $V_{CE} = 10\text{V}$ $I_C = 1\text{A}$	10 min
$H_{FE}$ @ $V_{CE} = 10\text{V}$ $I_C = .25\text{A}$	40 min
GBW @ $V_{CE} = 10\text{V}$ $I_C = 50\text{mA}$ $f = 5\text{MC}$	4 min

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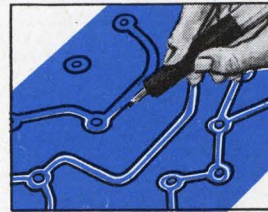
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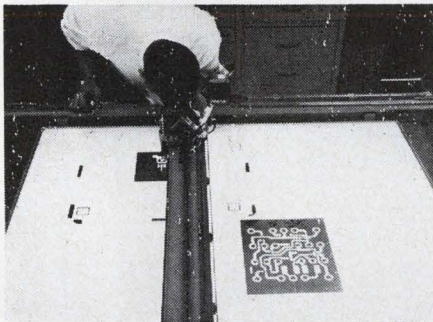


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ON READER-SERVICE CARD CIRCLE 72

# Unijunction

## Type 1. Pulse Generation (e.g., SCR Triggering)

	Type Number	Orig. Reg.	Type	V <sub>OB1</sub> [min] (volts)	I <sub>V</sub> [min] (mA)	V <sub>EB2</sub> [max] (volts)	$\eta$ [min-max]	R <sub>BBO</sub> [min] (k $\Omega$ )	I <sub>P</sub> [max] ( $\mu$ A)	I <sub>EO</sub> [max] ( $\mu$ A)	V <sub>E(SAT)</sub> [max] (volts)	Alternate Sources and Remarks
UJT 1	2N489A	GE	pn,si	3.0	8.0	60	0.51-0.62	4.7	12.0	2.0	4.0	TI, TO-5
	2N490A	GE	pn,si	3.0	8.0	60	0.51-0.62	6.2	12.0	2.0	4.0	TI, TO-5
	2N491A	GE	pn,si	3.0	8.0	60	0.56-0.68	4.7	12.0	2.0	4.3	TI, TO-5
	2N492A	GE	pn,si	3.0	8.0	60	0.56-0.68	6.2	12.0	2.0	4.3	TI, TO-5
	2N493A	GE	pn,si	3.0	8.0	60	0.62-0.75	4.7	12.0	2.0	4.6	TI, TO-5
	2N494A	GE	pn,si	3.0	8.0	60	0.62-0.75	6.2	12.0	2.0	4.6	TI, TO-5
	2N1671A	GE	pn,si	3.0	8.0	30	0.47-0.62	4.7	25.0	2.0	5.0	TI
	2N1671B	GE	n,si	3.0	8.0	30	0.47-0.62	4.7	6.0	0.2	5.0	TI
	2N2160	GE	pn,si	3.0	8.0	30	0.47-0.80	4.0	25.0	2.0	-	TI, TO-5
	2N2646	GE	pn,AE,si	3.0	4.0	30	0.56-0.75	4.7	5.0	12.0	2.0(typ)	MO, TI
	2N4893	TI	pn,si	3.0	2.0	30	0.55-0.82	4.0	5.0	1.0	4.0	Plastic(218) TO-92
	SJ1034	TI	pn,si	3.0	-	30	0.50-0.80	4.0	-	15.0	-	TO-5
	SJ5898	TI	pn,si	3.0	2.0	30	0.55-0.80	4.0	5.0	0.01	4.0	T-69 (Plastic Planar)
	2N2647	GE	pn,si	6.0	8.0	30	0.68-0.82	4.7	2.0	0.20	2.0(typ)	TI, TO-5
	SJ1158	TI	pn,si	6.0	3.0	30	0.56-0.85	4.0	5.0	0.01	4.0	TO-18 (Planar)
	SJ1159	TI	pn,si	6.0	4.0	30	0.65-0.85	4.7	2.0	0.01	4.0	TO-18 (Planar)

## Type 2. High-Frequency Control, Voltage-Sensing, Frequency Dividing and Short Timing Periods

	Type Number	Orig. Reg.	Type	I <sub>V</sub> [min] (mA)	$\eta$ [min-max]	R <sub>BBO</sub> [min] (k $\Omega$ )	I <sub>EO</sub> [max] ( $\mu$ A)	I <sub>P</sub> [max] ( $\mu$ A)	V <sub>E(SAT)</sub> [max] (volts)	V <sub>EB2</sub> [max] (volts)	V <sub>OB1</sub> [min] (volts)	Alternate Sources and Remarks
UJT 2	2N3980	TI	pn,AE,si	1.0	0.68-0.82	4.0	0.01	2.0	3.0	30	6.0	MO
	2N4891	TI	pn,si	2.0	0.55-0.82	4.0	1.0	5.0	4.0	30	3.0	TO-92
	2N4892	TI	pn,si	2.0	0.55-0.82	4.0	1.0	5.0	4.0	30	3.0	TO-92
	SJ993	TI	pn,si	4.0	0.56-0.75	4.7	0.01	5.0	4.0	30	3.0	TO-18 (Planar)
	2N4947	TI	pn,si	4.0	0.51-0.069	4.0	2.0	2.0	3.0	30	3.0	TO-18
	SJ1127	TI	pn,si	8.0	0.68-0.82	4.7	0.01	2.0	4.0	60	6.0	TO-18 (Planar)
	2N489	GE	pn,si	8.0	0.51-0.62	4.7	2.0	12.0	5.0	60	-	TI, TO-5
	2N490	GE	pn,si	8.0	0.51-0.62	6.2	2.0	12.0	5.0	60	-	TI, TO-5
	2N491	GE	pn,si	8.0	0.56-0.68	4.7	2.0	12.0	5.0	60	-	TI, TO-5
	2N492	GE	pn,si	8.0	0.56-0.68	6.2	2.0	12.0	5.0	60	-	TI, TO-5
	2N493	GE	pn,si	8.0	0.62-0.75	4.7	2.0	12.0	5.0	60	-	TI, TO-5
	2N494	GE	pn,si	8.0	0.62-0.75	6.2	2.0	12.0	5.0	60	-	TI, TO-5
	2N1671	TI	pn,si	8.0	0.47-0.62	4.7	12.0	25.0	5.0	30	-	GE, TO-5

## Type 3. Low-Frequency Control, Long Timing-Periods and Current-Sensing

	Type Number	Orig. Reg.	Type	I <sub>P</sub> [max] ( $\mu$ A)	I <sub>EO</sub> [max] ( $\mu$ A)	$\eta$ [min-max]	V <sub>OB1</sub> [min] (volts)	R <sub>BBO</sub> [min] (k $\Omega$ )	I <sub>V</sub> [min] (mA)	V <sub>E(SAT)</sub> [max] (volts)	V <sub>EB2</sub> [max] (volts)	Alternate Sources and Remarks
UJT 3	2N489B	GE	pn,si	6.0	2.0	0.51-0.62	3.0	4.7	8.0	4.0	60	TI, TO-5
	2N490B	GE	pn,si	6.0	2.0	0.51-0.62	3.0	6.2	8.0	4.0	60	TI, TO-5
	2N491B	GE	pn,si	6.0	2.0	0.56-0.68	3.0	4.7	8.0	4.3	60	TI, TO-5
	2N492B	GE	pn,si	6.0	2.0	0.56-0.68	6.2	6.2	8.0	4.3	60	TI, TO-5
	2N494B	GE	pn,si	6.0	2.0	0.62-0.75	3.0	6.2	8.0	4.6	60	TI, TO-5
	2N495B	GE	pn,si	6.0	2.0	0.62-0.75	3.0	4.7	8.0	4.6	60	TI, TO-5
	2N1671B	TI	pn,si	6.0	0.20	0.47-0.62	3.0	4.7	8.0	5.0	30	GE, TO-5
	2N4894	TI	pn,si	5.0	1.0	0.55-0.82	3.0	4.0	2.0	4.0	30	TO-92
	2N490C	GE	n,si	2.0	0.02	0.62-0.91	3.0	6.2	8.0	4.0	60	TI, TO-5
	2N492C	GE	n,si	2.0	0.02	0.62-0.91	3.0	6.2	8.0	4.3	60	TI, TO-5
	2N494C	GE	pn,si	2.0	0.02	0.62-0.75	3.0	6.2	8.0	4.6	60	TI, TO-5
	2N1671C	GE	pn,si	2.0	0.02	0.47-0.62	3.0	4.7	8.0	5.0	60	MO, TO-18 (Planar)
	2N2647	GE	pn,si	2.0	0.20	0.68-0.82	6.0	4.7	8.0	2.0(typ)	30	TO-18 (Planar)
	2N3980	TI	pn,si	2.0	0.01	0.68-0.82	6.0	4.0	1.0	3.0	30	TO-18 (Planar)
	2N4948	TI	pn,si	2.0	2.0	0.55-0.82	6.0	4.0	2.0	3.0	30	TO-18
	2N4949	TI	pn,si	1.0	2.0	0.74-0.86	3.0	4.0	2.0	3.0	30	TO-18



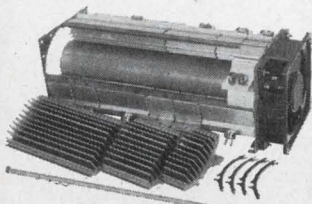
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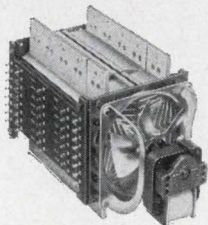
Confined Airflow Packages  
are custom engineered with  
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sections combined in a  
variety of ways for the  
desired cooling system.

4 Confined Airflow Series:  
FCA-700, 800, 820 and 900.



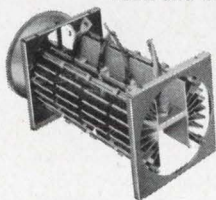
Modular assembly of an FCA-800.

Terminal board assemblies

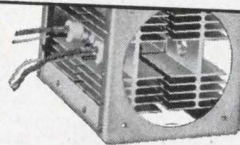


on a standard FCA-820 Package.

4 Open Airflow Series:  
FCA-1000, 1100,  
1122 and 1200.

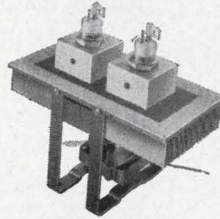


FCA-1000 for high power devices.



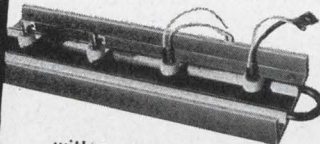
FCA-1122 utilizes 2 heat sinks.

Mounting blocks bonded on an  
FCA-1200



with thermally  
conductive adhesive.

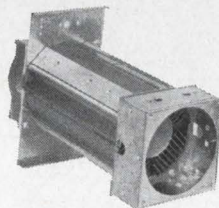
3 LIQUID COOLED PLATES:  
LCP-10, 11 (below) and 20



with custom mounting  
accommodations.

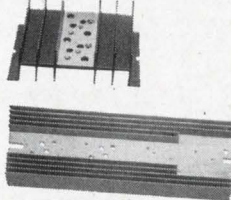
## Wakefield Special Coolers or Assemblies

Engineered Cooling Package . . .



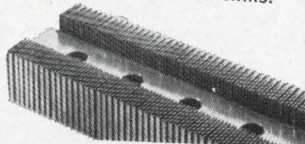
even outlet air cools  
semiconductors.

Unique hole and fin patterns on

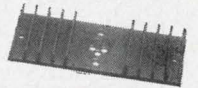


standard Series FSE Extrusions.

Special copper heat sinks.

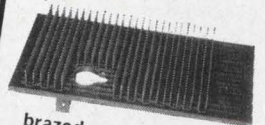


Extrusions  
designed for



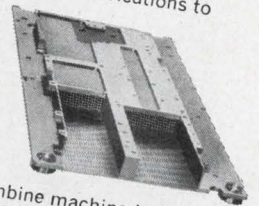
specific requirements.

Fins bonded, soldered,



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Special fabrications to



combine machined parts with  
the heat sink extrusion.

CATALOG  
No. 17

24 pages  
of complete  
technical  
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# Field-Effect (continued)

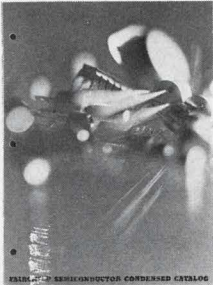
Cross Index Key	Type No.	Mfr.	Channel, Construction, Class And No. of Elements	$r_{ds(on)}$ [Max.] (ohms)	$I_D(off)$ [Max.] ( $\mu A$ )	$C_{dgs}$ or $C_{sgs}$ or $C_{iss}$ [Max.] (pF)	$BV_{GSS}$ or $*BV_{DSS}$ [Min.] (volts)	$V_{GS}$ (off) or $*V_{GS}(TH)$ [Max.] (volts)	$g_{fs}$ [Min.-Max.] ( $\mu mhos$ )	$I_{GSS}$ or $*I_{DGO}$ [max.] (nA)	$I_{DSS}$ [Min.-Max.] (mA)	TO-	Alternate Sources and Remarks
FET 9	CM601	CT	n,EP,F,3	50	0.003	15	15	10	10-30000	3	-	18	
	CM602	CT	n,EP,F,3	50	0.003	15	30	10	10-30000	10	-	18	
	CM642	CT	n,EP,F,3	50	0.001	5	20	3.0	-	0.4	10 (min)	18	
FET 10	TIXS36	TI	n,EP,F,4	50	-	-	30	10	10,000-20,000	10	10,000	18	
	2N4857	TI	n,EP,F,3	40	0.00025	$\dagger 18$	40	6	-	0.25	20-100	18	
	2N4860	TI	n,EP,F,3	40	0.00025	$\dagger 18$	30	6	-	0.25	20-100	18	
	U182	SI	n,DPE,F,3	40	.00025	$\dagger 25$ (Ciss)	40	-10	-	*0.25	50-150	18	
	CM603	CT	n,EP,F,3	35	0.003	15	15	10	20-60000	3	-	18	
	CM643	CT	n,EP,F,3	35	0.001	5	20	5.0	-	0.4	50 (min)	18	
	2N4091	AL	n,DP,F,3	30	.00002	5.0	40	10	-	0.2	30 (min)	18	
	2N4391	UC	n,EP,F,3	30	0.0001	14	-40	-10	-	-0.1	50-150	18	
	CM646	CT	n,EP,F,3	30	0.001	5	25	7.0	-	0.4	30 (min)	18	
UC250	UC	n,F,3	30	.001	6	30	10	-	0.1	50-150	18		
FET 11	TIXS41	TI	n,EP,F,3	25	0.5	-	30	10	-	0.2	50 (min)	18	
	2N4856	TI	n,EP,F,3	25	0.00025	$\dagger 18$	40	10	-	0.25	50 (min)	18	
	2N4859	TI	n,EP,F,3	25	0.00025	$\dagger 18$	30	10	-	0.25	50 (min)	18	
	CM647	CT	n,EP,F,3	25	0.001	5	25	10	-	0.4	50 (min)	18	
	TIS41	TI	n,EP,F,3	25	0.0005	$\dagger 18$	30	10	-	0.2	50 (min)	18	
	2N4448	CT	n,ED,F,3	12	0.003	20	20	10	100,000	3.0	100 (min)	46	
	2N4446	CT	n,EP,F,3	10	0.003	20	25	10	100,000	3.0	100 (min)	46	
	2N4447	CT	n,EP,F,3	6	3.0	20	20	10	150,000	3.0	150 (min)	46	
2N4445	CT	n,EP,F,3	5	0.003	20	25	10	150,000	3.0	150 (min)	46		
2N2386	TI	p,DP,F,3	-	0.01	-	-	8	1000 (min)	10	-	5	DIC, SI	
FET 12	2N2500	TI	p,DP,F,3	-	-	-	25	15	1000-2200	10	1-6	5	
	2N3277	FA	p,DP,F,3	-	1	4.5	25	5	100	0.4	0.15-0.50	33	
	2N3278	FA	p,DP,F,3	-	1	4.5	25	8	200	0.4	0.40-0.90	33	
	2N3332	TI	p,DP,F,3	-	-	-	-	6	1000-2200	10	1-6	72	
	2N3796	MO	n,DP,M,3	-	-	0.8	*25	-4	900-1800	-0.001	0.5-3	18	
	2N3797	MO	n,DP,M,3	-	-	0.8	*25	-4	1500-3000	-0.001	4-6	18	
	2N3819	TI	n,EP,F,3	-	-	-	25	8	2000-6500	2	2-20	92	
	2N3820	TI	p,PL,F,3	-	-	-	20	8	800-5000	20	0.3-1.5	92	
	2N3821	TI	n,EP,F,3	-	-	-	50	4	1500-4500	0.1	0.5-2.5	72	MO, SI
2N3822	TI	n,EP,F,3	-	-	-	50	6	3000-6500	0.1	2-10	72	MO, SI	
FET 13	2N3823	TI	n,EP,F,3	-	-	-	30	8	3500-6500	0.5	1-7.5	72	SI
	2N3909	TI	p,PL,F,3	-	-	-	20	0.3-7.9	1000-5000	10	0.3-1.5	72	SI
	2N4220	SI	n,DP,F,3	-	-	2	-30	-4	1000-4000	-0.1	0.5-3	72	
	2N4221	SI	n,DP,F,3	-	-	2	-30	-6	2000-5000	-0.1	2-6	72	
	2N4222	SI	n,DP,F,3	-	-	2	-30	-8	2500-6000	-0.1	5-15	72	
	3N124	MO	n,DP,F,3	-	-	2	-50	-2.5	500-2000	-0.25	0.2-2	72	
	3N125	MO	n,DP,F,4	-	-	2	-50	-4.0	800-2400	-0.25	1.5-4.5	72	
	3N126	MO	n,DP,F,4	-	-	2	-50	-6.5	1200-3600	-0.25	3.0-9.0	72	
	MFE2093	MO	n,DP,F,3	-	-	2	-50	-2.5	250-500	-0.1	0.1-0.7	72	
MFE2094	MO	n,DP,F,3	-	-	2	-50	-4.5	350-700	-0.1	0.4-1.4	72		
FET 14	MFE2095	MO	n,DP,F,3	-	-	2	-50	-5.5	400-800	-0.1	1-3	72	
	TIS14	TI	n,EP,F,3	-	-	-	30	6.5	1000-7500	1	0.5-1.5	72	
	TIS34	TI	n,EP,F,3	-	-	-	30	1-8	3500-6500	5	4-20	92	
	TIXS35	TI	n,EP,F,4	-	-	-	30	1-5	10,000-20,000	10	10-50	72	

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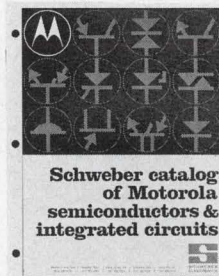


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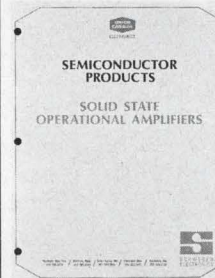


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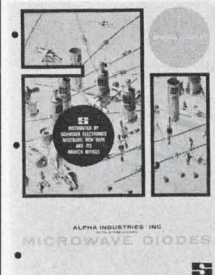


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Type 2(a). Low-drift, single-ended dc amplifiers

Table with columns: Cross Index Key, Type No., Mfr., Channel, Construction, Class And No. of Elements, IDX, gfsx, IGX or IGSS, BVGSS or BVDS, VGSX or VP, gossx, Ciss, NF, TO, Alternate Sources and Remarks.

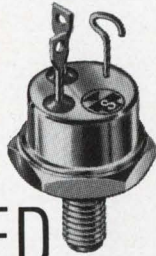
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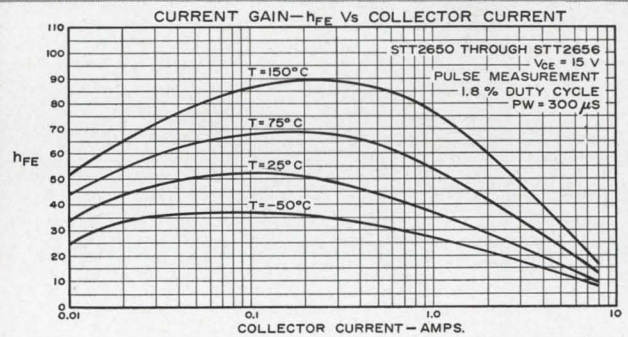
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# POWER

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	$V_{CE0}$	$V_{CBO}$	$V_{EBO}$	$I_{Cmax}$	$P_{max}$ (100°C)	$V_{BE(sat)}$	$V_{CE(sat)}$	$h_{FE}$	$f_t$ (typ)	$I_{CES}$
	Volts	Volts	Volts	Amps	Watts	Volts	Volts	—	MHz	Volts $\mu$ A
STT 2650	150	150	12	7.5	75	1.3	0.6	30-90	25	60 1
STT 2651	120	140	12	7.5	75	1.3	0.6	30-90	25	60 1
STT 2652	120	140	12	7.5	75	1.3	0.6	50-150	25	60 1
STT 2653	100	120	12	7.5	75	1.3	0.6	30-90	25	60 1
STT 2654	80	100	12	7.5	75	1.3	0.6	30-90	25	60 1
STT 2655	60	75	10	7.5	75	1.3	0.6	30-90	25	40 1
STT 2656	30	40	10	7.5	75	2.0	1.0	25	25	20 500

CONDI- TIONS	$I_C$	200mA	5mA	10mA		2A	2A	2A	0.15A	
	$I_B$					0.2A	0.2A			
	$V_{CE}$							15V	15V	

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ON READER-SERVICE CARD CIRCLE 75



# Field-Effect (continued)

## Type 2(b). Differential dc amplifiers

Cross Index Key	Type No.	Mfr.	Channel, Construction, Class And No. of Elements	$\frac{\Delta V_{GS}}{\Delta T}$ [Max.] ( $\mu$ volts/ $^{\circ}$ C)	$V_{GS1}-V_{GS2}$ [Max.] (volts)	$BV_{gss}$ or $*BV_{DSS}$ [Min.] (volts)	$V_p$ or $*V_{GS}$ (dff) [Min. - Max.] (volts)	$I_{GSS}$ or $*I_{GX}$ [Max.] (nA)	$I_{DSS}$ [Min. - Max.] (mA)	$I_{G1} - I_{G2}$ [Max.] (nA)	$g_{fsx}$ [Min. - Max.] ( $\mu$ mhos)	TO-	Alternate Sources and Remarks
FET 29	2N3336	TI	p,DP,F,6	520	0.050	20	0.3-1.6	10	0.3-1	200	600-1800	89	UC
	2N3335	TI	p,DP,F,6	280	0.040	20	0.3-1.6	10	0.3-1	100	600-1800	89	UC
	TIS27	TI	n,EP,F,6	210	0.015	50	6 (max)	0.25	0.5-8	10	1500-6000	5	
	2N3334	TI	p,DP,F,6	200	0.020	20	0.3-1.6	10	0.3-1	50	600-1800	89	UC
	TIS26	TI	n,EP,F,6	140	0.010	50	6 (max)	0.25	0.5-8	10	1500-6000	5	
FET 30	3N97	SI	p,DP,F,6	106	0.2	30	3.3	5	-0.5-2.5	3	250-500	5	
	2N3958	UC	n,PL,F,6	100	0.025	50	1.0-4.5	0.0001	0.5-5.0	10	1000-3000	71	
	MEM551	GI	p,MOS,C,7	100	0.200	*30	3-6	0.004	10nA	-	500 (min)	77	
	2N3333	TI	p,DP,F,6	80	0.015	20	0.3-1.6	10	0.3-1	50	600-1800	89	
	2N3957	UC	n,PL,F,6	75	0.020	50	1.0-4.5	0.1	0.5-5.0	10	1000-3000	71	
	TIS25	TI	n,EP,F,6	70	0.005	50	6 (max)	0.25	0.5-8	10	1500-6000	5	
	SU2079	AL	n,F,6	60	0.015	50	4 (max)	0.25	0.25-2	-	300 (min)	18	
	SU2081	AL	n,DP,F,6	60	0.015	50	4 (typ)	0.5	1.0-10	-	1500 (min)	18	
	2N3935	AL	n,DP,F,6	50	0.005	50	3 (typ)	0.1	0.25-1.3	-	300 (min)	18	UC
	2N3956	UC	n,PL,F,6	50	0.015	50	1.0-4.5	0.1	0.5-5.0	10	1000-3000	71	
FET 31	SU2078	AL	n,F,6	35	0.015	50	4 (max)	0.25	0.25-2	-	300 (min)	18	
	SU2080	AL	n,DP,F,6	35	0.015	50	4 (typ)	0.5	1.0-10	-	1500 (min)	18	
	2N3922	AL	n,DP,F,6	25	0.005	50	3 (typ)	0.25	1.0-10	-	1500 (min)	18	
	2N3955	UC	n,PL,F,6	25	0.010	50	1.0-4.5	0.0001	0.5-5.0	10	1000-3000	71	
	2N4083	AL	n,DP,F,6	25	0.015	50	3 (typ)	0.1	0.25-1.3	-	300 (min)	18	
	2N4085	AL	n,DP,F,6	25	0.015	50	3 (typ)	0.25	1.0-10	-	1500 (min)	18	
	3N96	SI	p,DP,F,6	13	0.1	30	3.3 (typ)	5	-0.5-2.5	1.0	250-500	5	
	2N3921	AL	n,DP,F,6	10	0.005	50	3 (typ)	0.25	1.0-10	-	1500 (min)	18	UC
	2N3934	AL	n,DP,F,6	10	0.005	50	3 (typ)	0.1	0.25-1.3	-	300 (min)	18	UC
	2N3954	UC	n,PL,F,6	10	0.005	50	1.0-4.5	0.0001	0.5-5.0	10	1000-3000	71	
FET 32	2N4082	AL	n,DP,F,6	10	0.015	50	3 (typ)	0.1	0.25-1.3	-	300 (min)	18	
	2N4084	AL	n,DP,F,6	10	0.015	50	3 (typ)	0.25	1.0-10	-	1500 (min)	18	

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Complete listing of semiconductor manufacturers starts on page 86.

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## Type 3(a). General-purpose ac amplifiers

Cross Index Key	Type No.	Mfr.	Channel, Construction, Class And No. of Elements	$I_{DSS}$ [Min. - Max.] (mA)	$g_{fs}$ [Min. - Max.] ( $\mu$ mhos)	$V_p$ or $*V_{GS}$ (dff) [Min. - Max.] (volts)	$I_{GSS}$ [Max.] (nA)	$BV_{GSS}$ or $*BV_{DSS}$ or $*BV_{DGO}$ [Min.] (volts)	$C_{iss}$ [Max.] (pF)	$C_{rss}$ [Max.] (pF)	$g_{oss}$ [Max.] ( $\mu$ mhos)	TO-	Alternate Sources and Remarks
FET 33	2N4353	GI	p,MOS,C,4	5nA	1000-4000	3-5	1.0	*30	12	4	350	72	
	MEM511	GI	p,MOS,C,4	10nA	1000 (min)	3-6	1.0	*30	8	3	350	72	
	MEM520	GI	p,MOS,C,4	10nA	1000 (min)	3-6	0.003	*30	8	3	350	72	
	517	GI	p,MOS,C,4	50nA	10,000 (min)	2.5-5.0	1.0	*30	25	10	-	33	
	UC852	UC	p,F,3	0.025 (min)	60	6 (max)	2	25	25	-	-	18	
FET 34	2N2841	SI	p,DP,F,3	-(.025-.12)	60 (min)	1.7 (max)	1	-	6	-	-	18	UC
	DNX3	DIC	n,DPE,F,3	0.025-0.25	200-700	-2 (max)	-1.0	50	-	-	-	18	
	2N4117	SI	p,DPE,F,3	0.03-0.09	70-210	-0.6-1.8	-0.01	40	3	1.5	3	72	
	2N4117A	SI	n,DPE,F,3	0.03-0.09	70-210	-(0.6-1.8)	-0.001	-40	3	1.5	3	72	
	2N3112	SI	p,DP,F,3	-(.035-.175)	50-115	1-4	0.05	20	3.5	-	-	72	
	2N3113	SI	p,DP,F,3	-(.035-.175)	50-115	1-4	0.05	-	2.0	-	-	-	Flatpack
	UC750	UC	n,F,3	0.05 (min)	120	6 (max)	2	30	-	-	-	18	
	2N3068	AL	n,DP,F,3	0.05-0.25	200-1000	2.5 (max)	1.0	±50	10	-	-	18	DIC,UC,SI
	2N3367	AL	n,DP,F,3	0.05-0.25	100-1000	2.5 (max)	5	-	-	-	-	18	DIC, UC, SI
	2N3454	AL	n,DP,F,3	0.05-0.25	100-600	2.5	0.1	±50	6	-	-	18	UC, SI

Reader-Service cards are good all year.

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# Field-Effect *(continued)*

## Type 3(c). High-frequency ( $f \geq 1\text{MHz}$ ) ac amplifiers

Cross Index Key	Type No.	Mfr.	Channel, Construction, Class And No. of Elements	$g_{fs}$ [Min.-Max.] ( $\mu\text{hos}$ )	$C_{rss}$ [Max.] (pF)	$C_{iss}$ [Max.] (pF)	$g_{fss}$ [Max.] ( $\mu\text{hos}$ )	$V_{GSS}$ or $*V_{DSS}$ [Min.] (volts)	$I_{DSS}$ [Min.-Max.] (mA)	$V_p$ or $*V_{GS}$ (off) [Min.-Max.] (volts)	NF [Max.] dB at (f in KHz / Rgen in K $\Omega$ )	TO-	Alternate Sources and Remarks
FET 67	3N89	SI	p,DP,F,4	450-1300	-	3	-	30	-(0.5-2.5)	3.3 (typ)	-	72	
	U89	SI	p,DP,F,4	450-1800	-	3	-	30	-(0.5-5.0)	3.3 (typ)	-	72	
	DE1004	PH	p,M,4	600 (min)	3	10	-	*-20	0.0001	-	-	18	
	2N3608	PH	p,M,4	800 (min)	2.5	8	-	*-30	0.00003	-	-	5	
	TIXS11	TI	p,PL,M,3	800 (min)	3	8	-	30	-	3-6	-	72	
FET 68	2N3376	SI	p,DP,F,3	800-2300	3	5	-	30	0.6-6	1-5	-	72	
	2N3377	SI	p,DP,F,3	800-2300	2	4	-	30	0.6-6	1-5	-	72	
	2N3820	TI	p,PL,F,3	800-5000	16	32	-	20	0.3-15	*8 (max)	-	72	
	K1001	KMC	n,M,4	1000 (min)	0.7	4.5	800	15	5-12	6 (max)	4.5 (200 MHz)	18	
	K1201	KMC	n,M,4	1000 (min)	0.3	3.0	800	15	1-5	5 (max)	4.5 (450 MHz)	18	
	K1202	KMC	n,M,4	1000 (min)	0.3	3.0	800	15	1-10	5 (max)	-	72	
	K1501	KMC	p,M,4	1000 (min)	0.6	2.0	800	50	-	3-7	-	72	
	K1502	KMC	p,M,4	1000 (min)	0.6	2.0	800	50	-	3-7	-	72	
	TIS14	TI	n,EP,F,3	1000-7500	4	8	-	30	0.5-15	*6.5 (max)	-	72	
TIS58	TI	n,EP,F,3	1300-4000	3	6	-	25	2.5-8	*0.5-5	-	92		
FET 69	2N3378	SI	p,DP,F,3	1500-2300	3	5	-	30	3-6	4-5	-	72	
	2N3379	SI	p,DP,F,3	1500-2300	2	4	-	30	3-6	4-5	-	FP	
	2N3380	SI	p,DP,F,3	1500-3000	3	5	-	30	3-20	5-9.5	-	72	
	2N3381	SI	p,DP,F,3	1500-3000	2	4	-	30	3-20	5-9.5	-	FP	
	2N4038	TRWS	n,DP,M,3	1500-3000	0.2	2.5	-	*20	0-0.1	0-2	3(100 MHz/1 M $\Omega$ )	72	
	2N4039	TRWS	n,DP,M,3	1500-3000	0.2	2.5	-	*20	0-0.1	-(2-6)	3(100 MHz/1 M $\Omega$ )	72	SI
	2N3821	TI	n,EP,F,3	1500-4500	3	6	-	50	0.5-2.5	*4 (max)	5(0.01 kHz/1 M $\Omega$ )	72	
	2N3819	TI	n,EP,F,3	2000-6500	4	8	-	25	2-20	*8 (max)	-	72	
	2N4224	MO	n,DP,F,3	2000-7500	2	6	800	30	2-20	*-(1-7.5)	-	72	
	TIS59	TI	n,EP,F,3	2300-5000	3	6	-	25	6-25	*1-9	-	92	
FET 70	2N3822	TI	n,EP,F,3	3000-6500	3	6	-	50	2-10	*6	5(0.01 kHz/1 M $\Omega$ )	72	
	2N4223	MO	n,DP,F,3	3000-7000	2	6	800	30	3-18	*-(1-7)	5(200 MHz/1 k $\Omega$ )	72	
	2N3823	TI	n,EP,F,3	3500-6500	2	6	-	30	1-7.5	*8 (max)	2.5(100 MHz/1 k $\Omega$ )	72	
	40460	RCA	n,DP,MOS,4	3500 (typ)	1.2	5	-	$\pm 25$	9 (typ)	-	-	72	
	40461	RCA	n,DP,MOS,4	3500 (typ)	1.2	5	-	$\pm 25$	4-14	-6 (max)	-	72	
	TIS34	TI	n,EP,F,3	3500-6500	2	6	-	30	4-20	1-8	-	72	
	K1003	KMC	n,M,4	4000 (min)	1.0	3.5	800	15	12-20	6 (max)	4.5(200 MHz)	18	
	2N4416	UC	n,F,PL,3	4500-7500	0.8	4.0	1000	-30	5.0-15	-6.0 (max)	-	72	
	2N4417	UC	n,F,PL,3	4500-7500	0.8	3.5	1000	-30	5.0-15	-6.0	-	3	
	3N128	RCA	n,DP,MOS,4	5000-12,000	0.2	5.8	-	20	5-30	-	-	104	
FET 71	TIXM12	TI	p,DPE,ge,F,3	5000-20,000	4	15	1000	20	-(5-25)	*1-3.5	-	-	
	FT57	FA	n,EP,M,4	6000 (min)	0.8	2.7	60 (typ)	25	9-26	10 (max)	4 at 0.1 GHz/2.5 k $\Omega$	-	
	TIXM301	TI	p,DPE,F,ge,3	6500-20,000	4	15	3000	20	-(5-25)	*1-3.5	-	72	
	TIXS35	TI	n,EP,F,4	10,000-20,000	5	12	-	30	10-50	*1-5	-	72	
	CP651	CT	n,EP,F,3	75,000-200,000	20	50	-	20	100-500	2-10	-	5	
	CP650	CT	n,EP,F,3	100,000-250,000	20	50	-	25	300-1200	2-10	-	5	

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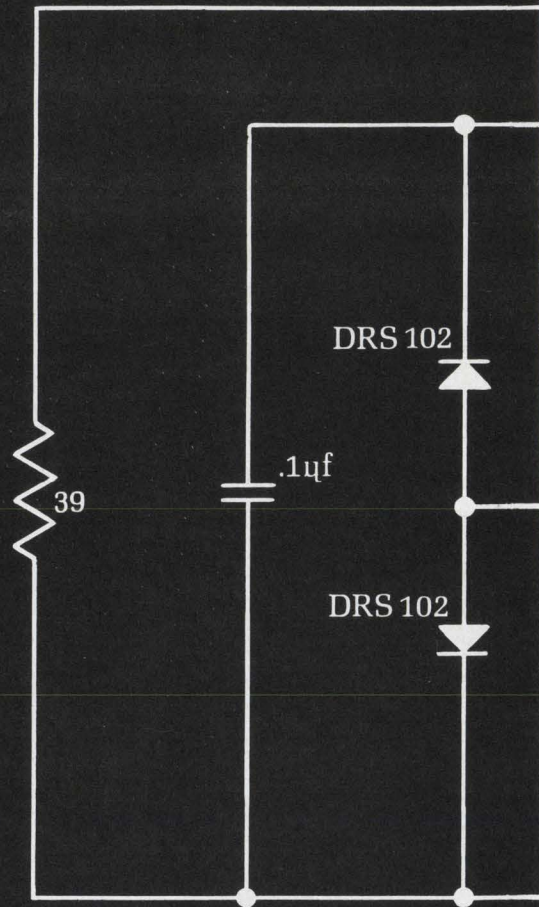
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# Want to convert high energy at high efficiency?



## Convert to circuit designs using Delco high voltage silicon power.

The DC to DC converter above operates directly from a 150V DC source and delivers 180 watts to the load at an efficiency of over 94 percent. The 1.1 kHz circuit operates over a temperature range of  $-65^{\circ}\text{C}$  to  $100^{\circ}\text{C}$ . Frequencies of up to 25 kHz may be obtained with selected transformer core materials. And the switching job is handled easily by just two Delco NPN DTS-423 silicon transistors—priced at just \$4.95 each in 1,000 and up quantities.

Delco pioneered the development of high voltage silicon power transistors to provide you high energy capability at the lowest cost. Among the many circuit benefits you get are: high reliability, reduced assembly time, and a reduction in the number, weight and

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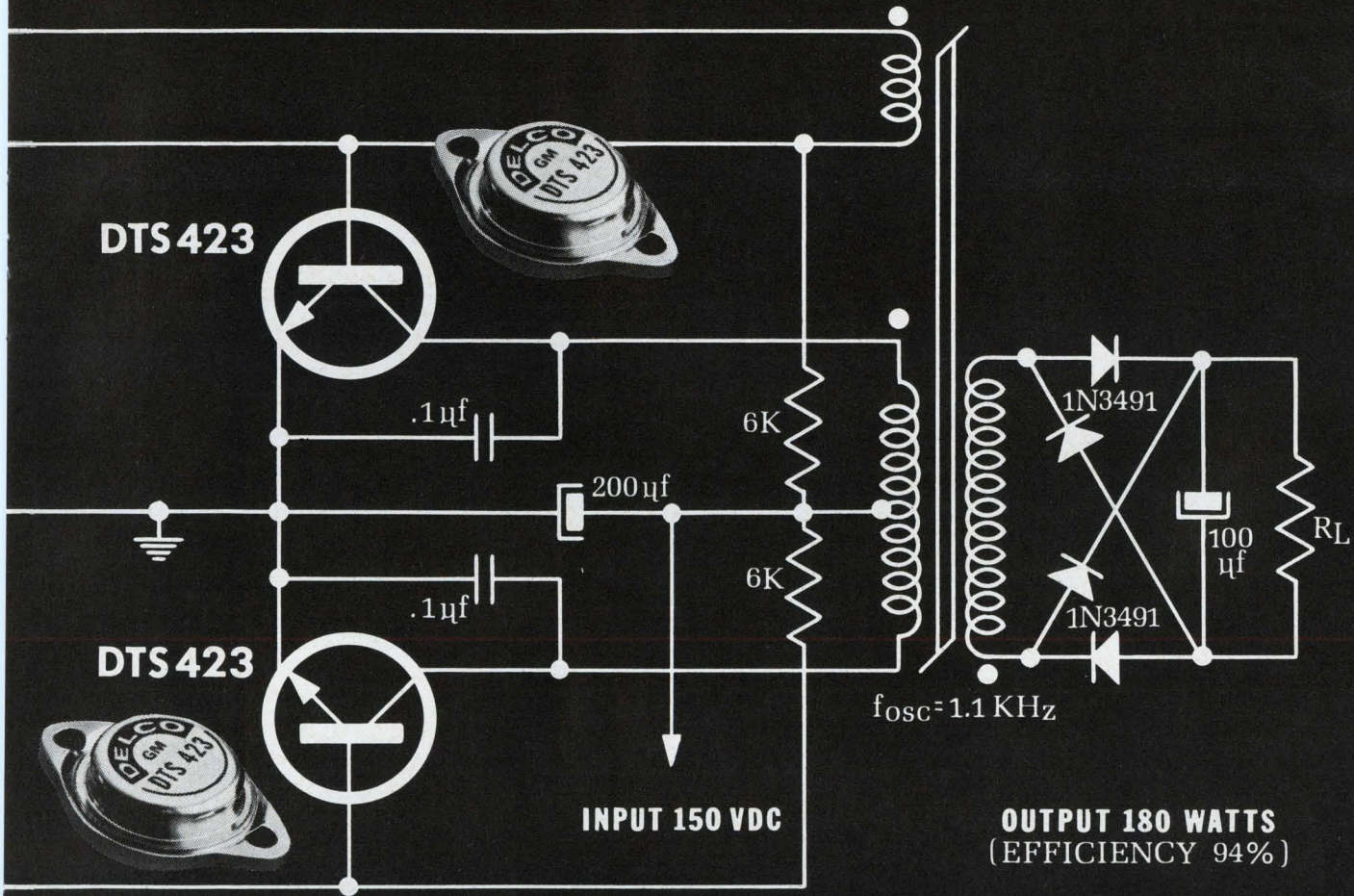
complexity of the electronic components needed. Coupled with the low prices of the Delco silicon power line, these benefits mean real cost advantages to you.

Other applications? They've proven their capability in such high energy circuits as: DC and switching regulators, ultrasonic power supplies, VLF class C amplifiers, off-line class A audio output and CRT deflection (several major TV manufacturers use them for big screen horizontal and vertical deflection).

Availability? With Delco's lead in know-how and plant facilities it's no problem. Samples or production quantities can be shipped promptly. Contact one of our distributors or a Delco sales office right now and see.

For more details on the DC-DC converter circuit—ask for application note number 32.

# Application of Delco high voltage silicon power transistors: the DC to DC Converter.



DEVICE TYPE	V <sub>CEX</sub>	V <sub>CEO/SUS</sub> (min.)	h <sub>FE</sub> min. @ I <sub>C</sub> V <sub>CE</sub> = 5 V		I <sub>C</sub> max.	P <sub>D</sub> max.
DTS-410	200	200	10	2.5A	3.5A	80W
DTS-411	300	300	10	2.5A	3.5A	100W
DTS-413	400	325	15	1.0A	2.0A	75W
DTS-423	400	325	10	2.5A	3.5A	100W
DTS-430	400	300	10	3.5A	5.0A	125W
DTS-431	400	325	10	3.5A	5.0A	125W

NPN silicon transistors packaged in solid copper TO-3 case.

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**DELCO RADIO**  
DIVISION OF GENERAL MOTORS • KOKOMO, INDIANA

# How To Use The Transistor Cross Index

Types are listed in numerical sequence. JEDEC numbered devices come first, followed by house-numbered types. The code following each type identifies its application category and the block of ten types in which it is located. A3, for example, means that the type can be found in the third block of the Audio section.

Key to the Letter Codes	
A	= audio and general purpose
P	= power
HF	= high frequency
LL	= low-level switching
HL	= high-level switching
FET	= field-effect
UJT	= unijunction

2N35	A46	2N244	A15	2N336	A35	2N406	A16
2N43A	A21	2N250A	P68	2N336A	A31	2N407	A28
2N78A	HF6	2N251A	P68	2N337	LL40	2N408	A28
2N94	HF2	2N257	P68	2N337A	LL14	2N409	HF5
2N94A	HF3	2N262	HF93	2N338	LL40	2N410	HF5
2N102	A4	2N268	P68	2N338A	LL18	2N411	HF7
2N109	A29	2N268A	P68	2N339	P2	2N412	A30
2N117	A4	2N270	A28	2N339A	A11	2N414	LL11
2N118	A11	2N274	HF11	2N340	P2	2N418	P35, HL42
2N119	A22	2N277	P86	2N340A	A11	2N419	P35
2N120	A35	2N278	P86	2N341	P2	2N420	P35, HL42
2N122	P22	2N279	A13	2N341A	A11, P1	2N420A	P35, HL42
2N128	HF14	2N280	A22	2N342	P2	2N424	P62
2N139	HF3	2N281	A28	2N342A	P2	2N424A	HL42
2N140	HF7	2N282	A28	2N342B	P2	2N426	LL5
2N144	HF93	2N284	LL40	2N343	P2	2N427	LL7
2N156	P31	2N284A	LL40	2N343A	P2	2N428	LL12
2N158	P31	2N285A	P35	2N343B	P3	2N441	P87
2N158A	P31	2N285B	P35	2N344	HF11	2N442	P87
2N167A	HF6	2N297A	P69	2N345	HF11	2N443	P87
2N169	A25	2N301	P26	2N346	HF19	2N444	HF1
2N173	P86	2N301A	P26	2N350A	P69	2N444A	HF1
2N174	P86	2N306	A13	2N351A	P69	2N445	HF2
2N174A	P86	2N315	LL7	2N356	LL5	2N445A	HF2
2N175	A27	2N315A	LL7	2N356A	LL5	2N446	HF3
2N176	P68	2N315B	LL7	2N357	LL8	2N446A	HF3
2N178	P68	2N316	LL13	2N357A	LL8	2N447	HF7
2N211	HF3	2N316A	LL13	2N358	LL11	2N447A	HF7
2N212	HF3	2N317	LL16	2N358A	LL12	2N447B	HF7
2N213	A29	2N317A	LL17	2N370	HF19	2N449	A25
2N213A	A36	2N326	P20	2N374	HF93	2N456A	P51
2N214	A23	2N327A	LL1	2N375	P69	2N456B	HL14
2N215	A21	2N328A	LL1	2N376A	P69	2N457A	P51
2N217	A30	2N328B	LL1	2N384	HF30	2N457B	HL14
2N218	HF3	2N239	LL1	2N388	LL7	2N458A	P51
2N219	HF7	2N329A	LL1	2N388A	LL7	2N458B	HL14
2N219A	HL36	2N329B	LL2	2N389	P62	2N463	P51
2N220	A27	2N330A	A12	2N389A	P62	2N466	HF30
2N231	HF93	2N331	A46	2N393	HF13	2N470	A3
2N233	HF2	2N332	A4	2N398	LL40	2N471	A4
2N233A	HF2	2N332A	A3	2N398A	LL21	2N471A	HF5
2N234A	P34	2N333	A11	2N399	P35	2N472	A4
2N235A	P34	2N333A	A7	2N400	P44	2N472A	A4, HF5
2N235B	P35	2N334	A18	2N401	P35	2N473	HF5
2N236A	P53	2N334A	A7	2N404	LL6	2N474	HF5
2N236B	P53	2N335	A22	2N404A	LL6	2N474A	HF5
2N243	A6	2N335A	A18	2N405	A15	2N475	HF6



2N475A	HF6	2N529	A6	2N656A	P15	2N739	A18, HF94
2N476	HF9	2N530	A10	2N657 HF93, P14,	HL43	2N739A	HF46
2N477	HF9	2N531	A13	2N657A	P15	2N740	A31, HF94
2N478	HF10	2N532	A14	2N658	A13	2N740A	HF48
2N479	HF10	2N533	A16	2N659	A20	2N741	HF74
2N479A	HF10	2N538	P42	2N660	A27	2N741A	HF74
2N480	HF10	2N538A	P43	2N661	A31	2N742	LL34
2N480A	A20	2N539	P43	2N662	A13	2N743	HF94
2N489	UJT2	2N539A	P43	2N663	P45	2N743/46	HF88
2N489A	UJT1	2N540	P43	2N665	P45	2N743/51	HF88
2N489B	UJT3	2N540A	P43	2N669	P70	2N744	HF94, LL42
2N490	UJT2	2N541	HF7	2N677	P70	2N744/46	HF89
2N490A	UJT1	2N542	HF7	2N677A	P70	2N744/51	HF89
2N490B	UJT3	2N542A	HF7	2N677B	P70	2N752	HF49
2N490C	UJT3	2N543	HF8	2N677C	P70	2N753	HF95
2N491	UJT2	2N543A	A32	2N678	P51	2N754	HF11
2N491A	UJT1	2N545	HL22	2N678A	P51	2N755	HF11
2N491B	UJT3	2N546	HL23	2N678B	P51	2N756	A4
2N492	UJT2	2N547	HL23	2N678C	P51	2N756A	A5
2N492A	UJT1	2N548	HL23	2N696 HF27, P7,	HL30	2N757	A7
2N492B	UJT3	2N549	HL23	2N697	HF30, P7	2N758	A7
2N492C	UJT3	2N550	HL23	2N698 HF19, P12,	HL26	2N758A	A7
2N493	UJT2	2N551	HL22	2N699 HF27, P8,	HL31	2N758B	HF42
2N493A	UJT1	2N552	HL22	2N699B	P15	2N759	A17
2N494	UJT2	2N554	P58	2N700	HF80	2N759A	A17
2N494A	UJT1	2N555	P58	2N700A	HF90	2N759B	HF46
2N494B	UJT3	2N563	A12	2N702	HF42, LL25	2N760	A31
2N494C	UJT3	2N564	A12	2N703	HF42, LL25	2N760A	A31
2N495	HF6	2N566	A25	2N705	LL41	2N760B	HF49
2N495B	UJT3	2N567	A35	2N706	HF74, P3	2N768	HF39
2N496	HF10	2N568	A35	2N706/51	HF48	2N769	HF83
2N497	P14	2N569	A38	2N706A	HF94, LL33	2N779A	HF70
2N497A	P15	2N570	A39	2N706A/51	HF48	2N780	A16
2N498	P14	2N571	A43	2N706B	HF75, LL33	2N781	HF95, LL42
2N498A	P15	2N572	A43	2N706B/46	HF48	2N782	HF95, LL42
2N499	HF56	2N574	P99	2N706B/51	HF48	2N783	HF49
2N499A	HF56	2N574A	P99	2N706C	HF75	2N784	HF64
2N501	HF29	2N575	P99	2N706C/46	HF48	2N784A	HF64, LL29
2N501A	HF37	2N575A	P99	2N706C/51	HF48	2N784/51	HF64
2N502	HF80	2N579	LL11	2N707 HF75, P3,	LL33	2N794	HF13, LL20
2N502A	HF85	2N580	LL15	2N707A	LL41	2N795	HF13, LL20
2N502B	HF85	2N581	HF6, LL11	2N708 HF75, P3,	LL34,	2N796	HF16, LL21
2N503	HF69	2N582	HF10, LL16		HL39	2N797	HF95, LL42
2N504	HF15	2N583	LL11	2N709 HF87, P1,	LL39	2N827	LL28
2N508A	A35	2N585	LL5	2N709/46	HF83	2N828	HF75, LL34
2N511	P87	2N586	LL41	2N709/51	HF83	2N828A	HF75
2N511A	P87	2N588	HF48	2N709A	HF87	2N829	HF75
2N511B	P87	2N594	LL4	2N709A/46	HF87	2N834	HF78, LL32
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2N513B	P88	2N605	HF16	2N715	HF94	2N838	LL30
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2N514A	P88	2N607	HF16	2N717 HF19, P5,	HL27	2N841	HF13
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2N525	LL4	2N651A	A24	2N734	A7	2N860	LL10
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2N526A	LL20	2N653	A15	2N736	A31	2N863	LL12
2N527	LL5	2N654	A24	2N736A	A26	2N864	LL16
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2N1304	LL44	2N1475	A17	2N1547A	P78	2N1669	HL15
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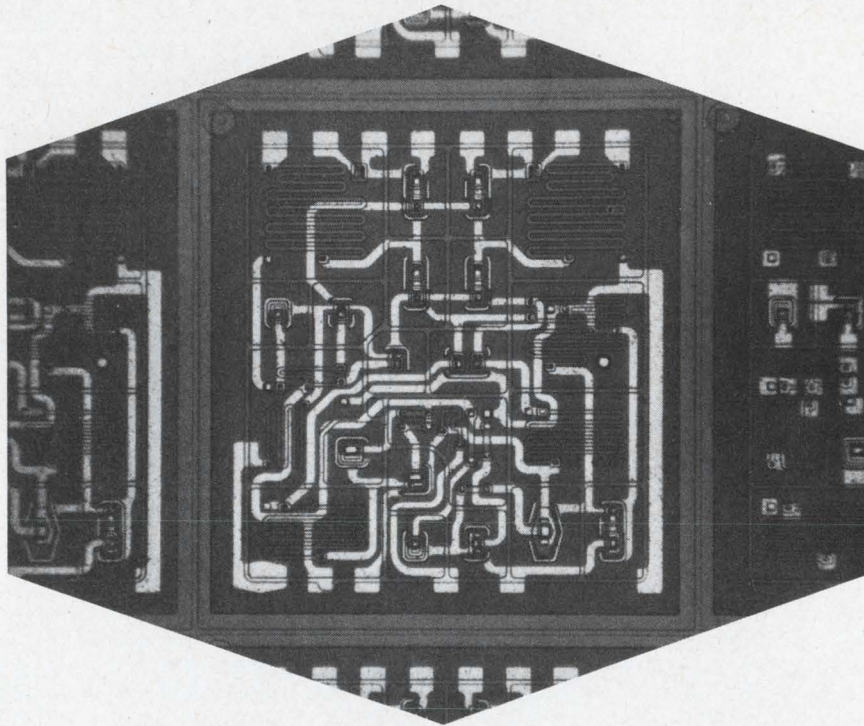
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2N2837	HF38	2N2919	HF23	2N3022	P36	2N3151	P108
2N2838	HF39	2N2920	HF24	2N3023	P36	2N3154	P45
2N2841	FET23, FET34, FET57	2N2921	HF51	2N3024	P37	2N3155	P45
2N2842	FET24, FET36, FET57	2N2922	HF52	2N3025	P37	2N3156	P45
2N2843	FET24, FET39	2N2923	A34	2N3026	P37	2N3157	P45
2N2844	FET25, FET43	2N2924	A39	2N3043	HF67	2N3158	P45
2N2845	HF72	2N2925	A43	2N3049	HF84	2N3163	P64
2N2846	HF72	2N2926	A16	2N3053	HL35	2N3164	P64
2N2847	HF72	2N2927	HF43	2N3054	HL22	2N3165	P64
2N2848	HF72	2N2929	HF91	2N3055	HL20	2N3166	P64
2N2849	HL32	2N2936	HF102	2N3056	HF26, P18	2N3167	P64
2N2850	HL28	2N2937	HF102	2N3056A	P18	2N3168	P64
2N2851	HL29	2N2942	HF43	2N3057	HF26, P19	2N3169	P65
2N2852	HL26	2N2943	HF39	2N3057A	P19	2N3170	P65
2N2853	HL29	2N2944	HF8, LL12	2N3058	A34	2N3171	P60
2N2854	HL32	2N2944A	A35, LL15	2N3059	A43	2N3172	P60
2N2855	HL29	2N2945	HF4, LL8	2N3060	A34	2N3173	P60
2N2856	HL26	2N2945A	A29, LL13	2N3061	A41	2N3174	P61
2N2857	HF91	2N2946	HF2, LL6	2N3062	A28	2N3175	P65
2N2858	P22	2N2946A	A23, LL8	2N3063	A28	2N3176	P65
2N2859	P22	2N2947	HF35	2N3064	A19	2N3177	P65
2N2860	A13	2N2948	HF35	2N3065	A19	2N3178	P66
2N2861	HF102	2N2949	HF35	2N3066	FET46	2N3179	P66
2N2862	HF102	2N2950	HF35	2N3067	FET39	2N3180	P66
2N2863	HF102	2N2951	HF52	2N3068	FET34	2N3181	P66
2N2864	HF102	2N2952	HF52	2N3068A	FET35	2N3182	P66
2N2865	HF102	2N2953	A44	2N3069	FET52	2N3183	P61
2N2866	A19	2N2955	HF72	2N3070	FET44	2N3184	P61
2N2869	P39	2N2956	HF74	2N3071	FET37	2N3185	P61
2N2870	P39	2N2957	HF76	2N3074	HF47	2N3186	P61
2N2871	LL47	2N2958	HF61	2N3075	HF26	2N3187	P66
2N2872	LL47	2N2959	HF61	2N3076	P85, HL27	2N3188	P66
2N2874	HF42, P28	2N2962	HF86	2N3077	A45	2N3189	P66
2N2875	P33	2N2963	HF86	2N3078	A44	2N3190	P66
2N2876	HF50	2N2964	HF86	2N3081	HF44	2N3191	P66
2N2877	P39	2N2965	HF86	2N3081/46	HF44	2N3192	P67
2N2878	P39	2N2966	HF88	2N3081/51	HF44	2N3193	P67
2N2879	P39	2N2968	LL12	2N3084	FET46	2N3194	P67
		2N2969	LL12	2N3085	FET46	2N3195	P61
		2N2970	LL11	2N3086	FET46	2N3196	P61

2N3197	P61	2N3311	P98	2N3404	A30	2N3499	HL13
2N3198	P61	2N3312	P98	2N3405	A42	2N3500	HL13
2N3199	P49	2N3313	P98	2N3409	HF58	2N3501	HL14
2N3200	P49	2N3314	P98	2N3410	HF58	2N3502	HF62, HL38
2N3201	P49	2N3315	P98	2N3411	HF58	2M3503	HF62, HL38
2N3202	P23	2N3316	P98	2N3414	A31	2N3504	HF63, HL19
2N3203	P23	2N3317	HF8, LL9	2N3415	A42	2N3505	HF63, HL38
2N3204	P23	2N3318	HF5, LL10	2N3416	A31	2N3506	HL13
2N3205	P49	2N3319	HF8, LL14	2N3417	A42	2N3507	HL13
2N3206	P49	2N3320	HF84	2N3418	P25	2N3508	HL21
2N3207	P50	2N3321	HF84	2N3419	P25	2N3409	HL21
2N3208	P23	2N3322	HF84	2N3420	P26	2N3510	HL20
2N3209	HL41	2N3323	HF53	2N3421	P26	2N3511	HL20
2N3212	P26	2N3324	HF53	2N3423	HF84, HL41	2N3512	HL39
2N3213	P26	2N3325	HF53	2N3424	HF84, HL21	2N3544	HF84
2N3214	P27	2N3326	HF58	2N3426	HF53, HL15	2N3546	HL21
2N3215	P27	2N3327	A43, HF77	2N3427	A43	2N3547	LL20
2N3217	LL47	2N3328	FET48	2N3428	A44	2N3548	LL21
2N3218	LL47	2N3329	FET2, FET18	2N3429	P90, HL15	2N3549	LL21
2N3219	LL47	FET25, FET49, FET61		2N3430	P91, HL15	2N3551	P50
2N3220	P40	2N3330	FET2, FET18,	2N3431	P91, HL15	2N3552	P50
2N3221	P40	FET25, FET51, FET61		2N3432	P91, HL15	2N3553	HF80
2N3222	P40	2N3331	FET3, FET17,	2N3433	P91, HL16	2N3554	LL26
2N3223	P59	FET27, FET55, FET60		2N3434	P91, HL16	2N3563	HF90
2N3227	HF81, HL20	2N3332	FET12, FET18,	2N3436	FET4, FET54	2N3564	HF87
2N3229	HF52	FET26, FET49, FET62		2N3437	FET3, FET47	2N3565	HF14
2N3230	P37	2N3333	FET30	2N3438	FET40	2N3566	HF14
2N3231	P37	2N3334	FET29	2N3439	P19	2N3567	HF21
2N3241A	A39, P10,	2N3335	FET29	2N3440	P19	2N3568	HF21
	HL37	2N3336	FET29	2N3441	P37	2N3569	HF21
2N3242A	A43, P10,	2N3337	HF77	2N3442	P83	2N3570	HF92
	HL37	2N3338	HF77	2N3444	HL14	2N3571	HF91
2N3244	HF47	2N3339	HF77	2N3445	P83	2N3572	HF91
2N3245	HF44	2N3340	LL21	2N3446	P83	2N3576	HF77, HL35
2N3248	HF62	2N3341	LL21	2N3447	P84	2N3577	P67
2N3249	HF67	2N3342	LL3	2N3448	P84	2N3578	FET48
2N3250	HF62, LL28	2N3343	LL4	2N3452	FET47, FET62	2N3579	A10
2N3250A	HL18	2N3344	LL3	2N3453	FET40, FET62	2N3580	A20
2N3251	HF68, LL30	2N3345	LL3	2N3454	FET34, FET62	2N3581	A23
2N3251A	HL19	2N3346	LL3	2N3455	FET47, FET60	2N3582	A35
2N3252	HF52, HL15	2N3365	FET46	2N3456	FET40, FET60	2N3583	P44
2N3253	HF47, HL14	2N3366	FET39	2N3457	FET35, FET60	2N3584	P44
2N3262	HF44	2N3367	FET34	2N3458	FET4, FET54,	2N3585	P44
2N3263	P85	2N3368	FET53		FET59	2N3588	HF56
2N3264	P62	2N3369	FET44	2N3459	FET3, FET47,	2N3589	P29
2N3265	P85	2N3370	FET37		FET60	2N3590	P29
2N3266	P62	2N3371	HF77	2N3460	FET2, FET40,	2N3591	P30
2N3277	FET12, FET41	2N3374	P19		FET60	2N3592	P30
2N3278	FET12, FET46	2N3375	HF81	2N3462	A32	2N3593	P21
2N3279	HF76	2N3376	FET1, FET58,	2N3463	A32	2N3594	P21
2N3280	HF76		FET68	2N3467	HL14	2N3595	P30
2N3281	HF68	2N3377	FET1, FET58,	2N3468	HL13	2N3596	P30
2N3282	HF68		FET68	2N3469	P15	2N3597	P83
2N3283	HF62	2N3378	FET2, FET54,	2N3470	P91, HL20	2N3598	P83
2N3284	HF62		FET69	2N3471	P91, HL20	2N3599	P83
2N3285	HF62	2N3379	FET2, FET54,	2N3472	P91, HL20	2N3600	HF88
2N3286	HF62		FET69	2N3473	P91, HL20	2N3605	LL30
2N3287	HF72	2N3380	FET4, FET69	2N3474	P91, HL21	2N3506	LL30
2N3288	HF73	2N3381	FET4, FET69	2N3475	P92, HL21	2N3507	LL30
2N3289	HF68	2N3382	FET5	2N3476	P92, HL21	2N3608	FET5, FET19,
2N3290	HF68	2N3383	FET5	2N3477	P92, HL21		FET58, FET67
2N3291	HF62	2N3384	FET6	2N3478	HF90	2N3610	FET1
2N3292	HF58	2N3385	FET6	2N3485	LL26, HL16	2N3611	P67
2N3293	HF58	2N3386	FET6	2N3485A	LL26, HL16	2N3612	P67
2N3294	HF58	2N3387	FET6	2N3486	LL27, HL16	2N3613	P67
2N3295	HF2	2N3390	A44	2N3486A	LL27, HL16	2N3614	P67
2N3296	HF1	2N3391	A44	2N3487	P84	2N3615	P67
2N3297	HF1	2N3391A	A44	2N3488	P84	2N3616	P67
2N3298	HF53	2N3392	A39	2N3489	P84	2N3617	P68
2N3299	HF76, HL40	2N3393	A34	2N3490	P84	2N3618	P68
2N3300	HF76, HL40	2N3394	A25	2N3491	P84	2N3619	HF53
2N3301	HF77, HL40	2N3395	A45	2N3492	P84	2N3620	HF53
2N3302	HF77, HL40	2N3396	A45	2N3493	LL35	2N3621	HF53
2N3303	HF86, HL42	2N3397	A45	2N3494	HL16	2N3622	HF53
2N3304	HF86	2N3398	A45	2N3495	HL13	2N3623	HF53
2N3307	HF68	2N3399	HF84	2N3496	HL16	2N3624	HF54
2N3308	HF68	2N3402	A30	2N3497	HL13		
2N3309	HF68	2N3403	A41	2N3498	HL13		

(continued on p. 180)

# Union Carbide's New Integrated Circuit Operational Amplifier



## The 15nA Operational Amplifier

ADVANCED DATA SHEET FOR YOUR USE



- 15nA differential input offset current (max)
- 175pA/°C differential input offset current drift (max)
  - 5mV input offset voltage (max)
- 10μV/°C input offset voltage drift (max)
  - 50nA input biasing current (max)
  - ±10V common mode voltage (min)
  - ±10V output voltage swing (min)
  - 2mA output current drive (min)
  - 20,000 open loop voltage gain (min)
- -55°C to +125°C operating temp. in TO-101
- Offset Voltage adjustable to zero with external potentiometer
  - Off the shelf delivery

*applications:* A to D converter • Bridge amplifier • DC amplifier • Differential amplifier  
Integrator (DC to AC) • Sample and hold amplifier



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# MONOLITHIC OPERATIONAL AMPLIFIERS

## LINEAR INTEGRATED CIRCUITS

### UC4000/UC4001/UC4002

The UC4000 series of operational amplifiers are constructed on a single silicon chip. The amplifier has the following features:

- Offset voltage adjustable to zero with external potentiometer
- $\pm 10V$  common mode voltage
- 15 nA differential input offset current
- 100 pA/ $^{\circ}C$  differential input current drift
- 10  $\mu V/^{\circ}C$  input offset voltage drift

#### MAXIMUM RATINGS

$T_A = 25^{\circ}C$  (UNLESS OTHERWISE NOTED)

UC4000/UC4001/UC4002	
Supply Voltage	$\pm 18.0$ Volts
Internal Power Dissipation 125 $^{\circ}C$ Ambient Temp. (Note 1)	200 mW
Output Short Circuit Duration	5 sec
Differential Input Voltage	$\pm 10.0$ Volts
Input Voltage, Common Mode	$\pm 10.0$ Volts
Storage Temperature Range	$-65^{\circ}C$ to $+200^{\circ}C$
Operating Ambient Temperature Range	$-55^{\circ}C$ to $+125^{\circ}C$
Lead Temperature Soldering for 60 seconds	$+300^{\circ}C$

Note 1. Rating applies for ambient temperatures to 125 $^{\circ}C$ ; derate linearly at 2.6 mW/ $^{\circ}C$  for ambient temperatures above 125 $^{\circ}C$ .

#### ELECTRICAL CHARACTERISTICS

@ 25 $^{\circ}C$  and Supply Voltage  $\pm 15.0$  Volts in Test Circuit Figure No. 4 (UNLESS OTHERWISE NOTED)

SPECIFICATION	Sym.	UC4000			UC4001			UC4002			Unit	TEST CONDITIONS
		Min.	Typ.	Max.	Min.	Typ.	Max.	Min.	Typ.	Max.		
Large Signal, Open Loop Voltage Gain	$A_v$	20K		80K	20K		80K	20K		80K		$V_{IN} = 100 \mu V$ rms $R_L = 10 K$ ohms $f = 100$ Hz
Large Signal, Open Loop Voltage Gain	$A_v$	15K		15K						15K		$V_{IN} = 100 \mu V$ rms $R_L = 10 K$ ohms, $f=100$ Hz ( $T_A = -55^{\circ}C$ to $+125^{\circ}C$ )
Differential Input Impedance	$R_{in}$ $C_{in}$	0.8	3.0		0.8	3.0		0.8	3.0		M $\Omega$ pF	$V_{out} = 7 V$ rms $f = 1 KHz$
Open Loop Output Resistance	$R_{out}$		100			100			100		ohm	$V_{out} \leq 1 V$ p-p $f = 100$ Hz
Output Voltage Swing	$V_{out}$	$\pm 10$		$\pm 10$				$\pm 10$			V	$R_L = 10 K$ ohms ( $T_A = -55^{\circ}C$ to $+125^{\circ}C$ )
Output Current	$I_{out}$	$\pm 2$		$\pm 2$				$\pm 2$			mA	$R_L = 5 K$ ohms
Equivalent Input Offset Voltage (2)	$V_{os}$		3.0	5.0		5.0	10.0		7.0	10.0	mV	$R_L = 10 K$ ohms
Equivalent Input Offset Voltage Change with Temp.	$\Delta V_{os}$			1.8			3.6			7.2	mV	$R_L = 10 K$ ohms ( $T_A = -55^{\circ}C$ to $+125^{\circ}C$ )
Equivalent Average Offset Voltage Drift	$\Delta V_{os}$			10			20			40	$\mu V/^{\circ}C$	$R_L = 10 K$ ohms ( $T_A = -55^{\circ}C$ to $+125^{\circ}C$ )
Offset Voltage Change with Power Supply Variation	$\Delta V_{os}$		25	150		25	150		25	150	$\mu V/V$	$R_L = 10 K$ ohms, $V_{out} = 0$ $\Delta V_{PS} = 1 V$ rms, $f = 100$ Hz
Offset Voltage Drift with Time	$\Delta V_{os}$		40			100			160		$\mu V/24$ hr	$V_{os} = 0$ at start, $t = 24$ hrs.
Differential Input Offset Current	$I_{os}$			15			30			50	nA	$V_{out} = 0$ , $R_L = 10 K$ ohms
Differential Input Offset Current Change with Temp.	$\Delta I_{os}$			31.5			63.0			126	nA	$V_{out} = 0$ , $R_L = 10 K$ ohms ( $T_A = -55^{\circ}C$ to $+125^{\circ}C$ )

## ELECTRICAL CHARACTERISTICS

@ 25°C and Supply Voltage ±15.0 Volts in Test Circuit Figure No. 4 (UNLESS OTHERWISE NOTED)

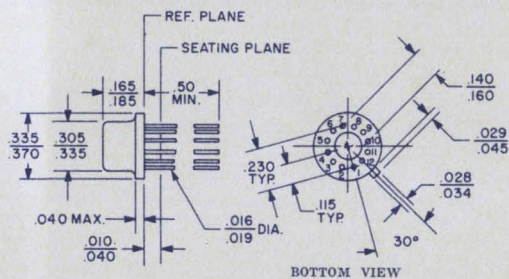
SPECIFICATION	Sym.	UC4000			UC4001			UC4002			Unit	TEST CONDITIONS
		Min.	Typ.	Max.	Min.	Typ.	Max.	Min.	Typ.	Max.		
Average Differential Input Offset Current Drift	$\Delta I_{os}$			175			350			700	pA/°C	$V_{out} = 0, R_L = 10 \text{ K ohms}$ ( $T_A = -55^\circ\text{C}$ to $125^\circ\text{C}$ )
Differential Input Offset Current Change with Power Supply Variation	$\Delta I_{os}$		500			500			500		pA/V	$V_{out} = 0, R_L = 10 \text{ K ohms}$ $\Delta V_{PS} = 1 \text{ V rms}, f = 100 \text{ Hz}$
Differential Input Offset Current Change with Time	$\Delta I_{os}$		1			3			5		nA/24 hr	$V_O = 0$ at start, $t = 24 \text{ hrs.}$ $R_L = 10 \text{ K } \Omega$
Common Mode Rejection	CMR	90	100		90	100		90	100		dB	$e_{in} = 1 \text{ V rms}, f = 100 \text{ Hz}$
Common Mode Voltage Range (Note 3)	$V_{CM}$	±10			±10			±10			V	$R_L = 10 \text{ K}, R_f = \infty$ $f = 100 \text{ Hz},$ $V_{out} = 7 \text{ V rms}$
Common Mode Input Resistance	$R_{CM}$		400			400			400		MΩ	$V_{out} = 7.0 \text{ V rms}$ $V_{CM} = 7.0 \text{ V rms}$
Input Bias Current	$I_{Bias}$		40	50		60	100		80	150	nA	$V_{out} = 0$
Input Bias Current	$I_{Bias}$		150	250		300	400		500	600	nA	$V_{out} = 0$ ( $T_A = -55^\circ\text{C}$ )
Input Spot Noise Voltage	$e_n$		200			200			200		nv/ $\sqrt{\sim}$	$f = 100 \text{ Hz}$ $R_L = 10 \text{ K } \Omega$
Small Signal Bandwidth—(Note 3)	BW	1.0	2.0		1.0	2.0		1.0	2.0		MHz	$R_f = 0, R_{in} = \infty,$ $e_{in} \leq 100 \text{ mV}$
P.S. Current Drain, +15 V				7.0			7.0			7.0	mA	$V_{out} = 0$
P.S. Current Drain, -15 V				8.0			8.0			8.0	mA	$V_{out} = 0$
Slewing Rate (Note 3)	$\Delta V/\Delta t$	1.0			1.0			1.0			V/ $\mu\text{s}$	$R_L = 10 \text{ K}$ $-10 \text{ V} < V_{out} < +10 \text{ V}$ $t_r = 10 \text{ ns}, \text{PRR} = 1 \text{ KHz}$
Full Power Frequency (Note 3)			15		15			15			KHz	$R_L = 10 \text{ K}, V_{out} = 7 \text{ V rms}$ $R_i = R_f = 100 \text{ K } \Omega$

Notes: 2) Adjustable to zero by external 20 KΩ potentiometer.

3) With compensation to provide 6 dB per octave roll-off (see Figure 3).

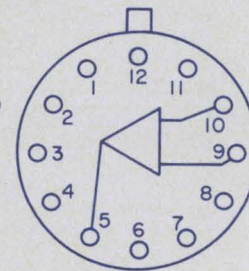
4) If balance potentiometer is not used, connect pins 7 and 12 through 10K ohm resistors to pin 6 (see Figure 4).

5) Case connected to negative supply pin 2.

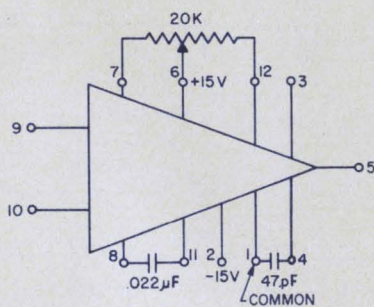


JEDEC OUTLINE TO-101.  
PHYSICAL DIMENSIONS  
FIGURE 1.

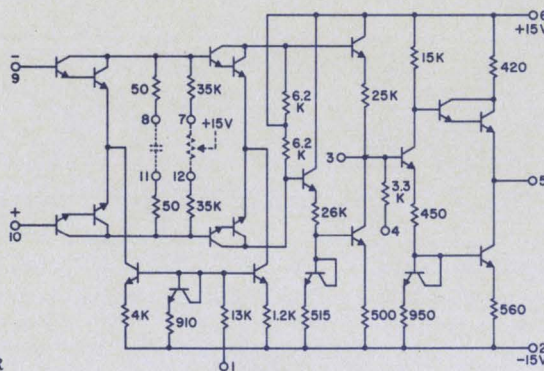
- (1) Common
- (2) Negative Supply (Ref: Note 5)
- (3) Output Compensation (Fig. 3 & 4)
- (4) Output Compensation (Internal Resistor)
- (5) Output
- (6) Positive Supply
- (7) Balance Potentiometer
- (8) Input Compensation (Fig. 3 & 4)
- (9) Input (Inverting)
- (10) Input (Non-inverting)
- (11) Input Compensation (Fig. 3 & 4)
- (12) Balance Potentiometer (Fig. 3 & 4)



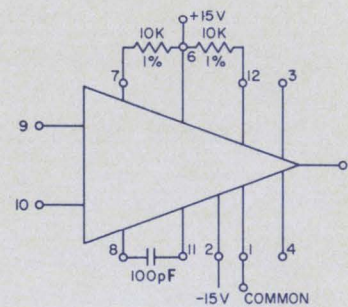
CONNECTION DIAGRAM  
FIGURE 2.



FREQUENCY COMPENSATION CIRCUIT FOR  
6 dB/OCTAVE ROLLOFF (Ref: Note 3)  
FIGURE 3.

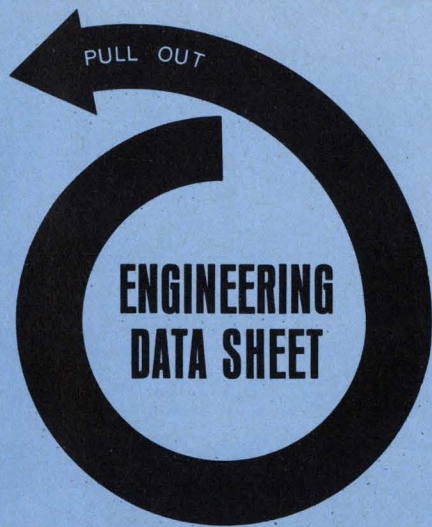


CIRCUIT DIAGRAM



STANDARD TEST CIRCUIT  
(Ref: Note 4)  
FIGURE 4.





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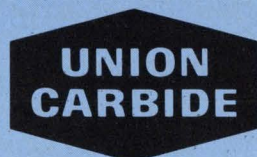
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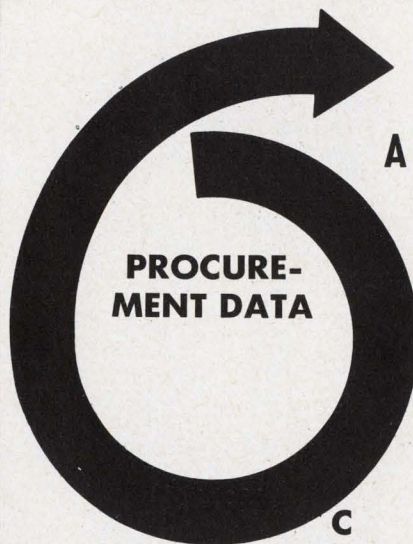
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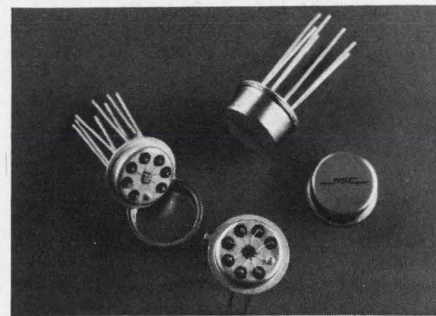
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2N3626	HF54	2N3733	HF78	2N3828	HF74
2N3627	HF54	2N3734	HF63, HL19	2N3829	HF73, LL32
2N3628	HF54	2N3735	HF63, HL19	2N3830	LL27
2N3629	HF54	2N3736	HF63, HL19	2N3831	LL27
2N3630	HF54	2N3737	HF63, HL19	2N3832	HF88, LL39
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2N3632	HF77	2N3939	P34, HL24	2N3838	A37, P38, LL27
2N3633	HF92	2N3740	P37, HL23	2N3839	HF91
2N3634	HL14	2N3741	P37, HL24	2N3840	LL9
2N3635	HL16	2N3742	HF12	2N3841	LL4
2N3636	HL14	2N3743	HF13	2N3842	LL4
2N3637	HL17	2N3744	P40	2N3843	HF40
2N3638	HF44	2N3745	P40	2N3943A	HF40
2N3638A	HL37	2N3746	P40	2N3844	HF40
2N3639	LL36	2N3747	P40	2N3844A	HF40
2N3640	LL37	2N3748	P40	2N3845	HF40
2N3641	LL28	2N3749	P41	2N3845A	HF40
2N3642	LL29	2N3750	P41	2N3846	P93
2N3643	LL29	2N3751	P41	2N3847	P93
2N3644	LL27	2N3752	P41	2N3848	P93
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2N3646	LL37	2N3763	HF44, HL37	2N3850	P41, HL12
2N3647	LL32, HL19	2N3764	HF48, HL38	2N3851	P42, P50, HL11
2N3648	LL35, HL20	2N3765	HF44, HL37	2N3852	P42, HL12
2N3660	P19	2N3766	HF55, P34, HL24	2N3853	P42, HL11
2N3661	P19	2N3767	P34, HL25	2N3854	HF68
2N3662	HF90	2N3771	P92	2N3854A	HF68
2N3663	HF90	2N3772	P92	2N3855	HF73
2N3665	P19	2N3773	P92	2N3855A	HF73
2N3666	P20	2N3783	HF88	2N3856	HF74
2N3677	LL8, LL15	2N3784	HF86	2N3856A	HF74
2N3683	HF84	2N3784	HF86	2N3857	LL6
2N3684	FET53, FET65	2N3785	HF87	2N3857	A27
2N3685	FET49, FET65	2N3789	P93	2N3858	A27
2N3686	FET42, FET65	2N3790	P83	2N3858A	A27
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2N3688	HF78	2N3792	P93	2N2859A	A36
2N3689	HF78	2N3793	A11	2N3860	A40
2N3690	HF78	2N3794	A35	2N3866	HF88
2N3691	A21, HF54	2N3796	FET12, FET25, FET45, FET59	2N3877	A10
2N3692	A37, HF54	2N3797	FET12, FET26, FET55, FET59	2N3877A	A10
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2N3694	HF55	2N3798	HF36	2N3879	HL29
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2N3697	FET39, FET64	2N3801	HF36	2N3900	A44
2N3698	FET35, FET64	2N3802	HF36	2N3900A	A44
2N3699	P20	2N3803	HF36	2N3903	HF63, LL29
2N3701	HF55	2N3804	HF36	2N3904	HF69, LL31
2N3702	HF35	2N3805	HF36	2N3905	HF63, LL27
2N3703	HF35	2N3806	HF37	2N3906	HF69, LL29
2N3704	HF35	2N3807	HF37	2N3909	FET13, FET21, FET24, FET41, FET66
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2N3707	A37	2N3810	HF37	2N3919	P30, HL33
2N3708	A22	2N3811	HF37	2N3920	P30, HL33
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2N3710	A34	2N3819,	FET12, FET17, FET27, FET53, FET66, FET69	2N3922	FET31
2N3711	A42			2N3924	HF82
2N3712	HF14	2N3820	FET12, FET17, FET24, FET41, FET66, FET68	2N3925	HF82
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2N3716	P92, HL23			2N3931	A32
2N3719	P20, HL29			2N3932	HF92
2N3720	P20, HL29			2N3933	HF92
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2N3722	LL35			2N3935	FET30
2N3723	LL35	2N3823	FET13, FET17, FET26, FET49, FET61, FET70	2N3946	HF63, LL29
2N3724	HL39			2N3947	HF69, LL31
2N3725	HL39	2N3824	FET5, FET17, FET21	2N3948	HF87, P3
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2N3729	HF78			2N3953	HF92
2N3730	P26	2N3825	HF55	2N3954	FET31
2N3731	P20	2N3826	A21, HF55	2N3955	FET31
				2N3956	FET30
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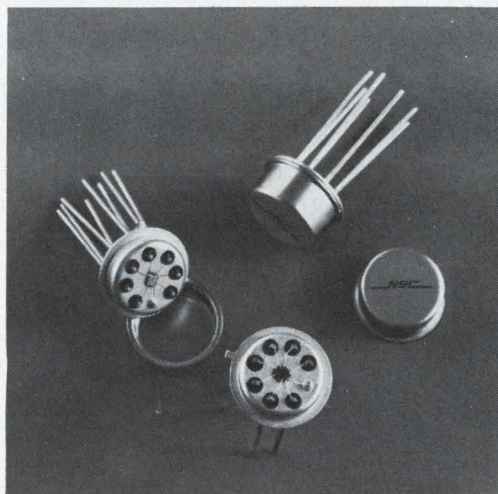
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ON READER-SERVICE CARD CIRCLE 80

ELECTRONIC DESIGN 9, April 26, 1967



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# Now... a Monolithic Voltage Regulator for less than \$20

## Second of a new line of monolithic linear integrated circuits

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- Can be used as either a linear or a high-efficiency switching regulator.

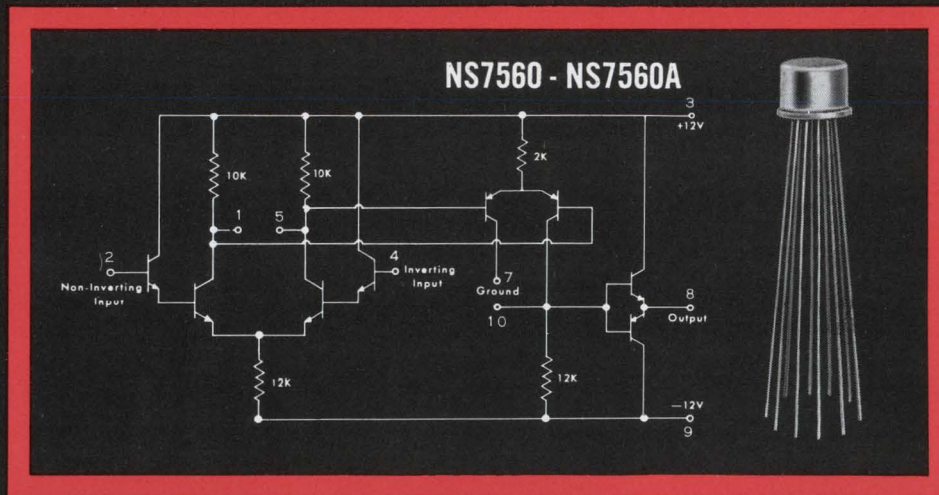
The new LM200 has the same performance characteristics as the LM100 over the commercial range.

These versatile regulators feature regulation better than 1 percent for widely varying load and line conditions. Temperature stability is better than 1 percent over full temperature range. As linear regulators, both devices provide current limiting, excellent transient response and unconditional stability with any combination of resistive or reactive loads. As

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- Investigate NCS's other standard hybrid products and custom circuit capability.

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Input Offset Voltage Temperature Coefficient (Maximum)	30 $\mu$ v/ $^{\circ}$ C	10 $\mu$ v/ $^{\circ}$ C
Input Bias Current (Maximum)	100 na	25 na
Differential Input Current (Maximum)	50 na	2 na
Input Bias Current Temperature Coefficient (Maximum)	2 na/ $^{\circ}$ C	1 na/ $^{\circ}$ C
Peak Output Current (Maximum)	$\pm 50$ ma,	$\pm 50$ ma

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ON READER-SERVICE CARD CIRCLE 84

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2N3959	HF92, LL40	2N4060	A22, LL48	2N4257	LL38	2N4430	HF85
2N3960	HF92, LL40	2N4061	A34, LL48	2N4258	LL39	2N4431	HF85
2N3961	HF82	2N4062	A42, LL48	2N4259	HF91	2N4433	HF55
2N3962	HF45	2N4063	P26	2N4260	HF92, LL40	2N4434	HF69
2N3963	HF45	2N4064	P26	2N4261	HF93, LL40	2N4435	HF56
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2N3965	HF45	2N4066	FET19	2N4265	HF69, LL31	2N4445	FET11
2N3966	FET6	2N4067	FET19	2N4267	FET19	2N4446	FET11
2N3967	FET27	2N4068	HL35	2N4268	FET20	2N4447	FET11
2N3968	FET26	2N4069	HL36	2N4284	A16	2N4448	FET11
2N3969	FET25	2N4070	P58	2N4285	A16	2N4854	A37, LL28
2N3970	FET16	2N4071	P59	2N4286	A40	2N4855	A21, LL28
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2N3976	LL32	2N4079	P108	2N4296	A24, P34, HL30	2N4863	P21
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2N3978	LL4	2N4083	FET31	2N4298	A13, P34, HL30	2N4865	P108
2N3979	LL4	2N4084	FET32	2N4299	A24, P34, HL30	2N4866	P108
2N3980	UJT2, UJT3	2N4085	FET31	2N4300	P30, HL25	2N4867	FET42, FET63
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2N4050	P98	2N4250	A36	2N4423	LL35	3N93	HF4
2N4051	P98	2N4251	HL42	2N4424	A42	3N94	HF4
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2N4053	P99	2N4253	HF85	2N4427	HF88	3N96	FET31
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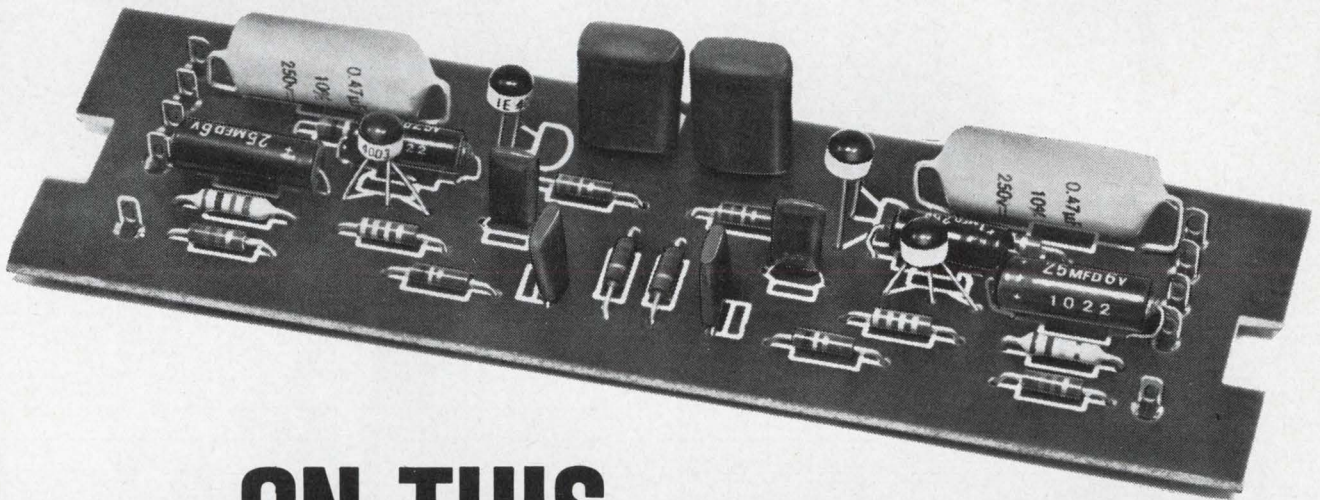
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517	FET33	M101	FET17, FET55	U204	FET63
40460	FET70	M103	FET6	U1277	FET50
40461	FET55, FET70	M511	FET7	U1278	FET45
C680	FET36	MEM511	FET33	U1279	FET41
C681	FET36	MEM520	FET33	U1280	FET38
C682	FET42	MEM551	FET30	U1281	FET56
C683	FET42	MFE2093	FET13, FET22, FET25, FET38	U1282	FET55
C684	FET50	MFE2094	FET13, FET22, FET25, FET42	U1283	FET49
C685	FET50	MFE2095	FET14, FET22, FET25, FET49	U1284	FET41
C6690	FET3	MFE2097	FET57	U1285	FET37
C6691	FET3	MFE2098	FET57	U1286	FET39
C6692	FET1	MFE2133	FET8	U1287	FET58
CM600	FET7	MFE3001	FET45	U1325	FET43
CM601	FET9	MPF103	FET49	UC20	FET42
CM602	FET9	MPF104	FET52	UC21	FET38
CM603	FET10	MPP105	FET56	UC22	FET42
CM640	FET5	P102	FET61	UC23	FET38
CM642	FET9	P1003	FET46	UC40	FET40
CM643	FET10	P1004	FET53	UC41	FET36
CM646	FET10	P1005	FET56	UC42	FET40
CM647	FET11	SJ993	UJT2	UC43	FET36
CP650	FET71	SJ1034	UJT1	UC200	FET57
CP651	FET71	SJ1127	UJT2	UC201	FET7
D1101	FET47	SJ1158	UJT1	UC210	FET55
D1102	FET40	SJ1159	UJT1	UC220	FET49
D1177	FET47	SJ5898	UJT1	UC240	FET50, FET65
D1178	FET40	SU2078	FET31	UC250	FET10
D1180	FET52	SU2079	FET30	UC251	FET7
D1181	FET44	SU2080	FET31	UC400	FET56
D1182	FET37	SU2081	FET30	UC401	FET6
D1183	FET4, FET54	TIS05	FET7, FET16	UC410	FET52
D1184	FET3, FET47	TIS14	FET14, FET17, FET25, FET45, FET66, FET68	UC420	FET45
D1185	FET40	TIS25	FET30	UC450	FET8
D1201	FET52	TIS26	FET29	UC451	FET7
D1202	FET44	TIS27	FET29	UC701	FET38
D1203	FET37	TIS34	FET14, FET21, FET27, FET55, FET66, FET70	UC703	FET38
D1301	FET4, FET54	TIS41	FET11, FET16	UC704	FET41
D1302	FET3, FET47	TIS42	FET8, FET16	UC705	FET45
D1303	FET2, FET40	TIS58	FET53, FET68	UC707	FET53
DE1004	FET5, FET19, FET58, FET67	TIS59	FET56, FET69	UC714	FET53
DN3066A	FET47, FET64	TIXM12	FET71	UC750	FET34
DN3067A	FET40, FET64	TIXM301	FET71	UC751	FET36
DN3068A	FET35, FET64	TIXS11	FET2, FET20, FET28, FET58, FET66, FET67	UC752	FET41
DN3069A	FET52, FET64	TIXS33	FET8, FET16	UC753	FET48
DN3070A	FET44, FET64	TIXS35	FET14, FET21, FET28, FET57, FET66, FET71	UC801	FET35
DN3071A	FET37, FET64			UC803	FET35
DNX1	FET47			UC804	FET38
DNX2	FET38			UC805	FET42
DNX3	FET34			UC807	FET48
DNX4	FET52			UC814	FET42
DNX5	FET44			UC850	FET38



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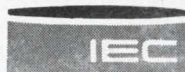
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# 1967 Diode Manufacturers' List

## (According to Device Type)

To find the manufacturers of a specific type of diode, locate the device type in the columns on top. Dots are placed in the column to identify the manufacturers, listed at the left.

To determine the diode product line of a specific manufacturer, locate the company name in the horizontal rows at the left. Dots are placed in that manufacturer's row under each type of diode device that forms a part of his product line.

Manufacturer	General Purpose	Rectifiers	R F	Computer & Hi-Speed	Four Layer	Noise	Matched	Microwave	Varactor & Varicap	Tunnel	Varistor	Zener (Regulator)	Reference (Low Temp. Coefficient Types)	SCR s	SCSS & Gate-Controlled Types	Photo	Special Purpose
Airtron Div., Litton Industries							•	•	•								
Alpha Industries Inc.	•		•	•			•	•	•								N, P
American Electronics Labs, Inc.			•					•	•								N, R, A, E
American Semiconductor Inc.							•					•	•				
Amperex Electronic Corp.	•	•	•	•	•		•		•			•	•	•	•	•	D, F, B
Atlantic Semiconductor Inc.			•														B, H, St
Bell, F. W., Inc.																	Ha
Bendix Semiconductor Div.	•	•															
Bradley Semiconductor Corp.	•	•															
Burroughs Corp.	•			•											•		
Computer Diode Corp.	•	•	•	•			•	•	•		•	•	•				C, B, D, Df, N, R, St, U
Conant Labs.			•														B, Se
Continental Device Corp.	•	•	•	•		•	•				•	•	•				D, F, Df, S, St
Crystalonics Inc.							•	•									
Delco Radio Div., Gen. Motors	•	•															D
Delta Semiconductors Inc.	•	•	•	•		•	•	•				•	•				F
Dickson Electronics Corp.			•				•	•	•			•	•				B, C, D, St, H
Diodes Inc.	•	•		•			•					•					B, D, H, St, S
Eastern Delta Corp.			•								•						B, S, St
Eastron Corp.							•				•						C, St
Edal Industries	•	•					•				•						B, Df, H, S, SE
Edgerton, Germeshausen & Grier																•	R
Electro-Optical Systems Inc.																•	
Electronic Control													•				
Electronic Devices Inc.	•	•										•					B, D, H, M, V
Erie Technological Products	•	•		•			•										B
Fairchild Semiconductor	•	•		•		•	•	•	•		•	•	•		•		A, E, B
Gemini Semiconductors	•		•	•	•		•	•	•	•							A, B, Bi, Df, E, N, P, T
General Electric Co.	•	•	•	•	•		•	•	•	•	•	•	•	•	•		La, P
General Instruments Corp.	•	•	•	•			•	•			•	•	•	•	•		

Need a FREE personal copy of this Directory? Circle number 419.

Complete listing of semiconductor manufacturers starts on page 86.

Get detailed spec sheets and application notes: use the reader-service card!

## Key to special purpose diodes category

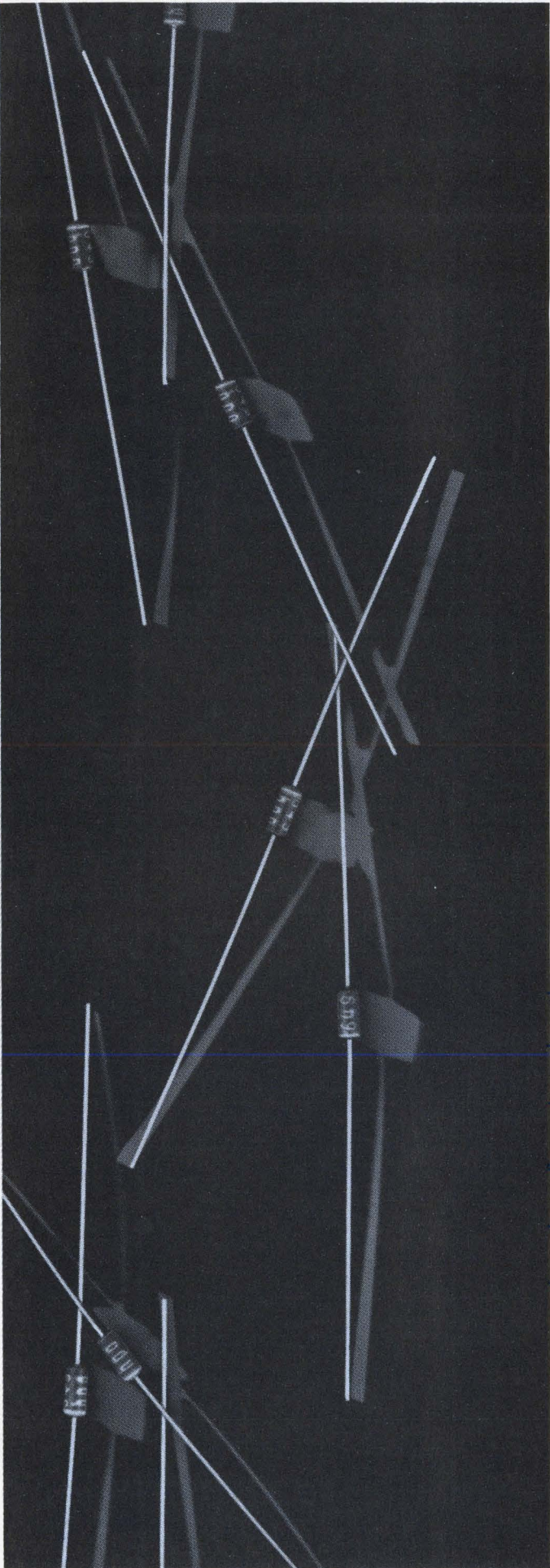
<b>A</b>	= Arrays	<b>N</b>	= Pin diodes
<b>B</b>	= Bridges, stacked, or special assemblies	<b>P</b>	= Snap diodes
<b>Bi</b>	= Bilateral switch	<b>Ph</b>	= Photo SCRs
<b>C</b>	= Multi-junction forward regulators	<b>R</b>	= Radiation detectors
<b>CC</b>	= Constant-current source	<b>S</b>	= Suppressors
<b>D</b>	= TV dampers	<b>Se</b>	= Selenium rectifiers
<b>Df</b>	= Specially diffused silicon diodes	<b>St</b>	= Stabistors
<b>E</b>	= Light emitting diodes	<b>Sym</b>	= Symmetrical switch
<b>F</b>	= Controlled forward conductance diodes	<b>T</b>	= Thin-film applications types
<b>H</b>	= High voltage elements	<b>Tr</b>	= Trigger diode
<b>Ha</b>	= Hall effect generators	<b>U</b>	= Multi-current reference
<b>La</b>	= Lasers	<b>Y</b>	= Relay diode

Manufacturer	Special Purpose																
	General Purpose	Rectifiers	R F	Computer & Hi-Speed	Four Layer	Noise	Matched	Microwave	Varactor & Varicap	Tunnel	Varistor	Zener (Regulator)	Reference (Low Temp. Coefficient Types)	SCRS	SCSs & Gate-Controlled Types	Photo	
General Semiconductors Inc.	•	•				•		•			•	•					B, C, H, U
Green Rectifier Corp.		•								•							B, S, St
H P Associates	•		•	•			•	•								•	E, N, P, F, B
Heliotek Div. Textron Electronics Inc.																•	
Hoffman Electronics Corp.	•	•		•					•		•	•	•				
Hughes Aircraft Co. Microelectronics Div.	•	•		•		•	•	•			•						A
Hunt Electronics Co.														•			Bi, Sym
ITT Semiconductor	•	•	•	•	•	•											
Instrument Systems Corp.																	Ha
International Diode Corp.	•			•			•										
International Electronics Corp.	•	•	•	•			•	•		•	•		•			•	
International Rectifier Corp.	•	•									•	•	•				
I R C Semiconductor	•	•									•	•	•				B
K M C Semiconductor Corp.				•		•	•		•								E, R
Kemtron Electron Prod.																	St, Y
Korad Corp.																	La
Ledex		•															
MSI Electronics Inc.							•	•									
Mallory Semiconductor Co.		•									•						B, Tr, St
MicroSemiconductor Corp.	•	•	•	•		•	•	•			•	•					T, A, B, C, F, H, J
Microstate Electronics Corp.				•		•	•	•	•								E, N, X
Microwave Associates Inc.			•			•	•	•	•								N, P, Df, F
Motorola Semiconductor Products Inc.		•	•		•	•	•	•			•	•	•				CC, B, Tr
National Electronics Corp.													•				
Nucleonic Products Co., Inc.	•	•	•	•		•	•		•	•	•	•			•		B
Ohmite Mfg. Co.	•		•	•			•										
Philco Corp.			•	•			•	•	•							•	B, CC, La, N, P, Sym, T, U, Y, E, A
Power Components Inc.	•	•		•		•		•			•	•					St
Radiation, Inc.																	A
Radio Corp. of America		•							•			•	•		•		B, La

## Key to special purpose diodes category

<b>A</b> = Arrays	<b>N</b> = Pin diodes
<b>B</b> = Bridges, stacked, or special assemblies	<b>P</b> = Snap diodes
<b>Bi</b> = Bilateral switch	<b>Ph</b> = Photo SCRs
<b>C</b> = Multi-junction forward regulators	<b>R</b> = Radiation detectors
<b>CC</b> = Constant-current source	<b>S</b> = Suppressors
<b>D</b> = TV dampers	<b>Se</b> = Selenium rectifiers
<b>Df</b> = Specially diffused silicon diodes	<b>St</b> = Stabistors
<b>E</b> = Light emitting diodes	<b>Sym</b> = Symmetrical switch
<b>F</b> = Controlled forward conductance diodes	<b>T</b> = Thin-film applications types
<b>H</b> = High voltage elements	<b>Tr</b> = Trigger diode
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Manufacturer	General Purpose	Rectifiers	R F	Computer & Hi-Speed	Four Layer	Noise	Matched	Microwave	Varactor & Varicap	Tunnel	Varistor	Zener (Regulator)	Reference (Low Temp. Coefficient Types)	S C R s	SCSS & Gate-Controlled Types	Photo	Special Purpose
Raytheon Co.	•		•	•			•	•	•	•		•				•	E, N
Rectico Inc.		•															
Sanford Miller		•															
Saratoga Semiconductor Div., Espey Mfg.												•	•				
Sarkes Tarzian Inc.	•	•										•		•	•		B, H, Ph, Se
Schauer Mfg. Corp.							•			•	•	•					
Semcor Div., Components Inc.	•				•	•					•	•					
Semicon Inc.	•	•				•							•				H, B, C, St
Semiconductor Devices Inc.				•				•	•								N, P
Semiconductor Specialists Inc.							•				•	•					
Semi-Elements Inc.	•	•	•		•		•	•	•		•					•	E, La
Semtech Corp.	•	•		•			•				•	•					B, H, St
Siemens America	•	•	•	•			•		•	•	•					•	
Silicon Transistor Corp.													•	•			
Slater Electric Inc.		•															B, D, Df, H
Solar Systems Inc.																	Df
Solid State Products Inc.					•								•	•	•		Ph
Solitron Devices Inc.	•	•	•			•	•		•		•	•					N
Sylvania Electric Products	•	•	•	•		•	•	•	•	•	•			•			N
Syntron Co.		•												•			B, H
T R W Semiconductors	•	•	•	•		•	•	•			•	•					St
Texas Instruments Inc.	•	•	•	•	•		•	•	•	•	•	•	•	•	•	•	E, St, A, F, N
Transitron Electronic Corp.	•	•	•	•		•	•	•	•		•	•	•	•			U
Trio Laboratories Inc.											•						
Unitrode Corp.	•	•		•	•		•				•	•					B, C, H, N, S
Vactec Inc.																•	
Varian/Bomac Div.							•	•	•								N, P
Varo, Inc., Special Products Div.		•		•													H, B, D, Df
Wagner Electric	•												•				B
Western Semiconductor Inc.	•	•		•	•		•	•			•	•	•	•			B, DF
Westinghouse Electric Corp., Semiconductor Div.	•	•		•									•	•			



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Typical specifications		
Forward Current $I_F$		Breakdown Voltage $V_{BR}$
20 mA min. @ $V_F=1.0$ V 1.0 mA min. @ $V_F=0.4$ V		10 V @ $I_R=10$ $\mu$ A
Leakage Current $I_R$	Lifetime $\tau$	Price
100 nA @ $V_R=-5.0$ V	120 ps	1 to 99, \$3.00 100 to 999, \$2.25

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# 1. DTL (continued)

Logic Function	Type	Model	Mfr.	Propaga- tion Delay (ns)	Fan-in		Fan-out		Power Diss. mW (/ = per gate)	Supply Voltage (Volts)	Logic Levels (Volts)		Noise Margin (mV)	Temp Range (°C)	Package Type	Remarks
					Typ.	Max.	Typ.	Max.			'0'	'1'				
Gates D	Exclusive-OR  17	Dual 4-input	MC844	MO	40	-	-	27	20	5	0.2	5	500	0 to 75	A, C	Modified DTL
		Dual 4-input	MC844P	MO	40	-	-	27	20	5	0.2	5	-	0 to 75	G, P, DIP	Mod-DTL
		Dual 4-input	MC944	MO	40	-	-	27	20	5	0.2	5	500	-	A, C	Modified DTL
			341BG	AL	60	4	-	6	70	12	1200	12000	4800	-	G	
			341CG	AL	60	4	-	6	70	12	1200	12000	4800	-	G	
			341CJ	AL	60	4	-	6	70	12	1200	12000	4800	-	G, DIP	
			SN5370	TI	90	-	-	-	10	20/	3-4	-	-	300	-	D
	SN7370	TI	90	-	-	-	10	20/	3-4	-	-	-	0-70	D		
Gate Expanders E	-	RC226	RA	2	2,3	6	-	-	-	-	-	-	-	-	-	-
	-	RC246	RA	2	-	6	-	-	-	-	-	-	-	-	-	-
	-	A04	SI	4	-	6	-	-	-	-	-	-	-	-	A, D	Diode Array
Interface F	Input	361BG	AL	30	1	-	8	50	12	1200	12000	4800	-	G, C	Dip	
	Input	361CG	AL	30	1	-	8	50	12	1200	12000	4800	0 to +100	G, C		
	Input	361CJ	AL	30	1	-	8	50	12	1200	12000	4800	0 to +70	G		
	Output	362BG	AL	11	1	-	6	150	12	1200	12000	4800	-	G, C		
	Output	362CG	AL	11	1	-	6	150	12	1200	12000	4800	0 to +100	G, C		
	Output	362CJ	AL	30	1	-	6	150	12	1200	12000	4800	0 to +70	G, DIP		
Inverter G	Hex	RD-220	RAD	7	-	1	-	8	10	5.0	0.25	4.5	800	-	D	*Node inputs
	Hex*	RD-234	RAD	7	-	-	-	8	10	5.0	0.25	4.5	-	D		
	Hex	RD-320	RAD	7	-	1	-	5	10	5.0	0.25	4.5	800	-	D	*Node inputs
	Hex*	RD-334	RAD	7	-	-	-	5	10	5.0	0.25	4.5	-	D		
	Hex	RD-520	RAD	7	-	1	-	8	10	5.0	0.25	4.5	800	0-75	D	*Node inputs
	Hex*	RD-534	RAD	7	-	-	-	8	10	5.0	0.25	4.5	-	D		
	Hex*	RD-553	RAD	7	-	-	-	8	10	5.0	0.25	4.5	-	D	*Node inputs *Output break-	
	Hex	RD-223	RAD	12	-	1	-	10	5.0	0.55	*35	800	-	D		
	Quad	SE181	SIG	20	-	1	-	6	20	+4	0.4	3.9	1000	-	A	
	Hex Inverter	937	SW	20	-	1	9	-	6	5	0.2	5.0	1000	-	A, C	
	Hex Inverter	936	SW	25	-	1	10	-	6	5	0.2	5.0	1000	-	A, C	
	Hex	993751	FA	30	-	-	-	7	150	4.5-5.5	0.4	3.8	1000	-	C, G	
	Hex	993759	FA	30	-	-	-	7	160	5	0.5	4.3	1000	0 to +75	C, G	
	Hex	993651	FA	35	-	-	-	8	90	4.5-5.5	0.4	2.6	1000	-	C, G	
	Hex	993659	FA	35	-	-	-	8	100	5	0.45	2.6	1000	0 to +75	C, G	
	Dual	MC1115	MO					-	250	-	-	-	-	-	A	
Logic Amplifier H	-	8201	VAR	10	1	-	4	-	50	6, 3, -3	0.5	3.5	-	-	-	TF
	-	8202	VAR	-	2	-	8	-	100	6, 3, -3	0.5	3.5	-	-	-	TF
Multivibrators I	Single-shot	NC/PC16	GI	8	-	-	-	5	200	12, 4, 2	0	5	-	-	A, E	MC RCDT
	Single-shot	PC-18	GI	8	-	-	-	5	200	12, 4, 2	0	5	-	-	E	MC RCDT
	Monostable	728	SW	24	-	5	-	16	25	5	0.2	5.0	1000	-	A, C	
	2-input	DT <sub>7</sub> L951	FA	25	-	-	-	10	35	5.0	0.2	5	950	-	A, C	RA, SSD, ITT
	Monostable	MC851	MO	25	-	-	-	10	30	5	0.2	5	-	0 to 75	A, C, G,	Mod-DTL
	Monostable	MC951	MO	25	-	-	-	10	30	5	0.2	5	-	-	A, C	Mod-DTL
	Monostable	951	SW	25	2	-	12	-	32	5	0.2	5.0	1000	-	A, C	Expandable
	Single-shot	A08	SI	30	-	1	-	5	42	5	1.0	2.7	900	-	A, D	
	Single-shot	A48	SI	30	-	1	-	5	42	5	1.1	2.7	700	0 to 70	A, D	TF
	Single-shot	8203	VAR	30	-	-	2	4	100	6, 3	0.5	3.5	-	-	A	
	Single-shot	WC218	WH	40	-	2	-	8	105	5.7-6.3	1.0	2.0	600	0 to 75	A, C	
	Monostable	SN15851	TI	50	-	-	-	-	-	4.5-5.5	-	-	750	0-75	D, DIP	
	Single-shot	SN15951	TI	50	-	-	-	-	-	4.5-5.5	-	-	750	-	D	
	Single-shot	342BG	AL	60	1	-	-	6	100	12	1200	12000	4800	-	G	
	Dual 1-shot	342CG	AL	60	1	-	-	6	100	12	1200	12000	4800	0 to +100	G	
	Dual 1-shot	342CJ	AL	60	1	-	-	6	100	12	1200	12000	4800	0 to +70	G, DIP	
	Dual 1-shot	SN5380	TI	100	-	-	-	10	30	3-4	-	-	300	-	D	Modified DTL
Single-shot	SN7380	TI	100	-	-	-	10	30	3-4	-	-	-	0-70	D		
Single-shot	SE160	SIG	-	-	2	-	4	25	+4,-2	0.4	3.9	1000	-	A, C		
Single-shot	SE161	SIG	-	-	1	-	4	25	+4	0.4	3.9	1000	-	A, F		
Shift Bit J	-	RC205T	RA	200	-	-	4	-	75	6	-	-	0.55	-	-	-

Temperature range is -55 to 125°C unless otherwise stated.

Circle as many numbers on the reader-service card as you like.

Complete listing of semiconductor manufacturers starts on page 86.

Reader-Service cards are good all year.











# 3. Transistor-Transistor Logic

	Logic Function	Type	Model	Mfr.	Propagati- on Delay (ns)	Fan-in		Fan-out		Power Diss. mW (/= per gate)	Supply Voltage (Volts)	Logic Levels (Volts)		Noise Margin (mV)	Temp Range (°C)	Package Type	Remarks	
						Typ.	Max.	Typ.	Max.			'0'	'1'					
A	Half		SG90, SG91	SY	12	-	-	6	20	15	-	-	-	1000	-	-	Differ in Temp & F.O.	
	2-bit		SN5482	TI	†15	-	-	-	10	175	4.5-5.5	0.4	2.4	1000	-	D	†Carry	
	2-bit		SN7482	TI	†15	-	-	-	10	175	4.75-5.25	0.4	2.4	1000	0 to 70	D, DIP	†Carry	
	4-bit		SN7483	TI	†29	-	-	-	10	350	4.75-5.25	0.4	2.4	1000	0 to 70	D, DIP	†Carry	
	Full		SN5480	TI	Add: 70 Carry: 8	-	-	-	-	105	4.5-5.5	-	-	1000	-	D	Includes gating	
Full		SN7480	TI	Add: 70 Carry: 8	-	-	-	-	105	4.75-5.25	-	-	1000	0 to 70	D	Includes gating		
B	R-S		SF10, SF11	SY	12	-	-	6	20	15	-	-	-	1000	-	-	Differ in Temp & F.O.	
	Clocked		SF12, SF13	SY	12	-	-	6	20	15	-	-	-	1000	-	-	Differ in Temp & F.O.	
	Single-phase		SF20, SF21	SY	12	-	-	-	-	-	-	-	-	-	-	-	Differ in Temp & F.O.	
			SF22, SF23	SY	12	-	-	-	-	-	-	-	-	-	-	-	Differ in Temp & F.O.	
	1	J-K		SF30, SF31	SY	12	-	-	6	20	15	-	-	-	1000	-	-	Differ in Temp & F.O.
		J-K		SF32, SF33	SY	12	-	-	-	-	-	-	-	-	-	-	-	Differ in Temp & F.O.
		J-K		SF50, 51	SY	12	-	4	-	15	15	8	0.26	3.3	1000	-	D, G	-
		J-K		SF52, 53	SY	12	-	4	-	12	15	8	0.26	3.3	1000	0, +75	D, G	-
		J-K Master Slave		900051	FA	15	-	-	-	10	50	4.5-5.5	0.2	2.7	1000	-	C, G	JJJ, KK̄, JK
		J-K Master Slave		900151	FA	15	-	-	-	10	70	4.5-5.5	0.2	2.7	1000	-	C, G	JJJ, KK̄, JK
		Dual J-K		902051	FA	15	-	-	-	10	-	4.5-5.5	0.2	2.7	1000	-	C, G	-
		Dual J-K-K̄		902151	FA	15	-	-	-	10	-	4.5-5.5	0.2	2.7	100	-	G	-
		J-K Flip-Flop		W6F251	WH	16.0	-	3	15	6	40	5.0	1.1	1.6	800	-	D	-
		J-K Master Slave		900059	FA	17	-	-	-	8	55	4.5-5.5	0.25	3.2	1050	0 to 70	C, G	JJJ, KK̄, JK
		J-K Master Slave		900159	FA	17	-	-	-	8	75	4.5-5.5	0.25	3.2	1050	0 to 70	C, G	JJJ, KK̄, JK
		Dual J-K		902059	FA	17	-	-	-	8	-	4.5-5.5	0.25	3.2	1050	0 to 70	C, G	-
		Dual J-K-K̄		902159	FA	17	-	-	-	8	-	4.5-5.5	0.25	3.2	1050	0 to 70	G	-
	J-K		SN54H71	TI	18	†4	-	-	10	90	4.5-5.5	0.4	2.4	1000	-	D	†Gated input	
	J-K		SN54H72	TI	18	†3	-	-	10	80	4.5-5.5	0.4	2.4	1000	-	D	†Gated input	
	J-K		SN74H71	TI	18	4	-	-	10	90	5.25	0.4	2.4	1000	0 to 70	D, DIP	-	
	J-K		SN74H72	TI	18	3	-	-	10	80	5.25	0.4	2.4	1000	0 to 70	D, DIP	-	
	Dual		TFF 3011	TR	18	-	3	-	20	30	5-6	0.20	3.0	1000	-	A, F	-	
	Dual		TFF 3013	TR	18	-	3	-	7	30	5-6	0.20	3.0	1000	-	A, F	-	
	Dual		TFF 3015	TR	18	-	2	-	20	30	5-6	0.20	3.0	1000	-	A, F	-	
	Dual		TFF 3017	TR	18	-	2	-	7	30	5-6	0.20	3.0	1000	-	A, F	-	
	2	AND inputs		TFF3241-44	TR	18	-	1	-	10	100	5	0.45	3.5	1000	0 to 75	D, P, DIP	High speed
		OR inputs		TFF3341-44	TR	18	-	1	-	10	100	5	0.45	3.5	1000	0 to 75	D, P, DIP	High speed
		Enable-OR input		TFF3441-44	TR	18	-	1	-	10	100	5	0.45	3.5	1000	0 to 75	D, P, DIP	High speed
		Dual		SE826	SIG	20	-	-	-	5	50	+5	0.4	2.4	1000	-	F	-
		J-K		579B	AL	20	3	-	-	9	30	5	400	3800	1000	-	-	-
		Dual		SF120-121	SY	50 MHz	-	-	6	11	55/ FF	-	-	-	-	-	D, G	Separate clock, RA
		Dual		SF122-123	SY	50 MHz	-	-	5	9	55/ FF	-	-	-	-	-	D, G	Separate clock
Dual			SF130-131	SY	50 MHz	-	-	6	11	55/ FF	-	-	-	-	-	D, G	Common clock, RA	
Dual			SF132-133	SY	50 MHz	-	-	5	9	55/ FF	-	-	-	-	-	D, G	Common clock	
3	J-K (AND inputs)		SF200-201	SY	50 MHz	-	-	6	11	55	-	-	-	-	-	D, G	RA	
	J-K (AND inputs)		SF202-203	SY	50 MHz	-	-	5	9	55	-	-	-	-	-	D, G	RA	
	J-K (OR inputs)		SF210-211	SY	50 MHz	-	-	6	11	55	-	-	-	-	-	D, G	RA	
	J-K (OR inputs)		SF212-213	SY	50 MHz	-	-	5	9	55	-	-	-	-	-	D, G	RA	
	J-K		SF60, 61	SY	25	-	4	-	15	45	5.0	.26	3.3	1000	-	D, G	Separate clock, RA	
	Dual		SF100-101	SY	35 MHz	-	-	6	11	55/ FF	-	-	-	-	-	D, G	RA	
4	Dual		SF102-103	SY	35 MHz	-	-	5	9	55/ FF	-	-	-	-	-	D, G	Common clock, RA	
	Dual		SF110-111	SY	35 MHz	-	-	6	11	55/ FF	-	-	-	-	-	D, G	Common clock	
	Dual		SF112-113	SY	35 MHz	-	-	5	9	55/ FF	-	-	-	-	-	D, G	Common clock	
	Single		SE825	SIG	30	-	-	-	10	50	+5	0.4	2.4	1000	-	F	-	
	Dual latch		SN5474	TI	30	-	-	-	10	40/ff	4.5-5.5	-	-	1000	-	D	-	
	Dual latch		SN7474	TI	30	-	-	-	10	40/ff	4.75-5.25	-	-	1000	0 to 70	D	-	
†Dual FF		SN7476N	TI	30	-	-	-	10	40/ff	4.75-5.25	0.4	2.4	1000	0 to 70	DIP	†Clear & Preset		
4	4-input with buffer		TFF3111-14	TR	30	-	1	-	15	75	5	0.45	3.5	1000	0 to 75	D, P, DIP	-	
	2-input with buffer		TFF3115-18	TR	30	-	1	-	15	75	5	0.45	3.5	1000	0 to 75	D, P, DIP	-	
	4-input w/o buffer		TFF3121-24	TR	30	-	1	-	15	75	5	0.45	3.5	1000	0 to 75	D, P, DIP	-	
	2-input w/o buffer		TFF3125-28	TR	30	-	1	-	15	75	5	0.45	3.5	1000	0 to 75	D, P, DIP	-	
	Dual J-K		TFF3173-74	TR	30	-	1	-	7	150	5	0.45	3.5	1000	0 to 75	D, P, DIP	-	
	3J-3K		TFF3161-64	TR	30	-	1	-	15	75	5	0.45	3.5	1000	0 to 75	D, P, DIP	-	
	2J-2K		TFF3165-68	TR	30	-	1	-	15	75	5	0.45	3.5	1000	0 to 75	D, P, DIP	-	
	Dual 3J-3K		TFF3181-84	TR	30	-	1	-	15	150	5	0.45	3.5	1000	0 to 75	D, P, DIP	22 leads	

Temperature range is -55 to 125°C unless otherwise stated.

### 3. TTL (continued)

Binary Elements	Logic Function	Type	Model	Mfr.	Propagati- on Delay (ns)	Fan-in		Fan-out		Power Diss. mW (/= per gate)	Supply Voltage (Volts)	Logic Levels (Volts)		Noise Margin (mV)	Temp Range (°C)	Package Type	Remarks	
						Typ.	Max.	Typ.	Max.			'0'	'1'					
B	Dual J-K	S8826	SIG	30 MHz	—	—	—	10	—	5.0	0.45	2.4	1000	—	F			
	J-K	SF250,251	SY	30MHz	—	—	—	12	55	—	0.25	3.5	1000	—	D, G			
	J-K	SF252,253	SY	30MHz	—	—	—	10	55	—	0.25	3.5	1000	0, +75	D, G			
	J-K	SF260,261	SY	30MHz	—	—	—	12	55	—	0.25	3.5	1000	—	D, G			
	J-K	SF262,263	SY	30MHz	—	—	—	10	55	—	0.25	3.5	1000	0, +75	D, G			
	J-K	SWF250	SW	30MHz	6	—	—	12	—	55	4.5-6	0.4	3	1000	—	—		
	J-K	SWF251	SW	30MHz	6	—	—	6	—	55	4.5-6	0.4	3	1000	—	—		
	J-K	SWF252	SW	30MHz	6	—	—	10	—	55	4.5-6	0.45	3	900	0 to +75	—		
	J-K	SWF253	SW	30MHz	6	—	—	5	—	55	4.5-6	0.45	3	900	0 to +75	—		
	J-K	SWF260	SW	30MHz	6	—	—	12	—	55	4.5-6	0.4	3	1000	—	—		
	J-K	SWF261	SW	30MHz	6	—	—	6	—	55	4.5-6	0.4	3	1000	—	—		
	J-K	SWF262	SW	30MHz	6	—	—	10	—	55	4.5-6	0.45	3	900	0 to +75	—		
	J-K	SWF263	SW	30MHz	6	—	—	5	—	55	4.5-6	0.45	3	900	0 to +75	—		
	Master/Slave	SN5472	TI	35	—	—	—	—	10	50	4.5-5.5	—	—	1000	—	D		
	Dual M/S	SN5473	TI	35	—	—	—	—	10	50	4.5-5.5	—	—	1000	—	D		
	Master/Slave	SN7472	TI	35	—	—	—	—	10	50	4.75-5.25	—	—	1000	0 to 70	D		
	Dual M/S	SN7473	TI	35	—	—	—	10	50/ff	5.25	—	—	—	1000	0 to 70	D		
		J-K	SN5470	TI	40	—	—	—	10	60	4.5 to 5.5	—	—	1000	—	D	Single-phase	
		J-K	SN7470	TI	40	—	—	—	10	60	4.75-5.25	—	—	1000	0-70	D	Single phase	
		J-K/R-S	SN54948	TI	40	—	—	—	10	60	4.5-5.5	—	—	1000	—	D		
		J-K/R-S	SN74948	TI	40	—	—	—	10	60	4.75-5.25	—	—	1000	0-70	D		
		J-K	SW5470	SW	40	6	—	—	10	—	65	4.5-5.5	0.4	3	1000	—	—	
		J-K	SW7470	SW	40	6	—	—	10	—	65	4.8-5.3	0.45	3	900	0 to +75	—	
		R-S	SN54L71	TI	47	†3	—	—	10	—	3.5	4.5-5.5	0.3	2.4	1000	—	D	†Gated input
		J-K	SN54L72	TI	47	†3	—	—	10	—	3.5	4.5-5.5	0.3	2.4	1000	—	D	†Gated input
	Dual J-K	SN54L73	TI	47	—	—	—	10	—	†3.5	4.5-5.5	0.3	2.4	1000	—	D	†per ff	
	J-K	MC516	MO	50	—	—	—	15	—	50	5	0.26	3.3	1000	—	C		
	J-K	MC566	MO	50	—	—	—	7	—	50	5	0.26	3.3	1000	—	C		
	J-K	S8825	SIG	20 MHz	—	—	—	10	—	5.0	0.45	2.4	1000	—	F			
	R-S	SWF10	SW	20MHz	6	—	—	15	—	30	4.5-6	0.4	3	1000	—	—		
	R-S	SWF11	SW	20MHz	6	—	—	7	—	30	4.5-6	0.4	3	1000	—	—		
	R-S	SWF12	SW	20MHz	6	—	—	12	—	30	4.5-6	0.45	3	900	0 to +75	—		
	R-S	SWF13	SW	20MHz	6	—	—	6	—	30	4.5-6	0.45	3	900	0 to +75	—		
	Dual	SWF20	SW	20MHz	6	—	—	15	—	35	4.5-6	0.4	3	1000	—	—		
	Dual	SWF21	SW	20MHz	6	—	—	7	—	35	4.5-6	0.4	3	1000	—	—		
	Dual	SWF22	SW	20MHz	6	—	—	12	—	35	4.5-6	0.45	3	900	0 to +75	—		
	Dual	SWF23	SW	20MHz	6	—	—	6	—	35	4.5-6	0.45	3	900	0 to +75	—		
	J-K	SWF50	SW	20MHz	6	—	—	15	—	50	4.5-6	0.4	3	1000	—	—		
	J-K	SWF51	SW	20MHz	6	—	—	7	—	50	4.5-6	0.4	3	1000	—	—		
	J-K	SWF52	SW	20MHz	6	—	—	12	—	50	4.5-6	0.45	3	900	0 to +75	—		
	J-K	SWF53	SW	20MHz	6	—	—	6	—	50	4.5-6	0.45	3	900	0 to +75	—		
	÷ 12 Counter	SN7492	TI	60	†2	—	—	10	—	32/ff	4.75-5.25	0.4	2.4	1000	0 to 70	D, DIP	†Gated reset	
	4-bit Binary	SN7493	TI	75	†2	—	—	10	—	32/ff	4.75-5.25	0.4	2.4	1000	0 to 70	D, DIP	†Gated reset	
	Gated RS FF	MC652	MO	80	—	6	—	4	—	200	10	10	.70	5V	0 to 75	A, C		
	J-K	S39B	AL	100	3	—	—	6	—	14	5	250	3800	1000	—	F		
	Dual, A.C.	S8424	SIG	9 MHz	—	—	—	7	—	—	5.0	0.35	3.4	1000	—	F		
	Dual, A.C.	SE424	SIG	9 MHz	—	—	—	7	—	9.0	4.0	0.2	2.8	1000	—	F, G	also 0°C to 70°C 15°C to 55°C	
	J-K	509B	AL	180	3	—	—	6	—	6	5	250	3800	1000	—	—		
	R-S	MC413	MO	—	—	—	—	12	—	30	5	0.26	3.3	1000	0 to 75	C, G, DIP		
	J-K	MC415	MO	—	—	—	—	12	—	40	5	0.26	3.3	1000	0 to 75	C, G, DIP		
	J-K	MC416	MO	—	—	—	—	12	—	50	5	0.26	3.3	1000	0 to 75	C, G, DIP		
	R-S	MC463	MO	—	—	—	—	6	—	30	5	0.26	3.3	1000	0 to 75	C, G, DIP		
	J-K	MC465	MO	—	—	—	—	6	—	40	5	0.26	3.3	1000	0 to 75	C, G, DIP		
	J-K	MC466	MO	—	—	—	—	6	—	50	5	0.26	3.3	1000	0 to 75	C, G, DIP		
	R-S	MC513	MO	—	—	—	—	15	—	30	5	0.26	3.3	1000	—	C		
	"AND" J-K	MC515	MO	—	—	—	—	15	—	40	5	0.26	3.3	1000	—	C		
	R-S	MC563	MO	—	—	—	—	7	—	30	5	0.26	3.3	1000	—	C		
	"AND" J-K	MC565	MO	—	—	—	—	7	—	40	5	0.26	3.3	1000	—	C		
C	Dual 4-input	900959	FA	8	—	—	—	25	22/	4.5-5.5	0.25	3.2	1050	0 to 70	C, G			
	Dual 4-input	900951	FA	—	—	—	—	30	20/	4.5-5.5	0.2	2.7	1000	—	C, G			
	Dual 4-input	S8855	SIG	12	—	—	4	—	26	—	5.0	0.45	2.4	1000	—	F		
D	Dual	SE855	SIG	15	—	4	—	30	25	+5	0.4	2.4	1000	—	F			
	Triple 2-input	SG160, 161	SY	15	—	—	—	15	15	—	0.26	3.3	1000	—	D, G			
	Triple 2-input	SG162, 163	SY	15	—	—	—	12	15	—	0.26	3.3	1000	0 to 75	D, G			
	Dual 4-input	SN54932	TI	18	—	—	—	30	25/	4.5-5.5	—	—	1000	—	D			
	Dual 4-input	SN74932	TI	18	—	—	—	30	25/	4.75-5.25	—	—	1000	0 to 70	D			
	Quad 2-input	TNG5511-14	TR	18	—	1	—	40	50	5	0.45	3.5	10000	0 to 75	D, P, DIP			
	Dual 4-input	SE4SJ	SIG	25	—	4	—	20	—	7.0	4.0	0.2	2.8	1000	—	F, G	also 0°C to 70°C 15°C to 55°C	
	Dual 4-input	SG130, 131	SY	25	—	—	—	30	30	—	0.26	3.3	1000	—	D, G			
	Dual 4-input	SG132, 133	SY	25	—	—	—	24	30	—	0.26	3.3	1000	0 to 75	D, G			
	Dual 4-input	540B	AL	25	4	—	—	25	30	5	250	3800	1000	—	—	w/ex & no pull up		
	Dual 4-input	541B	AL	25	4	—	—	25	40	5	250	3800	1000	—	—	w/ex & no pull up		
	2 NAND-2 NOR	542B	AL	25	2	—	—	15	30	7/4	250	3800	1000	—	—			

Temperature range is —55 to 125°C unless otherwise stated.

### 3. TTL (continued)

Drivers/Buffers	Logic Function	Type	Model	Mfr.	Propagation Delay (ns)	Fan-in		Fan-out		Power Diss. mW (/ = per gate)	Supply Voltage (Volts)	Logic Levels (Volts)		Noise Margin (mV)	Temp Range (°C)	Package Type	Remarks	
						Typ.	Max.	Typ.	Max.			'0'	'1'					
D	2	Dual 4-input	580B	AL	25	4	--	28	100	5	400	3800	1000	--	--	w/ex & no pull up		
		2 NAND-2 NOR	582B	AL	25	2	--	40	40	7/4	400	3800	1000	--	--			
		2 NAND-2 NOR	585B	AL	25	2	--	15	40	7/4	400	3800	1000	--	--			
		Dual 4-input	S8455	SIG	28	4	4	20	20	5.0	0.35	3.4	1000	--	F			
		Dual 4-input	511B	AL	30	4	--	10	20	5	250	3800	1000	--	--	w/ex & no pull up		
		Quad 2-input	TNG5611-12	TR	--	--	1	60mA	50	5	0.6	--	1000	0 to 75	D,P,DIP	External output		
E	1	Triple	SN54H11	TI	11	--	3	--	10	35	5,5	0,4	2,4	1000	--	D		
		Dual	SN54H21	TI	11	--	4	--	10	35	4,5-5,5	0,4	2,4	1000	--	D	tper gate	
		Triple	SN74H11	TI	11	--	3	--	10	35	5,25	0,4	2,4	1000	0 to 70	D, DIP		
		Dual	SN74H21	TI	11	--	4	--	10	35	5,25	0,4	2,4	1000	0 to 70	D, DIP		
		Dual 4-input	MC511	MO	--	--	--	--	--	5	--	--	--	--	--	C		
	Dual 4-input	MC561	MO	--	--	--	--	--	5	--	--	--	--	--	C	Expandable		
	2	Dual 4-input	900651	FA	2	--	--	--	--	4,5-5,5	--	--	--	--	0 to 70	C, G	Extender	
		Dual 4-input	900659	FA	2	--	--	10	--	4,5-5,5	--	--	--	--	0 to 70	C, G	Extender	
		Dual Exclusive OR	900551	FA	7	--	6	--	10	25	4,5-5,5	0,2	2,7	1000	--	C, G	Expandable	
		Quad 4-input	900851	FA	7	--	6	--	10	25	4,5-5,5	0,2	2,7	1000	--	C, G	Expandable	
		Dual Exclusive OR	900559	F	9	--	6	--	8	25	4,5-5,5	0,25	3,2	1050	0 to 70	C, G	Expandable	
		Quad 4-input	900859	FA	9	--	6	--	8	25	4,5-5,5	0,25	3,2	1050	0 to 70	C, G	Expandable	
		Dual 2-input	SG70-71	SY	12	--	--	7	15	20/	--	--	--	--	--	D, G	Expandable, RA	
			Dual 2-input	SG72-73	SY	12	--	6	12	20/	--	--	--	0 to 75	D, G	Expandable		
	3	AND/OR	Quad 2-input	MC409	MO	--	--	--	--	5	--	--	--	0 to 75	C, G, DIP			
			Dual 4-input	MC410	MO	--	--	--	--	5	--	--	--	0 to 75	C, G, DIP			
			Dual 4-input	MC411	MO	--	--	--	--	5	--	--	--	0 to 75	C, G, DIP			
			Quad 2-input	MC459	MO	--	--	--	--	5	--	--	--	0 to 75	C, G, DIP			
			Dual 4-input	MC460	MO	--	--	--	--	5	--	--	--	0 to 75	C, G, DIP			
			Dual 4-input	MC461	MO	--	--	--	--	5	--	--	--	0 to 75	C, G, DIP			
			Quad 2-input	MC509	MO	--	--	--	--	5	--	--	--	--	--	C		
			Dual 4-input	MC510	MO	--	--	--	--	5	--	--	--	--	--	C		
			Quad 2-input	MC559	MO	--	--	--	--	5	--	--	--	--	--	C		
			Dual 4-input	MC560	MO	--	--	--	--	5	--	--	--	--	--	C		
			Quad 2-input	SN54H52	TI	6	9	--	10	22	5,25	0,4	2,4	1000	0 to 75	C, G, DIP	Expandable	
			Quad 2-input	MC451	MO	12	--	--	6	30	5	0,26	3,3	1000	0 to 75	C, G, DIP	Expandable	
			J-K Flip-Flop	W6F261	WH	16.0	--	2	15	6	50	5,0	1,1	1,6	800	--	D	
	4	AND/OR/NOT	Quad 2-input	SG150-151	SY	4	--	--	--	20	--	--	--	--	--	D, G	RA	
			Quad 2-input	SG152-153	SY	4	--	--	--	15/	--	--	--	--	--	D, G		
			Dual 2 & 3-input	SG290-291	SY	7	--	--	--	15/	--	--	--	--	--	D, G	RA	
			Dual 2 & 3-input	SG292-293	SY	7	--	--	--	15/	--	--	--	--	--	D, G		
			Triple 3-input	SG300-301	SY	7	--	--	6	11	36	--	--	--	--	D, G	Expandable, RA-	
			Triple 3-input	SG302-303	SY	7	--	--	5	9	--	--	--	--	0 to 75	D, G	Expandable, RA-	
			Dual 2-input	SG310-311	SY	7	--	--	6	11	30/	--	--	--	--	D, G	Expandable, RA	
			Dual 2-input	SG312-313	SY	7	--	--	5	9	30/	--	--	--	0 to 75	D, G	Expandable	
			Dual 4-input	SWG210	SW	7	4	--	12	--	30	4,5-6	0,4	3	1000	--	--	Expandable
			Dual 4-input	SWG211	SW	7	4	--	6	--	30	4,5-6	0,4	3	1000	--	--	Expandable
			Dual 4-input	SWG212	SW	7	4	--	10	--	30	4,5-6	0,45	3	900	0 to +75	--	Expandable
			Dual 4-input	SWG213	SW	7	4	--	5	--	30	4,5-6	0,45	3	900	0 to +75	--	Expandable
			Expandable Quad	SWG250	SW	7,5	9	--	6	--	43	4,5-6	0,4	3	1000	--	--	
			Expandable Quad	SWG251	SW	7,5	9	--	6	--	43	4,5-6	0,4	3	1000	--	--	
			Expandable Quad	SWG252	SW	7,5	9	--	10	--	43	4,5-6	0,45	3	900	0 to +75	--	
			Expandable Quad	SWG253	SW	7,5	9	--	5	--	43	4,5-6	0,45	3	900	0 to +75	--	
			Dual shaper/delay	SG80-81	SY	11	--	--	7	15	30/	--	--	--	--	--	D, G	Non-inverting, RA
			Dual shaper/delay	SG82-83	SY	11	--	6	12	30/	--	--	--	0 to 75	D, G	Non-inverting		
			Dual 4-input	SG280-281	SY	11	--	5	10	38/	--	--	--	--	--	D, G	Non-inverting, RA	
	5	AND/OR/NOT	Dual 4-input	SG282-283	SY	11	--	4	8	38/	--	--	--	0 to 75	D, G	Non-inverting		
			Quad 2-input	MC401	MO	12	--	--	12	30	5	0,26	3,3	1000	0 to 75	C, G, DIP	Expandable	
			Triple 3-input	MC454	MO	12	--	--	6	25	5	0,26	3,3	1000	0 to 75	C, G, DIP	Expandable	
			Dual	SWG5A	SW	12	--	3	--	15	5	0,5	3,0	1000	--	A		
			Dual	SWG5B	SW	12	--	4	--	15	5	0,5	3,0	1000	--	A		
			Dual 4-input	SWG110	SW	13	20	--	15	--	20	4,5-6	0,4	3	1000	--	--	Expandable
			Dual 4-input	SWG111	SW	13	20	--	7	--	20	4,5-6	0,4	3	1000	--	--	Expandable
			Dual 4-input	SWG112	SW	13	20	--	12	--	20	4,5-6	0,45	3	900	0 to +75	--	Expandable
			Dual 4-input	SWG113	SW	13	20	--	6	--	20	4,5-6	0,45	3	900	0 to +75	--	Expandable
			Quad 2-input	SWG50	SW	14	20	--	15	--	20	4,5-6	0,4	3	1000	--	--	Expandable
			Quad 2-input	SWG51	SW	14	20	--	7	--	20	4,5-6	0,4	3	1000	--	--	Expandable
			Quad 2-input	SWG52	SW	14	20	--	12	--	20	4,5-6	0,45	3	900	0 to +75	--	Expandable
			Quad 2-input	SWG53	SW	14	20	--	6	--	20	4,5-6	0,45	3	900	0 to +75	--	Expandable
			Dual	SWG21	SW	15	3	--	7	--	15	5	0,5	3,0	1000	--	A	OR Expandable
			Triple 3-input	SWG100	SW	15	20	--	15	--	25	4,5-6	0,4	3	1000	--	--	Expandable
	Triple 3-input	SWG101	SW	15	20	--	7	--	25	4,5-6	0,4	3	1000	--	--	Expandable		
	Triple 3-input	SWG102	SW	15	20	--	12	--	25	4,5-6	0,45	3	900	0 to +75	--	Expandable		
	Triple 3-input	SWG103	SW	15	20	--	6	--	25	4,5-6	0,45	3	900	0 to +75	--	Expandable		
	Quad 2 -input	SN7453	TI	15	--	--	--	10	25	4,75-5,25	--	--	1000	0 to 70	D			
	6	AND-OR-Inverter	--	SN54H53	TI	6	24	--	--	10	22	5,25	0,4	2,4	1000	--	D	Expandable
			Dual	SN54H50	TI	6	20	--	--	10	22	5,5	0,4	2,4	1000	--	D	Expandable
			Dual	SN74H50	TI	6	20	--	--	10	22	5,25	0,4	2,4	1000	0 to 70	D, DIP	Expandable
			--	SN74H52	TI	6	9	--	--	10	22	5,25	0,4	2,4	1000	0 to 70	D, DIP	Expandable
			--	SN74H53	TI	6	24	--	--	10	22	5,25	0,4	2,4	1000	0 to 70	D, DIP	Expandable
			Dual 3-input	MC403	MO	11	--	--	12	30	5	0,26	3,3	1000	0 to 75	C, G, DIP		

Temperature range is —55 to 125°C unless otherwise stated.

### 3. TTL (continued)

Gates E	Logic Function	Type	Model	Mfr.	Propagati- on Delay (ns)	Fan-in		Fan-out		Power Diss. mW (/= per gate)	Logic Levels (Volts)		Noise Margin (mV)	Temp Range (°C)	Package Type	Remarks	
						Typ.	Max.	Typ.	Max.		"0"	"1"					
						Supply Voltage (Volts)											
7	AND-OR- Inverter	Dual 3-input	MC453	MO	11	-	-	6	30	5	0.26	3.3	1000	0 to 75	C, G, DIP	Expandable Expandable Expandable Expandable Expandable Expandable Expandable Expandable	
		Dual 3-input	MC503	MO	11	-	-	15	30	5	0.26	3.3	1000	-	C		
		Dual 3-input	MC553	MO	11	-	-	7	30	5	0.26	3.3	1000	-	C		
		Triple 3-input	MC404	MO	12	-	-	12	25	5	0.26	3.3	1000	0 to 75	C, G, DIP		
		Dual 4-input	MC405	MO	12	-	-	12	20	5	0.26	3.3	1000	0 to 75	C, G, DIP		
		Dual 4-input	MC455	MO	12	-	-	6	20	5	0.26	3.3	1000	0 to 75	C, G, DIP		
		Quad 2-input	MC501	MO	12	-	-	15	30	5	0.26	3.3	1000	-	C		
		Triple 3-input	MC504	MO	12	-	-	15	25	5	0.26	3.3	1000	-	C		
		Dual 4-input	MC505	MO	12	-	-	15	20	5	0.26	3.3	1000	-	C		
		Quad 2-input	MC551	MO	12	-	-	7	30	5	0.26	3.3	1000	-	C		
		Triple 3-input	MC554	MO	12	-	-	7	25	5	0.26	3.3	1000	-	C		
		Dual 4-input	MC555	MO	12	-	-	7	20	5	0.26	3.3	1000	-	C		
		Dual	SN54L51	TI	33	-	4	-	10	11.5	4.5-5.5	0.3	2.4	1000	-		D
Dual	SN74H60	TI	-	-	20	-	4	2	5.25	0.4	2.4	1000	0 to 70	D, DIP			
8	NAND	Dual 4-input	583B	AL	4	-	-	6	8	5	400	3800	1000	-	C	w/ex & no pull up	
		Triple	SN54H10	TI	6	-	3	-	10	20	5.5	0.4	2.4	1000	-	D	tper gate
		Dual	SN54H20	TI	6	-	4	-	10	20	4.5-5.5	0.4	2.4	1000	-	D	
		Dual	SN54H40	TI	6	-	4	-	10	35	5.5	0.4	2.4	1000	-	D	
		Quad	SN74H00	TI	6	-	2	-	10	20	4.75-5.25	0.4	2.4	1000	0 to 70	D, DIP	tper gate
		Triple	SN74H10	TI	6	-	3	-	10	20	5.25	0.4	2.4	1000	0 to 70	D, DIP	
		Dual	SN74H20	TI	6	-	4	-	10	20	5.25	0.4	2.4	1000	0 to 70	D, DIP	
		Single	SN74H30	TI	6	-	8	-	10	20	5.25	0.4	2.4	1000	0-70	D, DIP	
		Dual	SN74H40	TI	6	-	4	-	10	35	5.25	0.4	2.4	1000	-	D, DIP	
		Quad 2-input	SWG220	SW	6	2	-	12	-	22	4.5-6	0.4	3	1000	-	-	-
		Quad 2-input	SWG221	SW	6	2	-	6	-	22	4.5-6	0.4	3	1000	-	-	-
		Quad 2-input	SWG222	SW	6	2	-	10	-	22	4.5-6	0.45	3	900	0 to +75	-	-
		Quad 2-input	SWG223	SW	6	2	-	5	-	22	4.5-6	0.45	3	900	0 to +75	-	-
Dual 4-input	SWG240	SW	6	4	-	12	-	22	4.5-6	0.4	3	1000	-	-	-		
Dual 4-input	SWG241	SW	6	4	-	6	-	22	4.5-6	0.4	3	1000	-	-	-		
Dual 4-input	SWG242	SW	6	4	-	10	-	22	4.5-6	0.45	3	900	0 to +75	-	-		
9		Dual 4-input	SWG243	SW	6	6	4	-	5	22	4.5-6	0.45	3	900	0 to +75	-	-
		Quad 2-input	900251	FA	6	-	-	10	11/	4.5-5.5	0.2	2.7	1000	-	C, G	-	
		Triple 3-input	900351	FA	6	-	-	10	11/	4.5-5.5	0.2	2.7	1000	-	C, G	-	
		Dual 4-input	900451	FA	6	-	-	10	11/	4.5-5.5	0.2	2.7	1000	-	C, G	-	
		8-input	900751	FA	6	-	-	10	11/	4.5-5.5	0.2	2.7	1000	-	C, G	-	
		8-input	SWG260	SW	8	8	-	12	-	22	4.5-6	0.4	3	1000	-	-	-
		8-input	SWG261	SW	8	8	-	6	-	22	4.5-6	0.4	3	1000	-	-	-
		8-input	SWG262	SW	8	8	-	10	-	22	4.5-6	0.45	3	900	0 to +75	-	-
		8-input	SWG263	SW	8	8	-	5	-	22	4.5-6	0.45	3	900	0 to +75	-	-
		Quad 2-input	900259	FA	8	-	-	8	12/	4.5-5.5	0.25	3.2	1050	0 to 75	C, G	-	
		Triple 3-input	900359	FA	8	-	-	8	12/	4.5-5.5	0.25	3.2	1050	0 to 75	C, G	-	
		Dual 4-input	900459	FA	8	-	-	8	12/	4.5-5.5	0.25	3.2	1050	0 to 75	C, G	-	
		8-input	900759	FA	8	-	-	8	12/	4.5-5.5	0.25	3.2	1050	0 to 75	C, G	-	
Single	SE808	SIG	10	-	8	-	10	10	+5	0.4	2.4	1000	-	F	-		
Dual	SE816	SIG	10	-	4	-	10	10	+5	0.4	2.4	1000	-	F	-		
Triple	SE870	SIG	10	-	3	-	10	10	+5	0.4	2.4	1000	-	F	-		
Quad	SE880	SIG	10	-	2	-	10	10	+5	0.4	2.4	1000	-	F	-		
Dual	SW103	SW	10	-	4	-	15	20	5	0.4	3.0	1000	-	A	-		
10		-	SW104	SW	10	-	8	-	15	20	5	0.4	3.0	1000	-	A	-
		Dual	SWG4A	SW	11	-	3	-	15	15	5	0.5	3.0	1000	-	A	-
		Dual	SWG4B	SW	11	-	4	-	15	15	5	0.5	3.0	1000	-	A	-
		Dual	SWG14	SW	11	-	4	-	7	15	5	0.5	3.0	1000	-	A	-
		8-input	S8808	SIG	12	-	8	-	10	-	5.0	0.45	2.4	1000	-	F	-
		Dual 4-input	S8816	SIG	12	-	4	-	10	-	5.0	0.45	2.4	1000	-	F	-
		Triple 3-input	S8870	SIG	12	-	3	-	10	-	5.0	0.45	2.4	1000	-	F	-
		Quad 2-input	S8880	SIG	12	-	2	-	10	-	5.0	0.45	2.4	1000	-	F	-
		Dual 4-input	SWG40	SW	12	4	-	15	-	15	4.5-6	0.4	3	1000	-	-	-
		Dual 4-input	SWG41	SW	12	4	-	7	-	15	4.5-6	0.4	3	1000	-	-	-
		Dual 4-input	SWG42	SW	12	4	-	12	-	15	4.5-6	0.45	3	900	0 to +75	-	-
		Dual 4-input	SWG43	SW	12	4	-	6	-	15	4.5-6	0.45	3	900	0 to +75	-	-
		Power Driver	SWG130	SW	12	4	-	15	-	30	4.5-6	0.4	3	1000	-	-	-
		Power Driver	SWG131	SW	12	4	-	15	-	30	4.5-6	0.4	3	1000	-	-	-
		Power Driver	SWG132	SW	12	4	-	24	-	30	4.5-6	0.45	3	900	0 to +75	-	-
		Power Driver	SWG133	SW	12	4	-	12	-	30	4.5-6	0.45	3	900	0 to +75	-	-
		Quad 2-input	SWG140	SW	12	2	-	15	-	15	4.5-6	0.4	3	1000	-	-	-
		Quad 2-input	SWG141	SW	12	2	-	7	-	15	4.5-6	0.4	3	1000	-	-	-
		Quad 2-input	SWG142	SW	12	2	-	12	-	15	4.5-6	0.45	3	900	0 to +75	-	-
Quad 2-input	SWG143	SW	12	2	-	6	-	15	4.5-6	0.45	3	900	0 to +75	-	-		
Quad 2-input	SW5400	SW	13	2	-	10	-	10	4.5-5.5	0.4	3	1000	-	-	-		
Triple 3-input	SW5410	SW	13	3	-	10	-	10	4.5-5.5	0.4	3	1000	-	-	-		
Dual 4-input	SW5420	SW	13	4	-	10	-	10	4.5-5.5	0.4	3	1000	-	-	-		
Quad 2-input	SW7400	SW	13	2	-	10	-	10	4.8-5.3	0.45	3	900	0 to +75	-	-		
Triple 3-input	SW7410	SW	13	3	-	10	-	10	4.8-5.3	0.45	3	900	0 to +75	-	-		
Dual 4-input	SW7420	SW	13	4	-	10	-	10	4.8-5.3	0.45	3	900	0 to +75	-	-		
11		Quad 2-input	SN5400	TI	13	-	-	-	10	10/gate	4.5to	-	-	1000	-	D	-
		Triple 3-input	SN5410	TI	13	-	-	-	10	10/gate	4.5to	-	-	1000	-	D	-
		Dual 4-input	SN5420	TI	13	-	-	-	10	10/gate	4.5 to	-	-	1000	-	D	-
		Quad 2-input	SN7400	TI	13	-	-	-	10	10/gate	4.75 -	-	-	1000	0-70	D	-
		Triple 3-input	SN7410	TI	13	-	-	-	10	10/gate	4.75 -	-	-	1000	0-70	D	-
		Dual 4-input	SN7420	TI	13	-	-	-	10	10/gate	4.75 -	-	-	1000	0-70	D	-

Temperature range is -55 to 125°C unless otherwise stated.

### 3. TTL (continued)

Logic Function	Type	Model	Mfr.	Propagation Delay (ns)	Fan-in		Fan-out		Power Diss. mW (/ = per gate)	Supply Voltage (Volts)	Logic Levels (Volts)		Noise Margin (mV)	Temp Range (°C)	Package Type	Remarks		
					Typ.	Max.	Typ.	Max.			'0'	'1'						
Gates E	NAND	Dual 4-input	SN54930	TI	13	-	-	-	10	10/gate	4.5-5.5	-	-	1000	-	D		
		Quad 2-input	SN54946	TI	13	-	-	-	10	10/gate	4.5-5.5	-	-	1000	-	D		
		Triple 3-input	SN54962	TI	13	-	-	-	10	10/gate	4.5-5.5	-	-	1000	-	D		
		Dual 4-input	SN74930	TI	13	-	-	-	10	10/gate	4.75-5.25	-	-	1000	0 to 70	D		
		Triple 3-input	SN74962	TI	13	-	-	-	10	10/gate	4.75-5.25	-	-	1000	0 to 70	D		
		Quad 2-input	SN74946	TI	13	-	-	-	10	10/gate	4.75-5.25	-	-	1000	0 to 70	D		
		12	8-input	SW5430	SW	15	8	-	10	-	10	4.5-5.5	0.4	3	1000	-	-	
			8-input	SW7430	SW	15	8	-	10	-	10	4.8-5.3	0.45	3	900	0 to 75	-	
			8-input	SWG60	SW	15	8	-	7	-	15	4.5-6	0.4	3	1000	-	-	
			8-input	SWG61	SW	15	8	-	7	-	15	4.5-6	0.4	3	1000	-	-	
			8-input	SWG62	SW	15	8	-	12	-	15	4.5-6	0.45	3	900	0 to +75	-	
			8-input	SWG63	SW	15	8	-	6	-	15	4.5-6	0.45	3	900	0 to +75	-	
			8-input	SN5430	TI	15	-	-	-	10	10	4.5 to 5.5	-	-	1000	-	D	
			8-input	SN7430	TI	15	-	-	-	10	10	4.75-5.25	-	-	1000	0-70	D	
	8-input		SN54965	TI	15	-	-	-	10	10	4.5-5.5	-	-	1000	-	D		
	8-input		SN74965	TI	15	-	-	-	10	10	4.75-5.25	-	-	1000	0 to 70	D		
	-		SWG16	SW	15	-	8	7	-	15	5	0.5	3.0	1000	-	A		
	13		8-input	SWG120	SW	16	20	-	7	-	15	4.5-6	0.4	3	1000	-	-	Expandable
		8-input	SWG121	SW	16	20	-	7	-	15	4.5-6	0.4	3	1000	-	-	Expandable	
		8-input	SWG122	SW	16	20	-	12	-	15	4.5-6	0.45	3	900	0 to +75	-	Expandable	
		8-input	SWG123	SW	16	20	-	6	-	15	4.5-6	0.45	3	900	0 to +75	-	Expandable	
		Dual 4-input	SW5440	SW	17.5	4	-	30	-	10	4.5-5.5	0.4	3	1000	-	-		
		Dual 4-input	SW7440	SW	17.5	4	-	30	-	10	4.8-5.3	0.45	3	900	0 to +75	-		
		Dual 4-input	SN5440	TI	18	-	-	-	30	25/gate	4.5 to 5.5	-	-	1000	-	D	Power gate	
		Dual 4-input	SN7440	TI	18	-	-	-	30	25/gate	4.75-5.25	-	-	1000	0-70	D	Power gate	
		Quad 2-input	SE480	SIG	23	-	2	7	-	3.5	4.0	0.2	2.8	1000	-	F, G	also 0°C to 70°C 15°C to 55°C	
		Quad 2-input	S8480	SIG	25	-	2	7	-	-	5.0	0.35	3.4	1000	-	F		
		Dual 4-input	SE416	SIG	30	-	4	7	-	4.5	4.0	0.2	2.8	1000	-	F, G	also 0°C to 70°C 15°C to 55°C	
		Dual 3-input	SE417	SIG	32	-	3	7	-	4.5	4.0	0.2	2.8	1000	-	F, G	also 0°C to 70°C 15°C to 55°C	
		Quad	SN54L00	TI	33	-	2	-	10	†1	4.5-5.5	0.3	2.4	1000	-	D	†per gate	
		Triple	SN54L10	TI	33	-	3	-	10	†1	4.5-5.5	0.3	2.4	1000	-	D	†per gate	
		Dual	SN54L20	TI	33	-	4	-	10	†1	4.5-5.5	0.3	2.4	1000	-	D	†per gate	
		Single	SN54L30	TI	33	-	8	-	10	1	4.5-5.5	0.3	2.4	1000	-	D	†per gate	
		Dual 4-input	S8416	SIG	35	-	4	-	7	-	5.0	0.35	3.4	1000	-	F		
		Dual 4-input	543B	AL	35	4	-	-	6	2.4	5	250	3800	1000	-	-	w/ex & no pull up	
		Dual 4-input	544B	AL	35	4	-	-	6	4.8	5	250	3800	1000	-	-	w/ex & no pull up	
	14	Dual 4-input	547B	AL	35	4	-	-	6	4.8	5	250	3800	1000	-	-	w/ex + no pull up	
		Dual 4-input	548B	AL	35	4	-	-	6	2.4	5	250	3800	1000	-	-	w/ex + no pull up	
		Dual 4-input	570B	AL	35	4	-	-	6	8	5	400	3800	1000	-	-	w/ex + no pull up	
		Quad 2-input	571B	AL	35	2	-	-	6	16	5	400	3800	100	-	C	w/ex + no pull up	
		Dual 3-input	572B	AL	35	4	-	-	6	8	5	400	3800	1000	-	C	w/ex + no pull up	
		Triple 3-input	573B	AL	35	3	-	-	6	12	5	400	3800	1000	-	C	w/ex + no pull up	
		Dual 4-input	574B	AL	35	4	-	-	6	10.4	5	400	3800	1000	-	C		
		Quad 2-input	575B	AL	35	2	-	-	6	20.8	5	400	3800	1000	-	-		
		Dual 3-input	576B	AL	35	3	-	-	6	10.4	5	400	3800	1000	-	C	w/ex	
		Triple 3-input	577B	AL	35	3	-	-	6	15.6	5	400	3800	1000	-	C		
	Dual 4-input	584B	AL	35	4	-	-	6	10.2	5	400	3800	1000	-	C	w/ex & no pull up		
	Dual 4-input	587B	AL	35	4	-	-	6	8	5	400	3800	1000	-	C	w/ex & no pull up		
	15	Dual 3-input	S8417	SIG	50	-	3	-	7	-	5.0	0.35	3.4	1000	-	F	†per gate	
		Quad	SN54H00	TI	6	-	2	-	10	†20	4.5-5.5	0.4	2.4	1000	-	D		
Dual		SW402	SW	100	-	3	-	5	0.10	3.0	0.3	2.0	300	-	A			
Dual 4-input		530B	AL	100	4	-	-	6	2.4	5	250	3800	1000	-	C			
Quad 2-input		531B	AL	100	2	-	-	6	4.8	5	250	3800	1000	-	-			
Dual 3-input		532B	AL	100	3	-	-	6	2.4	5	250	3800	1000	-	-	w/ex + no pull up		
Triple 3-input		533B	AL	100	3	-	-	6	3.6	5	250	3800	1000	-	-			
Dual 4-input		534B	AL	100	4	-	-	6	4.8	5	250	3800	1000	-	-			
Quad 2-input		535B	AL	100	2	-	-	6	9.6	4	250	3800	1000	-	-			
Dual 3-input		536B	AL	100	3	-	-	6	4.8	4	250	3800	1000	-	-	w/ex		
Triple 3-input		537B	AL	100	3	-	-	6	7.2	5	250	3800	1000	-	-			
Dual 4-input		500B	AL	180	4	-	-	8	1	4	250	3800	1000	-	-	no pull up		
Quad 2-input	501B	AL	180	2	-	-	8	2	4	250	3800	1000	-	-				
Dual 3-input	502B	AL	180	3	-	-	8	1	4	250	3800	1000	-	-	w/ex & no pull up			

Temperature range is -55 to 125°C unless otherwise stated.

### 3. TTL (continued)

Gates	Logic Function	Type	Model	Mfr.	Propaga-tion Delay (ns)	Fan-in		Fan-out		Power Diss. mW (= per gate)	Supply Voltage (Volts)	Logic Levels (Volts)		Noise Margin (mV)	Temp Range (°C)	Package Type	Remarks	
						Typ.	Max.	Typ.	Max.			'0'	'1'					
E	NAND	Triple 3-input	503B	AL	180	3	-	-	8	1.5	4	250	3800	1000	-	-	-	
		Dual 4-input	504B	AL	180	4	-	-	8	2	4	250	3800	1000	-	-	-	
		Quad 2-input	505B	AL	180	2	-	-	8	4	4	250	3800	1000	-	-	-	
		Dual 3-input	506B	AL	180	3	-	-	8	2	4	250	3800	1000	-	-	w/ex	
		Triple 3-input	507B	AL	180	3	-	-	8	3	4	250	3800	1000	-	-	-	
		Dual	SN54L22	TI	-	20	-	-	10	†1	4.5-5.5	0.3	2.4	1000	-	-	D	†open collector
	NAND/NOR	Quad 2-input	SG220,221	SY	6	-	-	-	12	22	-	0.25	3.5	1000	-	-	D, G	RA
		Quad 2-input	SG222,223	SY	6	-	-	-	10	22	-	0.25	3.5	1000	0 to 75	-	D, G	-
		Dual 4-input	SG240,241	SY	6	-	-	-	12	22	-	0.25	3.5	1000	-	-	D, G	-
		Dual 4-input	SG242,243	SY	6	-	-	-	10	22	-	0.25	3.5	1000	0,+75	-	D, G	-
		Quad	WG6221	WH	6.0	-	2	15	6	19/	5.0	1.1	1.6	800	-	-	D	-
		Dual	WG6241	WH	6.0	-	4	15	6	19/	5.0	1.1	1.6	800	-	-	D	-
		Single 8-input	SG200-201	SY	8	-	-	6	11	22	-	-	-	-	-	-	D, G	Expandable,RA
		Single 8-input	SG202-203	SY	8	-	-	5	9	22	-	-	-	-	0 to 75	-	D, G	Expandable
		Single 8-input	SG260,261	SY	8	-	-	-	12	22	-	0.25	3.5	1000	-	-	D, G	-
		Single 8-input	SG262,263	SY	8	-	-	-	10	22	-	0.25	3.5	1000	0 to 75	-	D, G	-
		-	B01	SI	10	-	8	-	15	16.5	4.5	0.5	2.3	1000	-55 to 165	-	A, D	-
		Dual	B02	SI	10	-	4	-	15	16.5	4.5	0.5	2.3	1000	-55 to 165	-	A, D	-
		Dual 4-input	MC400	MO	10	-	-	-	12	30	5	0.26	3.3	1000	0 to 75	-	C, G, DIP	-
		Quad 2-input	MC408	MO	10	-	-	-	12	60	5	0.26	3.3	1000	0 to 75	-	C, G, DIP	-
		Triple 3-input	MC412	MO	10	-	-	-	12	45	5	0.26	3.3	1000	-	-	C, G, DIP	-
		Dual 4-input	MC450	MO	10	-	-	-	6	30	5	0.26	3.3	1000	0 to 75	-	C, G, DIP	-
		Quad 2-input	MC458	MO	10	-	-	-	6	60	5	0.26	3.3	1000	0 to 75	-	C, G, DIP	-
		Triple 3-input	MC462	MO	10	-	-	-	6	45	5	0.26	3.3	1000	-	-	C, G, DIP	-
		Dual 4-input	MC500	MO	10	-	-	-	15	30	5	0.26	3.3	1000	-	-	C	-
		Quad 2-input	MC508	MO	10	-	-	-	15	60	5	0.26	3.3	1000	-	-	C	-
Triple 3-input	MC512	MO	10	-	-	-	15	45	5	0.26	3.3	1000	-	-	C	-		
Dual 4-input	MC550	MO	10	-	-	-	7	30	5	0.26	3.3	1000	-	-	C	-		
Quad 2-input	MC558	MO	10	-	-	-	7	60	5	0.26	3.3	1000	-	-	C	-		
Triple 3-input	MC562	MO	10	-	-	-	7	45	5	0.26	3.3	1000	-	-	C	-		
Quad 2-input	SG140-141	SY	10	-	-	7	15	15	-	-	-	-	-	-	D, G	RA		
		Quad 2-input	SG142-143	SY	10	-	-	6	12	15	-	-	-	0 to 75	-	D, G	-	
		Single 8-input	TNG3041-44	TR	10	-	1	-	10	24	5	0.45	3.5	1000	0 to 75	-	D, P, DIP	High speed
		Dual 4-input	TNG3141-44	TR	10	-	1	-	10	45	5	0.45	3.5	1000	0 to 75	-	D, P, DIP	High speed
		Triple 3-input	TNG3341-44	TR	10	-	1	-	10	65	5	0.45	3.5	1000	0 to 75	-	D, P, DIP	High speed
		Quad 2-input	TNG3441-44	TR	10	-	1	-	10	90	5	0.45	3.5	1000	0 to 75	-	D, P, DIP	High speed
		-	TNG3041	TR	10	-	8	-	20	15	5-6	0.20	3.0	1000	-	-	A, F	-
		-	TNG3043	TR	10	-	8	-	7	15	5-6	0.20	3.0	1000	-	-	A, F	-
		-	TNG3045	TR	10	-	6	-	20	15	5-6	0.20	3.0	1000	-	-	A, F	-
		-	TNG3047	TR	10	-	6	-	7	15	5-6	0.20	3.0	1000	-	-	A, F	-
		Dual	TNG3141	TR	10	-	4	-	20	15	5-6	0.20	3.0	1000	-	-	A, F	-
		Dual	TNG3143	TR	10	-	4	-	7	15	5-6	0.20	3.0	1000	-	-	A, F	-
		Dual	TNG3145	TR	10	-	3	-	20	15	5-6	0.20	3.0	1000	-	-	A, F	-
		Dual	TNG3147	TR	10	-	3	-	7	15	5-6	0.20	3.0	1000	-	-	A, F	-
		Dual	TNG3241	TR	10	-	4	-	20	15	5-6	0.20	3.0	1000	-	-	A, F	-
		Dual	TNG3243	TR	10	-	4	-	7	15	5-6	0.20	3.0	1000	-	-	A, F	-
		Dual	TNG3245	TR	10	-	3	-	20	15	5-6	0.20	3.0	1000	-	-	A, F	-
Dual	TNG3247	TR	10	-	3	-	7	15	5-6	0.20	3.0	1000	-	-	A, F	-		
Triple 3-input	SG190,191	SY	10	-	-	-	15	15	-	0.26	3.3	1000	-	-	D, G	-		
Triple 3-input	SG192,193	SY	10	-	-	-	12	15	-	0.26	3.3	1000	0,+75	-	D, G	-		
8-input	MC402	MO	12	-	-	-	12	15	4	0.26	3.3	1000	0 to 75	-	C, G, DIP	-		
8-input	MC452	MO	12	-	-	-	6	15	5	0.26	3.3	1000	0 to 75	-	C, G, DIP	-		
		8-input	MC502	MO	12	-	-	-	15	15	5	0.26	3.3	1000	-	-	C	-
		8-input	MC552	MO	12	-	-	-	7	15	5	0.26	3.3	1000	-	-	C	-
		Dual 4-input	SG40, SG41, SG42, SG43	SY	12	-	-	6	20	15	-	-	-	1000	-	-	-	Differ in Temp & F.O.
		Single 8-input	SG60, SG61, SG62, SG63	SY	12	-	-	6	20	15	-	-	-	1000	-	-	-	Differ in Temp & F.O.
		Expandable	SG 120, 121, SG 122, 123	SY	12	-	-	6	20	15	-	-	-	1000	-	-	-	Differ in Temp & F.O.
		-	TNG3011	TR	15	-	8	-	20	15	5-6	0.20	3.0	1000	-	-	A, F	-
		-	TNG3013	TR	15	-	8	-	7	15	5-6	0.20	3.0	1000	-	-	A, F	-
		-	TNG3015	TR	15	-	6	-	20	15	5-6	0.20	3.0	1000	-	-	A, F	-
		-	TNG3017	TR	15	-	6	-	7	15	5-6	0.20	3.0	1000	-	-	A, F	-
		-	TNG3031	TR	15	-	4	-	7	15	5-6	0.20	3.0	1000	+10 to 60	-	A	-
		Dual	TNG3111	TR	15	-	4	-	20	15	5-6	0.20	3.0	1000	-	-	A, F	-
		Dual	TNG3113	TR	15	-	4	-	7	15	5-6	0.20	3.0	1000	-	-	A, F	-
		Dual	TNG3115	TR	15	-	3	-	20	15	5-6	0.20	3.0	1000	-	-	A, F	-
		Dual	TNG3117	TR	15	-	3	-	7	15	5-6	0.02	3.0	1000	-	-	A, F	-
		Dual	TNG3131	TR	15	-	2	-	7	15	5-6	0.20	3.0	1000	+10 to 60	-	A	-
		Dual	TNG3211	TR	15	-	4	-	20	15	5-6	0.20	3.0	1000	-	-	A, F	-
		Dual	TNG3213	TR	15	-	4	-	7	15	5-6	0.20	3.0	1000	-	-	A, F	-
		Dual	TNG3215	TR	15	-	3	-	20	15	5-6	0.20	3.0	1000	-	-	A, F	-
		Dual	TNG3217	TR	15	-	3	-	7	15	5-6	0.20	3.0	1000	-	-	A, F	-
		Dual	TNG3231	TR	15	-	2	-	7	15	5-6	0.20	3.0	1000	10 to 60	-	A	-
8-input	MC406	MO	18	-	-	-	12	15	5	0.26	3.3	1000	0 to 75	-	C, G, DIP	-		
8-input	MC456	MO	18	-	-	-	6	15	5	0.26	3.3	1000	0 to 75	-	C, G, DIP	-		
	20	8-input	MC506	MO	18	-	-	-	15	15	5	0.26	3.3	1000	-	-	C	-
		8-input	MC556	MO	18	-	-	-	7	15	5	0.26	3.3	1000	-	-	C	-
		Dual 4-input	TT <sub>μ</sub> L103	FA	25	-	4	-	15	25	5.0	0.33	4	750	-	-	A, C	-
		8-input	TT <sub>μ</sub> L104	FA	30	-	8	-	15	25	5.0	0.33	4	750	-	-	A, C	-
		Dual 4-input	μ7103	PH	30	-	4	10	-	25	5	0	3.0	500	-	-	-	-
		8-input	μ7104	PH	30	-	8	10	-	25	5	0	3.0	500	-	-	-	-
Dual 4-input	μ7105	PH	30	-	4	10	-	25	5	0	3.0	500	-	-	-	-		
Dual 4-input	μ7106	PH	30	-	8	10	-	25	5	0	3.0	500	-	-	-	-		

Temperature range is -55 to 125°C unless otherwise stated.

### 3. TTL (continued)

Logic Function	Type	Model	Mfr.	Propagation Delay (ns)	Fan-in				Power Diss. mW (/ = per gate)	Supply Voltage (Volts)	Logic Levels (Volts)		Noise Margin (mV)	Temp Range (°C)	Package Type	Remarks		
					Typ.	Max.	Typ.	Max.			"0"	"1"						
Gates <b>E</b>	Exclusive OR     2 1	Dual 4-input	SG210,211	SY	7	-	-	-	12	30	-	0.25	3.5	1000	-	D, G	Expandable Expandable RA Differ in Temp & F.O. Differ in Temp & F.O. Differ in Temp & F.O. High speed	
		Dual 4-input	SG212,213	SY	7	-	-	-	10	30	-	0.25	3.5	1000	0 to 75	D, G		
		Quad 2-input	SG250,251	SY	7.5	-	-	-	12	43	-	0.25	3.5	1000	-	D, G		
		Quad 2-input	SG252,253	SY	7.5	-	-	-	10	43	-	0.25	3.5	1000	0, +75	D, G		
		Dual	SE840	SIG	10	-	4	-	10	14	+5	0.4	2.4	1000	-	F		
		Expandable	SG90-91	SY	11	-	-	7	15	35	-	-	-	-	-	D, G		
		Expandable	SG92-93	SY	11	-	-	6	12	35	-	-	-	0 to 75	D, G			
		Dual	S8840	SIG	12	-	4	-	10	-	5.0	0.45	2.4	1000	-	F		
		Single 8-input	SG50,SG51	SY	12	-	-	6	20	15	-	-	-	1000	-	-		
	Maj. Voter	SG100,101	SY	12	-	-	6	20	15	-	-	-	1000	-	-			
	-	SG102,103	SY	12	-	-	6	20	15	-	-	-	1000	-	-			
	-	SG110,111	SY	12	-	-	6	20	15	-	-	-	1000	-	-			
	-	SG112,113	SY	12	-	-	6	20	15	-	-	-	1000	-	-			
	4 x 4 input	TNG3241-44	TR	12	-	1	-	10	22	5	0.45	3.5	1000	0 to 75	D,P,DIP	High speed		
	Expandable	TNG3281-84	TR	12	-	1	-	10	22	5	0.45	3.5	1000	0 to 75	D,P,DIP	High speed		
	2 2	Dual	TNG4241-44	TR	12	-	1	-	10	44	5	0.45	3.5	1000	0 to 75	D,P,DIP	High speed	
		Quad 2-input	TNG4446	TR	12	-	1	-	10	90	5	0.45	3.5	1000	0 to 75	D,P,DIP	High speed,	
			SWG90	SW	14	6	-	15	-	30	4.5-6	0.4	3	1000	-	-	-	
			SWG91	SW	14	6	-	7	-	30	4.5-6	0.4	3	1000	-	-	-	
			SWG92	SW	14	6	-	12	-	30	4.5-6	0.45	3	900	0 to +75	-	-	
		Dual	SWG93	SW	14	6	-	6	-	30	4.5-6	0.45	3	900	0 to +75	-	-	
		Dual	SW5450	SW	15	20	-	10	-	10	4.5-5.5	0.4	3	1000	-	-	Expandable	
		Dual	SW7450	SW	15	20	-	10	-	10	4.8-5.3	0.45	3	900	0 to +75	-	Expandable	
		Dual	SN5450	TI	15	-	-	-	10	14/ gate	4.5 to	-	-	1000	-	D	Expander	
		Dual	SN5451	TI	15	-	-	-	10	14/ gate	4.5-5.5	-	-	1000	-	D	Inputs	
Dual		SN7451	TI	15	-	-	-	10	14/ gate	4.75-	-	-	1000	0 to 70	D	-		
Dual		SN54966	TI	15	-	-	-	10	14/ gate	5.25	-	-	1000	-	D	-		
Dual		SN74966	TI	15	-	-	-	10	14/ gate	4.5-5.5	-	-	1000	0 to 70	D	-		
Dual		SE440	SIG	23	-	2	7	-	14/ gate	4.75-	-	-	1000	0 to 70	D	-		
Dual		S8440	SIG	25	-	2	-	7	4.5	4.0	0.2	2.8	1000	-	F, G	also 0°C to 70°C 15°C to 55°C		
Dual 4-input		578B	AL	35	8	-	-	6	10.4	5.0	0.35	3.4	1000	-	F	-		
Dual 4-input	538B	AL	100	8	-	-	6	4.8	5	250	3800	1000	-	C	-			
Dual 4-input	508B	AL	180	8	-	-	8	2	4	250	3800	1000	-	C	-			
Dual 4-input	TNG4041-42	TR	-	-	1	-	-	2	-	-	-	1000	0 to 75	D,P,DIP	High speed			
Quad 2-input	TNG4541	TR	-	-	1	-	-	-	-	0.45	3.5	1000	0 to 75	D,P,DIP	High speed			
Gate Expanders <b>F</b>	1	Quad 2-input	SWG230	SW	2	8	-	-	-	28	4.5-6	-	-	-	-	-	-	
		Quad 2-input	SWG231	SW	2	8	-	-	-	28	4.5-6	-	-	-	-	-	-	
		Quad 2-input	SWG232	SW	2	8	-	-	-	28	4.5-6	-	-	-	0 to +75	-	-	
		Quad 2-input	SWG233	SW	2	8	-	-	-	28	4.5-6	-	-	-	0 to +75	-	-	
		Dual 4-input	SWG270	SW	2	8	-	-	-	6.7	4.5-6	-	-	-	-	-	-	
		Dual 4-input	SWG271	SW	2	8	-	-	-	6.7	4.5-6	-	-	-	-	-	-	
		Dual 4-input	SWG272	SW	2	8	-	-	-	6.7	4.5-6	-	-	-	0 to +75	-	-	
		Dual 4-input	SWG273	SW	2	8	-	-	-	6.7	4.5-6	-	-	-	0 to +75	-	-	
		Quad 2-input	SG230,231	SY	2	-	-	-	12	28	-	0.25	3.5	1000	-	-	D, G	-
		Quad 2-input	SG232,233	SY	2	-	-	-	10	28	-	0.25	3.5	1000	0 to 75	D, G	-	
		Dual 4-input	SG270,271	SY	2	-	-	-	15	6.7	-	0.25	3.5	1000	-	-	D, G	-
		Dual 4-input	SG272,273	SY	2	-	-	-	12	6.7	-	0.25	3.5	1000	0 to 75	D, G	-	
		Dual	SE806	SIG	-	-	4	-	4	5	+5	0.4	2.0	1000	-	F	-	
		Dual 4-input	S8006	SIG	-	-	4	-	4	-	5.0	0.45	2.4	1000	-	F	-	
		Dual	SN54H60	TI	-	-	20	-	4	2	5.25	0.4	2.4	1000	-	D	-	
		Triple	SN54H61	TI	-	-	3	-	-	2	5.5	0.4	2.4	1000	-	D	-	
	AND-OR	SN54H62	TI	-	-	10	-	-	2	4.5	0.4	2.4	1000	-	D	-		
	Triple	SN74H61	TI	-	-	3	-	-	2	5.25	0.4	2.4	1000	0 to 70	D, DIP	-		
	AND-OR	SN74H62	TI	-	-	10	-	-	2	5.25	0.4	2.4	1000	0 to 70	D, DIP	-		
	Quad	SWG150	SW	-	-	10	-	-	5	4.5-6	-	-	-	-	-	-	-	
	Quad	SWG151	SW	-	-	10	-	-	5	4.5-6	-	-	-	-	-	-	-	
	Quad	SWG152	SW	-	-	10	-	-	5	4.5-6	-	-	-	-	-	-	-	
	2	Quad	SWG153	SW	-	-	10	-	-	5	4.5-6	-	-	-	-	-	-	-
		Dual 4-input	SWG170	SW	-	-	8	-	-	5	4.5-6	-	-	-	-	-	-	-
		Dual 4-input	SWG171	SW	-	-	8	-	-	5	4.5-6	-	-	-	-	-	-	-
		Dual 4-input	SWG172	SW	-	-	8	-	-	5	4.5-6	-	-	-	0 to +75	-	-	-
		Dual 4-input	SWG173	SW	-	-	8	-	-	5	4.5-6	-	-	-	0 to +75	-	-	-
		Dual 4-input	SWG180	SW	-	-	8	-	-	5	4.5-6	-	-	-	-	-	-	-
		Dual 4-input	SWG181	SW	-	-	8	-	-	1	4.5-6	-	-	-	-	-	-	-
		Dual 4-input	SWG182	SW	-	-	8	-	-	1	4.5-6	-	-	-	0 to +75	-	-	-
Dual 4-input		SWG183	SW	-	-	8	-	-	1	4.5-6	-	-	-	0 to +75	-	-	-	
Dual 4-input		SW5460	SW	-	-	4	-	-	5	4.5-5.5	-	-	-	-	-	-	-	
Dual 4-input		SW7460	SW	-	-	4	-	-	5	4.8-5.3	-	-	-	0 to +75	-	-	-	
3-input		SG170,171	SY	-	-	-	-	-	15	-	-	-	1000	-	-	-	Differ in Temp & F.O.	
Dual 3-input		SG172,173	SY	-	-	-	-	6	20	15	-	-	1000	-	-	-	Differ in Temp & F.O.	
Dual 4-input		SG180,181	SY	-	-	-	-	4	20	15	-	-	1000	-	-	-	Differ in Temp & F.O.	
Dual 4-input	SG182,183	SY	-	-	-	-	4	20	15	-	-	1000	-	-	-	Differ in Temp & F.O.		
Dual 4-input	SN5460	TI	-	-	-	-	4	5/exp	4.5 to 5.5	-	-	1000	-	D	-			
Dual 4-input	SN7460	TI	-	-	-	-	4	5/exp	4.75-5.25	-	-	1000	0 to 70	D	-			
-	TNG3051	TR	-	-	8	-	-	5	5-6	0.20	3.0	1000	-	A, F	-			
-	TNG3251	TR	-	-	4	-	-	5	5-6	0.20	3.0	1000	-	A, F	-			
Inverters <b>G</b>	Quad 2-input	SN5453	TI	15	-	-	-	10	25	4.5-5.5	-	-	1000	-	D	-		

Temperature range is -55 to 125°C unless otherwise stated.

# 4. Emitter-Coupled Logic

Logic Function	Type	Model	Mfr.	Propagation Delay (ns)	Fan-in		Fan-out		Power Diss. mW (/ = per gate)	Supply Voltage (Volts)	Logic Levels (Volts)		Noise Margin (mV)	Temp Range (°C)	Package Type	Remarks	
					Typ.	Max.	Typ.	Max.			'0'	'1'					
Adders A	Half	MC303	MO	7	-	-	-	ac 15 dc 25	63	-5.2	-1.55	-0.75	-	-	A, C		
	Half	MC353	MO	7	-	-	-	ac 15 dc 25	63	-5.2	-1.55	-0.75	-	0 to 75	A, C		
	Full	MC1019P	MO	10	-	-	-	ac 15 dc 25	110	-5.2	-1.55	-0.75	-	0 to 75	G, DIP		
	Full	MC1219F	MO	10	-	-	-	ac 15 dc 25	110	-5.2	-1.55	-0.75	-	-	C		
Binary Elements B	R-S FF	WC379	WH	6	-	-	4	8	223	-4.0	-0.70	-0.01	150	-	D		
	J-K	MC308	MO	7.5	-	2	-	ac 15 dc 25	87	-5.2	-1.55	-0.75	-	-	A, C		
	J-K	MC358	MO	7.5	-	2	-	ac 15 dc 25	50	-5.2	-1.55	-0.75	-	0 to 75	A, C		
	J-K	MC358A	MO	7.5	-	2	-	ac 15 dc 25	87	-5.2	-1.55	-0.75	-	0 to 75	A, C		
	Set-Reset	MC352	MO	10	-	-	-	25	35	10	1.55	0.75	-	0 to 75	A, C		
	J-K	MC358	MO	10	-	-	-	-	52	10	1.55	0.75	-	0 to 75	A, C		
	JK	SW308	SW	10	-	-	-	25	52	-5.2	-1.55	-0.75	-	-	A, C	Expandable	
	R-S	MC302	MO	10.5	2	15	-	ac 15 dc 25	42	-5.2	-1.55	-0.75	-	-	A, C	A, C	
	R-S	MC352A	MO	10.5	2	15	-	ac 15 dc 25	42	-5.2	-1.55	-0.75	-	0 to 75	A, C	Expandable	
	J-K	MC364	MO	12	-	2	-	ac 15 dc 25	118	-5.2	-1.55	-0.75	-	0 to 75	A, C		
J-K	MC314	MO	12	-	2	-	ac 15 dc 25	118	-5.2	-1.55	-0.75	-	-	A, C			
Ac coupled J-K	MC1013P	MO	-	-	-	-	ac 15 dc 25	105	-5.2	-1.55	-0.75	-	0 to 75	G, DIP			
J-K	MC1213F	MO	-	-	-	-	ac 15 dc 25	105	-5.2	-1.55	-0.75	-	-	C			
Drivers C	Single 6-input Line & Capacity	WC378	WH	3	-	6	12	20	100	-4	-0.70	-0.01	150	-	D	Expandable	
		MC315	MO	14	3	15	-	50 Ω line	270	-5.2	-1.55	-0.75	-	-	A, C		
	Line & Capacity	MC365	MO	14	3	15	-	50 Ω line	270	-5.2	-1.55	-0.75	-	0 to 75	A, C	Expandable	
	-	MC304	MO	-	-	-	-	ac 15 dc 25	18	-5.2	-	-	-	-	A, C		
	Lamp	MC316	MO	-	-	3	-	10 mA	135	-5.2	-1.55	-0.75	-	-	C		
	Lamp	MC366	MO	-	-	3	-	10 mA	135	-5.2	-1.55	-0.75	-	0 to 75	A, C		
	-	SW304	SW	-	-	-	5	25	18	-5.2	-	-	-	-	A, C		
-	MC354	MO	-	-	-	-	ac 15 dc 25	18	-5.2	-	-	-	0 to 75	A, C			
Gates D	NOR	Quad 2-input	CR2101	RCA	5.6	-	8	-	12	156	5.2	-1.55	-0.75	320	-	F	
		Dual 2-input	MC309	MO	6.5	-	2	-	ac 15 dc 25	54	-5.2	-1.55	-0.75	-	-	A, C	
		Dual 2-input	MC311	MO	6.5	-	2	-	ac 15 dc 25	41	-5.2	-1.55	-0.75	-	-	A, C	
		Dual 3-input	MC312	MO	7.5	-	3	-	ac 15 dc 25	70	-5.2	-1.55	-0.75	-	-	A, C	
		Dual	SW309 SW310 SW311	SW	6	-	2	-	26	49	-5.2	-1.5	-0.75	-	-	A, C	Units Differ in output configuration
	OR/NOR	Dual 4-input	WC377	WH	2	-	4	6	10	60/	-4.0	-0.70	-0.01	150	-	D	
		Dual 3-input	WC380	WH	2	-	3	6	10	60/	-4.0	-0.70	-0.01	150	-	D	
		Single 8-input	WC381	WH	2	-	8	6	10	100/	-4.0	-0.70	-0.01	150	-	D	
		Dual 4-input	CD2150	RCA	3.6	-	8	-	12	220	-5	-1.6	-0.76	330	10 to 60	F	
		Dual 4-input	CA2151	RCA	3.6	-	8	-	12	175	-5	-1.6	-0.76	330	10 to 60	F	
		8-input	CA2152	RCA	3.6	-	8	-	12	110	-5	-0.76	-1.6	330	10 to 60	F	
		Dual	SN7000	TI	5	-	-	-	40/ gate	-	+1.25- -3.5	-	-	250	0 to 70	D	4 load resistors
		Dual	SN7001	TI	5	-	-	-	40/ gate	-	+1.25- -3.5	-	-	250	0 to 70	D	2 load resistors
	Dual 4-input	CR2100	RCA	5.6	-	8	-	12	115	-5.2	-1.55	-0.75	320	-	F		
	-	SW301	SW	6	-	5	-	26	35	-5.2	-1.55	-0.75	-	-	A, C		
	-	SW306	SW	6	3	25	-	26	35	-5.2	-1.55	-0.75	-	-	A, C	Units Differ in Output Configuration	
	-	SW307	SW	6	3	25	-	26	35	-5.2	-1.55	-0.75	-	-	A, C		
NOR/NAND	Triple 3-input	MC1007P	MO	5	-	-	-	ac 15 dc 25	110	-5.2	-1.55	-0.75	-	0 to 75	G, DIP		
	Triple 3-input	MC1008P	MO	5	-	-	-	ac 15 dc 25	75	-5.2	-1.55	-0.75	-	0 to 75	G, DIP		
	Triple 3-input	MC1009P	MO	5	-	-	-	ac 15 dc 25	60	-5.2	-1.55	-0.75	-	0 to 75	G, DIP		
	Quad 2-input	MC1010P	MO	5	-	-	-	ac 15 dc 25	115	-5.2	-1.55	-0.75	-	0 to 75	G, DIP		
	Quad 2-input	MC1011P	MO	5	-	-	-	ac 15 dc 25	95	-5.2	-1.55	-0.75	-	0 to 75	G, DIP		
	Quad 2-input	MC1012F	MO	5	-	-	-	ac 15 ad 25	115	-5.2	-1.55	-0.75	-	-	C		
	Quad 2-input	MC1012P	MO	5	-	-	-	ac 15 dc 25	65	-5.2	-1.55	-0.75	-	-	C		
	Triple 3-input	MC1207F	MO	5	-	-	-	ac 15 dc 25	110	-5.2	-1.55	-0.75	-	-	C		
Triple 3-input	MC1208F	MO	5	-	-	-	ac 15 dc 25	75	-5.2	-1.55	-0.75	-	-	C			

Temperature range is -55 to 125°C unless otherwise stated.



## 4. ECL (continued)

Logic Function	Type	Model	Mfr.	Propagation Delay (ns)	Fan-in		Fan-out		Power Diss. mW (/ = per gate)	Supply Voltage (Volts)	Logic Levels (Volts)		Noise Margin (mV)	Temp Range (°C)	Package Type	Remarks	
					Typ.	Max.	Typ.	Max.			'0'	'1'					
Gates D	NOR/NAND	Triple 3-input	MC1209F	MO	5	-	-	-	ac 15 dc 25	60	-5.2	-1.55	-0.75	-	-	C	
		Quad 2-input	MC1211F	MO	5	-	-	-	ac 15 dc 25	95	-5.2	-1.55	-0.75	-	-	C	
		Quad 2-input	MC1212F	MO	5	-	-	-	ac 15 dc 25	65	-5.2	-1.55	-0.75	-	-	C	
		Dual 2-input	MC310	MO	6.5	-	2	-	ac 15 dc 25	54	-5.2	-1.55	-0.75	-	-	A, C	
		Quad 2-input	MC313F	MO	6.5	-	2	-	ac 15 dc 25	124	-5.2	-1.55	-0.75	-	-	C	
		Dual 2-input	MC359	MO	6.5	-	2	-	ac 15 dc 25	54	-5.2	-1.55	-0.75	-	0 to 75	A, C	
		Dual 2-input	MC360	MO	6.5	-	2	-	ac 15 dc 25	54	-5.2	-1.55	-0.75	-	0 to 75	A, C	
		Dual 2-input	MC361	MO	6.5	-	2	-	ac 15 dc 25	41	-5.2	-1.55	-0.75	-	0 to 75	A, C	
		Quad 2-input	MC363F	MO	6.5	-	2	-	ac 15 dc 25	124	-5.2	-1.55	-0.75	-	0 to 75	C	
	Dual 3-input	MC362	MO	7.5	-	3	-	ac 15 dc 25	70	-5.2	-1.55	-0.75	-	0 to 75	A, C		
	NAND-AND	Dual 4-input	MC369F	MO	3	-	4	-	ac 15 dc 100	250	-5.2	-1.55	-0.75	-	0 to 75	C	
		Dual 2-input	MC369G	MO	3	-	4	-	ac 15 dc 100	250	-5.2	-1.55	-0.75	-	0 to 75	A	
		Dual 4-input	MC1050	MO	4	-	-	-	10	-	-5.2	-1.55	-0.75	-	0 to 70	C	Comp. out Wired OR Comp. out
		Dual 4-input	MC1051	MO	4	-	-	-	10	-	-5.2	-1.55	-0.75	-	0 to 70	C	
		8-input	MC1052	MO	4	-	-	-	10	-	-5.2	-1.55	-0.75	-	0 to 70	C	
		6-input	MC1001P	MO	5	-	-	-	ac 45 dc 75	115	-5.2	-1.55	-0.75	-	0 to 75	G, DIP	
		6-input	MC1002P	MO	5	-	-	-	ac 45 dc 75	80	-5.2	-1.55	-0.75	-	0 to 75	G, DIP	
		6-input	MC1003P	MO	5	-	-	-	ac 45 dc 75	40	-5.2	-1.55	-0.75	-	0 to 75	G, DIP	
		Dual 4-input	MC1004P	MO	5	-	-	-	ac 15 dc 25	95	-5.2	-1.55	-0.75	-	0 to 75	G, DIP	
		Dual 4-input	MC1005P	MO	5	-	-	-	ac 15 dc 25	65	-5.2	-1.55	-0.75	-	0 to 75	G, DIP	
		Dual 4-input	MC1006P	MO	5	-	-	-	ac 15 dc 25	45	-5.2	-1.55	-0.75	-	0 to 75	G, DIP	
		6-input	MC1201F	MO	5	-	-	-	ac 45 dc 75	115	-5.2	-1.55	-0.75	-	-	C	
	6-input	MC1202F	MO	5	-	-	-	ac 45 dc 75	80	-5.2	-1.55	-0.75	-	-	C		
	6-input	MC1203F	MO	5	-	-	-	ac 45 dc 75	40	-5.2	-1.55	-0.75	-	-	C		
	6	Dual 4-input	MC1204F	MO	5	-	-	-	ac 15 dc 25	95	-5.2	-1.55	-0.75	-	-	C	
		Dual 4-input	MC1205F	MO	5	-	-	-	ac 15 dc 25	65	-5.2	-1.55	-0.75	-	-	C	
		Dual 4-input	MC1206F	MO	5	-	-	-	ac 15 dc 25	45	-5.2	-1.55	-0.75	-	-	C	
		3-input	MC356	MO	6	3	25	-	26	35	10	1.55	0.75	-	0 to 75	A, C	Expandable
		3-input	MC306	MO	7.0	3	15	-	ac 15 dc 25	37	-5.2	-1.55	-0.75	-	-	A, C	
		3-input	MC307	MO	7.0	3	15	-	ac 15	15	-5.2	-1.55	-0.75	-	-	A, C	Expandable, Comp. out
3-input		MC356	MO	7.0	3	15	-	ac 15 dc 25	37	-5.2	-1.55	-0.75	-	0 to 75	A, C	Expandable	
3-input		MC357	MO	7.0	3	15	-	ac 15 dc 25	15	-5.2	-1.55	-0.75	-	0 to 75	A, C	Expandable	
5-input		MC301	MO	7.5	-	5	-	ac 15 dc 25	37	-5.2	-1.55	-0.75	-	-	A, C		
5-input	MC351	MO	7.5	-	5	-	ac 15 dc 25	37	-5.2	-1.55	-0.75	-	0 to 75	A, C			
Gate Expanders E	5-input	MC305	MO	5	-	5	-	-	-	-5.2	-	-	-	-	A, C		
	5-input	MC355	MO	5	-	5	-	-	-	-5.2	-	-	-	0 to 75	A, C		
	-	SW305	SW	6	-	-	-	-	-	-5.2	-	-	-	-	A, C		
Level Translators F	DTL to ECL	MC318	MO	17	-	2	-	ac 15 dc 25	105	-5.2 & +6	-1.55	-0.75	-	-	A, C		
	DTL to ECL	MC368	MO	17	-	2	-	ac 15 dc 25	105	-5.2 & +6	-1.55	-0.75	-	0 to 75	A, C		
	ECL to DTL	MC317	MO	30	-	3	-	7	63	-5.2 & +6	-1.55	-0.75	-	-	A, C		
	ECL to DTL	MC367	MO	30	-	3	-	7 & +6	63	-5.2 & +6	-1.55	-0.75	-	0 to 75	A, C		
	DTL to ECL	MC1017P	MO	-	-	-	-	ac 15 dc 25	110	-5.2 & +6	-1.55	-0.75	-	0 to 75	G, DIP		
	MECL to DTL	MC1018P	MO	-	-	-	-	DTL 7	70	-5.2 & +6	-1.55	-0.75	-	0 to 75	G, DIP		
	DTL to ECL	MC1217F	MO	-	-	-	-	ac 15 dc 25	110	-5.2 & +6	-1.55	-0.75	-	-	C		
	MECL to DTL	MC1218F	MO	-	-	-	-	DTL 7	70	-5.2 & +6	-1.55	-0.75	-	-	C		
	DTL to CML CML to DTL	MC1511 MC1512	MO MO	- -	- -	1 25	- -	25 -	25 80	- -	-1.97 -0.75	-0.75 2.95	400 -	- -	A A		

Temperature range is -55 to 125°C unless otherwise stated.

# 5. Resistor-Capacitor Transistor Logic

Logic Function	Type	Model	Mfr.	Propagation Delay (ns)	Fan-in		Fan-out		Power Diss. mW (/ = per gate)	Supply Voltage (Volts)	Logic Levels (Volts)		Noise Margin (mV)	Temp Range (°C)	Package Type	Remarks	
					Typ.	Max.	Typ.	Max.			'0'	'1'					
Binary Elements A	J-K	FF7317E	IN	8	2	2	-	4	96	6	0.2	<6	1500	-	G	TF	
	R-S-T	FF8317E	IN	8	3	3	-	4	96	6	0.2	<6	1500	-	G	TF	
	Schmitt Trigg	ST2514B	IN	20	1	1	-	6	145	12	0.2	<12	2500	-	G	TF	
	R-S FF/Counter	SN510B	TI	300	-	-	-	4	2@3V	3-6	-	-	200	-	D	With Emitter Follower Dual Presets Dual Preset	
	R-S	SN511B	TI	300	-	-	-	20	2@3V	3-6	-	-	200	-	D		
	FF/Counter																
	R-S	SN5101B	TI	300	-	-	-	4	2@3V	3-6	-	-	200	-	D		
	R-S	SN5111	TI	300	-	-	-	20	3@3V	3-6	-	-	200	-	D		
	Ripple-Counter	SN5112	TI	300	-	-	-	16	3@3V	3-6	-	-	200	-	D		
	Ripple-Counter	SN5113	TI	300	-	-	-	16	4@4V	3-6	-	-	200	-	D		
	-	USO100A	SPR	-	-	-	-	4	2-7	3-6	2.5	0.3	-	-	-		
-	USO101A	SPR	-	-	-	-	20	2-7	3-6	2.5	0.3	-	-	-	USO101A		
-																	
Clock Driver B	-	SN517B	TI	-	-	-	-	20	3@3V	3-6	-	-	200	-	D		
Gates C	NAND/NOR	Dual 3-input	GG3317	IN	4	3	3	-	5	96	6	0.2	<6	1500	-	G	TF
		Dual	GG3317C	IN	6	3	-	-	5	96	6	0.2	<6	1000	-	G	
		R-S-J-K	FF0451B	IN	12	4	-	-	5	60	7	0.2	<7	1.5	-	G	
		R-S-T	FF6451B	IN	12	3	-	-	5	60	7	0.2	<7	1.5	-	G	
		Dual	GG3714C	IN	50	3	-	-	6	5	9	0.2	<9	2.5	-	G	
		6-input	SN512B	TI	65@6V	-	-	-	5	2@3V	3-6	-	-	200	-	D	
		6-input	SN513B	TI	65@6V	-	-	-	25	3@3V	3-6	-	-	200	-	D	
		Dual 3-input	SN514B	TI	65@6V	-	-	-	5	2@3V	3-6	-	-	200	-	D	
		Dual 2-input	SN516B	TI	65@6V	-	-	-	25	2@3V	3-6	-	-	200	-	D	
		Triple 2-input	SN5161B	TI	65@6V	-	-	-	5	2/ gate	3-6	-	-	200	-	D	
		Triple 2-input	SN5162B	TI	65@6V	-	-	-	25	2/ gate	3-6	-	-	200	-	D	
-	USO102A	SPR	100	-	6	-	5	2-7	3-6	2.5	0.3	-	-	-			
-	USO103A	SPR	100	-	6	-	25	2-7	3-6	2.5	0.3	-	-	-			
Exclusive OR	SN515B	TI	100@6V	-	-	-	5	3@3V	3-6	-	-	200	-	D			
Exclusive OR	SN5191	TI	-	-	-	-	5	6@3V	3-6	-	-	200	-	D			
Multivibrators D	Medium Delay	DM3510B	IN	-	1	1	-	5	96	12	0.2	<12	2500	-	G	TF	
		SN518B	TI	-	-	-	-	5	2@3V	3-6	-	-	200	-	D		

Temperature range is -55 to 125°C unless otherwise stated.

# 6. Complementary Transistor Logic

Logic Function	Type	Model	Mfr.	Propagation Delay (ns)	Fan-in		Fan-out		Power Diss. mW (/ = per gate)	Supply Voltage (Volts)	Logic Levels (Volts)		Noise Margin (mV)	Temp Range (°C)	Package Type	Remarks	
					Typ.	Max.	Typ.	Max.			'0'	'1'					
Binary Elements A	Dual-rank Dual Rank	CT <sub>μ</sub> L951	FA	15-20	-	-	15	-	150	4.5,-2	0.36	2.25	400	15 to 55	G		
		9957	FA	15	-	-	-	15	150	4.5,-2	-0.5	2.5	1100	15 to 55	G		
Buffers B	Dual 2-input J-K Master Slave R-S Master Slave Dual Latch	CT <sub>μ</sub> L956	FA	12	-	-	-	25	125	4.5,-2	0.36	2.25	400	15 to 55	G		
		9956	FA	12	-	-	-	25	125	4.5,-2	-0.5	2.5	1100	15 to 55	G		
		9967	FA	20	-	-	-	12	170	4.5,-2	-0.5	2.5	1100	15 to 55	G		
		9973	FA	20	-	-	-	12	150	4.5,-2	-0.5	2.5	1100	15 to 55	G		
		9968	FA	20	-	-	-	11	190	4.5,-2	-0.5	2.5	1400	15 to 55	G		
Gates C	AND 1	2, 2, 3 input	CT <sub>μ</sub> L953	FA	3	8	-	12	-	4.5,-2	0.36	2.25	400	15 to 55	G		
		Dual 4-input	CT <sub>μ</sub> L954	FA	3	8	-	12	-	4.5,-2	0.36	2.25	400	15 to 55	G		
		Single 8-input	CT <sub>μ</sub> L955	FA	3	8	-	12	-	4.5,-2	0.36	2.25	400	15 to 55	G		
	NOR 2	Dual 2-input	CT <sub>μ</sub> L952	FA	9	-	-	10	-	55	4.5,-2	0.36	2.25	400	15 to 55	G	
			9952	-	9	-	-	12	-	55	4.5,-2	-0.5	2.5	1100	15 to 55	G	
	AND/OR 3	2, 2, 3 input Dual 4-input Single 8-input 3, 1, 3 input 1, 1, 1, 1 input 2, 2, 2, 2 input 2, 2, 2, 2 input	9953	FA	3	-	-	-	11	35/ 4.5,-2	-5	2.5	-	15 to 55	G		
			9954	FA	3	-	-	-	11	35/ 4.5,-2	-5	2.5	-	15 to 55	G		
			9955	FA	3	-	-	-	11	35/ 4.5,-2	-5	2.5	-	15 to 55	G		
			9964	FA	3	-	-	-	11	35/ 4.5,-2	-5	2.5	-	15 to 55	G		
9965			FA	3	-	-	-	11	35/ 4.5,-2	-5	2.5	-	15 to 55	G			
9966			FA	3	-	-	-	11	35/ 4.5,-2	-5	2.5	-	15 to 55	G			
9971	FA	3	-	-	-	11	35/ 4.5,-2	-5	2.5	-	15 to 55	G	3 inputs 2 outputs				

Temperature range is -55 to 125°C unless otherwise stated.

# 7. MOS Arrays

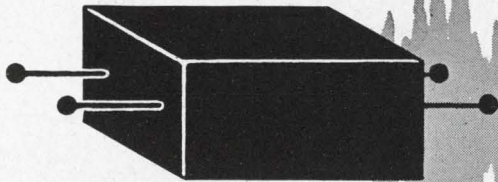
Logic Function	Type	Model	Mfr.	Propaga- tion Delay (ns)	Fan-in		Fan-out		Power Diss. mW (/ = per gate)	Supply Voltage (Volts)	Logic Levels (Volts)		Noise Margin (mV)	Temp Range (°C)	Package Type	Remarks
					Typ.	Max.	Typ.	Max.			'0'	'1'				
Gates <b>A</b>	Quad	MC1020P	MO	5	-	-	-	ac 15 dc 25	115	-5.2	-1.55	-0.75	-	0 to 75	G, DIP	
	Quad	MC1220F	MO	5	-	-	-	ac 15 dc 25	115	-5.2	-1.55	-0.75	-	-	C	
	Quad	MC1221F	MO	10	-	-	-	ac 15 dc 25	110	-5.2	-1.55	-0.75	-	-	C	
	Quad	MC1021P	MO	10	-	-	-	ac 15 dc 25	110	-5.2	-1.55	-0.75	-	0 to 75	G, DIP	
	Dual	SC126	SI	40	-	1	-	10	100	5 & 12	adj	adj	adj	-	D	
	Dual	SC426	SI	40	-	1	-	10	100	5 & 12	adj	adj	adj	0-75	D	
	Dual	MEM1000	GI	500	1	-	5	-	56	-13±1V	-2.0	-10.0	1000	-55 to 85	F	
	Dual 3-input	MEM1002	GI	330	1	-	5	-	36	-27±1V	-2.0	-10.0	1000	-55 to 85	-	
	-	MEM5014	GI	-	1	-	5	-	150	-27±1V	-2.0	-10.0	1000	-55 to 85	-	
	Dual	MEM1008	GI	500	1	-	5	-	42	-27±1V	-2.0	-10.0	1000	-55 to 85	G	
	9-bit	MEM1022	GI	1000	1	-	5	-	50	-27±1V	-2.0	-10.0	1000	-55 to 85	F	
	4-bit	MEM1050	GI	3200	1	-	5	-	240	-27±1V	-2.0	-10.0	1000	-55 to 85	-	
	Ternary	MEM5021	GI	500	1	-	5	-	78	13±1V	-2.0	-10.0	1000	-55 to 85	-	
Binary to Decimal	9960	FA	50	-	-	-	-	30	3.3-5.0	1.0	60.0	250	0 to 75	G	Nixie Driver	
Resistance	TEBR-2	BR	10	-	-	-	-	>60	>28	AR	AR	-	-	G	TF, ±5PPM	
NAND/NOR <b>B</b>	Dual 4-input	PL4G01	GME	1000	-	-	-	-	20	-12, -24	-3	-9	1000	-	G	-24v clock
	Dual	9302	FA	18	-	-	-	10	100	4.5-5.5	0.2	2.7	1000	-	C, G	
	2-Channel	D111F	SI	550	-	-	-	-	180	30	-	-	-	D	Buffer/Level Shifter	
	6-Channel	G116F	SI	-	-	-	-	-	-	-30	-	-	-	D		
Flip-Flop <b>C</b>	Dual J-K	PL4M01	GME	2500	-	-	-	-	100	-12, -24	-3	-9	1000	-	G	
	R-S-T F/F	MEM1005	GI	950	1	-	5	-	72	-27±1V	-2.0	-10.0	1000	-55 to 85	G	
Analog Switch <b>D</b>	4-channel	PL4S01	GME	-	-	-	-	-	150	-15-30+	10	0	1000	-	G	
	6-Channel	D/123F Series	SI	550	-	-	-	-	180	30	-	-	-	D	Buffer/Level Shifter	
Converter <b>E</b>	BCD to Decimal	PL4G02	GME	-	-	-	-	-	100	-12, -24	-3	-9	1000	-	G	
	BCD to Binary	PL4G03	GME	-	-	-	-	-	50	-24	-3	-9	1000	-	G	
	D to A	PL4S02	GME	-	-	-	-	-	75	-12, -24	-3	-9	1000	-	G	
Counter <b>F</b>	BCD Decade	PL4C01	GME	2500	-	-	-	-	75	-12, -24	-3	-9	1000	-	G	
	Binary to BCD	SN7441	TI	-	-	-	-	-	90	5.25	-	-	-	-	DIP	
Binary to Decimal	9301	FA	20	-	-	-	8	80	4.5-5.5	0.2	2.8	800	-	G		
Shift Reg. <b>G</b>	9-bit	PL4R01	GME	-	-	-	-	-	75	-12, -24	-3	-9	1000	-	G	
	9-bit	PL4R07	GME	-	-	-	-	-	75	-12, -24	-3	-9	1000	-	G	
	-	PL5200	GME	-	-	-	-	-	2.5/ bit	-20	-3	-9	1000	-	A	

Temperature range is -55 to 125°C unless otherwise stated.

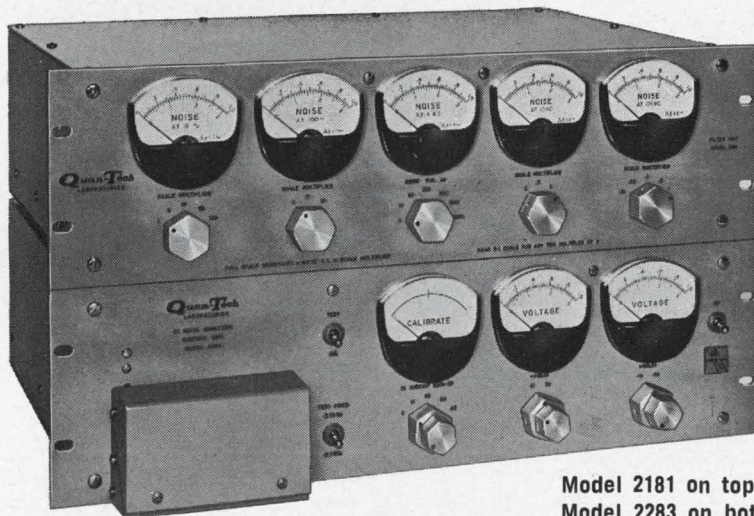
# 8. Miscellaneous Digital Circuits

	Logic Function	Type	Model	Mfr.	Propaga- tion Delay (ns)	Fan-in		Fan-out		Power Diss. mW (/= per gate)	Supply Voltage (Volts)	Logic Levels (Volts)		Noise Margin (mV)	Temp Range (°C)	Package Type	Remarks
						Typ.	Max.	Typ.	Max.			'0'	'1'				
Counter A	BCD decade	BCD decade	SN5490	TI	†12 MHz	-	-	-	-	150	4.5-5.5	-	-	1000	-	D	† Count freq.
	BCD decade	BCD decade	SN7490	TI	†12 MHz	-	-	-	-	150	4.75 to 5.25	-	-	1000	-	D	† Count freq.
	Decade BCD	Decade BCD	9075	FA	80	-	-	4	-	120	3.6-5.5	0.25	2.5	250	-	G	Preset from 0-9
	Modulo 16	Modulo 16	9076	FA	80	-	-	4	-	120	3.6-5.5	0.25	2.5	250	-	G	Preset from 0-9
Diode Matrix B	-	-	*	RAD	†10	-	-	-	-	450	40	-	-	-	-	D, G	†Reverse Recovery Time
	-	-	*20 matrix sizes, from 4 x 10	MC1116	MO	-	-	-	-	-	40(max)	-	-	-	-	A	
	-	-	to 15 x 15 in RM series.	MC1117	MO	-	-	-	-	-	40(max)	-	-	-	-	A	
	-	-		MC1118	MO	-	-	-	-	-	40(max)	-	-	-	-	A	
	Dual 3-input	Dual 3-input	MC217	MO	-	-	-	-	-	-	4	.3	-	-	-	A, C	
Dual 3-input	Dual 3-input	MC267	MO	-	-	-	-	-	-	4	.3	-	0 to 75	-	A, C		
Dual	Dual	WC217	WH	-	-	7	-	-	-	-	-	-	-	-	A		
Triple	Triple	WC227	WH	-	-	10	-	-	-	-	-	-	-	-	D		
Level Detector	C	-	WM208T	WH	1 MHz	-	-	-	-	6	-	-	-	-	-	A, C, D	
Memory D	16-bit	16-bit	SN5481	TI	Read: 25 Write: 25	-	-	-	-	150	4.5-5.5	-	-	1000	-	D	
	16-bit	16-bit	SN7481	TI	Read: 25 Write: 25	-	-	-	-	150	4.75 to 5.25	-	-	1000	0-70	D, J	
	8-bit	8-bit	9030	FA	-	-	-	10	100	4.5-5.5	0.2	2.7	1000	-	C, G		
	16-bit	16-bit	9033	FA	18	-	-	10	160	4.5-5.5	0.2	2.7	1000	-	G		
	4-bit	4-bit	9959	FA	80	-	-	6	125	3.3-5.0	0.25	2.5	250	-	G	Buffer	
16-bit	16-bit	TMC3162-64	TR	20	-	1	-	40mA	250	5	0.45	3.5	1000	0 to 75	D, P, DIP		
Pulse Source E	-	-	NM4002	NOR	25	-	-	-	-	590	+20	0	+3	-	-	A, B	Apollo pre core driver
Schmitt Trigger F	-	-	NC/PC17	GI	8	-	1	-	5	200	12, 4.2, -3	0	5	-	-	A, E	MC RCT
	-	-	WC208	WH	-	-	-	-	4	15	5.7-6.3	-	-	-	0 to 75	A, D	
Shift Register G	22-bit	22-bit	TEBR-1	BR	50	-	-	-	-	160	5	0.2	2.4	1000	-	G	MC; TF; 1"x1" FP
	4-bit	4-bit	9300	FA	17	-	-	-	10	100	4.5-5.5	0.2	2.7	1000	-	C, G	S/P, P/S
	4-bit	4-bit	9303	FA	17	-	-	-	10	100	4.5-5.5	0.2	2.7	1000	-	C	S/P, P/S
	4-bit	4-bit	9997	FA	40	-	-	-	7	110	3.6-5.5	0.25	2.5	250	-	C, G	S/P, P/S
	4-bit	4-bit	9998	FA	40	-	-	-	7	110	3.6-5.5	0.25	2.5	250	-	C, G	Complementary Outputs
	5-bit Parallel in/ 8-bit	5-bit Parallel in/ 8-bit	MEM SN5491	GI	-	1	-	5	-	15	-13±1V	-2.0	-10.0	1000	-55 to 85	F	
	8-bit	8-bit	SN7491	TI	†15 MHz	-	-	-	-	190	4.5-5.5	-	-	1000	-	D	† Shift freq.
	Parallel out	Parallel out	3005PP	TI	†15 MHz	-	-	-	-	190	4.75 to	-	-	1000	0-70	D	† Shift freq.
	8-bit Parallel in/ Serial out	8-bit Parallel in/ Serial out	MEM 3008PS	GI	-	1	-	5	-	24	-13±1V	-2.0	-10.0	1000	-55 to 85	F	
	12-bit Serial in/ Parallel out	12-bit Serial in/ Parallel out	MEM 3012SP	GI	-	1	-	5	-	170	-27±1V	-2.0	-10.0	1000	-55 to 85	C	
	Dual 16-bit	Dual 16-bit	MEM 3016-2	GI	-	1	-	5	-	100	-13±1V	-2.0	-10.0	1000	-55 to 85	G	
	Dual 16-bit	Dual 16-bit	MEM 3016-2D	GI	-	1	-	5	-	40	-27±1V	-2.0	-10.0	1000	-55 to 85	G	
	20-bit	20-bit	MEM3020	GI	-	1	-	5	-	50	-13±1V	-2.0	-10.0	1000	-55 to 85	G	
1-bit, 4-bit, 16-bit	1-bit, 4-bit, 16-bit	MEM3021	GI	-	1	-	5	-	150	-27±1V	-2.0	-10.0	1000	-55 to 85	G		
Dual 25-bit	Dual 25-bit	MEM3050	GI	-	1	-	5	-	30	-27±1V	-2.0	-10.0	1000	-55 to 85	G		
Serial Accumulator	Serial Accumulator	MEM3064	GI	-	1	-	5	-	40	-27±1V	-2.0	-10.0	1000	-55 to 85	F		
Steering Gate	H	-	NC/PC9	GI	-	-	-	-	-	-	-	-	-	-	-	A, E	MC RCDT
Utllogic I	AND Gate	Single	SU305	SIG	15	-	6	-	10	5	+4.5	-	-	-	-20, +85	A, C	
	AND Gate	Dual	SU306	SIG	15	-	3	-	10	5	+4.5	-	-	-	-20, +85	A, C	
	NOR Gate	Single	SU314	SIG	20	-	7	-	17	18	+4.5	0.6	3.3	1200	-20, +85	A, C	
	NOR Gate	Dual	SU315	SIG	20	-	3	-	17	18	+4.5	0.6	3.3	1200	-20, +85	A, C	
	NOR Gate	Dual	SU316	SIG	20	-	2	-	17	18	+4.5	0.6	3.3	1200	-20, +85	A, C	
	OR Gate	Dual	SU331	SIG	20	-	2	-	17	36	+4.5	0.6	3.3	1200	-20, +85	A, C	
	OR Gate	Dual	SU332	SIG	20	-	3	-	17	36	+4.5	0.6	3.3	1200	-20, +85	A, C	
	Expander	Dual	SU300	SIG	-	-	-	-	5	5	+4.5	-	-	-	-20, +85	A, C	
	J-K Binary	Single	SU320	SIG	65	-	-	-	17	90	+4.5	0.6	3.3	1200	-20, +85	A, C	

Temperature range is -55 to 125°C unless otherwise stated.



## HOW MUCH NOISE IN A BLACK BOX?



Model 2181 on top.  
Model 2283 on bottom.

Now you can measure noise in Linear IC's, Operational Amplifiers, and other "Black Boxes" SIMPLY, RAPIDLY, and EFFICIENTLY with

**Quan-Tech's** new

**Model 2283-2181  
Integrated Circuit  
Noise Analyzer**

Perhaps we should have called this instrument a Black Box Noise Analyzer — it's that versatile. Basically, it will measure anything from the thermal noise of a 10K ohm resistor up to a complete amplifier with 50db or more gain, or any combination of things in between. The Model 2283 Control Unit consists of a pair of extremely low-noise power supplies, one plus and one minus, each independently variable from zero to 30 volts at 100 milliamperes for biasing IC's and Op Amps. Included in the control unit is an amplifier having a voltage gain of 10,000 and a bandwidth of 5Hz to 125KHz. A 50db variable-plus-step attenuator compensates for the gain of the device under test, and a 1KHz calibrating signal is provided for standardizing overall gain.

Printed circuit cards that plug into the test jig provide almost unlimited versatility in the types of devices that can be tested. We have available standard cards with test sockets for the more commonly used linear IC's, or we'll design and build one for your pet devices, whether they be zener diodes, FET's, bi-polars or what. If you're the do-it-yourself type, be our guest and make your own.

The Model 2181 Filter Unit, when used with the Control Unit, permits noise measurements to be made at five frequencies simultaneously from 10Hz to 100KHz. If you don't need the simplicity and multiple frequency readout of the Model 2181, the Model 2283 Control Unit can be used with a wave analyzer to measure noise. Naturally, we recommend either our Model 303, 304, or 305, which have bandwidths and time constants especially suited for noise measurements. Whatever your requirements, this instrument can solve many noise measuring problems in connection with the new devices now becoming available.

Price: Model 2283 Control Unit \$1450.  
Model 2181 Filter Unit \$2500.

**Quan-Tech** LABORATORIES, INC.

10

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ON READER-SERVICE CARD CIRCLE 89

# 9. Linear Circuits

Function	Model	Mfr.	Frequency Range	Input (Volts)	Gain (db) or *(Volts)	Output (mW) or *(Volts)	Input Impedance (ohms)	Output Impedance (ohms)	Supply Voltage (Volts)	Noise Figure (db) or *(Volts)	Package Type	Remarks
Analog switch <b>A</b>	E16-501	AL	Ton <500 ns Toff <600 ns	±5	†40	-	-	-	40	-	A	†hFE
	45P912	GE	100 MHz	0.0006	-	-	-	-	20	-	A	
	4JP913	GE	100 MHz	0.0006	-	-	-	-	20	-	A	
	PC402H	GI	200	3	-	-	10 k/3.9 k	-	+45, +28	-	E	
	PC401H	GI	200	3	-	-	10 k/3.9 k	-	+45, +28	-	E	
	NM2017	NOR	200	5	-	-	10 k	-	10	-	D	
	2107B	AL	350 ns	5.6	-	*5.6	†0.4 nA	100	+12	-	A	
	2108B	AL	350 ns	6.5	-	*6.5	†0.4 nA	50	+18	-	A	
	2109B	AL	350 ns	8.5	-	*8.5	†0.4 nA	100	+12	-	A	†Cut-off current
	2110B	AL	350 ns	10	-	*10	0.4 nA	50	†18	-	A	
	8502	VAR	10 Hz - 100	0-20	46	10	10 k	1000	10 to 20	10	-	
2114B	VAR	900	9	46	*9	1.0	100	+15	-	G		
Audio Amp. <b>B</b>	AMC101	AMP	dc-20	-	80	.002	-	-	5	6	G	
	TAA310	AMP	15+	-	90	-	-	-	7	4	A	
	μA702	FA	dc to 30 MHz	±1.2 mV	67-70	*10	25-30 k	200	+12-6/-6-3	-	A, C	†Offset Voltage
	μA716C	FA	0 to 200	0-20	†	175	10 k	10	12 to 24	-70 dBm	A	†Selectable
	PA222	GE	70-14 k	-	-	1000	-	-	22-24	-60	DIP	
	NS7558	NA	dc-500	-	56	50	1 k	-	12	-	G	
	CA3000	RCA	1000	1.4	37	-	195	8000	+6,-6	-	A	
	CA3007	RCA	1000	0.57	22	-	4000	60	6,-6	-	A	
	CA3020	RCA	1000	-	58	550	40,000	-	+9	-	A	
	TAA111	SA	0.08-150	-	65	-	3000 (min)	-	7	-	5	
	TAA121	SA	0.05-150	-	65	-	3000 (min)	-	7	-	-	
	TAA131	SA	up to 20	-	64	-	-	-	5	-	-	Sub Min Case
	WC183	WH	.5-10	-	94	45	40 k	1 k	5	-	-	
	WC183	WH	.5-10	-	94	45	40 k	1 k	9	*3	A, D	
Broadband Amp. <b>C</b>	4JP108	GE	6 MHz	-	*20	-	50 k	1 k	15	-	A	
	HX610	HX	dc-150 MHz	±3V	52	32	300 k	300	±12	-	TO-100	
	PA7600	PH	0-200 MHz	-	†43	2.5	-	-	6	5	A	†MHz Video Bandwidth
	CA3011	RCA	4500	-	70	-	3000	31.5	7.5	8.7	A	
	CA3012	RCA	4500	-	65	-	3000	31.5	7.5	8.7	A	
	CA3013	RCA	100 to 20,00	-	75	-	3000	31.5	7.5	8.7	A	
	CA3014	RCA	100 to 20,000	-	75	-	3000	31.5	7.5	8.7	A	
	SE501	SIG	40	-	28	-	1.3 k	-	6.0	4 dB†	A, C	
	WM1146Q	WH	dc-100 MHz	-	16	-	-	-	12	4	C	
	D/A Switch <b>D</b>	4JP380	GE	250 MHz	-	-	-	-	20	5	-	A
Demodulator Chopper <b>E</b>	NM2024	NOR	5	26	-	-	-	-	28	-	D	
Differential Amp. <b>F</b>	D13-000	AL	400	-	45	6-V	20 k	5 k	±12	-	A, C	
	D13-001	AL	400	-	45	6 V	10 k	5.5 k	±12	-	A, C	
	D13-002	AL	400	-	45	5 V	5 k	5.5 k	±12	-	A, C	
	831A	AL	dc-400	*2.5 mV	66	*6 k	40 k	5 k	±12	-	A, C	* Offset Voltage
	831B	AL	dc-400	*8 mV	66	*6	20 k	5.5 k	±12	-	A, C	* Offset Voltage
	831C	AL	dc-400	*20 mV	63.5	*5	20 k	5.5 k	±12	-	A, C	* Offset Voltage
	831D	AL	dc-400	*10 mV	63.5	*6	20 k	6V	±12	-	A	* Offset Voltage
	μA711	FA	40 ns	†1 mV	63	*±4.5,-0.5	200	200	+12,-6	-	A	dual input †offset voltage
	PC200	GI	0-20	-	73	-	100 k Diff.	200	±2 to ±22	5μV	E	
	PC201	GI	0-20	-	73	-	200 k Diff.	200	+6 to ±22	5μV	F	
	MC1429	MO	250 kHz @ 3dB BW	±5	38	*±6	40 k	17 k	±12	-	A	†CE/CC
	MC1519	MO	1 MHz	±5	73/45†	-	2.6 k/1.2 k†	2.7 k/48†	±14	-	A	
	MC1525	MO	1400	±5	140	-	2 k	11 k	±14	-	A	
	MC1526	MO	500	±5	65	-	60 k	11 k	±14	-	A	
	MC1529	MO	300 kHz @ 3dB BW	±5	38	*±6	50 k	15 k	±12	-	A	Darlington (npn)
	NM1005	NOR	300	†2 mV	75	*16	3.2 k	100	†12,-6	*2.5 mV	A, D	†Offset Voltage
	NM1006	NOR	1 MHz	†8 mV	66	*8	250 k	100	10	*2 mV	D	†Offset Voltage
	NM1021	NOR	1 MHz	†4 mV	60	*6	1.5 M	5 k	†12,-25	-	-	†Offset Voltage
	SE505	SIG	1000	-	1500	-	4 k	-	+6,-3	-	A, C	
	203	SSD	500	±3	40	150	75,000	300	25	2 μV*	C	
SN523A	TI	dc-3 MHz	±5	66	4	10 k	10 k	±12	-	A, D		
SN525A	TI	dc-1 MHz	±5	88	4	100 k	10 k	±12	-	D		
SN723	TI	dc-3 MHz	±5	64	4	10 k	10 k	±12	-	A, D		
SN725	TI	dc-45	†2 mV	86	*16	140 k	10 k	±12	-	D	†Offset voltage	
SN5231L	TI	dc-3 MHz	±5	66	*±12	15 k	200	±12	-	G		
SN5510	TI	dc-300 MHz	±4	40	0.4	3.5 k	35	±6	-	D		
SNX1312	TI	50	†1 mV	58	*±10	100 k	45	±12	-	G	†Offset voltage	
WC115T	WH	0-300	240M	60V/V	*5	150 k	8 k	±12	-	A		
WC750T	WH	dc-2 MHz	-	2000 V/V	72	32 k	1 k	±15	-	A	Two circuits/pkg.	
Differential Comparator <b>G</b>	μA710	FA	40 ns	†2 mV	63	*±3.2,-0.5	-	200	+12,-6	-	A, C	† offset voltage
	μA710C	FA	40 ns	†2 mV	63	*±3.2,-0.5	-	200	+12,-6	-	A, C	† offset voltage
	μA711C	FA	40 ns	†1 mV	63	*±4.5,-0.5	-	200	+12,-6	-	A	dual input †offset voltage
	NM1037	NOR	100	±10	*1000	*6	-	3 k	30	-	A	Min-Max Limit Detector
	PA710	PH	40 ns	†2 mV	64	*±3.2,-0.5	-	200	±12-6	-	A, C	†Offset
	SE560	SIG	10 MHz	-	1700	-	-	-	-	-	A, C	
	SN52710	TI	40 ns	†2 mV	63	*±3.2,-0.5	-	200	+12,-6	-	D, G	†Offset voltage
	SN52711	TI	40 ns	†1 mV	63	*±4.5,-0.5	-	200	+12,-6	-	D, G	†Offset voltage
	SN72710	TI	40 ns	†2 mV	63	*±3.2,-0.5	-	200	†12,-6	-	D, G	†Offset Voltage
	SN72711	TI	40 ns	†1 mV	63	*±4.5,-0.5	-	200	+12,-6	-	D, G	†Offset voltage

## 9. Linear Circuits (continued)

Function	Model	Mfr.	Frequency Range	Input (Volts)	Gain (db) or *(Volts)	Output (mW) or *(Volts)	Input Impedance (ohms)	Output Impedance (ohms)	Supply Voltage (Volts)	Noise Figure (db) or *(Volts)	Package Type	Remarks	
Driver Switch	H	NM1038	NOR	50	±10	—	11 k	—	34, 6, -6	—	D		
Emitter Coupled Amp.	I	MC1110	MO	dc-300 MHz	0.114	26	10	2 k	5 k	±12	6	A	
		TAA293	AMP	0-600	—	80	—	—	—	7	5	A	
		12X218	GE	10-100	—	—	—	50 M	250	25	B	E	
		4JPA113	GE	100	—	85	50	20 k	50	15	—	A	
		4JP114	GE	1 MHz	—	†3,000	45	1.5 k	10 k	6	—	A	†Current gain
		NM1032	NOR	dc - 190	—	45	—	34 k	2 k	6, -12	—	D	
		NM1033	NOR	dc - 190	—	66	—	3.4 k	2 k	12, 6, -12	—	D	
		PA7602	PH	0-100	—	76	*6	†>25 k	†<50	12	—	A	†Gain of 40dB
		UC1501A	SPR	3 - 250	—	84	500	2 k	150	15	—	—	
		UC1503A	SPR	200 Hz - 3 MHz	—	60	600	20 k	150	15	—	—	
		UC1505A	SPR	30 Hz - 11 MHz	—	40	600	47 k	150	15	—	—	
		UC1507A	SPR	10 Hz - 10 MHz	—	34	600	47 k	150	15	—	—	
		WC-934	WH	0-1500	—	30 mV	32	—	180 k	100	±9	4	D
General Purpose Amp.	J	12X207	GE	10-100	0.0001	*600	—	10 k	1 M	30	10 mV rms	A	
Limiter	K	UC1508A	SPR	50 Hz - 12 kHz	2	40	16	40 k	15	15	—	—	
Operational Amp.	L	A13-251	AL	10 MHz	—	86	*10	250 k	1 k	±12	—	A	
		800B	AL	dc-10 MHz	†5 mV	86	*±10	1 M	400	±12	—	A	†Offset voltage
		800D	AL	dc-10 MHz	†10 mV	86	*±9	500 k	400	±12	—	A	†Offset voltage
		801B	AL	dc-10 MHz	*5 mV	86	*±10	1M	400	±12	—	A	* Offset Voltage
		801D	AL	dc-10 MHz	*10 mV	86	*±9	500 k	400	±12	—	A	* Offset Voltage
		805B	AL	dc-10 MHz	*3 mV	94	*±13	1M	150	±15	—	A, C	* Offset Voltage
		805C	AL	dc-10 MHz	*3 mV	94	*±13	1M	150	±15	—	A	* Offset Voltage
		806B	AL	dc-10 MHz	*3 mV	94	*±10	1M	150	±12	—	A	* Offset Voltage
		806C	AL	dc-10 MHz	*3 mV	94	*±10	1M	150	±12	—	A	* Offset Voltage
		807B	AL	dc-10 MHz	*1 mV	94	*±13	1M	150	±15	—	A, C	* Offset Voltage
		2404B	AL	dc-10 MHz	*3 mV	100	±11	10 <sup>11</sup>	500	±15	—	G	* Offset Voltage
		2405B	AL	dc-10 MHz	*3 mV	100	±25	10 <sup>11</sup>	500	±30	—	G	* Offset Voltage
		ATF401	AMP	dc to 2 MHz	4-10	88	25	200 k	—	±15	—	—	
		TEBR-3	BR	dc-500	0.001	93	*±14	10 k	0.1	±15	—	G	TF; multi-gain
		805-3	CDC	1 MHz	100 μV	96	90	1000 k	24	±15	—	A	
		805-4	CDC	1 MHz	100 μV	96	90 dB	1000 kΩ	150	±15	—	A	
		806-3	CDC	1 MHz	100 μV	96	90 dB	1000 kΩ	150	±15	—	A	
		806-4	CDC	1 MHz	100 μV	96	90 dB	1000 KΩ	150	±15	—	A	
		807-4	CDC	1 MHz	50 μV	96	90 dB	1000 KΩ	150	±15	—	A	
		μA702A	FA	dc-30MHz	†2 mV	68	*±5.3	25 k	200	+12,-6	—	A, C	RA, ITT
		μA702C	FA	dc-30 MHz	†5 mV	68	*±5.3	20 k	200	+12,-6	—	A, C	RA, ITT
		μA709	FA	0 to 1 MHz	±1 mV	96	*24	500 k	150	±15,±9	—	A, C	RA, ITT
		μA709C	FA	0 to 1 MHz	±2. nV	93	*27	300 k	150	±15,±9	—	A, C	RA, ITT
		4JPA107	GE	200	—	70	±10	750 k	100	±12	—	A	
		4JPA135	GE	200	—	70	*±4	1 M	100	±6	—	A	
		TMC40006	MEP	100	—	60	—	100 k	5 k	±12	—	G	
		MC1430	MO	1 MHz @ 3dB BW	±5	74	*±5	15 k	25	±6	—	A, C	2 mV noise voltage
		MC1431	MO	150 kHz @ 3dB BW	±5	71	*±5	600 k	25	±6	—	A, C	5 mV noise voltage
		MC1433	MO	200 kHz @ 3dB BW	±10	†60,000	*±13	600 k	100	±15	—	A, C	†V/V, 0.3μV noise voltage
MC1530	MO	1.2 MHz	±5	74	10	10 k	25	±9	—	A			
MC1531	MO	400	±5	71	10	1 M	25	±9	—	A			
MC1533	MO	200 kHz @ 3dB BW	±10	†60,000	*±13	1 M	100	±15	—	—			
MC1709	MO	200 kHz @ 3dB BW	±5	†45,000	*±14	400 k	150	±15	0.8μV	A	†V/V		
NS7560	NA	dc-10 MHz	5	63	—	2.5M	70	+12,-12	—	G	† Offset Voltage		
NS7560A	NA	dc-10 MHz	1	74	—	2.5M	70	+12,-12	—	G	† Offset Voltage		
PA702A/712	PH	0.8 MHz	†2 mV	68	*±5.3	25 k	200	12-6, 6-3	—	A, C	† Offset Voltage		
PA7026	PH	0-8 MHz	†7 mV	68	*±5.3	20 k	200	12-6	—	A, C	† Offset Voltage		
Q25AH	PR	0-2	±10	86-116	24	10 <sup>12</sup>	100 k	±15	0.5	G	FETs		
Q82AH	PR	dc-70 MHz	±10	86-92	100	2M	150 (Open Loop)	±15	4	G			
Q85AH	PR	0-2000	±11	86-116	24	10 <sup>8</sup>	100 k	±15	2	G			
RA-238	RAD	7000	±12	68	*21	250,000	250	-15,+25	—	D	Offset Voltage Adjustable		
RA-239	RAD	dc-15,000	±12	68	*21	100,000	150	-15,+25	—	D	Offset Voltage Adjustable		
RA-240	RAD	dc-6000	±6	84	*9.6	150,000	100	-15,+25	—	D	Offset Voltage Adjustable		
RA-335	RAD	7000	±12	68	*21	250,000	250	-15,+25	—	D	Offset Voltage Adjustable		
RA-338	RAD	7000	±12	68	*21	250,000	250	-15,+25	—	D	Offset Voltage Adjustable		
RA-339	RAD	dc-15,000	±12	68	*21	150,000	150	-15,+25	—	D	Offset Voltage Adjustable		
RA-339	RAD	dc-15,000	±12	68	*21	100,000	150	-15,+25	—	D	Offset Voltage Adjustable		
RA-340	RAD	dc-6000	±6	84	*9.6	150,000	100	-15,+25	—	D	Offset Voltage Adjustable		
RA-340	RAD	dc-6000	±6	84	*9.6	150,000	100	-15,+25	—	D	Offset Voltage Adjustable		
RA-538	RAD	dc-7000	±12	68	*21	250,000	250	-15,+25	—	D	Offset Voltage Adjustable		
RA-539	RAD	dc-15,000	±12	68	*21	100,000	150	-15,+25	—	D	Offset Voltage Adjustable		
RA-540	RAD	0-6000	±6	84	*9.6	150,000	100	-15,+25	—	O	Offset Voltage Adjustable		
CA3008	RCA	300	—	-4 to +1	60	—	14K	200	+6,-6	—	A, F		
CA3015,6	RCA	320	—	-8,+1	70	—	7.8 k	92	+12,-12	—	A, F		
CA3029	RCA	1000	—	1	60	—	14,000	200	+6,-6	—	A		

# 9. Linear Circuits (continued)

Function	Model	Mfr.	Frequency Range	Input (Volts)	Gain (db) or *(Volts)	Output (mW) or *(Volts)	Input Impedance (ohms)	Output Impedance (ohms)	Supply Voltage (Volts)	Noise Figure (db) or *(Volts)	Package Type	Remarks		
Operational Amp. L	CA3031	RCA	-	-8,+1.5	85	-	25 k	130	+12,-6	-	A	Emitter follower  f <sub>RL</sub> = 0.6 k $\Omega$ †Offset voltage †Offset voltage †Offset voltage †Offset voltage		
	CA3032	RCA	-	-8,+1.5	85	-	20 k	200	+12,-6	-	A			
	SE506	SIG	300	-	13,000	-	200 k	-	+15,-15	-	A, C			
	SN521A	TI	dc - 50	+4	62	-	12 k - 100 k	10 k	10, 6, -9	-	D			
	SN522A	TI	dc - 50	+4	62	-	12 k - 100 k	160	10, 6, -9	-	D			
	SN524A	TI	dc-3 MHz	±5	60	4	1 M	75	±12	-	A, D			
	SN526A	TI	dc-1 MHz	±5	88	70	1000 k	12 k	±12	-	D			
	SN724	TI	dc-3 MHz	±5	54	4	750 k	75	±12	-	A, D			
	SN726	TI	dc-1 MHz	±5	56	*±5	†200 k	-	±12	-	D			
	SN52702	TI	dc-30 MHz	†2 mV	67	*±5.3	25 k	200	+12 -6	-	D, G			
	SN52709	TI	dc-500	†1 mV	93	*±14	400k	150	±15	-	D, G			
	SN72702	TI	dc-30 MHz	†5 mV	67	*±5.3	20 k	200	+12, -6	-	D, G			
	SN72709	TI	dc-500	+2 mV	93	*±14	250 k	150	±15	-	D, G			
	UC4000	UC	1500	+10	86	20	1.5M	30	±15	-	101			
	UC4001	UC	1500	+10	86	20	1.5M	30	±15	-	101			
UC4002	UC	1500	+10	86	20	1.5M	30	±15	-	101				
WC161Q	WH	500	+6.25	*2200	50	300 k	40	±12	-	C	Single & Diff Output			
PC-210H	GI	1.5 MHz	+8	70	*±15	30 k	50	±18	4 $\mu$ V	E				
PC212H	GI	1.2 MHz	±8	64	*±10	100 k	50	±12	4 $\mu$ V	E				
PC250	GI	30	±20	50	-	10 $\mu$	150	±12	-	E				
PC-251	GI	30	±20	50	-	10 $\mu$	150	±12	-	E	Short-circuit proof			
Phase Splitter Amp. M	UC1502A	SPR	3 - 250	-	84	160	2 k	100	15	-	-			
	UC1504A	SPR	200 Hz - 3 MHz	-	58	230	20 k	100	15	-	-			
	UC1506A	SPR	30 Hz - 11 MHz	-	39	230	20 k	100	15	-	-			
Power Amp. N	MC1524	MO	300	+5	*10/20/40	1000	8.5 k	0.58	±12	-	A	Modified To-53 Modified To-53		
	NM1003	NOR	dc - 20	0-60	54	8000	10 k	500	36	-	G			
	NM1008	NOR	dc - 20	0-60	46	8000	10 k	300	36	-	G			
Pulse Amp. O	UC1509A	SPR	-	5	22	-	20 k	100, 10	15	-	-			
	UC1510A	SPR	-	6.7	0	-	40 k	100, 10	15	-	-			
12X264	GE	10 MHz	-	25	-	-	-	15	-	-	A			
RF/IF Amp. P	903B	AL	dc-110 MHz	-	15	*4	25 pF/10 m $\mu$ c	7 pF/0.5 m $\mu$ c	+12, -6	-	A	†12 MHz Video Bandwidth		
	903C	AL	dc-110 MHz	-	15	*4	25 pF/10 m $\mu$ c	7 pF/0.6 m $\mu$ c	+12, -6	-	A			
	MC1550	MO	22 MHz	+5	26	*4.2	1800	100 k	+6	<5	A			
	PA7602	PH	10-200 MHz	-	18	*1	90	95	+6	-	A			
	PA713	PH	0-200 MHz	-	†33	-	450	900	6	7	A-C			
	CA3002	RCA	11,000	2.2	20	-	100,000	70	6,-6	4	A			
	CA3004	RCA	100,000	-2.5, +3.5	12	-	1.2 k	2200	+6,-6	6.3	A			
	CA3005	RCA	100,000	-2.5 +3.5	16	-	1.4 k	200	+6,-6	7.8	A			
	CA3006	RCA	100,000	0.8	16	-	1.4k	2000	+6,-6	7.8	A			
	CA3028	RCA	100,000	-	16	-	-	-	-	6.8	A			
	Sense Amp. Q	MC1540	MO	0-40 MHz	17 mV	39	*5.9	-	-	+6	-		A	Core Memory Appl †Offset Voltage †Offset Voltage †Offset Voltage Temp. Compensated
		NM2012	NOR	0-1 MHz	†1 mV	49	*4	-	-	13	-		A, D	
NM2016		NOR	0-1 MHz	†4 mV	54	*4	-	-	30	-	A, D			
SE500		SIG	0-3 MHz	-	31	-	-	-	+13,+4,+1.5	-	A, C			
SE504		SIG	3000	-	30	-	-	-	13.0	-	A, C			
SA10 SA11		SY	7 MHz	17 mV	-	-	240	-	-25, 12, +5	-	D, G			
SN5500		TI	†125 ns	6	-	-	-	-	+6	-	A, D			
SN7500		TI	†125 ns	6	-	-	-	-	+6	-	D			
SN7501		TI	0.7 $\mu$ s-cycle time	†12-20mV	-	*0.4, 2.6	5 k	-	±5	-	D			
SN7502		TI	1.5 $\mu$ s-cycle time	†14-24mV	-	*0.4, 2.6	5 k	-	-	±5	D			
Summing Amp. R		4JP116	GE	100 MHz	-	1 x 10 <sup>6</sup>	-	1	1	+25	-	A		
Video Amp. S	E13-511	AL	50 MHz	0.26	22	-	520	520	+12	-	A	* Offset Voltage		
	901B	AL	dc-60 MHz	*260 mV	24	*7	550	500	+12	-	A			
	901C	AL	dc-60 MHz	260 mV	24	*7	550	500	+12	-	A			
	NC/PC101	GI	40 MHz	0.2	20	4.5	1 k	500	6	3	A, E			
	MC1552	MO	40 MHz	+1,-5	40	*2.9	10 k	50	+6	5 @ 30 MHz	A			
	MC1553	MO	35 MHz	+1,-5	52	*2.9	10 k	50	+6	5 @ 30 MHz	A			
	NS7512A	NA	dc-100 MHz	-	25	-	500	500	+12	-	G			
	CA3001	RCA	11,700	1.5	19	-	50,000	70	-	-	A			
	CA3021	RCA	56,000	1.8	56	-	550	300	-	-	A			
	CA3022	RCA	2500	2	57	-	360	120	-	-	A			
	CA3023	RCA	5000	1	53	-	180	98,000	-	-	A			
	SA20	SY	up to 100 MHz	-	45	-	2.6 k	>5	24	15	A			
	SN7510	TI	dc-40 MHz	-	39	-	6 k	35	+6	*5 $\mu$ V	D, G			
	WC1146	WH	0-45,000	-	23	-	90	2000	12	4	A, C			
	WM1146	WH	0-35 MHz	-	20	-	100	2 k	12	4	C			
	Voltage Reg. T	2802B	AL	-	+20,+14	60	†*12	-	.5	-	-		G	†0.2% †0.2% MC; TF; up to 1 amp.
2803B		AL	-	-20,-14	60	†*-12	-	.5	-	-	G			
BR-801		BR	100	±10 to ±40	-	*1.5 to ±38	-	2	+10 to ±40	-	G			
NC511/PC511H		GI	100	+15 to +24	-	150mA	-	0.1	+12	0.4 mV	A or E			
NC512/PC512H		GI	100	+27 to +36	-	140mA	-	0.2	+24	1 mV	E			
NC513/PC513H		GI	100	-15 to -24	-	150mA	-	0.1	-12	0.4 mV	A or E			
NC514/PC514H		GI	100	-27 to -36	-	140mA	-	0.2	-24	1 mV	E			

Reader-Service cards are good all year.



# 9. Linear Circuits (continued)

Function	Model	Mfr.	Frequency Range	Input (Volts)	Gain (db) or *(Volts)	Output (mW) or *(Volts)	Input Impedance (ohms)	Output Impedance (ohms)	Supply Voltage (Volts)	Noise Figure (db) or *(Volts)	Package Type	Remarks	
Voltage Reg. T	NC521/PC521H	GI	100	+28	-	*+6	-	0.05	-	-	E	I <sub>max</sub> =200 mA	
	NC523/PC523H	GI	-	-28	-	*-6	-	0.05	-	-	E	I <sub>max</sub> =200 mA	
	NCS-675A	GI	-	+28	-	*+5	-	0.1	-	-	A	I <sub>max</sub> =200mA	
	PC501H	GI	100	+16to+24	-	150mA	-	0.2	+12	0.4 mV	E		
	PC502H	GI	100	-16 to -24	-	150mA	-	0.2	-12	0.4 mV	E		
	PC503H	GI	100	+28 to +36	-	140mA	-	0.4	+24	1 mV	E		
	PC504H	GI	100	-28 to -36	-	140 mA	-	0.4	-24	1 mV	E		
	NM1004	NOR	-	>20, >30	-	+1.25mA	-	-	715	1 mV	-	†Drive Current	
	1APU6	TRI	dc	10-31	-	*6	-	0.06	-	-	G	1A	
	1APU12	TRI	dc	16-37	-	*12	-	0.12	-	-	G	1A	
	1APU18	TRI	dc	22-40	-	*18	-	0.18	-	-	G	1A	
	1APU24	TRI	dc	28-40	-	*24	-	0.24	-	-	G	1A	
	3APL2	TRI	-	4-15	80	*2	-	0.006	-	-	G	3A	
	3APL3	TRI	-	5-15	80	*3	-	0.008	-	-	G	3A	
	3APL4	TRI	-	6-15	75	*4	-	0.010	-	-	G	3A	
	3APL5	TRI	-	7-18	75	*5	-	0.012	-	-	G	3A	
	3APL6	TRI	-	8-20	70	*6	-	0.014	-	-	G	3A	
	3APL8	TRI	-	10-20	70	*8	-	0.016	-	-	G	3A	
	3APL10	TRI	-	12-25	80	*10	-	0.005	-	-	G	3A	
	3APL12	TRI	-	14-30	80	*12	-	0.006	-	-	-	3A	
	3APL15	TRI	-	17-35	75	*15	-	0.008	-	-	G	3A	
	3APL18	TRI	-	20-35	75	*18	-	0.010	-	-	G	3	
	3APL22	TRI	dc	24-40	70	*22	-	0.012	-	-	G	3A	
	3	3APL27	TRI	dc	29-45	70	*27	-	0.014	-	-	G	3A
		3APL33	TRI	dc	35-50	70	*33	-	0.016	-	-	G	3A
		75TE3.9	TRI	dc	>out	-	*3.9	-	0.006	-	-	G	3A or 75W
		75TE4.7	TRI	dc	>out	-	*4.7	-	0.008	-	-	G	3A or 75W
		75TE5.6	TRI	dc	>out	-	*5.6	-	0.010	-	-	G	3A or 75W
		75TE6.8	TRI	dc	>out	-	*6.8	-	0.012	-	-	G	3A or 75W
		75TE8.2	TRI	dc	>out	-	*8.2	-	0.015	-	-	G	3A or 75W
		75TE10	TRI	dc	>out	-	*10	-	0.005	-	-	G	3A or 75W
		75TE12	TRI	dc	>out	-	*12	-	0.006	-	-	G	3A or 75W
		75TE15	TRI	dc	>out	-	*15	-	0.008	-	-	G	3A or 75W
		75TE18	TRI	dc	>out	-	*18	-	0.009	-	-	G	3A or 75W
		75TE22	TRI	dc	>out	-	*22	-	0.011	-	-	G	3A or 75W
		75TE27	TRI	dc	>out	-	*27	-	0.013	-	-	G	3A or 75W
		75TE33	TRI	dc	>out	-	*33	-	0.015	-	-	G	3A or 75W
		75TE39	TRI	dc	>out	-	*39	-	0.018	-	-	G	3A or 75W
		75TE47	TRI	dc	>out	-	*47	-	0.021	-	-	G	3A or 75W
		75TE56	TRI	dc	>out	-	*56	-	0.025	-	-	-	3A or 75W
		80TF3.9	TRI	dc	>out	-	*3.9	-	0.006	-	-	G	3A or 80W
		80TF4.7	TRI	dc	>out	-	4.7	-	0.008	-	-	G	3A or 80W
		80TF5.6	TRI	dc	>out	-	5.6	-	0.010	-	-	G	3A or 80W
	80TF6.8	TRI	dc	>out	-	*6.8	-	0.012	-	-	G	3A or 80W	
	80TF8.2	TRI	dc	>out	-	*8.2	-	0.015	-	-	G	3A or 80W	
80TF10	TRI	dc	>out	-	*10	-	0.005	-	-	G	3A or 80W		
80TF12	TRI	dc	>out	-	*12	-	0.006	-	-	G	3A or 80W		
80TF15	TRI	dc	>out	-	*15	-	0.008	-	-	-	3A or 80W		
4	80TF18	TRI	dc	>out	-	*18	-	0.009	-	-	G	3A or 80W	
	80TF22	TRI	dc	>out	-	*22	-	0.011	-	-	G	3A or 80W	
	80TF27	TRI	dc	>out	-	*27	-	0.013	-	-	-	3A or 80W	
	80TF33	TRI	dc	>out	-	*33	-	0.015	-	-	-	3A or 80W	
	80TF39	TRI	dc	>out	-	*39	-	0.018	-	-	G	3A or 80W	
	80TF47	TRI	dc	>out	dc	*47	-	0.021	-	-	G	3A or 80W	
	80TF56	TRI	dc	>out	-	*56	-	0.025	-	-	G	3A or 80W	
	WC110T	WH	100	10-50	-	2A	-	0.004	-	-	TO-3		

Complete listing of semiconductor manufacturers starts on page 86.

Circle as many numbers on the reader-service card as you like.

Valuable reprints are FREE if you circle them on the reader-service card.

# Microelectronic Cross-Index

This cross-index helps you locate any microelectronic circuit quickly and easily. The first digit indicates the type of logic. The letter indicates the location of the circuit in the logic family. The last digit pinpoints the location of the circuit.

For example, to look up the DT $\mu$ L930, turn to letter "D" and find the entry DT $\mu$ L930. The cross-index directs you to 1D12. The number "1" refers to the first microelectronic category, "1. Diode Transistor Logic." "D" is the function category (in the case "gates"). Number 12 pinpoints the DT $\mu$ L930 in the gate table.

NUMERICAL							
1APU6	9T2	75TE56	9T3	124B	2E3	342BG	1I
1APU12	9T2	80TF3.9	9T3	124C	2E3	342CG	1I
1APU18	9T2	80TF4.7	9T3	125A	2E3	342CJ	1I
1APU24	9T2	80TF5.6	9T3	125B	2E3	361BG	1F
3APL2	9T2	80TF6.8	9T3	125C	2E3	361CG	1F
3APL3	9T2	80TF8.2	9T3	126A	2E3	361CJ	1F
3APL4	9T2	80TF10	9T3	126B	2E3	362BG	1F
3APL5	9T2	80TF12	9T3	126C	2E3	362CG	1F
3APL6	9T2	80TF15	9T3	128A	2E3	362CJ	1F
3APL8	9T2	80TF18	9T4	128B	2E3	500B	3E15
3APL10	9T2	80TF22	9T4	128C	2E3	501B	3E15
3APL12	9T2	80TF27	9T4	131A	2F	502B	3E15
3APL15	9T2	80TF33	9T4	131B	2F	503B	3E16
3APL18	9T2	80TF39	9T4	131C	2F	504B	3E16
3APL22	9T2	80TF47	9T4	132A	2G	505B	3E16
3APL27	9T3	80TF56	9T4	132B	2G	506B	3E16
3APL33	9T3	101A	2C1	132C	2G	507B	3E16
4APL08	9C	101B	2C3	141A	2A1	508B	3E22
4JP114	9I	102A	2C1	141B	2A2	509B	3B7
4JP116	9R	102B	2C3	141C	2A2	511B	3D
4JP380	9D	111A	2B1, 2I2	142A	2D	530B	3E15
4JP912	9A	111B	2B2, 2I2	142B	2D	531B	3E15
4JP913	9A	111C	2B2, 2I2	142C	2D	532B	3E15
4JPA107	9L2	112A	2B1, 2I2	203	9F2	533B	3E15
4JPA113	9I	112B	2B2, 2I2	301BG	1C2	534B	3E15
4JPA135	9L2	112C	2B2, 2I2	301CG	1C2	535B	3E15
12X207	9J	114A	2B2, 2I2	301CJ	1C2	536B	3E15
12X218	9I	114B	2B2, 2I2	311BG	1B4	537B	3E15
12X264	9F2	114C	2B2, 2I2	311CG	1B4	538B	3E22
75TE3.9	9T3	116A	2B1	311CJ	1B4	539B	3B8
75TE4.7	9T3	116B	2B1	321BG	1D9	540B	3D
75TE5.6	9T3	116C	2B1	321CG	1D9	541B	3D
75TE6.8	9T3	117A	2I1	321CJ	1D9	542B	3D
75TE8.2	9T3	117B	2I2	322BG	1D9	543B	3E13
75TE10	9T3	117C	2I2	322CG	1D9	544B	3E13
75TE12	9T3	121A	2E3	322CJ	1D9	547B	3E14
75TE15	9T3	121B	2E3	323BG	1D9	548B	3E14
75TE18	9T3	121C	2E3	323CG	1D9	570B	3E14
75TE22	9T3	122A	2E3	323CJ	1D9	571B	3E14
75TE27	9T3	122B	2E3	331BG	1D1	572B	3E14
75TE33	9T3	122C	2E3	331CG	1D1	573B	3E14
75TE39	9T3	123A	2E3	331CJ	1D1	574B	3E14
75TE47	9T3	123B	2E3	341BG	1D17	575B	3E14
		123C	2E4	341CG	1D17	576B	3E14
		124A	2E3	341CJ	1D17	577B	3E14

578B	3E14	9033	8D	999329	2E5	CA3008	9L3
579B	3B2	9075	8A	999421	2B2	CA3011	9C
580B	3D	9076	8A	999422	2B2	CA3012	9C
582B	3D	9300	8G	999429	2B2	CA3013	9C
583B	3E7	9301	7F	999521	2C2	CA3014	9C
584B	3E14	9302	7B	999529	2C2	CA3015, 6	9L3
585B	3D	9303	8G	999552	1D15	CA3020	9B
587B	3E14	9952	6C2	999621	2G	CA3021	9S
727	1D3	9953	6C3	999622	2G	CA3022	9S
728	1I	9954	6C3	999626	2G	CA3023	9S
729	1C1	9955	6C3	9997021	2A1	CA3028	9P
800B	9L1	9956	6B	9997022	2A1	CA3029	9L3
800D	9L1	9957	6A	9997029	2A1	CA3031	9L4
801B	9L1	9958	8A			CA3032	9L4
801D	9L1	9959	8D	-A-		CD2150	4D2
805B	9L1	9960	7A	A01	1D10	CD2202	1D6
805C	9L1	9964	6C3	A02	1D10	CD2203	1B4
805-3	9L1	9965	6C3	A03	1B3	CD2205	1D8
805-4	9L1	9966	6C3	A04	1E	CR2100	4D2
806B	9L1	9967	6B	A05	1D10	CR2101	4D1
806C	9L1	9968	6B	A06	1D10	CS700	1D11
806-3	9L1	9971	6C3	A07	1D10	CS701	1D11
806-4	9L1	9973	6B	A08	1I	CS704	1B4
807B	9L1	9989	8A	A09	1B2	CS705	1D2
807-4	9L1	9997	8G	A10	1D10, 3E8	CS709	1D2
831A	9F1	9998	8G	A11	2A2, 3E8	CS715	1C1
831B	9F1	900051	3B1	A12	1D10	CS716	1D11
831C	9F1	900059	3B1	A13	1D10, 2B2	CS720	1D11
831D	9F1	900151	3B1	A13-251	9L1	CS721	1D11
900	2C3	900159	3B1	A14	1D10	CS727	1D11
901B	9S	900251	3E9	A15	1D11	CS729	1B4
901C	9S	900259	3E9	A16	2B2	CS730	1D11
903B	9P	900351	3E9	A17	2B3	CS731	1D3
903C	9P	900359	3E9	A20	1C2	CS732	1D3
914	2E3	900451	3E9	A41	1D11	CT <sub>μ</sub> L951	6A
923	2B3	900459	3E9	A42	1D11	CT <sub>μ</sub> L952	6C1
930	1D13	900551	3E2	A43	1B3	CT <sub>μ</sub> L953	6C1
932	1C1	900559	3E2	A44	1D1	CT <sub>μ</sub> L954	6C1
933	1D3	900651	3E2	A45	1D10	CT <sub>μ</sub> L955	6C1
936	1G	900659	3E2	A46	1D11	CT <sub>μ</sub> L956	6B
937	1G	900751	3E9	A47	1D11	-D-	
944	1D13	900759	3E2	A48	1I	D13-000	9F1
945	1B3	900851	3E2	A49	1B2	D13-001	9F1
946	1D13	900859	3E2	A50	1D10	D13-002	9F1
948	1B2	900951	3C	A51	1A	DM3510B	5D
949	1D13	900959	3C	A52	1D10	DT <sub>μ</sub> L930	1D12
950	1B1	902051	3B1	A53	1D11	DT <sub>μ</sub> L931	1B3
951	1I	902059	3B1	A54	1D11	DT <sub>μ</sub> L932	1C1
961	1D12	902151	3B1	A55	1D11	DT <sub>μ</sub> L933	1D2
962	1D13	902159	3B1	A60	1C2	DT <sub>μ</sub> L944	1D16
963	1D12	909351	1B3	AMC101	9B	DT <sub>μ</sub> L945	1B3
2107B	9A	909356	1B3	ATF401	9L1	DT <sub>μ</sub> L946	1D12
2108B	9A	909359	1B3	-B-		DT <sub>μ</sub> L948	1B2
2109B	9A	909451	1B2	B01	3E17	DT <sub>μ</sub> L950	1B1
2110B	9A	909456	1B2	B02	3E17	DT <sub>μ</sub> L951	1I
2114B	9A	909459	1B2	B11004	2C1	DT <sub>μ</sub> L962	1D12
2404B	9L1	909751	1B2	BC11001	2C2	-E-	
2405B	9L1	909756	1B2	BR-801	9T1	E11001	2F
2802B	9T1	909759	1B2	-C-		E11004	2F
2803B	9T1	909951	1B2	C11001	2D	E13511	9S
4002A	2H	909956	1B3	CA2151	4D2	E16-501	9A
4002B	2H	909959	1B2	CA2152	4D2	-F-	
4002C	2H	911151	1B2	CA2200	1D9	FF0451B	5C
8200	1B1	911159	1B2	CA2201	1D5	FF1514B	2B2
8201	1H	993651	1G	CA2204	1D9	FF5551B	2B2
8202	1H	993659	1G	CA3000	9B	FF7317E	5A
8203	1I	993751	1G	CA3001	9S	FF6451B	5C
8204	1D15	993759	1G	CA3002	9P	FF8317E	5A
8207	1D1	999121	2E5	CA3004	9P	FF9551B	2B2
8208	1D1	999122	2E5	CA3005	9B	F <sub>μ</sub> L90029	2C3
8209	1D1	999129	2E5	CA3007	9B	F <sub>μ</sub> L90329	2E1
8210	1D1	999221	2E5				
8213	1C1	999222	2E5				
8214	1D5	999229	2E5				
8502	9A	999321	2E5				
9030	8D	999322	2E5				

MICROELECTRONIC CROSS-INDEX

F <sub>μ</sub> L90529	2I1	MC265	1D2	MC461	3E3	MC786P	2F
F <sub>μ</sub> L91029	2E4	MC267	8B	MC462	3E17	MC787P	2B3, 2C4, 2G
F <sub>μ</sub> L91129	2E4	MC281G	1D10	MC463	3B8	MC788P	2C3
F <sub>μ</sub> L91429	2E1	MC282G	1B1	MC465	3B8	MC789P	2G
F <sub>μ</sub> L91529	2E1	MC284G	1D10	MC466	3B8	MC790P	2B1
F <sub>μ</sub> L92129	2F	MC301	4D6	MC500	3E17	MC792P	2E1
F <sub>μ</sub> L92329	2B2	MC302	4B	MC501	3E7	MC793P	2E4
		MC303	4A	MC502	3E19	MC798P	2C3
		MC304	4C	MC504	3E7	MC799	2C3
		MC305	4E	MC505	3E7	MC799P	2C2
		MC306	4D6	MC506	3E19	MC800	2C2
		MC307	4D6	MC508	3E17	MC801	2D
		MC308	4B	MC509	3E3	MC802	2B1
		MC309	4D1	MC510	3E3	MC803	2E1
		MC310	4D4	MC511	3E1	MC804	2A1
		MC311	4D1	MC512	3E17	MC805	2I1
		MC312	4D1	MC515	3B8	MC806	2I1
		MC313F	4D4	MC516	3B6	MC807	2E1
		MC314	4B	MC550	3E17	MC814	2E2
		MC315	4C	MC551	3E7	MC815	2E2
		MC316	4C	MC552	3E19	MC815C	2E2
		MC317	4F	MC553	3E7	MC816	2B1
		MC318	4D6	MC554	3E7	MC816P	2B1
		MC351	4D6	MC555	3E7	MC822P	2B3
		MC352	4B	MC556	3E19	MC825P	2E2
		MC352A	4B	MC558	3E17	MC826	2B1
		MC353	4A	MC559	3E3	MC826P	2B1
		MC354	4C	MC560	3E3	MC827	2G
		MC355	4E	MC561	3E1	MC829	2E2
		MC356	4D6	MC562	3E17	MC829P	2E2
		MC357	4D6	MC563	3B8	MC830	1D12
		MC358	4B	MC565	3B8	MC830P	1D12
		MC358A	4B	MC566	3B6	MC831	1B2
		MC359	4D4	MC650G	1D14	MC831P	1B2
		MC360	4D4	MC651F	1D14	MC832	1C1
		MC361	4D4	MC652	3B7	MC832P	1C1
		MC362	4D4	MC700	2C2	MC833	1D1
		MC363F	4D4	MC701	2D	MC833P	1D2
		MC364	4B	MC702G	2B1	MC844	1D17
		MC365	4C	MC703	2E1	MC844P	1D17
		MC366	4C	MC704	2A1	MC845	1B3
		MC367	4F	MC705	2I1	MC845P	1B2
		MC368	4F	MC706	2I1	MC846	1D12
		MC369F	4D5	MC707	2E1	MC846P	1D12
		MC369G	4D5	MC708	2A2	MC848	1B2
		MC400	3E17	MC709	2C3	MC848P	1B2
		MC401	3E3	MC710	2E4	MC850	1B1
		MC402	3E18	MC711	2E4	MC851	1I
		MC403	3D6	MC712	2A2	MC862	1D12
		MC404	3E7	MC713	2B2	MC862P	1D12
		MC405	3E7	MC714	2E1	MC875P	2F
		MC406	3E19	MC715	2E1	MC879P	2C4, 2F
		MC408	3E17	MC717	2E4	MC885P	2F
		MC409	3E3	MC718	2E4	MC887P	2B3, 2C4, 2G
		MC410	3E3	MC719	2E4	MC888P	2C3
		MC411	3E3	MC720	2B2	MC889P	2F
		MC412	3E17	MC721	2F	MC890P	2B1
		MC413	3B8	MC722P	2B2	MC892P	2E2
		MC415	3B8	MC723	2B1	MC893D	2E4
		MC416	3B8	MC723P	2B1	MC898P	2C4
		MC450	3E17	MC724P	2E1	MC899	2C3
		MC451	3E3	MC725P	2E1	MC899P	2C2
		MC452	3E18	MC726	2B1	MC900	2C2
		MC453	3E7	MC726P	2B1	MC901	2D
		MC454	3E3	MC727	2G	MC902	2D
		MC455	3E7	MC728	2E4	MC903	2E2
		MC456	3E19	MC729	2E1	MC904	2A1
		MC458	3E17	MC778P	2B2	MC905	2I1
		MC459	3E3	MC779P	2B3, 2C4, 2F	MC906	2I1
		MC460	3E3	MC785P	2F	MC907	2E2

MC908	2A2	MC1213F	4B	$\mu$ L907	2E5	PC201	9F1
MC909	2C4	MC1217F	4F	$\mu$ L914	2E2	PC210H	9L4
MC910	2E4	MC1218F	4F	$\mu$ L915	2E2	PC212H	9L4
MC911	2E4	MC1219F	4A	$\mu$ L916	2B2	PC222	9B
MC912	2A2	MC1220F	7A	$\mu$ L927	1D10	PC250	9L4
MC913	2B2	MC1221F	7A			PC251	9L4
MC914	2E2	MC1429	9F1	—N—		PC401H	9A
MC915	2E2	MC1430	9L2			PC402H	9A
MC916	2B1	MC1431	9L2	NB1000	2B3	PC501H	9T2
MC918	2E4	MC1433	9L2	NB1001	2D	PC502H	9T2
MC920	2B2	MC1511	4F	NB1002	2B1	PC503H	9T2
MC921	2F	MC1512	4F	NB1003	2E5	PC504H	9T2
MC926	2B1	MC1519	9F1	NB1004	2A1	PL4C01	7F
MC927	2G	MC1524	9N	NB1005	2I1	PL4G01	7C
MC928	2E4	MC1525	9F1	NN1007	2E5	PL4G02	7E
MC929	2E2	MC1526	9F1	NB1014	2E5	PL4G03	7E
MC930	1D12	MC1529	9F1	NB1015	2E5	PL4M01	7C
MC931	1B2	MC1530	9L2	NC-10	1D15	PL4R01	7G
MC932	1C1	MC1531	9L2	NC-11	1D5	PL4R07	7G
MC933	1D2	MC1533	9L2	NC511/PC511H	9T1	PL4S01	7D
MC944	1D17	MC1540	9Q	NC512/PC512H	9T1	PL4S02	7E
MC945	1B3	MC1550	9P	NC513/PC513H	9T1	PL5200	7G
MC946	1D12	MC1552	9S	NC514/PC514H	9T1	PL900	2C2
MC948	1B2	MC1553	9S	NC521/PC521H	9T2	PL901	2D
MC950	1B1	MC1709	9L2	NC523/PC523H	9T2	PL902	2B1
MC951	1I	MEM1000	7A	NC/PC8	1B1	PL903	2E3
MC962	1D12	MEM1002	7A	NC/PC9	8H	PL904	2A1
MC999	2C3	MEM1005	7A	NC/PC12	1B1	PL905	2F, 2I1
MC1001P	4D5	MEM1008	7A	NC/PC16	1I	PL906	2I1
MC1002P	4D5	MEM1022	7A	NC/PC17	8E	PL907	2E3
MC1003P	4D5	MEM1050	7A	NC/PC19	1B4	PL908	2A2
MC1004P	4D5	MEM3005PP	8G	NC/PC101	9S	PL909	2C4
MC1005P	4D5	MEM3008PS	8G	ND1002	1C2	PL910	2E4
MC1006P	4D5	MEM3012SP	8G	ND1003	1B1	PL911	2E4
MC1007P	4D3	MEM3016-2	8G	ND1006	1D16	PL912	2A2
MC1008P	4D3	MEM3016-2D	8G	NM1003	9N	PL913	2I2
MC1009P	4D3	MEM3020	8G	NM1004	9T2	PL915	2E3
MC1010P	4D3	MEM3021	8G	NM1005	9F1	PL916	2B1
MC1011P	4D3	MEM3050	8G	NM1008	9N	PL921	2F
MC1012F	4D3	MEM3064	8G	NM1021	9F1	PL930	1D5
MC1012P	4D3	MEM5014	7A	NM1021	9F1	PL931	1B3
MC1013P	4B	MEM5021	7A	NM1032	9I	PL932	1C1
MC1017P	4F	MW $\mu$ L908	2A2	NM1033	9I	PL933	1D2
MC1018P	4F	MW $\mu$ L909	2C4	NM1037	9F1	PL946	1D5
MC1019P	4A	MW $\mu$ L910	2E4	NM1038	9H	PL5200	7G
MC1020P	7A	MW $\mu$ L911	2E4	NM2012	9Q		
MC1021P	7A	MW $\mu$ L912	2A2	NM2016	9Q	—Q—	
MC1050	4D5	MW $\mu$ L913	2B2	NM2017	9A		
MC1051	4D5	MW $\mu$ L921	2F	NM2024	9E	Q25AH	9L2
MC1052	4D5	$\mu$ 7095	2E5	NM4002	8E	Q82AH	9L2
MC1110	9I	$\mu$ 7103	3E20	NS7558	9B	Q85AH	9L2
MC1111	1D1	$\mu$ 7104	3E20	NS7512A	9S		
MC1112	1D1	$\mu$ 7105	3E20	NS7560	9L2	—R—	
MC1113	1D1	$\mu$ 7106	3E20	NS7560A	9L2		
MC1114	1D1	$\mu$ A702	9B			R11001	2I1
MC1115	1G	$\mu$ A702A	9L1	—P—		R11004	2I1
MC1116	8B	$\mu$ A702C	9L1	P11001	2I2	R12001	2B2
MC1117	8B	$\mu$ A709	9L1	P11004	2I2	RA238	9L2
MC1118	8B	$\mu$ A709C	9L1	PA702A/712	9L2	RA239	9L2
MC1201F	4D5	$\mu$ A710	9G	PA710	9G	RA240	9L3
MC1202F	4D5	$\mu$ A710C	9A	PA713	9P	RA335	9L3
MC1203F	4D5	$\mu$ A711	9F1	PA726	9L2	RA338	9L3
MC1204F	4D6	$\mu$ A711C	9G	PA7600	9P	RA339	9L3
MC1205F	4D6	$\mu$ A716C	9B	PC-10	1D15	RA340	9L3
MC1206F	4D6	$\mu$ L900	2C3	PC-11	1D5	RA538	9L3
MC1207F	4D3	$\mu$ L902	2B1	PC-13	1B1	RA539	9L3
MC1208F	4D3	$\mu$ L903	2E2	PC-14	1D15	RA540	9L3
MC1209F	4D4	$\mu$ L904	2A1	PC-15	1D5	RC103	2E5
MC1211F	4D4	$\mu$ L905	2I	PC-18	1I	RC123	2E5
MC1212F	4D4	$\mu$ L906	2I	PC200	9F1	RC124	2E5
						RC144	2E5

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RC203T	1B4	S1931D	1B3	SE825	3B3	SG102	3E21
RC204T	1D9	S1932	1C1	SE840	3E21	SG103	3E21
RC205T	1J	S1932D	1C1	SE855	3D	SG110	3E21
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RC210G	1C2	S1933D	1D2	SE880	3E9	SG112	3E21
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RC211T	1D8	S1944D	1D14	SF11	3B1	SG120	3E19
RC212T	1B1	S1945	1B3	SF12	3B1	SG121	3E19
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RC221T	1D8	S1948D	1B3	SF23	3B1	SG132	3D
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RC243	1D6	S8440	3E22	SF51	3B1	SG150	3E4
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RC323	2E5	S8816	3E10	SF61	3B2	SG160	3D
RC324	2E7	S8825	3B6	SF62	3B2	SG161	3D
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RC1032	2E8	S8880	3E10	SF112-113	3B3	SG172	3F2
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RD-211	1D2	SE110	1D14	SF260	3B5	SG203	3E17
RD-220	1G	SE111	1D11	SF261	3B5	SG210	3E21
RD-221	1B1	SE112	1D11	SF262	3B5	SG211	3E21
RD-223	1G	SE113	1D11	SF263	3B5	SG212	3E21
RD-234	1G	SE115	1D13	SG40	3E19	SG213	3E21
RD-235	1C1	SE124	1B4	SG41	3E19	SG220	3E16
RD-305	1D10	SE125	1B3	SG42	3E19	SG221	3E16
RD-306	1D10	SE155	1C1	SG43	3E19	SG222	3E16
RD-307	1B1	SE156	1C1	SG50	3E21	SG223	3E16
RD-308	1B1	SE157	1C1	SG51	3E21	SG230	3F1
RD-309	1C1	SE160	1I	SG52	3E21	SG231	3F1
RD-310	1D10	SE161	1I	SG53	3E21	SG232	3F1
RD-320	1G	SE170	1D12	SG60	3E19	SG233	3F1
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RD-334	1G	SE181	1G	SG62	3E19	SG241	3E16
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RD-508	1B1	SE440	3E22	SG72	3E2	SG251	3E21
RD-509	1C1	SE480	3E13	SG73	3E2	SG252	3E21
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RD-520	1G	SE504	9Q	SG82	3E4	SG261	3E17
RD-534	1G	SE505	9F2	SG83	3E4	SG262	3E17
		SE506	9L4	SG90	3A, 3E21	SG263	3E17
		SE560	9G	SG91	3A, 3E21	SG270	3F1
		SE750	1C2	SG92	3A, 3E1	SG271	3F1
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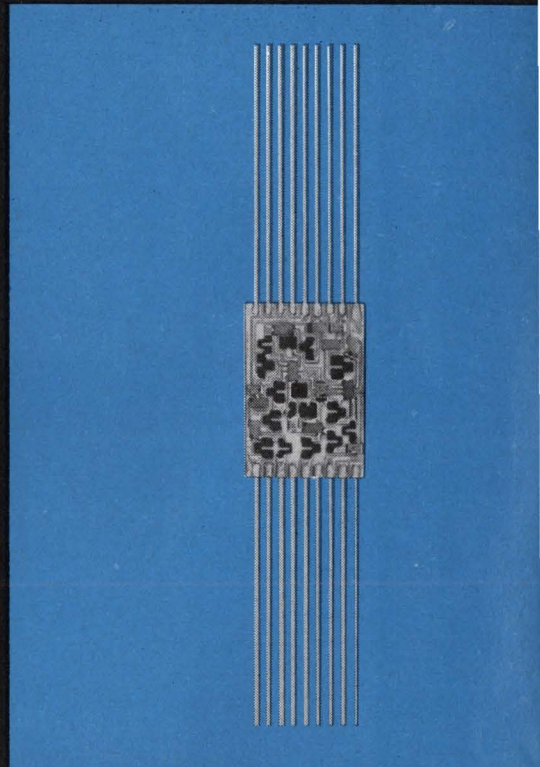
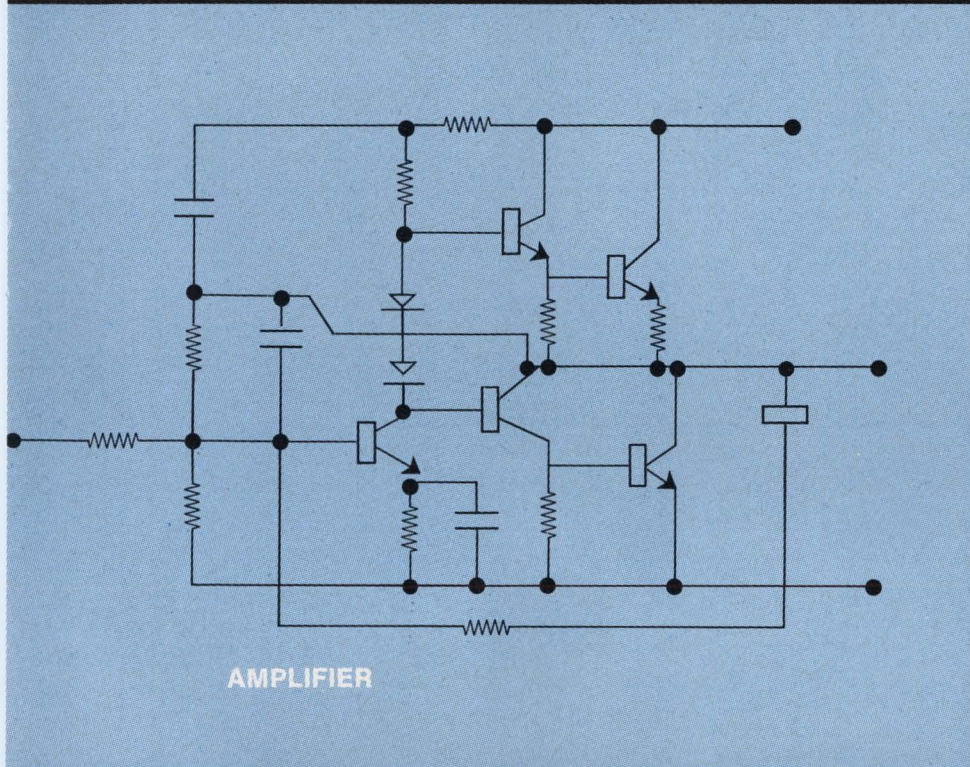
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SG293	3E4	SN518B	5D	SN7430	3E12	SN74962	3E12
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SG301	3E4	SN522A	9L4	SN7441	7F	SN74966	3E12
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SG303	3E4	SN524A	9L4	SN7453	3E5	SP616	1D8
SG310	3E4	SN525A	9F2	SN7460	3F2	SP620	1B4
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SG313	3E4	SN530	1B4	SN7472	3B5	SP631	1D3
SG314	3E4	SN531	1D14	SN7473	3B5	SP659	1C1
SI930	1D13	SN532	1D4	SN7474	3B3	SP670	1D8
SI930D	1D13	SN533	1D14	SN7476	3B3	SP680	1D9
SI931	1B3	SN534	1D4	SN7480	3A	ST2514B	5A
SI931D	1B3	SN535	1C2	SN7481	8D	SU300	8I
SI932	1C1	SN723	9F2	SN7482	3A	SU305	8I
SI932D	1C1	SN724	9L4	SN7483	3A	SU306	8I
SI933	1D2	SN725	9F2	SN7490	8A	SU314	8I
SI933D	1D2	SN726	9L4	SN7491	8G	SU315	8I
SI945	1B3	SN5101B	5A	SN7492	3B7	SU316	8I
SI945D	1B3	SN5111	5A	SN7493	3B7	SU320	8I
SI946	1D13	SN5112	5A	SN7500	9Q	SU331	8I
SI946D	1D13	SN5113	5A	SN7501	9Q	SU332	8I
SI962	1D13	SN5161B	5C	SN7502	9Q	SW101	1D5
SI962D	1D13	SN5162B	5C	SN7510	9S	SW102	1D5
SN54H00	3E15	SN5191	5C	SN15830	1D6	SW103	3E9
SN54H10	3E8	SN5231L	9F2	SN15831	1B3	SW104	3E10
SN54H11	3E1	SN5301	1B4	SN15832	1C1	SW115	1D6
SN54H20	3E8	SN5302	1B4	SN15833	1D3	SW201	1G1, 1D6
SN54H21	3E1	SN5304	1B4	SN15844	1D6	SW204	1D6
SN54H40	3E8	SN5311	1D14	SN15845	1B3	SW211	1D6
SN54H50	3E6	SN5331	1D14	SN15846	1D7	SW212	1B1
SN54H52	3E3	SN5360	1D14	SN15848	1B3	SW221	1D6
SN54H53	3E3	SN5370	1D17	SN15850	1B3	SW224	1D6
SN54H60	3F1	SN5380	1I	SN15851	1I	SW231	1D6
SN54H61	3F1	SN5400	3E11	SN15862	1D7	SW301	4D2
SN54H62	3F1	SN5410	3E11	SN15930	1D7	SW304	4B
SN54H71	3B1	SN5420	3E11	SN15931	1B3	SW305	4E
SN54H72	3B1	SN5430	3E12	SN15932	1C2	SW306	4D2
SN54L00	3E13	SN5440	3E13	SN15933	1D3	SW307	4D2
SN54L10	3E13	SN5450	3E22	SN15944	1D7	SW308	4B
SN54L20	3E13	SN5451	3E22	SN15945	1B3	SW309	4D1
SN54L22	3E16	SN5453	3F2	SN15946	1D7	SW310	4D1
SN54L30	3E13	SN5460	3F2	SN15948	1B3	SW311	4D1
SN54L51	3E7	SN5470	3B6	SN15950	1B3	SW402	3E15
SN54L71	3B6	SN5472	3B5	SN15951	1I	SW708	1D5
SN54L72	3B6	SN5473	3B5	SN15962	1D7	SW930	1D5, 1D6
SN54L73	3B6	SN5474	3B3	SN17908L	2A2	SW931	1B3
SN74H00	3E8	SN5480	3A	SN17909L	2C4	SW932	1C1
SN74H10	3E8	SN5481	8D	SN17910L	2E4	SW933	1D3
SN74H11	3E1	SN5482	3A	SN17911L	2E4	SW944	1C1
SN74H12	3E1	SN5490	8A	SN17912L	2A2	SW945	1B3
SN74H20	3E8	SN5491	8G	SN17913L	2C2	SW946	1D6
SN74H30	3E8	SN5500	9Q	SN17921L	2F	SW948	1B3
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SN74H50	3E6	SN7000	4D2	SN52709	9L4	SW5400	3E10
SN74H52	3E6	SN7001	4D2	SN52710	9G	SW5401	3E10
SN74H53	3E6	SN7300	1B4	SN52711	9G	SW5420	3E10
SN74H60	3E7	SN7301	1B4	SN54930	3E12	SW5430	3E12
SN74H61	3F1	SN7302	1B4	SN54932	3D	SW5440	3E13
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SN74H71	3B1	SN7310	1D14	SN54948	3B6	SW5460	3F2
SN74H72	3B1	SN7311	1D14	SN54962	3E12	SW5470	3B6
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SN346A	1C2	SN7330	1D14	SN54966	3E22	SW7410	3E10
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SN511B	5A	SN7350	1C2	SN72709	9L4	SW7430	3E12
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SW7470	3B6	SWG150	3F1	TNG3017	3E19	W6G221	3E17
SWA01	1D5	SWG151	3F1	TNG3031	3E19	W6G241	3E17
SWA02	1D5	SWG152	3F1	TNG3041	3E18	WC110T	9T4
SWA04	1D1	SWG153	3F2	TNG3043	3E18	WC115T	9F2
SWA05	1D5	SWG170	3F2	TNG3045	3E18	WC161Q	9L4
SWF10	3B6	SWG171	3F2	TNG3047	3E18	WC183	9B
SWF11	3B6	SWG172	3F2	TNG3051	3F2	WC206	1D7
SWF12	3B6	SWG173	3F2	TNG3111	3E19	WC208	8F
SWF13	3B7	SWG180	3F2	TNG3113	3E19	WC210	1C2
SWF20	3B7	SWG181	3F2	TNG3115	3E19	WC211	1C7
SWF21	3B7	SWG182	3F2	TNG3117	3E19	WC213	1B2
SWF22	3B7	SWG183	3F2	TNG3131	3E19	WC215	1B2
SWF23	3B7	SWG210	3E4	TNG3141	3E18	WC216	8B
SWF50	3B7	SWG211	3E4	TNG3143	3E18	WC217	8B
SWF51	3B7	SWG212	3E4	TNG3145	3E18	WC218	1I
SWF52	3B7	SWG213	3E4	TNG3147	3E18	WC220	1C2
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SWF251	3B5	SWG222	3E8	TNG3215	3E19	WC225	1B2
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SWF253	3B5	SWG230	3F1	TNG3231	3E19	WC227	8B
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SWG4B	3E10	SWG242	3E9	TNG3251	3F2	WC261	1D8
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SWG21	3E5	SWG253	3E4	TNG4241-44	3E22	WC378	4C
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SWG41	3E10	SWG261	3E9	TNG4541	3E22	WC380	4D2
SWG42	3E10	SWG262	3E9	TNG5511-12	3D	WC381	4D2
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SWG63	3E12			UC1003B	1C1	WM211	1D6
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SWG91	3E22	TAA111	9B	UC1005B	1D3	WM214	1D8
SWG92	3E22	TAA121	9B	UC1006B	1D3	WM215	1B4
SWG93	3E22	TAA131	9B	UC1501A	9I	WM216	1D6
SWG100	3E5	TAA293	9I	UC1502A	9M	WM217	1D3
SWG101	3E5	TAA310	9B	UC1503A	9I	WM221	1D6
SWG102	3E5	TFF3011	3B1	UC1504A	9M	WM224	1D8
SWG103	3E5	TFF3013	3B1	UC1505A	9I	WM225G	1B4
SWG110	3E5	TFF3015	3B1	UC1506A	9M	WM226G	1D5, 1D8
SWG111	3E5	TFF3017	3B1	UC1507A	9I	WM227	1D3
SWG112	3E5	TFF3111-14	3B4	UC1508A	9K	WM231	1D6
SWG113	3E5	TFF3115-18	3B4	UC1509A	90	WM234G	1C1, 1D5
SWG120	3E13	TFF3121-24	3B4	UC1510A	90	WM236G	1D5, 1D8
SWG121	3E13	TFF3125-28	3B4	UC4000	9L4	WM241G	1D8
SWG122	3E13	TFF3161-64	3B4	UC4001	9L4	WM246	1D6
SWG123	3E13	TFF3165-68	3B4	UC4002	9L4	WM246G	1D9
SWG130	3E10	TFF3173-74	3B4	US0100A	5A	WM261G	1D5, 1D8
SWG131	3E10	TFF3181-84	3B4	US0101A	5A	WM286G	1D9
SWG132	3E10	TFF3241-44	3B2	US0102A	5C	WM296G	1D5, 1D8
SWG133	3E10	TFF3341-44	3B2	US0103A	5C	WM503	1B4
SWG140	3E10	TFF3441-44	3B2			WM1146	9S
SWG141	3E10	TMC3162-64	8D	—W—		WM1146Q	9C
SWG142	3E10	TMC40006	9L2	W6F251	3B1		
		TNG3011	3E19				
		TNG3013	3E19				



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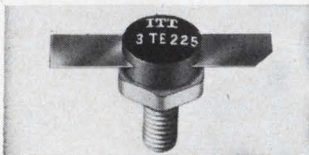
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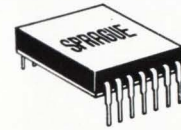
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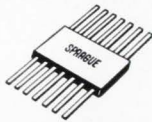


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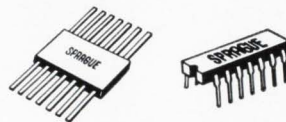
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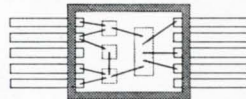
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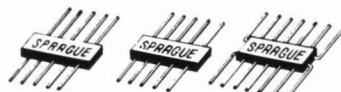


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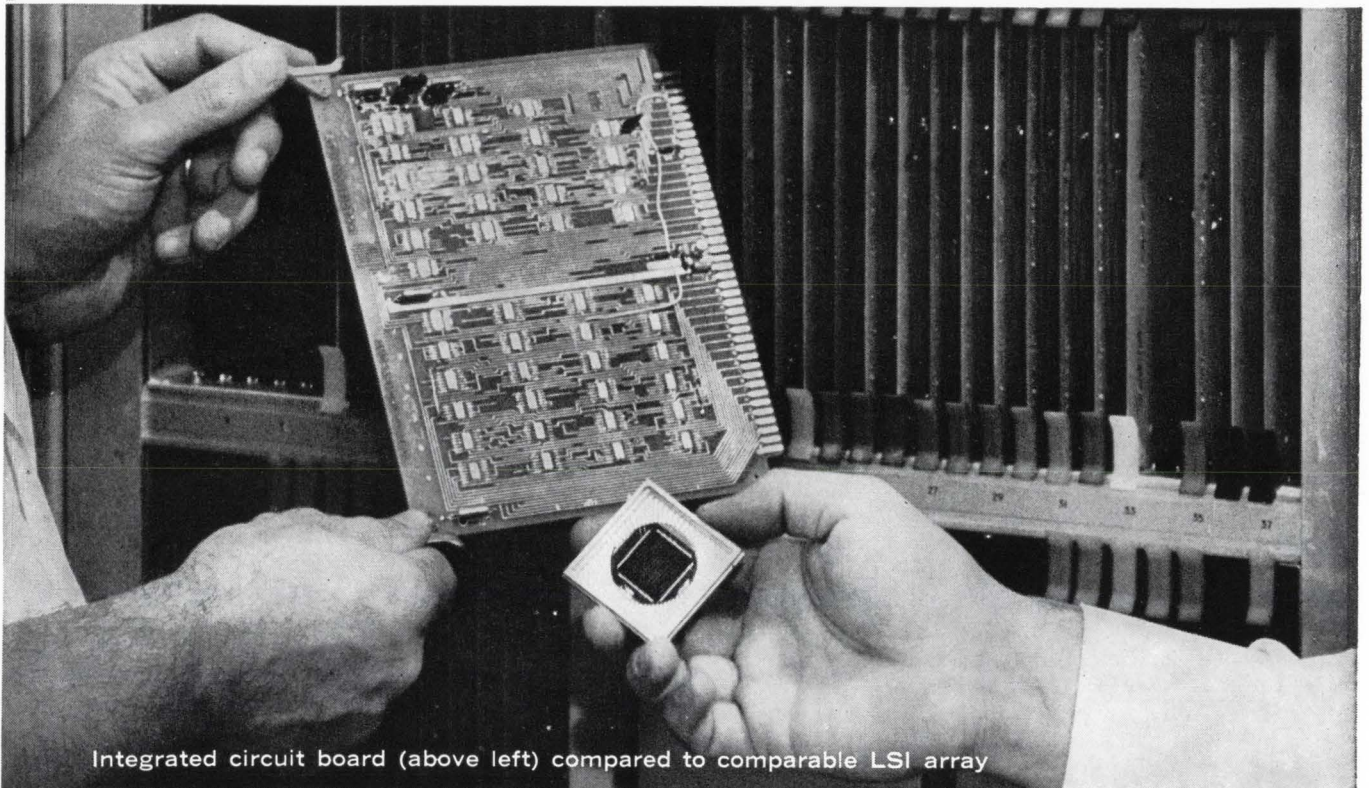
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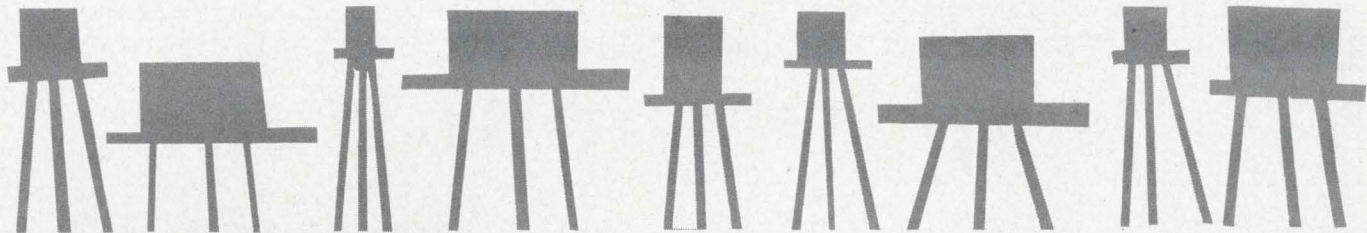


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# Check the 0-TC point in your FETs.

Experiments show that theoretical values of bias current for 0-TC are not accurate.

A zero-temperature-coefficient (0-TC) point that is inherently present in junction- and MOS-FETs is the devices' ideal operating point because no changes due to temperature take place there.

The theoretical explanation of this phenomenon is already well documented.<sup>1, 2, 3, 4, 5</sup> Experience shows, however, that theoretical expressions cannot be relied on for detailed circuit design. In fact, to use the 0-TC point in practical circuits, a designer must determine it for every FET type, and, quite often, for each FET of the same type.

The purpose of this article, then, is to describe the 0-TC measuring techniques, to present test data for several commercially available FETs, and to review briefly applications where the 0-TC point can be used advantageously.

## Theoretical model may give imprecise results

The temperature variation of drain current in J-FETs is largely due to two opposing factors. The first is the change in width of the thermally generated depletion layer at the gate-channel junction. The second is the majority-carrier mobility between the source and drain.

In the references cited above it is shown that the first factor tends to increase the drain current at a rate equivalent to a change of 2.2 mV/°C at the gate. The second factor tends to decrease the gate current at a rate of approximately 0.7%/°C.

These two factors combined result in the following equations:<sup>1</sup>

$$I_{DZ} = 0.4 I_{DSS} / V_p^2 = \text{drain current} \quad (1)$$

for zero TC

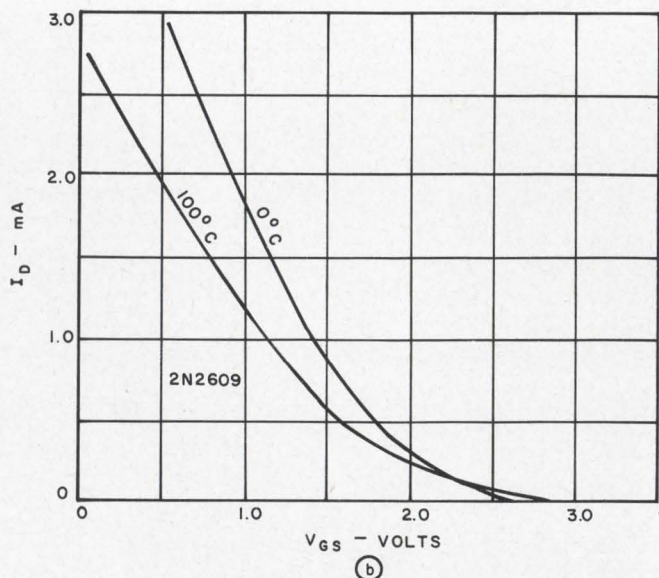
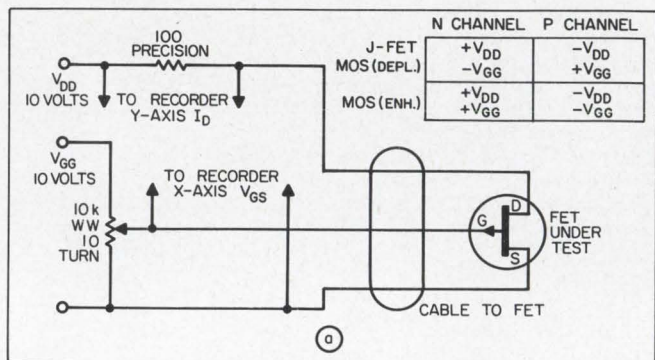
$$V_{GSZ} = V_p - 0.63 = \text{gate-source voltage} \quad (2)$$

for zero TC

These equations, having been developed from a theoretical model, often do not give correct results in practice. The semiconductor doping and diffusion account for most of the differences between the actual and theoretical results. Of the two foregoing equations, the first is the more meaningful because the result,  $I_{DZ}$ , is independ-

ent of the drain-to-source voltage.  $V_{GSZ}$ , on the other hand, is dependent on the drain-to-source voltage, a variable known only in the final circuit configuration.

From practical considerations, therefore, the best way to establish the 0-TC point is experimentally.  $I_{DZ}$ , being a unique value, should be determined first. A second test should then be performed to determine  $V_{GSZ}$  at  $I_{DZ}$  and the proper drain-to-source voltage. The 0-TC point can be determined easily by making a plot of  $V_{GS}$  vs  $I_D$  for various temperatures, using the circuit shown in Fig. 1a. The equipment needed is an X-Y recorder, two



1. 0-TC point of a FET can be quickly determined using a simple test setup (a). A sample curve (b) has been obtained for the 2N2609 FET.

Thomas H. Lynch, Systems Engineer, Perkin Elmer Aerospace Systems, Pomona, Calif.

low-voltage dc supplies, and an environmental oven. A ten-turn potentiometer is used to control the gate-to-source voltage so that a smooth curve is produced on the X-Y recorder. A sample  $V_{GS}$ -vs- $I_D$  plot of a p-channel FET is shown in Fig. 1b. In lieu of using an oven, a simpler and possibly quicker method would be the use of ice water and boiling water. This method would produce both an accurate temperature reference and a very good heat sink.

It is frequently impractical to bias the FET at exactly  $I_{DZ}$ . In order to determine the temperature drift errors at other drain currents, a plot similar to that of Fig. 2 can be used. It was developed by determining graphically the drift at various drain currents with the  $V_{GS}$ -vs- $I_D$  plot of Fig. 1b. It can be seen that for moderate drift requirements (less than 1 mV/°C) the J-FET is well behaved over a wide range of currents.

A large spread in  $I_{DZ}$  values often occurs from one sample to the next of a particular type of J-FET. This is a result of the many device conditions that affect  $I_{DZ}$ . When production requirements necessitate a specific  $I_{DZ}$ , the J-FETs can usually be specially ordered from a manufacturer.

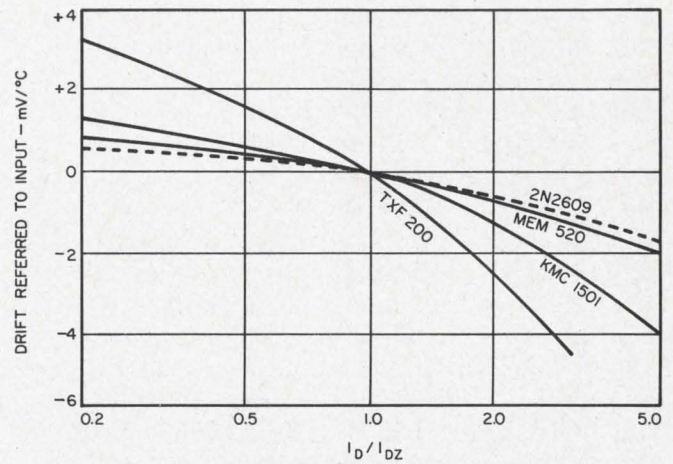
### MOS-FET characteristics are hard to determine

The temperature dependence of MOS-FET characteristics is much more difficult to define than that of J-FETs'. For this reason, an easily handled mathematical model has not as yet been developed. One of the most difficult factors to control in MOS-FET fabrication is the interface structure between the silicon drain-source channel and the silicon dioxide gate insulator. Large changes in the surface properties of the transistor are to be expected as a result of variations in cooling rate, in atmospheric purity, and in general cleanliness during the formation of the gate insulator.

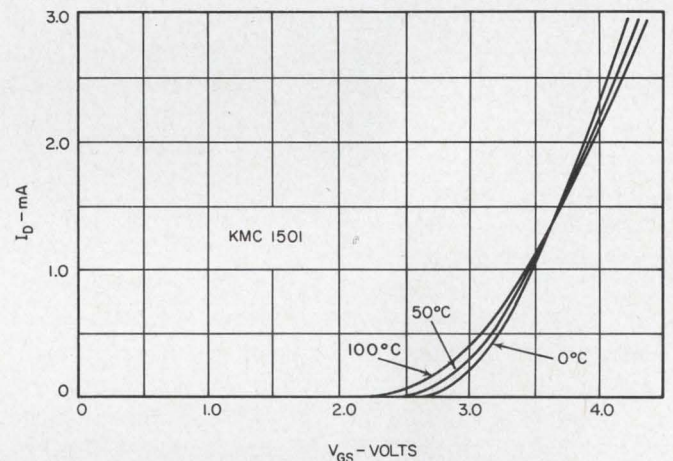
A theoretical explanation of the temperature-dependent properties can, however, be made.<sup>2</sup> It can be theorized that there is a particular drain current for which a 0-TC exists. But in practice, this drain current,  $I_{DZ}$ , is impossible to predict and requires experimental determination.

The same method outlined for J-FETs can be used to determine the 0-TC point of MOS-FETs experimentally. Fig. 3 shows the results of a temperature-dependent  $V_{GS}$ -vs- $I_D$  plot for a p-channel enhancement-mode MOS-FET. For a closer analysis of the 0-TC point, it is advantageous to use zero suppression in the X-Y recorder. This quickly demonstrates nonlinearities (Fig. 4).

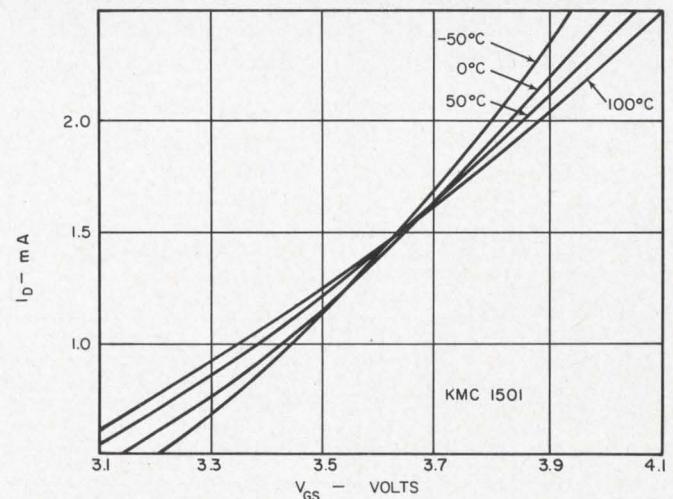
One problem seldom admitted, yet sometimes encountered, is sodium ion drift.<sup>3</sup> This can complicate the search for a 0-TC point because the gate voltage may not be a true indication of drain current. The ion drift rate is very temperature-



2. Maximum allowable drift for condition when a FET must be biased at an  $I_D$  different from  $I_{DZ}$  can be determined from the data of Fig. 1b. Devices of four manufacturers were used for this photo.



3. MOS-FETs also possess a 0-TC point, as can be seen from the plot above. Yet it is more difficult to predict and may vary from unit to unit. The existing theoretical models are not accurate.



4. A blow-up view of the 0-TC shown in Fig. 3, obtained through zero suppression in the X-Y recorder, demonstrates the nonlinearities in the  $V_{GS}$ -vs- $I_D$  plot. Note the large variations in  $I_D$ .

dependent. At 100°C the mobility of sodium ions through the silicon dioxide gate insulator is many times greater than at room temperature. The magnitude of the drift is vividly portrayed in Fig. 5, a plot of the drain current versus time. This defect is present in varying degrees in all MOS-FETs presently manufactured and depends on the purity of the manufacturing conditions. The problem can be alleviated by first making the  $V_{GS}$ -vs- $I_D$  plot at the highest temperature after the drift has gone to its limit under biased conditions; then, while maintaining the gate bias voltage, cooling the device down for its lower-temperature runs. The result will be a true indication of  $I_{DZ}$  alone, if a significant drift is present.

Most MOS-FETs that were tested possessed a 0-TC point. Several units checked are listed below with their approximate  $I_{DZ}$ :

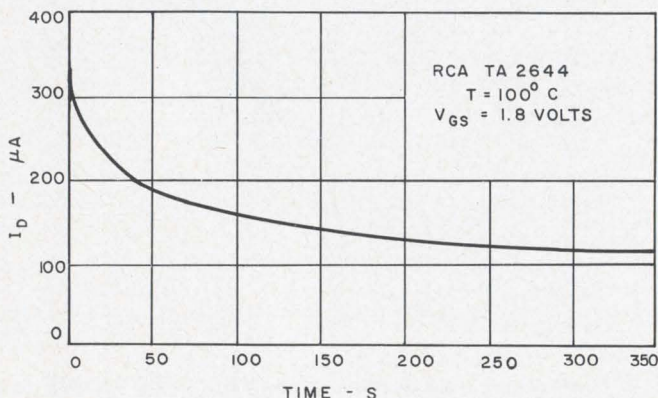
Sprague	TXF200	50 $\mu$ A
Fairchild	F1100	100 $\mu$ A
General	MEM520	0.5 mA
Instrument	MEM551	0.5 mA
KMC	1501	1.5 mA
TRW	2N4308	2.5 mA
Siliconix	2N3631	4.0 mA

Because of variations in the manufacturing conditions, however, these approximate values must not be relied on as constant.

MOS-FETs, as a rule, will not perform as well as J-FETs under wide ranges of temperature because of the complex temperature compensation present at the 0-TC point. Of the types tested, the General Instrument MEM520, MEM 551 and the KMC 1501 exhibited the most stable 0-TC point over a temperature range of 0°C to 100°C.

### Where to use FETs

J-FETs offer the widest latitude in design because of the diversity of the types available. Since the transconductance,  $g_m$ , of a FET is proportional to the drain current, high gain in



5. Drift due to the sodium ion migration is demonstrated in this graph. This effect renders theoretical predictions of FET behavior very difficult.

conventional circuitry requires the J-FET's  $I_{DZ}$  to be near its  $I_{DSS}$ . From Eq. 2,  $V_p$  must be about 0.63 volt if  $I_{DZ}$  is to equal  $I_{DSS}$ . Devices such as the Union Carbide 2N3687 and 2N3698 satisfy this requirement. Equation 1 shows that low  $I_{DZ}$  operation can be obtained from J-FETs that have a  $V_p$  of 4 to 6 volts. However, the stage gain will suffer unless techniques like that shown in Fig. 6 are used. In this application, a constant-current load at  $I_{DZ}$  is used to give the highest possible stage gain. A temperature-compensated power supply regulator combination ( $Q1$  and  $CR1$ ) and  $R1$  comprise the current source. The composite stage gain can easily exceed several thousand.

The use of MOS-FETs in dc amplifiers, because of the difficulties involved, is usually limited to high-input-impedance applications. The small number of different types available often limits the circuit design. Some of the problems that have to be considered are:

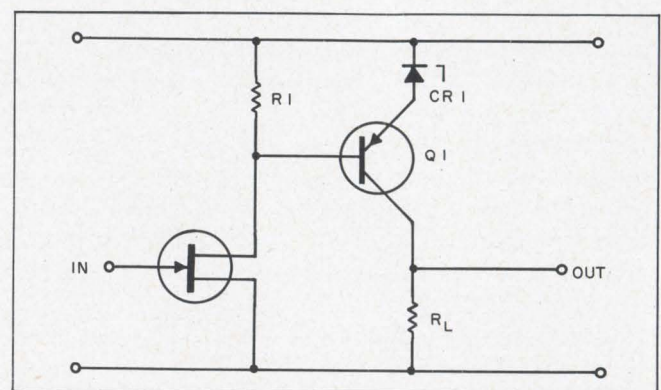
- The unpredictability of the 0-TC point.
- The 0-TC point variability with the temperature range.
- Gate voltage drift due to ion migration.

It is therefore necessary to design the circuit around the device once the MOS-FET's limitations have been thoroughly investigated.

Large-swing open-loop dc amplifiers should be avoided. This is to prevent drift errors when a signal causes operation at a point far removed from the  $I_{DZ}$  value. The magnitude of this drift error can be calculated with a curve similar to those in Fig. 2. The effects of drift can be reduced by limiting 0-TC biased FET stages to low signal levels or by going to closed-loop operation. Closed-loop amplifiers are the best approach since they have the advantage of reducing the drift error by the loop gain.

### FETs for amplifiers and current sources

The FET version of the differential amplifier poses a problem (absent with transistors) because



6. Stage gain of several thousands can be obtained by "feeding" the FET from a simple constant-current (equal to  $I_{DZ}$ ) source.



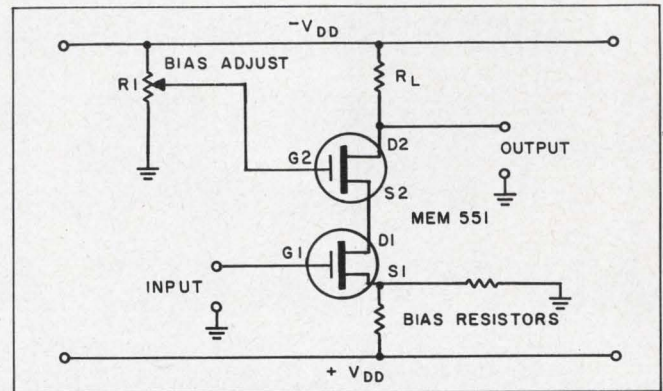
of the 0-TC point. When a dc signal is applied to a 0-TC biased differential FET stage, differential drift errors will occur. These drift errors, which appear only when a signal is applied, are caused by one FET operating above, and the other operating below, the 0-TC bias point. To reduce dynamic-differential drift errors, the bias points should be a little below the 0-TC values, depending on the signal swing. This can be deduced from an analysis of the curves of Fig. 2. If high input impedances are not required, a good differential transistor such as the 2N4044 should be used instead of a FET.

It has been implied that the operating point of a FET preceding a transistor can be adjusted to compensate for the drift in the transistor. A circuit of this nature should not be designed for production-line fabrication, however, because of the setup time required. Each circuit has to be individually trimmed to minimize drift, since drift rates of the FET and transistor vary from unit to unit.

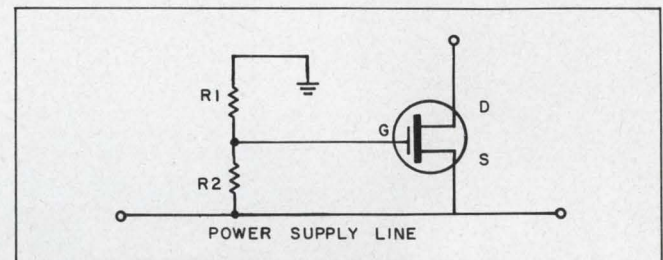
MOS-FETs can easily be adapted for use in a dc-coupled cascode amplifier. Because of the compound connection, both MOS-FETs should have nearly the same 0-TC point. Rather than match two units that have the same 0-TC point, use a dual-monolithic MOS-FET. Tests were performed on a General Instrument MEM551 dual unit to verify the similarity between the 0-TC points of each MOS-FET. On the whole, they were virtually identical. When properly biased in the circuit, as shown in Fig. 7, the result is an exceptionally stable dc-input amplifier.

Due to the constant-current nature of FETs in the pinch-off region, they lend themselves to use as simple current sources. When using J-FETs for this application, a low  $V_p$  is desirable. This will minimize the voltage drop for current-limiting in the circuit of Fig. 7.  $R_1$  can be adjusted to produce the  $I_{DZ}$  current. Enhancement-mode MOS-FETs make simple current sources in the circuit of Fig. 8. The ratio of  $R_1$  and  $R_2$  can be adjusted to give the proper current level. The big advantage of FET current sources over conventional transistor-Zener combinations is their low minimum voltage drop for current-limiting.

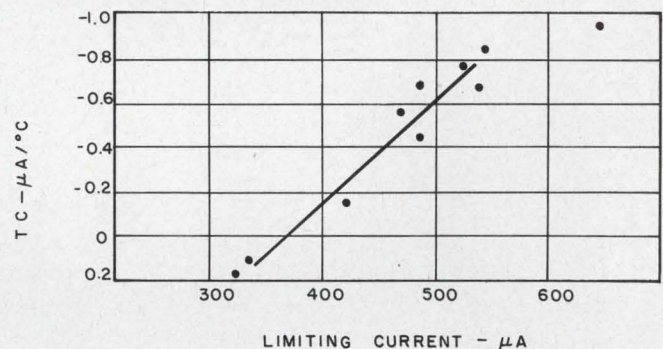
Motorola is producing a series of current-limiting diodes (type number MCL 1300) that are actually J-FETs with gate and source shorted. When FETs are used in this configuration,  $I_{DSS}$  current is limited. If these current-limiting diodes are to have a 0-TC current level, the J-FET used must have a  $V_p$  of about 0.63 volt. Since no data on temperature stability were supplied, tests were run on enough diodes to verify the possible existence of  $I_{DZ}$  current level. The results, shown in Fig. 9, indicate that the  $I_{DZ}$  current level exists at approximately 0.37 mA. Motorola can supply



7. Stable single-ended dc amplifier results when a dual MOS-FET unit is used.



8. Enhancement-mode MOS-FET can be used to build a simple constant-current source.



9. Tests on a number of current-limiting FET diodes indicate that they also possess 0-TC points. They can be obtained on special orders only.

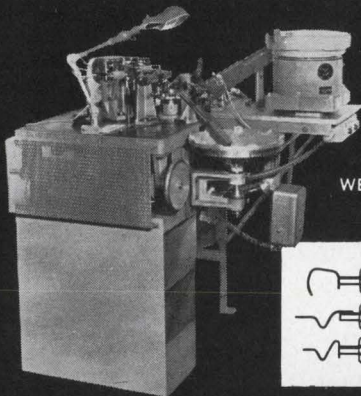
diodes selected to this current at an additional cost. All the same, of course, this particular  $I_{DZ}$  value will vary, depending upon the manufacturing control. ■ ■

#### References:

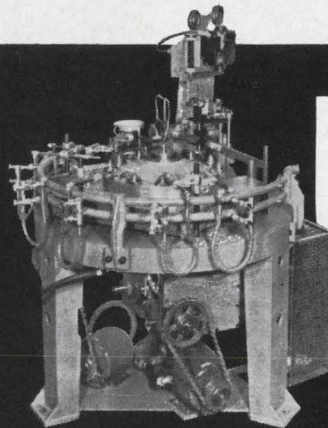
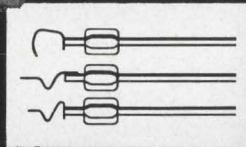
1. James S. Sherwin, "The Fet as an Amplifier," 1966 WESCON Convention Record (New York: IEEE, 1966), Session 11/2.
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3. A. S. Grove, P. Lamond *et al.*, "Stable MOS Transistors," *Electro Technology*, LXXVI, No. 6 (Dec., 1965), 40.
4. Lee L. Evans, "Biasing FETs for Zero dc Drift," *Electro Technology*, LXXIV, No. 2 (Aug., 1964).
5. James S. Sherwin, "Take the Fog out of Field-Effect Design," *ELECTRONIC DESIGN*, XIV, No. 13 (May 24, 1966), 38-44; "Gain Insight into FET Amplifiers," *Op. cit.*, No. 14 (June 7, 1966), 40-45; "Simplify Low Frequency FET Designs," *Op. cit.*, No. 15 (June 21, 1966), 86-90.

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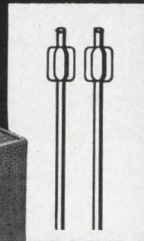
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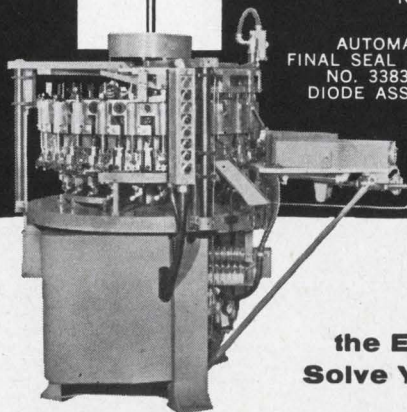
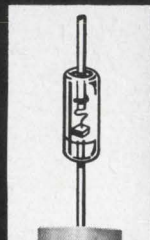
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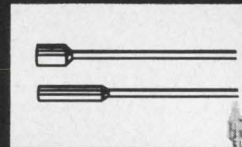
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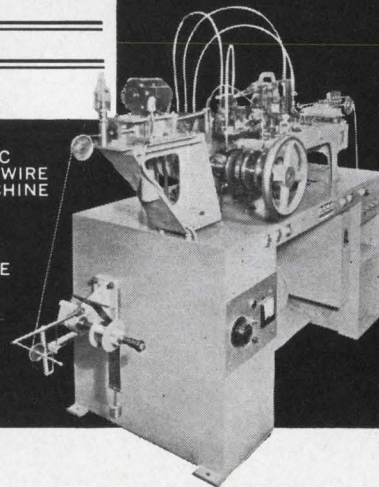
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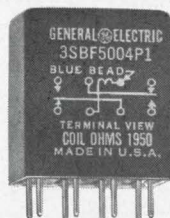
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# Stagger-tune the IC amplifier stages

in an IF or RF strip design. It will have just the right gain and selectivity curve.

Stagger tuning—tuning each stage of an amplifier at slightly different frequencies—can achieve:

- A gain-bandwidth product greater than that of synchronously tuned cascade stages.
- A selectivity curve of prescribed response.

It is possible to stagger-tune  $n$  single stages to attain a flat band pass, an equal-ripple (Chebyshev) band pass, or many other selectivity curves with very good gain.<sup>1</sup>

The stagger-tuned circuit can be implemented with discrete transistors, but the availability of high-performance, integrated high-frequency amplifiers at prices comparable to those of single transistors offers an attractive alternative. One such amplifier, with characteristics that are particularly suited to stagger-tuned circuits, is the Motorola MC1550.\*

The simplified schematic in Fig. 1 serves to explain the ac and dc operation of the MC1550. Considering dc operation first, voltage  $V_S$  and resistor  $R_S$  establish current  $I_{D1}$  in diode  $D1$ . Since this diode is on the same silicon die as transistor  $Q1$  and they are laid out very close to each other, the emitter current of  $Q1$  will be within 5% of the diode current. This biasing technique exploits the matching characteristics that are available with integrated circuits and illustrates a method that would be difficult to accomplish with discrete components but is easy with integrated circuits. The current established in the emitter of  $Q1$  will be shared between  $Q2$  and  $Q3$ , depending on the relationship between  $V_{agc}$  and  $V_R$ . Where  $V_{agc}$  is at least 114 mV greater than  $V_R$ ,  $Q3$  is turned off and all the collector current of  $Q2$  is transferred to  $Q1$ . Since  $Q3$  is off, the ac gain will be at its minimum point. If, on the other hand,  $V_{agc}$  is less than  $V_R$  by 114 mV or more, all the collector current present in  $Q1$  will flow through

\*Similar integrated amplifiers are Fairchild's  $\mu A703C$  and RCA's CA3028.

**Brent Welling**, IC Applications Engineer, Motorola Semiconductor Products, Inc., Phoenix, Ariz.

$Q3$ . This, then, is the operating point for maximum ac gain.

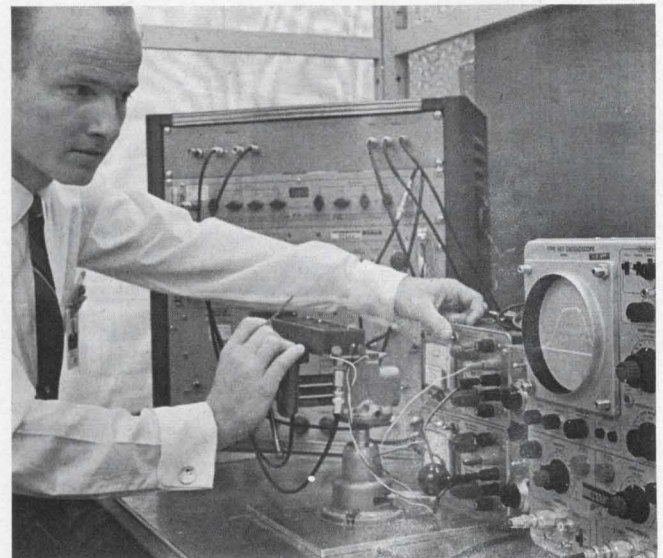
In ac operation, the input is applied to the base of  $Q1$  and the output taken from the collector of  $Q3$ . Thus, the combination of  $Q1$ - $Q3$  acts as a common-emitter, common-base pair. This pair offers the distinct performance advantage of reducing internal feedback ( $y_{12}$ ) two orders of magnitude in comparison with a single transistor. With a General Radio 1607-A immittance bridge,  $y_{12}$  was too small to measure up to frequencies of 300 MHz. This indicates that the magnitude of  $y_{12}$  is less than 0.001 mmhos over the useful frequencies of operation of the amplifier, and can, for all practical purposes, be neglected. This property of the integrated amplifier is particularly important to its tuning.

Basic two-port theory gives the expressions for input and output admittances of a discrete-component amplifier as:

$$Y_{in} = y_{11} - [y_{21} y_{12} / (y_{22} + Y_L)]; \quad (1)$$

$$Y_{out} = y_{22} - [y_{21} y_{12} / (y_{11} + Y_S)]. \quad (2)$$

Equations 1 and 2 show that a change in the load



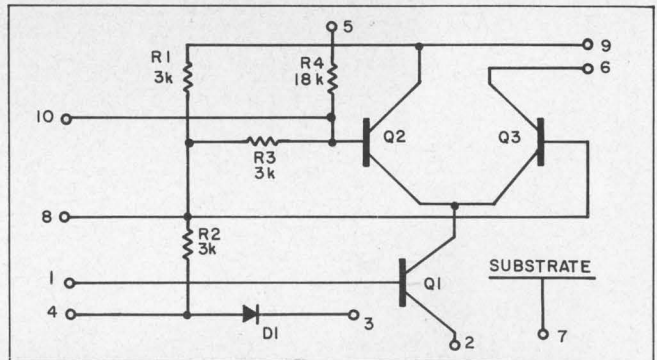
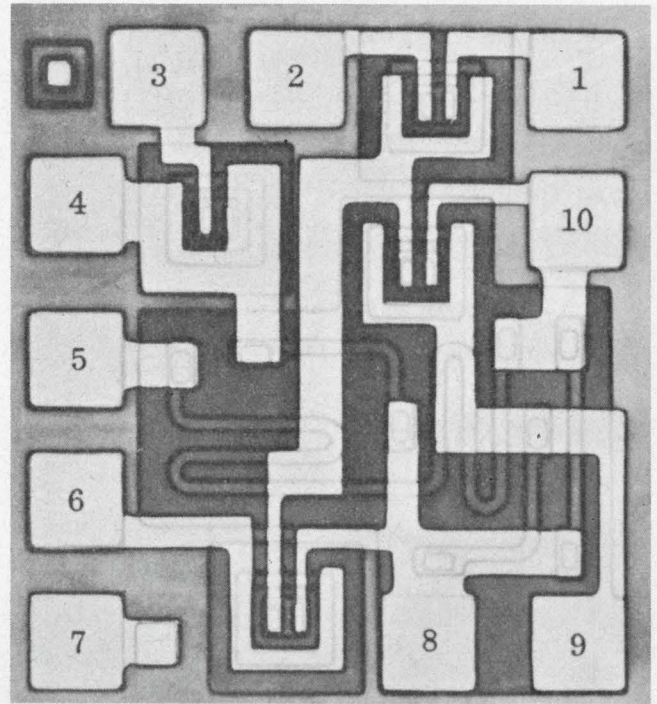
**Author Brent Welling** checks the pass band of a stagger-tuned, integrated-circuit IF strip of his own design. The integrated-circuit amplifiers simplify final tuning.

due to tuning of the output circuitry changes the input admittance and hence the input tuned circuit. The output tuned circuit is likewise changed when the input tuned circuitry is altered. As a result the input and output tuned circuitry must be alternately juggled until some degree of accuracy is obtained. With the integrated amplifier this is not the case. Since  $y_{12} \approx 0$ , Eqs. 1 and 2 above reduce to  $Y_{in} \approx y_{11}$  and  $Y_{out} \approx y_{22}$ . Hence, the input and output admittances remain constant and each tuned circuit may be tuned individually with little effect on the other. This minimizes the time needed for tuning alignment.<sup>2</sup>

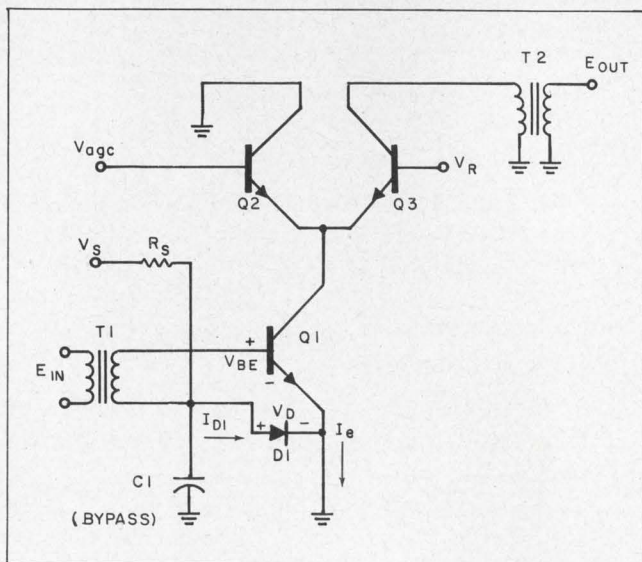
The gain of this circuit can be varied—a performance advantage over a single transistor. A dc analysis of the amplifier shows that for full agc operation the change in emitter current of transistor  $Q1$  (see Fig. 2) is very small ( $\approx 2\%$ ). Because  $I_{e1}$  varies only slightly, the input impedance variation, which depends on  $r_e = KT/qI_{e1}$ , is very small. As a result there is no detuning of the input circuitry with agc.

Figure 3 shows how the input resistance,  $R_{in}$ , and input capacitance,  $C_{in}$ , vary with applied agc voltage at 60 MHz when  $V_{CC} = 6$  volts. As can be seen, the input impedance of the amplifier is relatively unaffected by variations in agc voltage.

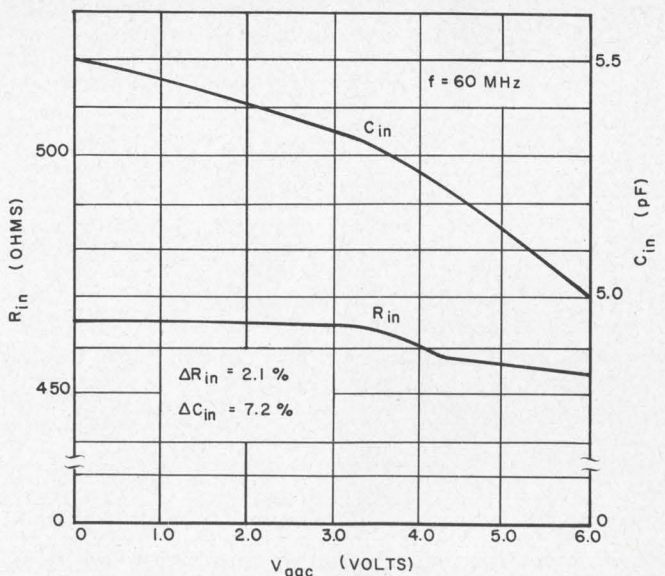
A schematic of the MC1550 amplifier including biasing resistors is shown in Fig. 2 with a picture of the monolithic die. The circuit is constructed on a 30-by-32-mil die using 200 ohm/square sheet resistance material and 1-by-0.5-mil emitters in the box geometry transistors. Resistors  $R1$  and  $R2$  bias the diode  $D1$  and also establish a base voltage for transistor  $Q3$ . Resistors  $R3$  and  $R4$  serve to widen the agc voltage range from 114 mV to about 0.86 volt. This is necessary if the agc line is to be less susceptible to external noise.



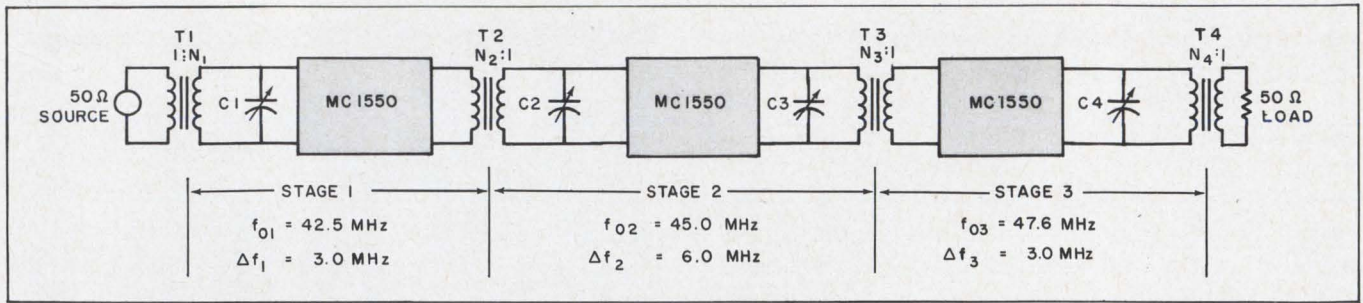
2. Diode  $D1$  lies right near transistor  $Q1$ ; hence, the emitter current and diode current are within 5% of each other. The matching characteristics obtainable with integrated amplifiers are hard to match with their discrete-circuit equivalents.



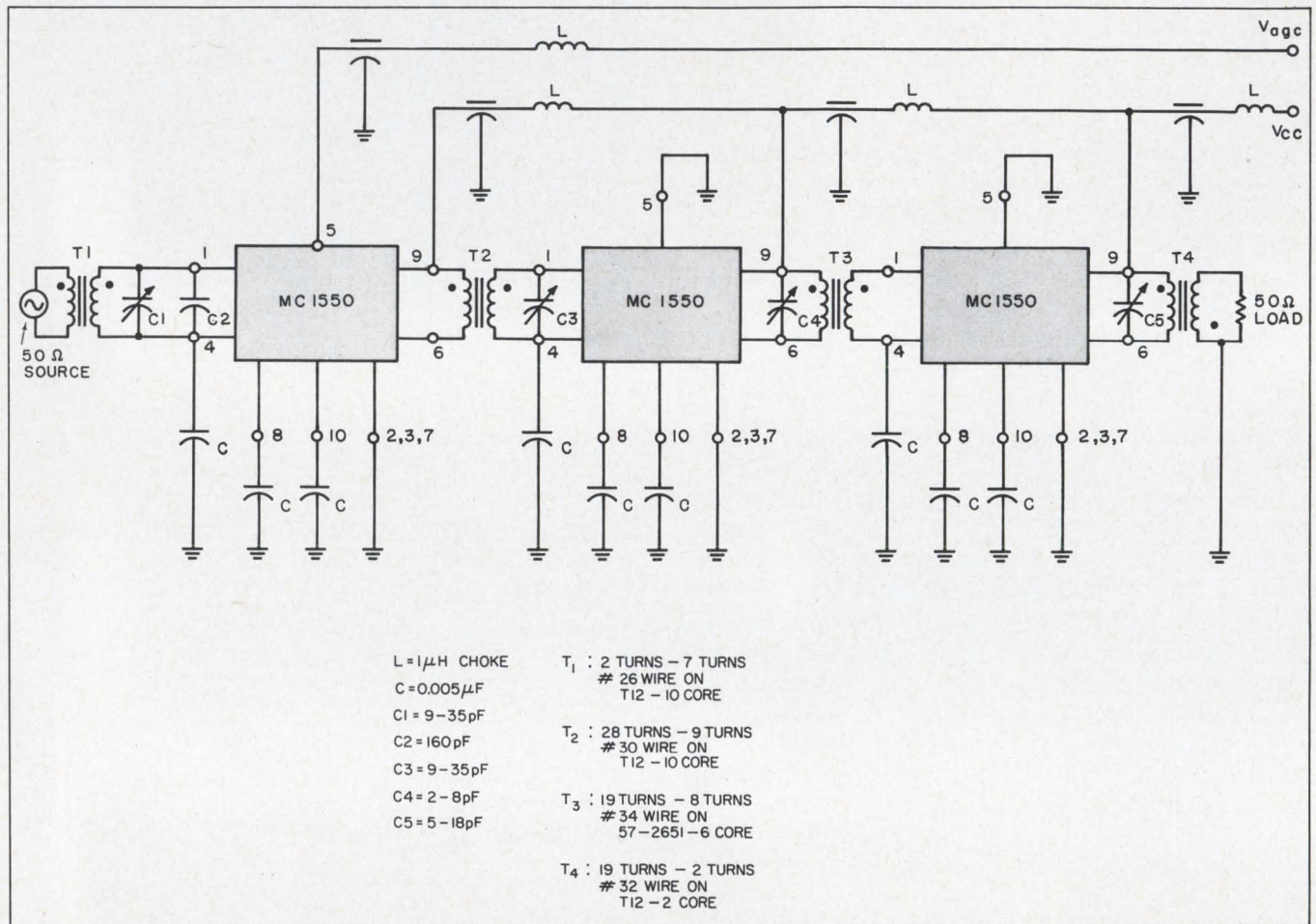
1. This simplified schematic shows how voltage  $V_{agc}$  controls the gain of the amplifier by controlling the flow of current through  $Q3$ .



3. Input impedance  $R_{in}$  is relatively unaffected by changes in the agc voltage.



4. This cascaded tuned amplifier is for operation at a center frequency of 45 MHz with a 6-MHz bandwidth.



5. Final schematic of the 45-MHz tuned amplifier shows all pin connections and component values.

### Design steps illustrate the technique

Consider the following hypothetical design for an IF amplifier:

Center frequency ( $f_0$ )	= 45 MHz.
Bandwidth ( $\Delta f$ )	= 6 MHz.
Power gain ( $G_T$ )	= 70 dB.
Agc control	> 50 dB.
Source impedance	= 50 $\Omega$ .
Load impedance	= 50 $\Omega$ .

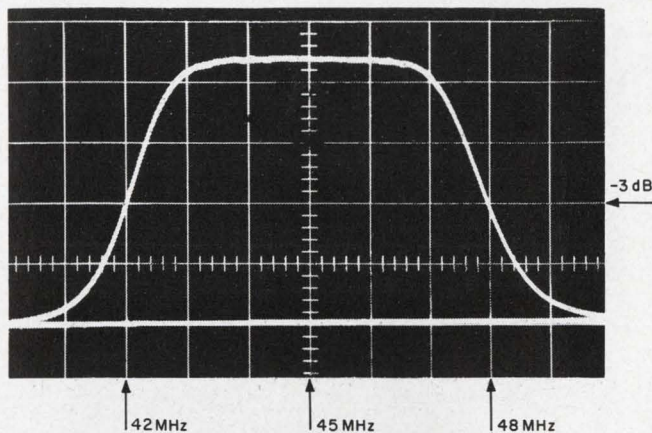
A typical circuit for this application with transformer interstage coupling appears in Fig. 4. The individual stage requirements of this flat, staggered amplifier are as follows:<sup>3</sup>

- One stage tuned to  $f_0$  with bandwidth  $\Delta f$ .
  - One stage tuned to  $f_0 \alpha$  with  $Q = 2.0/\delta$ .
  - One stage tuned to  $f_0/\alpha$  with  $Q = 2.0/\delta$ .
- ( $\delta = \Delta f/f_0$  and  $\alpha = 1 + 0.433\delta$ )

With these amplifier specifications, the following results are obtained:

- $\delta = 0.1333$                        $\alpha = 1.0578$
- One stage tuned to 45 MHz with a 6-MHz bandwidth.
  - One stage tuned to 47.60 MHz with a 3-MHz bandwidth.
  - One stage tuned to 42.50 MHz with a 3-MHz bandwidth.

There is nothing new or tricky involved in the



6. Scope trace shows frequency response of 45-MHz stagger-tuned circuit.

interstage design. The most expedient procedure is to assume that the coupling transformers are ideal, form equivalent models with one side of the transformer referred to the other side, then compute the band and center frequency from Eqs. 3 and 4 for the parallel tuned circuits:

$$\Delta f = 1/2 \pi R_T C_T, \quad (3)$$

$$f = 1/2 \pi (L_T C_T)^{1/2}, \quad (4)$$

where

$R_T$  = total parallel resistance,

$C_T$  = total parallel capacitance,

$L_T$  = total parallel inductance.

Because there are two tuned circuits associated with each stage, there will, however, be an over-all bandwidth shrinkage of each stage. This is easily handled by broadbanding the output tuned circuit of stage 1 while achieving the desired selectivity and bandwidth with the input tuned circuit and vice versa with stage 3. The same procedure could be followed in the design of stage 2, broadbanding the output tuned circuit while achieving the desired bandwidth and selectivity with the input tuned circuit. In this particular instance, however, the procedure adopted was to tune synchronously both the input and the output circuits of stage 2 and take the shrinkage factor into account. A schematic of the final design showing all the pin connections is given in Fig. 5.

A first prototype circuit was tuned in the following manner. Each stage was disconnected from the other stages and loading applied to each stage to simulate the actual circuitry in cascade. Each stage was then tuned to the desired center frequency with the correct bandwidth. Once each stage was tuned, the circuits were connected in cascade and final fine tuning adjustments made. With the experience gained in tuning the first prototype, a second prototype was tuned merely by sweeping the amplifier with a Jerrold 890 sweep generator and tuning while observing the output on an oscilloscope. A photograph of the sweep is shown in Fig. 6. The final results were:

Agc voltage	Power gain dB	Center frequency MHz	Bandwidth MHz
0.0	70.0	45.0	6.0
0.5	70.0	45.0	6.0
1.0	70.0	45.0	6.0
1.5	70.2	45.0	6.0
2.0	70.2	45.0	6.0
2.5	63.5	45.0	5.9
3.0	58.4	45.0	5.8
3.5	46.1	45.0	5.8
4.0	28.7	45.0	5.8
4.5	6.2	45.0	5.7

7. The agc voltage of the first stage controls the gain of the strip without severely affecting the bandwidth.

Center frequency = 45 MHz.

Bandwidth = 6 MHz.

Power gain = 70.0 dB.

The choice of which stage or stages to apply agc to is more or less arbitrary. Various agc combinations of the three stages were tried to study their effectiveness. With agc applied only to the first stage, 64 dB of agc control were obtained with a maximum deviation from flatness in the pass band of 0.7 dB. With agc applied to all three stages, 90 dB of agc control were obtained with a maximum deviation from flatness in the pass band of 1 dB. These represent the two extremes. When combinations of the three stages taken two at a time were tried, they all fell within this range. Thus, for the design specification, it was sufficient to apply agc only to the first stage. The variation of bandwidth and center frequency were measured and the results are given in Fig. 7. These data indicate a maximum of 5% bandwidth deviation occurring at the low-gain (maximum agc) condition, with full agc occurring over a 2.5-volt range. With an input of 50  $\mu$ V rms, the output signal into 50 ohms is 156 mV with a noise level of 6.8 mV.

The results of this design strongly indicate that the MC1550, and similar integrated amplifiers, have good potential for use in both the RF and IF stages of television, radio, radar, and communications gear where high gain, wide agc, and low cost are of prime importance.

The use of an integrated-circuit, high-frequency amplifier has been considered only in a stagger-tuned IF strip with a design frequency of 45 MHz. The design and tuning procedure is similar, however, for designs throughout its full range of operation—dc to 300 MHz. ■ ■

#### References:

1. H. Wallman, *Stagger-Tuned IF Amplifiers* (MIT Radiation Laboratory Report 524, Feb., 1944).
2. Robertson-Welling, *An Integrated-Circuit RF-IF Amplifier* (Motorola Semiconductor Products, Inc., Application Note AN247).
3. D. G. Fink, *Television Engineering Handbook* (1st ed.; New York: McGraw-Hill Book Co., Inc., 1957).

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ON READER-SERVICE CARD CIRCLE CAREER NUMBER 901

ELECTRONIC DESIGN 9, April 26, 1967



# MOS-FET and bipolar form RC phase-shift oscillator

An RC phase-shift oscillator which effectively exploits the unique characteristics of bipolar and MOS transistors is shown in the figure. This circuit configuration has several distinct advantages over other phase-shift oscillators.

The feedback network is a three-section, low-pass filter. This simultaneously provides a dc bias path for the MOS transistor and an ac phase-shift network. Because of the extremely high input impedance of the MOS transistor and the low output impedance of the bipolar transistor, the filter is subjected to near ideal drive and load conditions, thus simplifying design calculations. Large resistors may be used, making very low-frequency operation practical without the necessity of large capacitors.

Thus the circuit is simple to design, uses few components, and is suitable for a wide range of frequencies.

$R_L$  controls the total loop gain and should be adjusted for best output waveform. Once set, the oscillator is very stable because of its "self-bias" arrangement. The choice of a low-pass feedback network results in improved harmonic rejection. If the output is taken by another MOS-FET to

prevent loading, an exceptionally pure sine wave can be obtained.

The output dc level is approximately  $V_{CC} - V_{Gth}$ . For identical RC sections the frequency of oscillation is:

$$f_0 = 1/(2\pi 6^{1/2} RC).$$

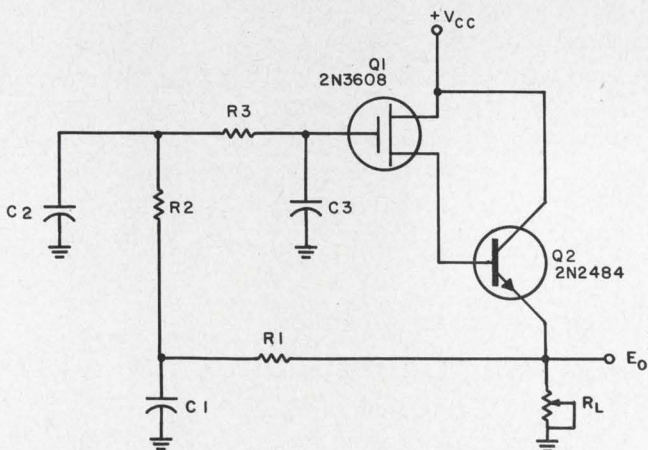
If the time constant of each section is the same, but  $R3 \gg R2 \gg R1$  and  $C1 \gg C2 \gg C3$ , each stage will contribute very close to  $60^\circ$  of phase shift and the frequency of oscillation is:

$$f_0 = 3^{1/2}/(2\pi RC),$$

where  $RC$  is any filter section.

*Charles R. Bond, Design Engineer, Electromec Design and Development Co., Santa Clara, Calif.*

VOTE FOR 110



**High input impedance** of a MOS-FET combined with low output impedance of the bipolar result in a simplified RC phase-shift oscillator.

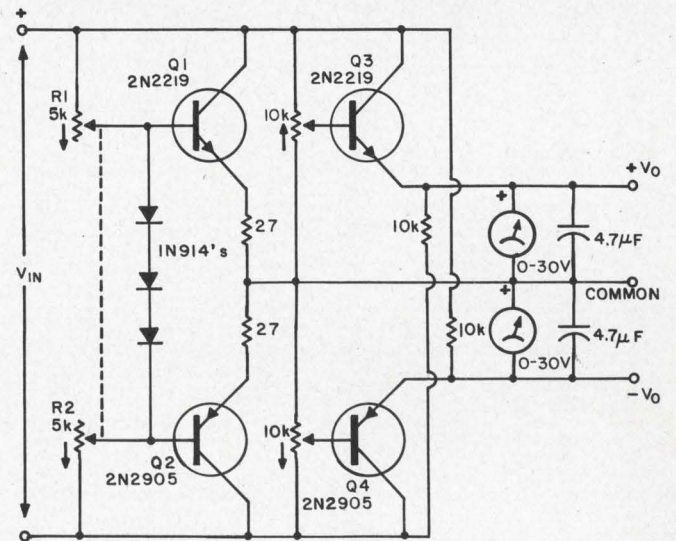
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# One power supply does the work of two

A common problem in a development laboratory is that of keeping several bench power supplies available. Most circuit development work requires at least two different supply voltages, but an engineer will all too often find only one power supply.

The circuit shows a "little black box" that can be plugged into a single, ungrounded power supply to furnish both a positive and a negative



**Negative and positive voltages** can be obtained from one power supply with the circuit shown.

voltage, each individually adjustable. The dual control,  $R1$  and  $R2$ , together with dual emitter follower  $Q1$  and  $Q2$ , sets the ratio of maximum available positive to negative outputs. The other two potentiometers, with their emitter followers, allow individual control of the positive and negative outputs.

If the input voltage is varied, both outputs will vary by approximately the same percentage, thus simplifying certain circuit tests. The values shown were selected to allow an input voltage of up to 40 volts. Maximum output current depends on the setting of the controls, but may be up to 50 mA.

**Acknowledgment:**

This work was performed under the auspices of the U.S. Atomic Energy Commission.

*Curtis Sewell, Jr., Electronic Engineer, Lawrence Radiation Laboratory, Livermore, Calif.*

VOTE FOR 111

## Modified capacitive iris provides design flexibility

The capacitive iris is a transverse shunt discontinuity in rectangular waveguides that is occasionally used in certain impedance matching and filter design problems. This iris is usually described quantitatively by a normalized susceptance. In standard construction (see Fig. 1a), larger values of normalized susceptance can be realized by decreasing the iris width,  $W$ . This can become quite difficult when large values of nor-

malized susceptance are desired.

In a standard X-band waveguide (RG-52/U), a 0.031-inch iris width (with rounded corners) with a 0.031-inch iris thickness provides a measured normalized susceptance of only 3.0 at 9.0 GHz. This can be increased to 8.5 by increasing the iris thickness to 0.187 inch. Further increases in iris thickness are usually not desirable for a simple shunt susceptance. Further decreases in iris width are not feasible, because end mill cutters smaller than 0.031 inch are not available.

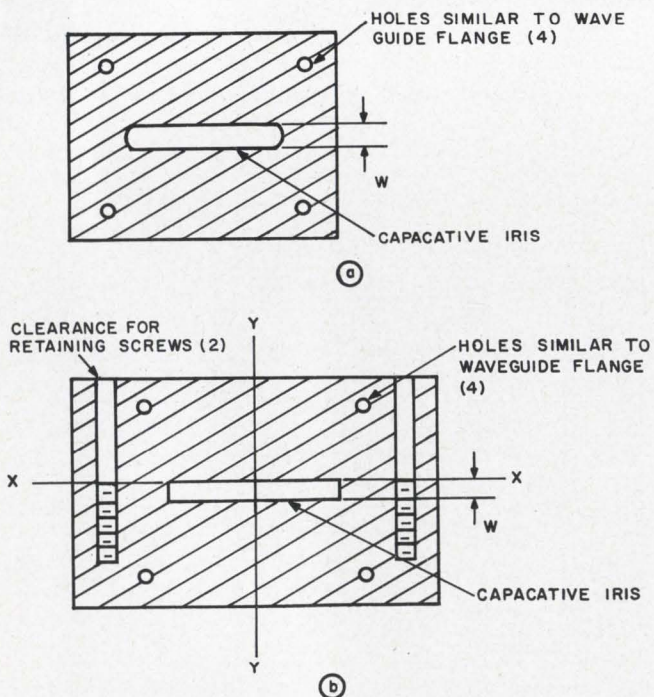
Use of the thick iris (0.187-inch thickness) makes possible iris widths smaller than 0.031 inch by constructing the iris from two pieces. This modified iris (see Fig. 1b) consists of two pieces joined together at plane X-X by two retaining screws. With a 0.187-inch iris thickness, No. 4-40 retaining screws can be used. A standard 1/16-inch end mill cutter can be used to cut irises of any width (with square corners) in the lower piece prior to assembly. In the RD-52/U waveguide, at 9.0 GHz, the following data were obtained for the modified thick irises:

Iris Width (Inches)	Normalized Susceptance
0.020	12
0.010	19
0.005	40

Another advantage of the thick iris is the possibility of providing a means to adjust the normalized susceptance of the iris. For the RG-52/U waveguide and an iris thickness of 0.187 inch, a No. 4-40 capacitive trimming screw can be used at plane Y-Y parallel to the retaining screws. At 9.0 GHz, with an iris width of 0.031 inch, a 0.025-inch insertion of the trimming screw increased the normalized susceptance from 8.5 to 11.0.

*Richard M. Kurzrok, Consulting Engineer, New York. (Work performed while the author was employed at the Advanced Communications Laboratory, Radio Corporation of America, New York.)*

VOTE FOR 112

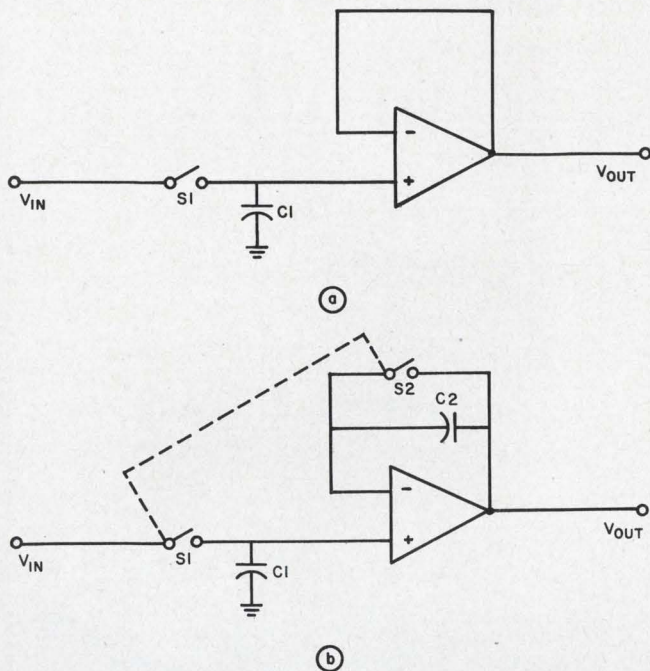


1. Increased susceptance is possible when a standard capacitive iris (a) is made out of two pieces (b). This allows greater flexibility in machining the opening.

## Capacitor improves sample-and-hold circuit

Conventional sample-and-hold circuits using operational amplifiers have the general form of Fig. 1a. The voltage to be held is sampled through switch  $S1$  and stored on capacitor  $C1$ . The amplifier functions as a high-input-impedance, unity-gain buffer between the voltage on the capacitor and the outside world. The charge on the storage capacitor leaks off at a rate determined by the amplifier input bias current and the shunt resistance to ground.

The addition of capacitor  $C2$ , equal to  $C1$ ,



Marked improvement in voltage-holding ability of a sample-and-hold circuit is possible when a capacitor is added (b) to the conventional circuit (a).

between the output and the inverting input of the amplifier (see Fig. 1b) improves the decay time of the circuit by better than a factor of ten. The circuit operates as before, except that leakage across  $C1$  is now compensated for by an equivalent leakage across  $C2$  such that the output voltage remains almost constant, depending on the degree of match between the two input bias currents and the capacitors. The output drift can even be adjusted to zero by trimming one of the capacitors to compensate for the small difference in bias currents.

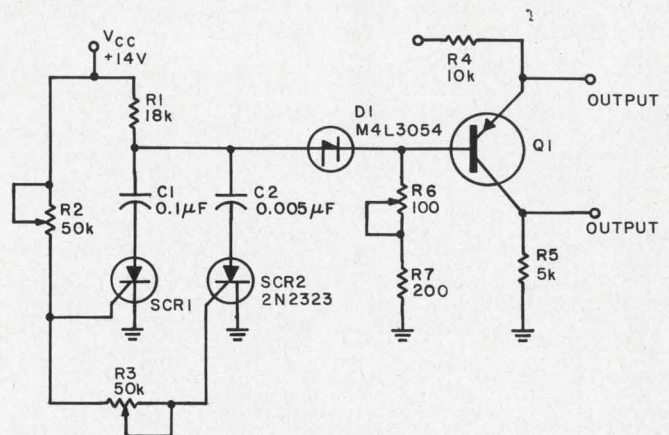
J. N. Giles, Fairchild Semiconductor, Mountain View, Calif.

VOTE FOR 113

## A four-layer diode forms double-pulse generator

A combination of a four-layer diode and two SCRs can be used to form a single, double, triple or even burst pulse generator.

This circuit (see figure) performs all these functions with a minimum of components. The cost of this unit is low and the stability is quite high.  $R1$  and  $C1$ ,  $C2$  are RC time constants selected by the gating of  $SCR1$  or  $SCR2$  to ground.  $R2$  and  $R3$  are the gate threshold controls.  $R3$  is used primarily to effect the mode change of the generator (single, double, triple pulse).  $R6$  controls the pulse width of the unit by changing the discharge time of the selected RC component through  $D1$ .  $R7$  functions as a current limiter for



Versatile pulse generator can be built quickly with the few components shown above.

$D1$ ,  $Q1$  serves as an isolation stage and an inverter.

$R3$  is adjusted for maximum resistance.  $R2$  is adjusted for single pulse.  $R3$  is adjusted for double- or triple-pulse groups. If the range of  $R3$  is increased, double pulse with a 4- $\mu$ s delay adjust can be made. The circuit develops 5-volt pulses with a rise time of 200 ns. The cost is about \$20.00. The frequencies available are approximately 400 Hz to 15 kHz.

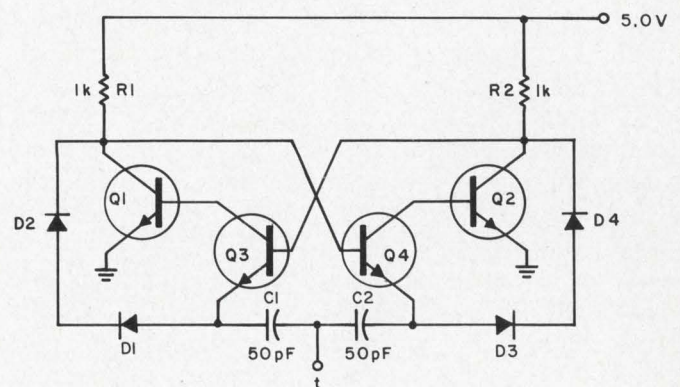
Gerald Lawson, PRD Electronics, Inc., Jericho, N. Y.

VOTE FOR 114

## Simple trigger circuit controls flip-flop

This circuit uses transistors  $Q3$  and  $Q4$  to provide coupling to  $Q1$  and  $Q2$  of the flip-flop and to trigger the flip-flop.

Prior to a trigger pulse, the circuit is stable with  $Q1$  on and  $Q2$  off, or vice versa.  $Q1$  is held on with base drive current from  $R2$  and the forward-biased collector-base diode of  $Q3$ . With  $Q1$  saturated,  $Q4$  and  $Q2$  are held off. On arrival of a positive trigger pulse,  $C1$  charges through  $D1$ ,  $D2$



$Q3$  and  $Q4$  provide coupling to  $Q1$  and  $Q2$  and trigger the flip-flop.

and  $Q1$ . As the trigger pulse falls back to zero, the potential at the emitter of  $Q3$  goes negative, which forward-biases the emitter-base diode and pulls the collector down to a saturation voltage. This has the effect of removing base charge from  $Q1$ , thus turning it off. The current through  $R1$  is then directed through the collector-base diode of  $Q4$  and forward-biases the emitter-base diode of  $Q2$ , turning  $Q2$  on. This turns  $Q3$  and  $Q1$  off. The cycle is now repeated on the opposite side with initiation by another positive trigger pulse. Note that the basic trigger scheme may be used with any multi-vibrator which turns off the normally on transistor.

Randy Brandt, Design Engineer, Raytheon Co., Mountain View, Calif.

VOTE FOR 115

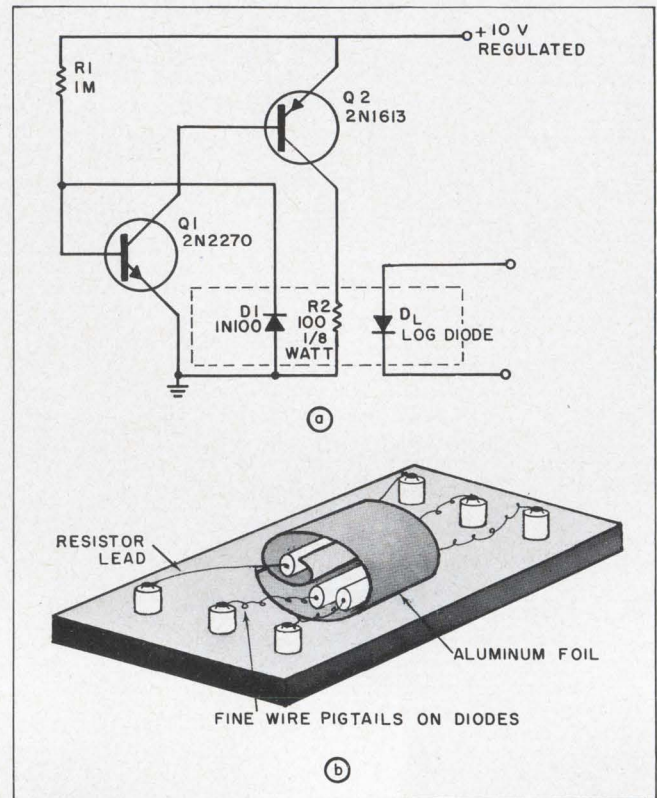
## Temperature regulator circuit stabilizes log converter

The forward-biased semiconductor diode characteristic is useful in many applications where a logarithmic data conversion is desired. The diode voltage and current have the general form:  $V = A \log I$ . However, the constant  $A$  in this characteristic is highly temperature-dependent, giving rise to conversion errors as high as 1 dB/°C. The coefficient of the diode temperature is indispensable for converter accuracy and repeatability.

The circuit shown is a simple temperature feedback control system which uses reverse-biased germanium diode  $D1$  as a temperature sensor. The two transistors form a direct-coupled current amplifier. Resistor  $R2$  heats diodes  $D1$  and  $D_L$  by thermal conduction in response to current from the amplifier. As  $D1$  heats, its saturation current increases; this in turn reduces the base current of  $Q1$ . Consequently, the heating current through  $R2$  is reduced until system equilibrium is established. The value of  $R1$  is adjusted so that about half the supply voltage is dropped across  $R2$  at equilibrium.

Diodes  $D1$  and  $D_L$  should have good thermal coupling to  $R2$  and be isolated as much as possible from other environmental changes. To achieve this, resistor  $R2$  and the diodes are coated with heat-conducting silicone grease and wrapped in a narrow strip of aluminum foil. In addition, the diode leads are cut short and fine wire pigtailed attached with low-temperature solder.

The system reduces output errors due to ambient-temperature changes by a factor greater than five. The system time constant is about 30



Temperature of a diode ( $D_L$ ) is maintained constant with the circuit (a). Packaging of the components enclosed by the dashed lines is shown in (b).

seconds, making warm-up time less than 5 minutes. Component types and values are not critical, except that diode  $D1$  should be germanium and transistor  $Q1$  should be silicon.

Alex Klooster, Jr., Willow Run Laboratories, Institute of Science and Technology, University of Michigan, Ann Arbor, Mich.

VOTE FOR 116

## RF voltage blocks receiver during transmit

This circuit provides antenna switching between transmit and receive modes. With 5 watts of transmit signal, upwards of 35 volts of RF must be controlled by a 12-volt power source. The relay is operated by applying these 12 volts to either  $TB+$  or  $RB+$  terminals. The opposite terminal will be grounded.

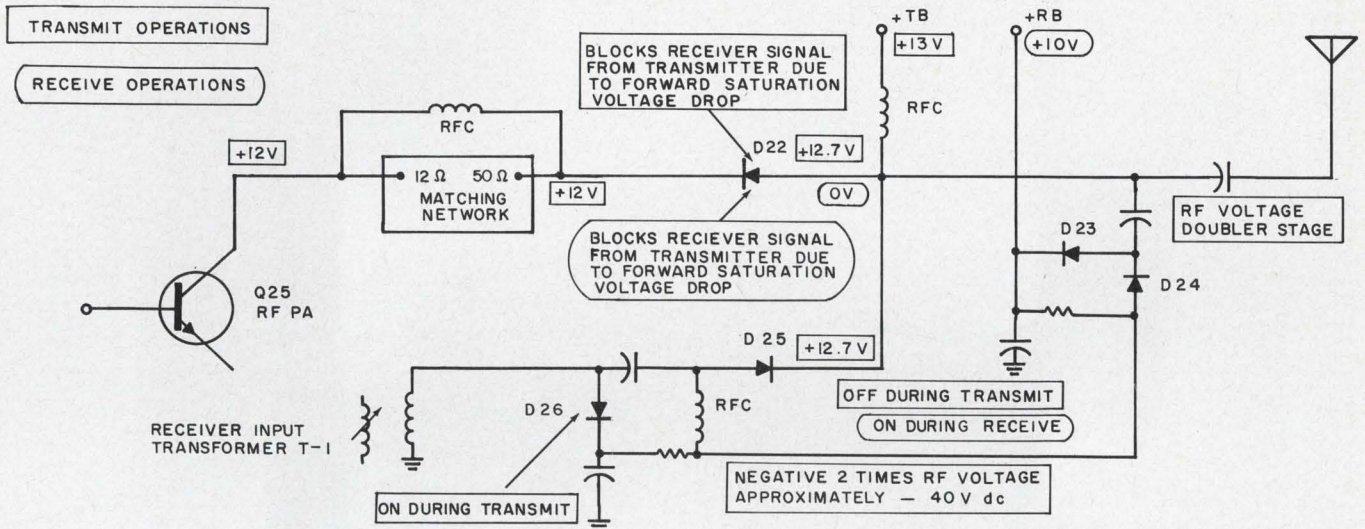
The basic requirement is to conduct a transmitted signal from the transmitter power amplifier stage to the antenna while keeping high RF voltage out of the receiver. The approach is to connect the power amplifier stage to the antenna through diode  $D22$ , which is turned on by  $TB+$  current flowing through it to the transmitter. Since this diode will not conduct with less than 0.5-volt

forward bias, it also disconnects the transmitter during receive. Diode *D25*, which connects the receiver to the antenna, is turned on during receive by *RB+* and is reversed-biased during transmit by the sum of *TB+* and twice the peak RF voltage. This RF-derived voltage is developed by a half-wave voltage doubler, composed of *D23*

and *D24* and connected in the RF line from the transmitter. Diode *D26* provides a low-impedance circuit across the receiver terminals during transmit.

*Arleigh B. Baker, Development Engineer, E. F. Johnson Co., Waseca, Minn.*

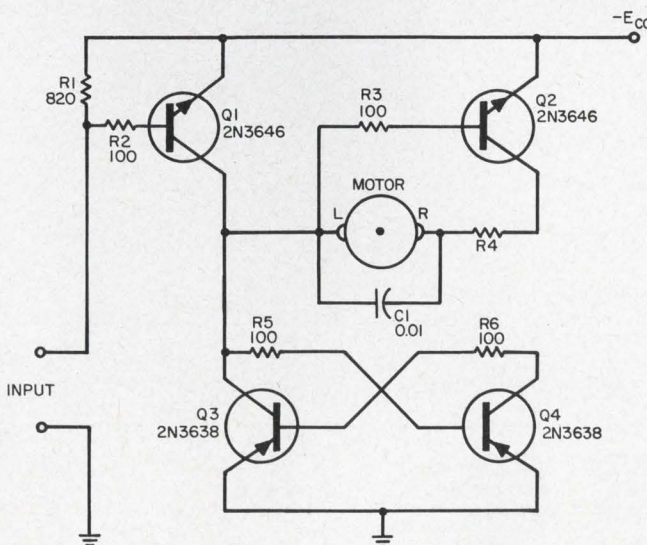
VOTE FOR 117



Solid-state antenna relay employs RF voltage to block receiver during transmitting mode.

## Spst switch reverses PM dc motor rotation

The circuit operates as follows: with input open, *Q1* is in the nonconducting state, *Q2* and *Q3* are conducting. *L* is positive with respect to *R*. The voltage across the motor terminals will cause the motor to rotate.



Any switch, spst or a transistor, placed across the input terminals will control the PM dc motor.

With input closed (either by switch or transistor) *Q1* conducts and causes *Q4* to conduct also. The decreasing collector voltage at *Q1* and *Q4* causes *Q2* and *Q3* to turn off. *R* will now be positive with respect to *L*. The voltage across the motor terminals will then cause the motor to reverse direction.

*R4* is a current-limiting resistor and speed control. *C1* is used to reduce arcing.

The circuit shown was used in a miniature pulse control system, but could have many applications, such as battery-powered tape recorders and strip-chart recorders.

*C. B. Smith, Specialist, Assembly Processes, General Electric Co., Memory Equipment Dept., Oklahoma City, Okla.*

VOTE FOR 118

## IFD Winner for Jan. 18, 1967

*J. C. Rich, Engineer, Test Equipment Engineering Quality Control, General Electric, St. Petersburg, Fla.*

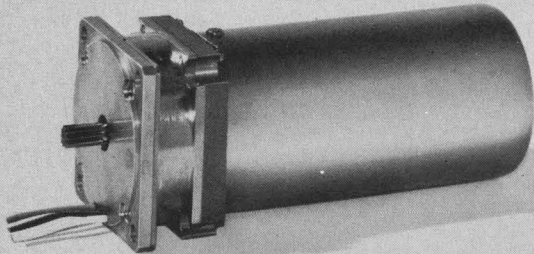
His Idea, "UJT and ac current source used to divide frequency," has been voted the \$50 Most Valuable of Issue Award.

Cast Your Vote for the Best Idea in this Issue.

# high performance motors

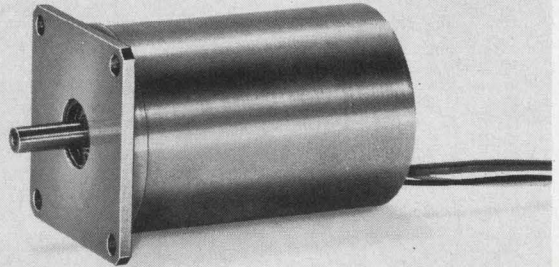
By Wright Division of Sperry Rand Corporation

## High Density DC Motors with clutch-brake



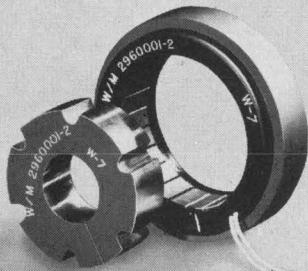
Enormous power is provided in small packages 2" to 4" in diameter. Offered in shunt, series, compound, and permanent magnet types.

## Synchronous Motors



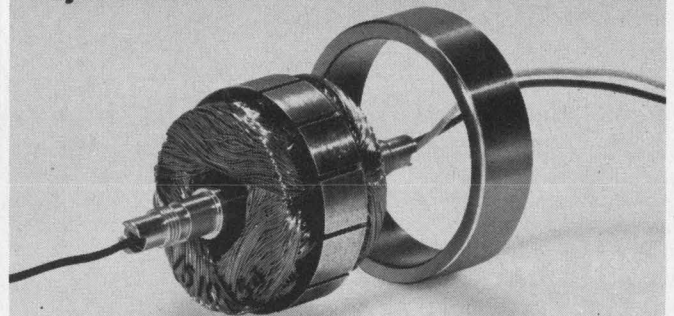
High efficiency designs available in single phase and polyphase types. They feature low noise and flutter. Six different speeds available in one unit.

## Brushless DC Torque Motors



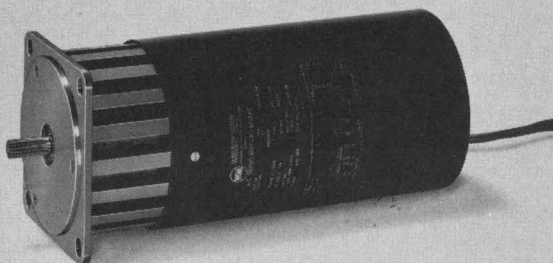
Torque motors with a response of four hundred millionths of a second for incremental rotation. Diameter 1 inch to 10 inches.

## Gyro Motors



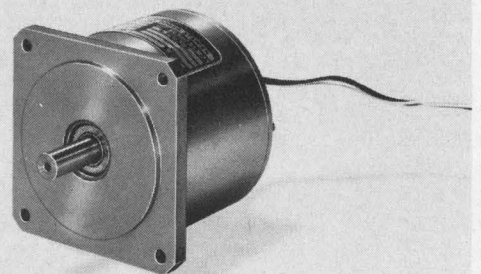
This new type of gyro motor features low power, high torque, and fast acceleration. Synchronous and induction. Half inch to seven inches in diameter.

## AC Drive Motors



Recommended for continuous drive duty in antenna, optical, stabilizing systems. Available with synchronous or servo characteristics. Inverted or conventional. Wide variety of windings and sizes.

## Power Stepper Motors



Powerful, permanent magnet stepper motors open whole new fields of application for the direct drive of all types of mechanical systems. Up to 600 ounce-inches torque at 15° step angle.

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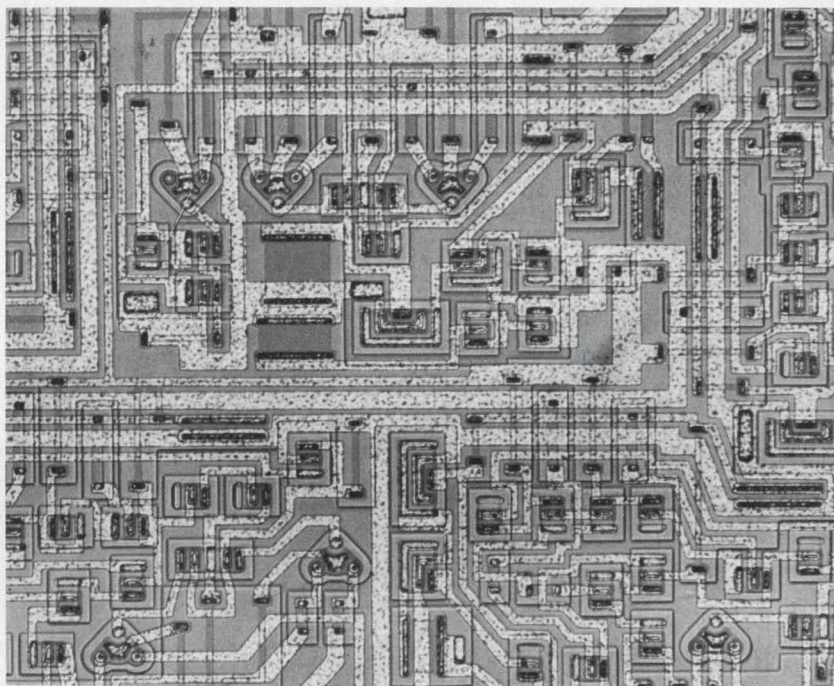
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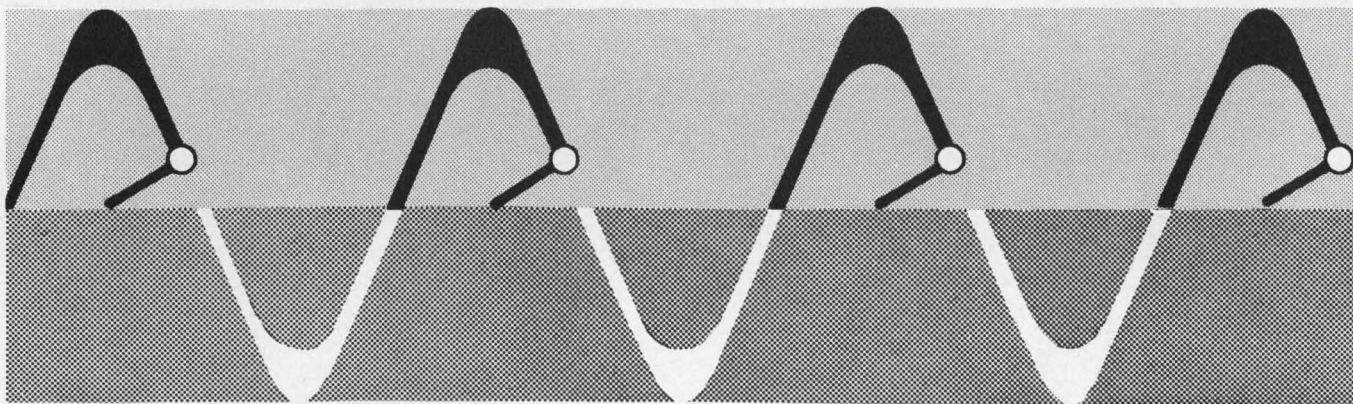
# Products



**Oxide won't penetrate** boron de-oxidized copper wire. Page 254



**Bipolar LSI array shifts** left or right, parallel or serial, at shift frequencies greater than 25 MHz. Page 253



**Zero-voltage switching** of resistive loads to 3600 watts is provided by a tiny module. A

monolithic IC triggers the Triac for full-wave ac power control with less RFI. Page 248

## Also in this section:

**Silicon FETs** are quiet down to sub-audio frequencies. Page 248

**Teflon-tipped probe** treats tiny chips gently. Page 257

**Design Aids**, Page 268 . . . **Application Notes**, Page 266 . . . **New Literature**, Page 269

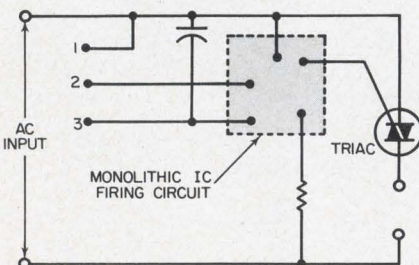
## IC triggers Triac for zero-voltage switching

General Electric, Semiconductor Products Dept., Electronics Park, Syracuse, N. Y. Phone: (518) 374-2211. Price: \$10 to \$20 (100 lots).

An ac power control module, (a Triac triggered by a monolithic IC) is a high-gain threshold and power control switch for resistance heater or tungsten lamp loads and resistance sensors. The modules are basically on-off controllers. The power switching is done by the Triac which is triggered by the monolithic integrated control circuit only at line voltage zero crossings. This mode of operation produces less RFI than mechanical switching elements.

The integrated control circuit, in addition to generating the proper triggering signals for the Triac, provides its own power supply and uses a differential amplifier to sense offset of a resistance bridge. The bridge consists of a user-supplied sensor resistance and reference resistance on one side, and a matched pair of resistors in the IC on the other. The usable range of sensor resistance is 5 to 50 k $\Omega$  or up to 100 k $\Omega$  at slightly less accuracy.

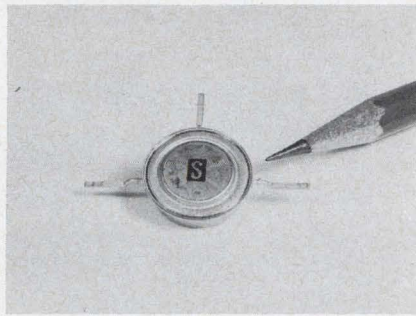
Models are available in ratings of 10 and 15 A rms at 120 and 240 V rms, 50 and 60 Hz, for controlling resistive loads from 500 to 3600 watts. All forms of the module have an extruded aluminum heat sink, electrically isolated from all current-carrying components.



IC triggers Triac for zero-voltage switching. It uses a diff-amp to sense offset of the resistance bridge formed by a sensor and reference resistance across points 1 and 3 and a matched pair of resistors in the IC. When sensor resistance is less than the reference resistance, trigger pulses are generated. Ten volts are developed across points 1 and 3.

CIRCLE NO. 420

## Darlington amplifier available in flatpack



Solitron Devices, Inc., Riviera Beach, Fla. Phone: (305) 848-4311.

Ten-ampere silicon Darlington amplifiers are packaged in a 3/4-inch flatpack. The devices have a minimum gain of 2000 at a collector current of 5 A with  $V_{CE}$  of 5 volts. Under the same conditions,  $V_{BE}$  is 2 volts. Saturation voltage ( $V_{CE}$ ) is 1.5 volts at a collector current of 5 A and a circuit gain of 500. Leakage currents are typically in the nanoampere range for both  $I_{CBO}$  and  $I_{EBO}$ . Typical gain is 50 at 5 MHz.

CIRCLE NO. 421

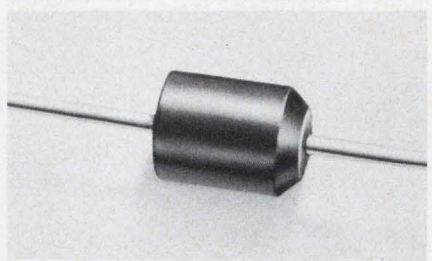
## Silicon FETs are quiet even at sub-audio

Siliconix, Inc., 1140 W. Evelyn Ave., Sunnyvale, Calif. Phone: (408) 245-1000. Price: \$11.75, \$10, \$9.40 (100 lots).

The 2N4867, 68 and 69 FET series is designed for minimum noise audio and sub-audio frequency applications. Equivalent short-circuit input noise voltage is 20 nV/ $\sqrt{\text{Hz}}$  at 10 Hz and 1 kHz. Thus, the FETs contribute less than the equivalent thermal noise of the signal source from 100 Hz to 10 kHz for generator resistance of 5 k $\Omega$  to 10 M $\Omega$ . Even at 20 Hz equivalent noise resistance is less than 20 k $\Omega$ . Excess noise at 10 Hz rises at 2 dB/octave. The FETs exhibit less noise than vacuum tubes, and are quieter than bipolar transistors when generator resistance exceeds 2 k $\Omega$ . Other specifications on the 2N4867, 68 and 69 include 700, 1000 and 1300- $\mu\text{mho}$  minimum transconductance, 3-to-1 spread in  $I_{DSS}$ , and 40-V breakdown voltage. They are packaged in the TO-72 case.

CIRCLE NO. 422

## Three-amp rectifier recovers in 300 ns



Electronic Devices, Inc., 21 Gray Oaks Ave., Yonkers, N. Y. Phone: (914) 965-4400. P&A: \$3.37; stock.

An axial-lead silicon rectifier has a forward current rating of 3 A, a surge rating of 300 A and recovery time of 300 ns from 1 A forward to 250 mA reverse. In addition to units with standard voltages of 50 to 600 PIV, 800- and 100-PIV rectifiers are available. The series is designed for use with square wave inputs of 5 to 40 kHz and sine wave inputs up to 300 kHz.

CIRCLE NO. 423

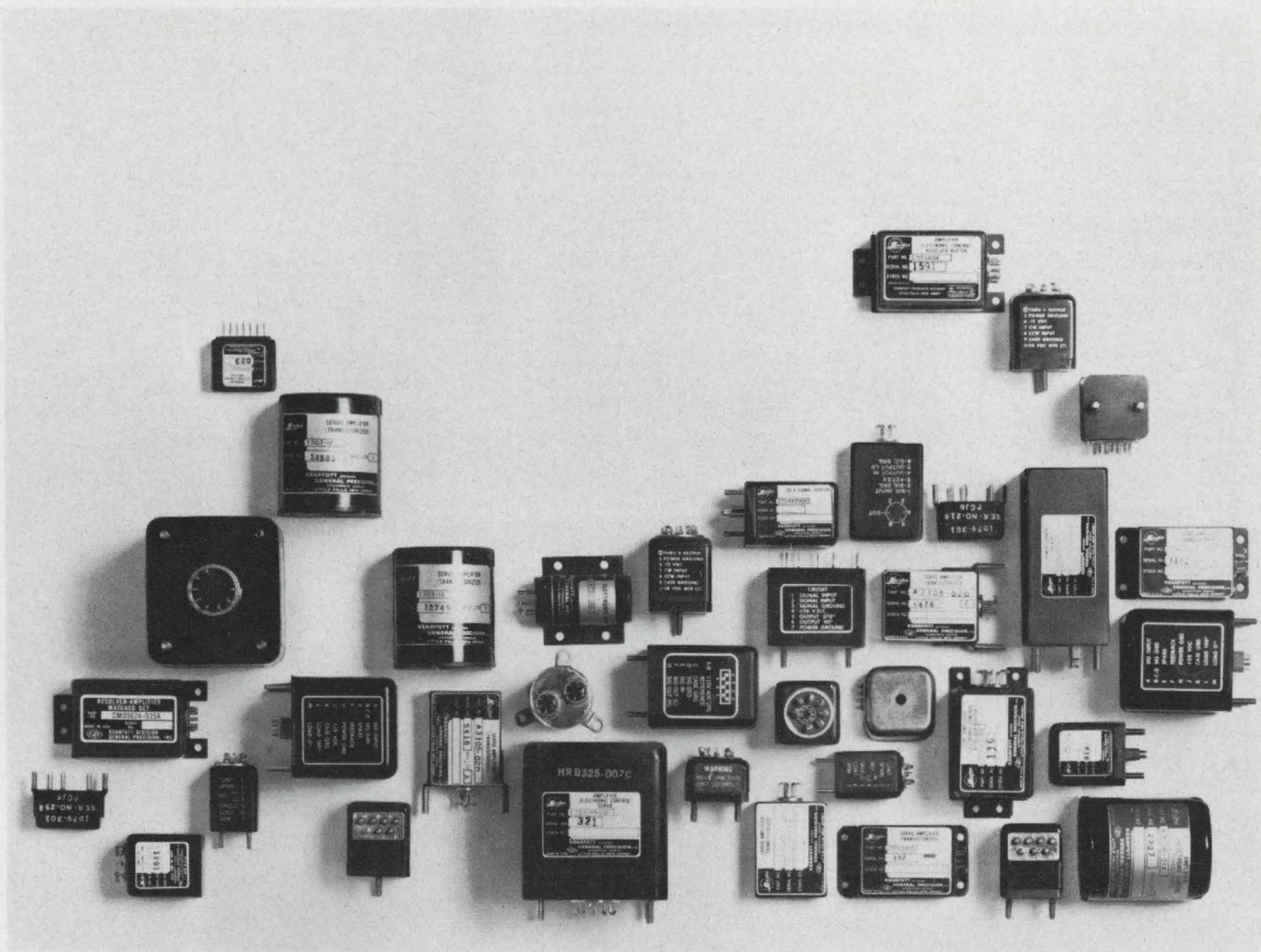
## Npns, pnps, stacked 4 to a TO-5 can

Industro Transistor Corp., 35-10 36th Ave., Long Island City, N. Y. Phone: (212) 392-8000.

Four pnp and npn high-voltage transistors stacked in one TO-5 package represent the only multi-component transistor package in the high-voltage field, according to the manufacturer, Industro Transistor Corp. The units are designed to be used for high-voltage switches and solid-state relay circuits. The space savings offers an advantage over series-stacking conventional transistors to reach a required voltage.  $V_{CEO}$  up to 2000 volts is obtainable or 1000 volts for the pnp and 1000 volts for the npn. Four npns or four pnps can also be built into one unit. The 10-pin units can be customized to specific voltage requirements compatible with standard hybrid microcircuit components. To manufacture the four-in-one transistors, one metallizing pattern is used on a ceramic disc. Each disc could accommodate two transistors in the Darlington amplifier configuration. Each base lead is accessible to outside connections.

CIRCLE NO. 424





We make a pile of electronic assemblies at

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SERVO AMPLIFIERS, PREAMPLIFIERS QUADRATURE REJECTION CIRCUITS, SOLID STATE CHOPPERS, MODULATOR/DEMODULATORS, AMPLIFIER-DEMODULATORS, BUFFER AMPLIFIERS, ISOLATION AMPLIFIERS, SUMMING ISOLATION AMPLIFIERS, AC-DC AMPLIFIERS, SIGNAL SENSORS, COMPARATOR AMPLIFIERS, MAGNETIC AMPLIFIERS, STEPPER MOTOR DRIVERS AND LOGIC.

In fact, we have just added another 24 new units in our latest catalog on electronic assemblies bringing the total to over 115 miniature solid state problem solvers. Among the units added is a 50-watt-output, 90°-phase-shift servo amplifier that weighs only 14 ounces. We also have a 16-watt unit for less demanding applications. We've been producing solid state half-wave and full-wave choppers for some time, and to these we've now added DC-to-AC modulators and AC-to-DC demodulators featuring full-wave modulation or demodulation at frequencies from 50-5000 Hz. Major new additions to the product line are fourteen new stepper motor driver/logic assemblies to satisfy almost every size

8, 11, or 15 stepper motor. Like all our electronic modules, these are transistorized, lightweight, potted in high-strength epoxy and can operate over a wide temperature range. Typically, these driver/logic assemblies consist of sequential logic controlled by CW or CCW input pulse commands and output drivers to control motor-winding current. Operating in the switching mode, these drivers minimize internal power dissipation.

We'd like to send you the new catalog, describing all 115 units. Just write to Kearfott Products Division, General Precision, Inc., Aerospace Group, Dept. 1450, 1150 McBride Avenue, Little Falls, New Jersey 07424.

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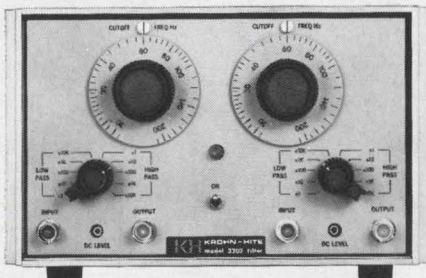
**GP GENERAL PRECISION INC.**

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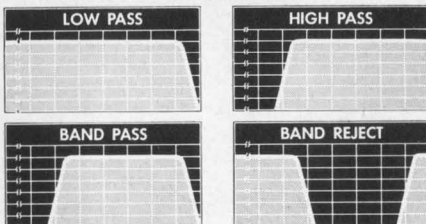
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**MULTIFUNCTION  
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 THAN HIGH-PASS and LOW-PASS  
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MODEL 3202 provides continuously adjustable high-pass, low-pass, bandpass and band-reject functions over frequency range of 20 Hz to 2 MHz. Two-channel bench unit shown; 5 1/4" x 8 5/8" x 1 5/4" - rack units available.

The unlimited flexibility of the K-H Multifunction Variable Filters is essential for complex frequency- or time-domain measurements. Don't settle for limited single-function capability when you can take advantage of K-H's two-channel Model 3202 or the one-channel Model 3200. See functions, below.



These responses are fully adjustable and may be set independently. This performance typifies the extra value you get from modern Krohn-Hite electronic instruments. Other values increase user confidence further by providing simpler, faster and lower-cost operation.

**Functions:** Low-pass — direct coupled with low drift. High-pass — upper 3 db at 10 MHz. Bandpass — continuously variable. Band rejection — Variable Broad Band or Null.

**Two Response Characteristics:** (1) fourth-order Butterworth or (2) simple R-C (transient free)

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**90-db Dynamic Range:** Low hum and noise (100 microvolts) eliminates costly preamplifiers.

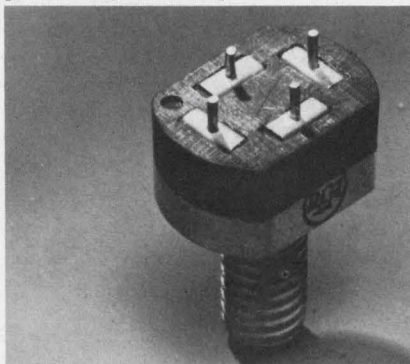
**Output Impedance:** 50 ohms, or lower. There's more in K-H Data Sheet 3200/3202. Write for a copy.

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SEMICONDUCTORS

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 packaged in plastic**



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The first plastic stud package for RCA's RF overlay transistor utilizes a terminal block structure that permits a choice of stripline, bottom-mounted printed-circuit board or lumped circuit mounting. The 2N5017 overlay transistor is suited for class B and class C RF amplifier applications in military and industrial uhf communications equipment.

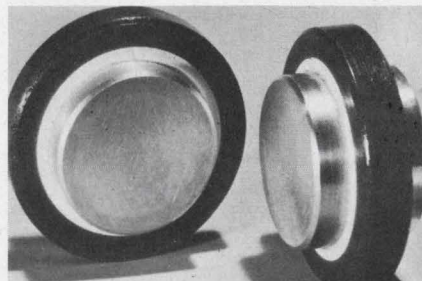
It provides outputs of 23 watts (typical), at 225 MHz and 15 watts (minimum) at 400 MHz, operating from a 28-volt power source. Performance is reportedly improved because of low emitter and base inductances which optimize power and gain. The low base lead inductance is of particular importance in wide-band equipment applications. The use of an isolated package technique eliminates circuit restrictions associated with grounded-emitter designs.

The package has all electrodes embedded in the top of the case, permitting circuit components to be placed as close to the chip as possible. Small pins are placed in the electrodes to provide mechanical support to the attached components. A reduction in lead length, with a corresponding reduction in emitter lead inductance, has been achieved by bringing the leads directly out of the top of the case.

CIRCLE NO. 425

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**Silicon rectifiers  
 withstand 7000-A surges**

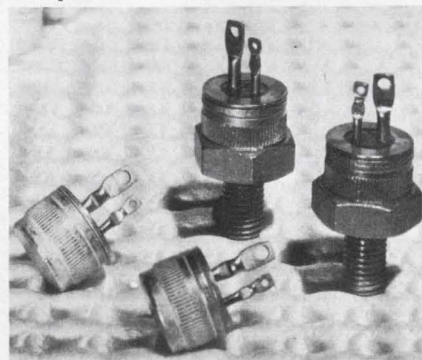


Cogenel, Inc., 50 Rockefeller Plaza, New York. Phone: (212) 757-9130.

Rated at values up to 700 A (average) and 2800 V (peak reverse voltage), a new silicon rectifier can withstand surge currents up to 7000 A (1 cycle at 60 Hz). Mechanical symmetry permits use of the same rectifier as a direct or reverse polarity device. Junction-to-case thermal resistance is 0.05°C/W. Encapsulated in a flatpack 2-1/4 inches OD and 1-1/8 inches thick, the rectifier is designed for heat-sink mounting.

CIRCLE NO. 426

**Triacs control 15 A rms  
 at peaks to 500 V**

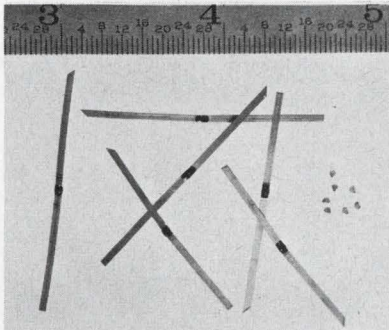


General Electric, Semiconductor Products Dept., Syracuse, N. Y. Phone: (315) 456-2798. P&A: \$3.29 in 1000 lots (200 volts); stock.

Types SC50 and SC51 Triacs are capable of controlling 15 A rms at peak voltages up to 500 V. They can withstand a peak one-cycle forward current of 100 A at 80°C junction temperature. Peak forward blocking voltage rating is 500 V. The operating temperature range is -40 to 115°C. The Triacs are available as either a press-fit or a stud-mounted unit.

CIRCLE NO. 427

## Silicon pin microdiodes rated to 1 kV PIV



Microsemiconductor Corp., 11250 Playa Court, Culver City, Calif. Phone: (213) 391-8271. P&A: \$6 (100 lots); stock to 2 wks.

Silicon pin microwave switching and limiting microdiodes have the glass hermetic seal integrally bonded to the silicon crystal surface. This provides semiconductor surface protection in excess of 1000 volts PIV. Average dissipation is 0.75 to 5 watts depending on heat sinking. Applications are phase shifters, modulators, attenuators and high-power switches. Units meet or exceed MIL-S-19500C.

CIRCLE NO. 428

## GaAs Schottkys for high-power, low-noise

Micro State Electronics Corp., 152 Floral Ave., Murray Hill, N. J. Phone: (201) 464-3000. Price: \$50, \$90 in evaluation quantities.

Epitaxial gallium arsenide Schottky barrier diodes are designed for high-power low-noise applications. The MS-1650-X and 1651-X can withstand repetitive pulses of 10 ergs (2-ns duration) at X-band. Higher burn-out resistance is realized at lower frequencies. High cutoff frequencies and low noise follow from the low dielectric constant, low skin resistance and low series resistance. At about 10 GHz, the 1650 has a single-ended noise figure of 7 dB maximum; 6.5 dB for the 1651. These ratings are based on an IF amplifier noise figure of 1.5 at 30 MHz. The diodes are available in a low-reactance microwave pill package. Capacitance values to match system impedance requirements and matched pairs are also available.

CIRCLE NO. 429

Eliminate Power Supply  
Obsolescence... Simplify  
Stocking Problems  
With These

# New Wide Range Compacts from ERA!



## Small Size, Wide Range DC Power Modules Permit Improved Design & Procurement Flexibility

The new Transpac® WR Series are ultra-compact, fully repairable, 71°C silicon power modules which provide regulated DC power over an extremely wide, adjustable voltage range.

Now you can use a single model for all your regulated power requirements... simplify your stocking requirements... eliminate power supply obsolescence... and enjoy significant purchasing economies.

### STANDARD MODELS

Output Voltage (DC)	Current (71°C)	Size WxDxH (inches)	Weight (lbs.)	Model	Price
1-33	0-500 ma	3¼ x 3¼ x 5¼	3.5	WR33P5	\$120.
1-33	0-1 amp	3¼ x 4 x 5½	5.1	WR331	\$155.
1-18	0-2 amps	4 x 4½ x 5½	6.5	WR182	\$170.
1-33	0-2 amps	4¼ x 5 x 6¾	7.8	WR332	\$185.
1-33	0-4 amps	5½ x 7¼ x 6¼	13.3	WR334	\$255.
1-33	0-8 amps	8¾ x 7¾ x 6¼	22.5	WR338	\$305.

### SPECIFICATIONS

**Input:** 105-125 VAC, 50-400 cps  
**Ripple:** Less than 800 microvolts RMS or 0.005%, whichever is greater  
**Line Regulation:** Better than ±0.01% or 5 mv for full input change  
**Load Regulation:** Better than 0.05% or 8 mv for 0-100% load change  
**Voltage Adjustment:** Continuous (Taps and screwdriver adjustment)  
**Short Circuit Protection:** Microseconds response, automatic recovery

**Vernier Voltage:** External provision  
**Transient Response:** Less than 50 microseconds  
**Maximum Case Temperature:** 130°C  
**Operating Temperature:** -20°C to +71°C free air, full ratings  
**Temperature Coefficient:** Less than 0.01% per degrees C or 3 millivolts  
**Long-Term Stability:** Within 5 millivolts (8 hours reference)



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## ELECTRONIC RESEARCH ASSOCIATES, INC.

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Subsidiaries: ERA Electric Co. • ERA Acoustics Corp. • ERA Dynamics Corp. • ERA Pacific, Inc.

ON READER-SERVICE CARD CIRCLE 99

Cinch  
Creative  
Problem  
Solving

# for the most accurately plated contacts



## develop new QC techniques

Consistently high levels of quality control for precious metal plating requires measurement of plating thickness—in microinches—with reproducible results!

To be sure that Cinch equipment would produce contacts meeting even the most rigid plating specifications, an elaborate, continuing program of quality control was developed. Based on beta ray backscatter measurements, it involved—

1. Devising a new BetaScope calibration system traceable to the Bureau of Standards.
2. Designing new methods for consistent contact alignment in the BetaScope.
3. Establishing new procedures for the statistical analysis of data obtained from plating thickness measurements.

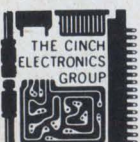
**RESULT:** Cinch can provide the exact plating thickness required at any point, or at all points, on a contact. Plating processes can be controlled to guarantee minimum plating depth because variations can be detected immediately.

At Cinch, the Quality Control Director reports directly to the President. Cinch is the *only* connector manufacturer whose products are accepted without incoming inspection by one of the nation's leading communications equipment manufacturers.

This sophisticated approach to quality control is another example of the extra dimension in Cinch's capabilities. Beyond the ability to develop fine products, we also offer in-depth production engineering, and tool, die, mold and equipment design and fabrication.

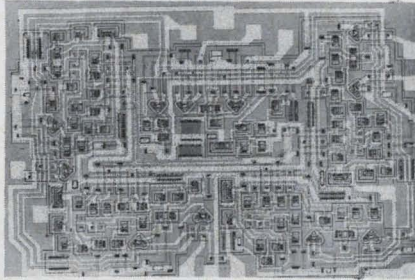
**CINCH**  
DIVISION OF UNITED-CARR

MEMBER



CONSISTING OF CINCH MANUFACTURING COMPANY, CINCH-GRAPHIK, CINCH-MONADNOCK, CINCH-NULINE, UCINITE (ELECTRONICS) AND PLAXIAL CABLE DEPT.

## Bipolar LSI array shifts at 25 MHz



*Sylvania Electric Products, Inc., 100 Sylvan, Woburn, Mass. Phone: (617) 933-3500.*

A universal 4-bit shift register, containing the equivalent of 175 components on a 60 x 85-mil chip, shifts at speeds exceeding 25 MHz. The register is capable of performing parallel and serial to parallel and serial or serial to parallel conversion, storage, delay and shifting operations in all parts of digital computers or control systems and can perform arithmetic operations such as multiplication and division. The register can shift left or right from parallel units. The SM100 can also perform a serial shift right. There is a simple control signal which, upon command, will permit parallel entry into all four bits which then again, upon command, can be shifted serially. By simple wiring at the package terminals, it can be converted to a shift register that can shift left and right. It can be clocked by either of two separate clock signals. Packaging is 14-lead dual-in-line.

CIRCLE NO. 430

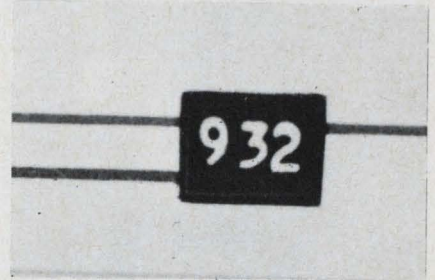
## 16-flip-flops on one card assembly

*Cambridge Thermionic Corp., 445 Concord Ave., Cambridge, Mass. Phone: (617) 876-2800.*

As many as 16 reset-set flip-flops come on a single card assembly. Eight quadruple 2-input DTL integrated circuits are used to achieve high speed and excellent noise immunity by cross-coupling gate pairs. Customer options of 2 through 16 flip-flops are available. The set and reset inputs and outputs of all flip-flops are accessible through a 70-pin connector.

CIRCLE NO. 431

## Resistor networks ratio-matched to 0.2%



*Microtek Electronics, Inc., 138 Alewife Brook Pkwy., Cambridge, Mass. Phone: (617) 491-4330.*

Matched thick-film resistor networks in values from 100  $\Omega$  to 100 k $\Omega$  are offered. The networks are fired on a common alumina substrate to assure stability and temperature tracking. Temperature tracking of 25 ppm/ $^{\circ}$ C from  $-55^{\circ}$  to  $+125^{\circ}$ C is standard. Networks show less than 0.05% change in absolute resistor value after 1000 hours load life. The network shown above consists of two resistors ratio-matched to 0.2% and meets MIL-STD 202C method 106B.

CIRCLE NO. 432

## IC op-amp priced at a low of \$5

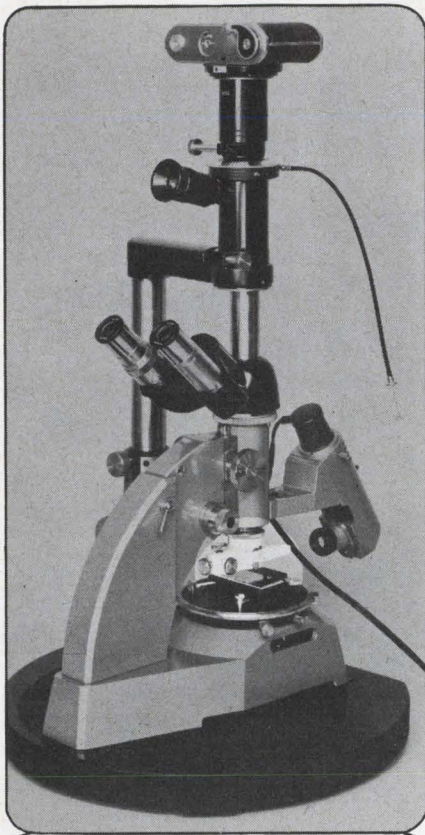
*Fairchild Semiconductor, 313 Fairchild Dr., Mountain View, Calif. Phone: (415) 962-2530. P&A: \$4.95 (over 10,000); stock.*

Fairchild Semiconductor's  $\mu$ A709-C op-amp is designed for industrial users now paying \$15 to \$35 for op-amp modules. The unit is available in a hermetic metal TO-5 can with typical input offset current of 100 nA with an input offset voltage of 2 nA. The large signal voltage gain is 45,000 with an input voltage range of  $\pm 10$  V. The typical output voltage swing is  $\pm 14$  V. In industrial use, the amplifier is suitable for dc servo systems, high-impedance analog computers, low-level instrumentation applications and for the generation of special linear and nonlinear transfer functions.

CIRCLE NO. 433

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**WILLIAM J. HACKER & CO., INC.**  
Box 646, W. Caldwell, N.J., CA 6-8450 (Code 201)

ON READER-SERVICE CARD CIRCLE 101

## MATERIALS

### Boron-deoxidized copper resists oxidation



Anaconda American Brass Co., 414 Meadow St., Waterbury, Conn. Phone: (203) 757-2021.

Boron-deoxidized copper alloy offers superior resistance to oxygen penetration, high purity, high electrical and thermal conductivity and good joining characteristics. Key to the resistance to oxygen penetration is the presence of the boron (approximately 0.01%) which "ties up" any oxygen already in the alloy by combining with it, thus rendering it harmless, and also "tying up" any oxygen that may be present during processing. Temperatures in excess of 2730°F are required to release the oxygen. The alloy is virtually equivalent to oxygen-free copper in other respects. Potential uses are seen in magnetrons, synchrotrons, klystrons and other electron accelerator components, transistor and diode bases, lead frames for ICs, armature and transformer windings, coaxial cables, generator connectors, connectors in signal systems, commutator bars and risers and ground and motor leads.

CIRCLE NO. 435

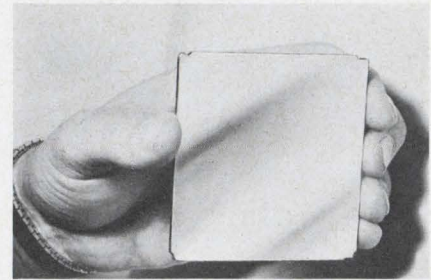
### Magnetic film seals and shields

Emerson & Cuming, Inc., 59 Walpole, Canton, Mass. Phone: (617) 828-3300. P&A: \$3 to \$5/foot; stock.

RF and mechanical sealing is simplified by a flexible plastic magnet core, bonded to a highly conductive plastic film. By applying a strip of the film around the edge of an opening, the plastic magnet draws the door or cover into contact with the conductive plastic, forming the RF and mechanical seal.

CIRCLE NO. 436

### Mirror-finish metal for IC substrates



Sherman Industries, Inc., American Silver Co. Div., 36-07 Prince St., Flushing, N. Y. Phone: (212) 353-8012.

Mirror-finish metal strip is designed for use as metal substrates for integrated circuitry. Metal substrates tend to eliminate many of the problems of expansion usually encountered with ceramics. In addition, the metal substrates provide an integral return path, thus making it unnecessary to include a return path in the circuitry. The strip is available in copper and aluminum in widths up to 3 inches.

CIRCLE NO. 437

### Clean contacts from spray can

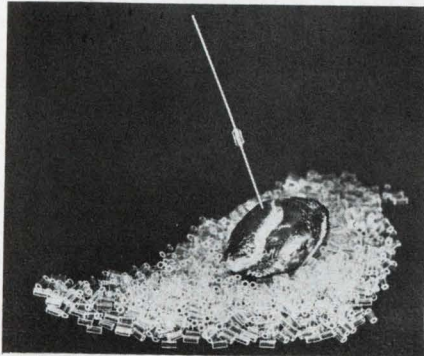


Spray Products Corp., Industrial Div., P. O. Box 1988, Camden, N. J. Phone: (609) 663-7040.

A specially formulated solvent is designed for use on electric and electronic contacts. Applied as an aerosol spray from a pushbutton can, SPC electrical contact cleaner combines high density with low surface tension and viscosity to penetrate microscopic cracks and crevices. Dirt, grease and other foreign matter is either dissolved or lifted to the surface where the force of the aerosol propellant blows it away. The cleaner evaporates completely and leaves no residue.

CIRCLE NO. 438

## Low-alkali glass seals at 740°C



Corning Glass Works, Corning, New York. Phone: (607) 962-4444.

Heat damage and electrical degradation due to alkali poisoning are minimized when semiconductor devices are encapsulated in this sealing glass. The glass is a lead-alumino-borosilicate composition with an alkali content of less than 0.1%. It can be sealed at approximately 740°C. The expansion and viscosity of the glass provides good hermetic seals to molybdenum, Kovar and tungsten. Loss tangent is 0.001 and dielectric constant is 6.91, both at 1 MHz. The glass is available as cut tubing.

CIRCLE NO. 439

## Silicon tetrachloride for wafer makers

Dow Corning, 500 S. Saginaw, Midland, Mich. Phone: (517) 636-8000.

Semiconductor-grade silicon tetrachloride is a clear, nonflammable, low-boiling liquid for use in the manufacture of epitaxial silicon wafers. The high-purity material enables device manufacturers to produce uncompensated epitaxial depositions with consistent control of resistivity at levels above 50  $\Omega$ -cm, n-type. The silicon tetrachloride may also be doped with either n-type or p-type carriers to meet specific resistivity specifications. It is packaged in nine-liter Pyrex bottles with a 2-inch flange at the mouth. About 24 pounds of product is shipped in each bottle. With a modified cap, the bottle may be converted into a vaporizer for direct use in an epitaxial system. This makes it unnecessary to transfer to another container.

CIRCLE NO. 440

# best delivery

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SPECIFICATIONS  
FOR YOUR  
APPLICATIONS\*

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The American Semiconductor Zener Diodes Line is the prestige line for military and quality industrial installations. In many cases, they are the only types specified for critical space applications. Complete voltage range, lower dynamic impedances, higher than MIL specification performances, and immunity to shock and vibration in magnitudes exceeding 100,000 G's are the characteristics of the American Line.

Write for complete details and prices on the complete zener family line in all voltage ranges and standard power ratings for your commercial applications. Dept. ED 4.

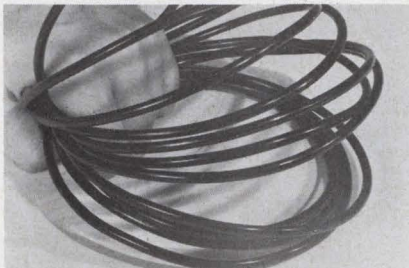
# american

SEMICONDUCTOR CORP.

4 North Hickory Avenue  
Arlington Heights, Ill. 60004

## MATERIALS

### RFI-proof coax aluminum-sheathed



*Amphenol Corp., Amphenol Cable Div., 6235 S. Harlem Ave., Chicago. Phone: (312) 261-2000.*

Solid aluminum-sheath coaxial cable claims RFI shielding performance far superior to existing cables. Designated BC-59, the new cable is equivalent in size to RG59/U (0.242 inch OD). On shielding tests it was rated at 80 to 90 dB down, as opposed to 30 dB down for standard RG59/U. It is also 30% lighter and has 5% better attenuation performance. Other electrical characteristics are the same. The performance is achieved by replacing standard braided sheath with a sheath of solid aluminum foil. The foil is applied to the cable core during the jacket extrusion process. Extrusion of the polyethylene jacket over the foil chemically bonds the foil to itself and to the polyethylene.

CIRCLE NO. 434

### Potting compound makes it clear

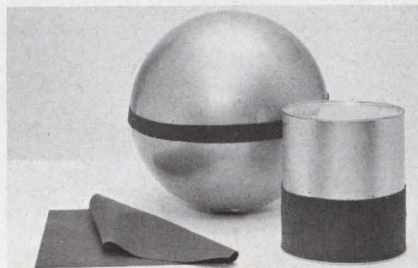


*Emerson & Cuming, Inc., Canton, Mass. Phone: (617) 828-3300. P&A: \$5 to \$6; stock.*

Eccosil 2 CN is a transparent, water-clear potting silicone. It can be cured by catalyst addition at room or somewhat higher temperature. Because of its flexibility, it provides good protection to embedded components against shock and vibration.

CIRCLE NO. 441

### Flexible silicone sheet cuts reflectivity

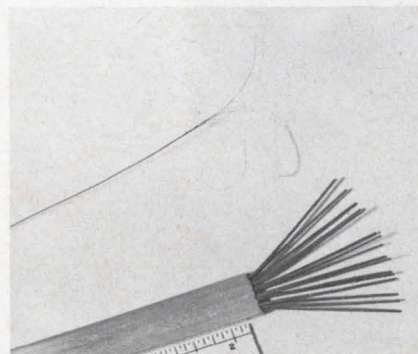


*Emerson & Cuming, Inc., Microwave Products Div., Canton, Mass. Phone: (617) 828-3300. Price: \$10/square foot.*

A high-loss flexible silicone material when bonded to a metal surface will effectively prevent the flow of microwave currents. It will therefore reduce the back-scatter or reflectivity of metal structures caused by surface currents. It can also be draped over objects to alter reflectivity characteristics. Radiation patterns of antennas can be modified by the application of Eccosorb GDS to elements, dishes, horns, etc.

CIRCLE NO. 442

### Superconductive wire useful to 100 kilogauss



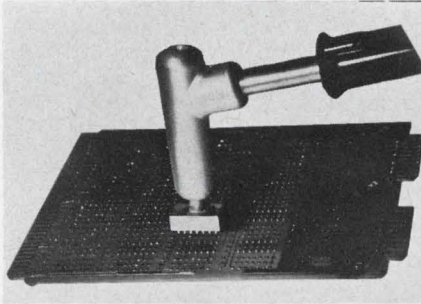
*Avco Corp., 2385 Revere Beach Pkwy., Everett, Mass. Phone: (617) 389-3000.*

Composite superconductors consist of fine, high-current-density niobium-titanium wires encased in copper. They are available in round, square and strip configurations with one to 20 wires. They are useful at fields up to 100 kilogauss. Ratio between the superconductor and the copper substrate varies from one to over five. Overall current densities of more than 20,000 A per square centimeter at 45 kilogauss have been achieved.

CIRCLE NO. 443



### Multipin tip fits any soldering iron

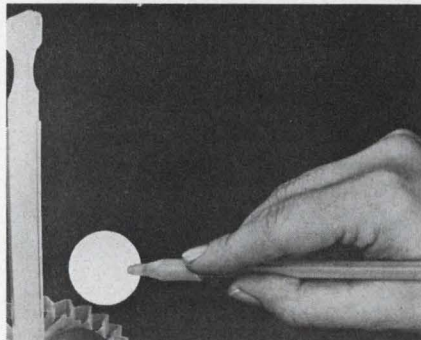


*Air-Vac Engineering Co., Inc., 100 Gulf St., Milford, Conn. Phone: (203) 874-2541.*

A tip for soldering and desoldering multipin components fits any standard soldering iron. The head can be used in conjunction with ring-shaped solder preforms to speed assembly of electronic circuit boards by simultaneously soldering 14 component pins. The same unit can also be used for desoldering electronic components. When placed over the pin connectors, it will simultaneously melt the solder in all the eyelets for each part. The 14-hole tip is iron-plated copper.

CIRCLE NO. 444

### Teflon-tipped probe treats chips gently

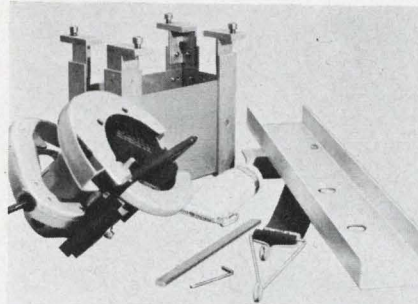


*Fluoroware, Inc., County Road 17, Chaska Industrial Park, Chaska, Minn. Phone: (612) 448-3131. Price: \$6.75, \$2 (tip only).*

A vacuum operated probe ensures gentle handling of chips, wafers, substrates and other miniature semiconductor materials. It features a Dupont Teflon FEP tip to prevent damage. Tip hole diameter is 1/16 inch. The vacuum pickup body has a tapered end to accept 3/16- to 1/4-inch ID hoses.

CIRCLE NO. 445

### Waveguide cut, assembled in the field



*Dielectric Products Engineering Co., Inc., Littleton, Mass. Phone: (617) 486-3575.*

Waveguide may be cut and assembled in the field with this kit of tools and materials. It is possible to cut waveguide and mount flanges to close tolerances without welding, machining, heating or resorting to the use of dissimilar metal assemblies. Waveguide sizes from W/R 430 to W/R 2100 can be handled. The kit includes positioning and cutting guides, tools, sealant and a power saw. Vswr of field-assembled flanges is 1.02 over the waveguide band at waveguide rated power.

CIRCLE NO. 446

### Air-operated tool makes solderless connections



*Gardner-Denver Co., Gardner Expressway, Quincy, Ill. Phone: (217) 222-5400.*

A lightweight, quiet, air-operated Wire-Wrap tool is designed for use with wire in size from 20 to 30 AWG. The air motor requires only 4 cfm of air. The tool is available in wrapping speeds of 3500 and 5500 rpm.

CIRCLE NO. 447

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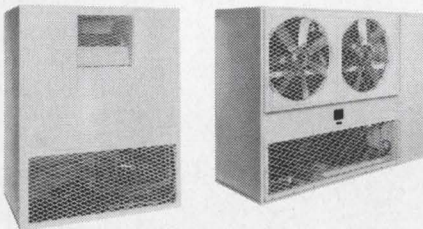
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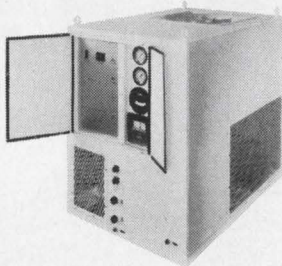
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One of the new Ellis and Watts Heat Exchangers may be the answer to a need for tailoring a cooling system to your type of electronic equipment. Minimum space, low noise level and optimum performance have been achieved in each of a wide range of designs which include indoor/outdoor types in ratings from 5 to 300 KW. Proved in military, aerospace and commercial applications, these designs offer flexibility for quick modification to meet any specific cooling requirements.

Why not put the widely recognized Ellis and Watts custom-cooling "know-how" to work for you. Write us at the address below.



\*Liquid-to-Liquid Heat Exchangers also available.



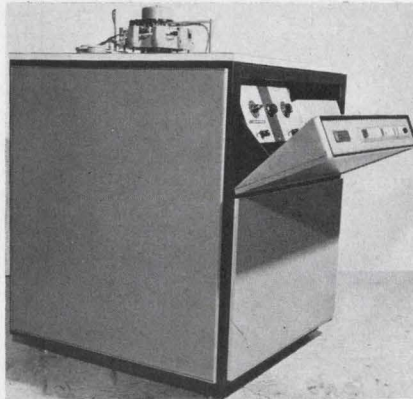
**ELLIS AND WATTS COMPANY**  
Ellis and Watts Company, P.O. Box 36033  
Cincinnati, Ohio 45236

ON READER-SERVICE CARD CIRCLE 136

258

## TEST EQUIPMENT

### Machine tests chips, sorts into 10 bins



*Bulova Watch Co., Inc., Systems and Instruments Div., Bulova Pk., Flushing, N. Y. Phone: (212) 335-6000. P&A: \$24,300; dual version, about \$32,000; 16 wks.*

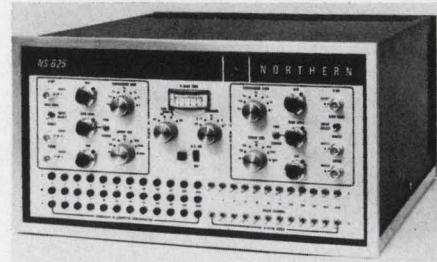
Transistors, diodes and integrated circuits can be tested, classified and placed in bins, automatically, at the rate of 7200 per hour, by a new system from Bulova Watch Co.'s Systems and Instruments Div. The chip tester-classifier, model 85002, tests the units before they are packaged, avoiding the waste of packaging rejects. The system will automatically feed, orient, test and sort into 10 categories square or rectangular chips from 20 to 250 mils long. It will then feed each selected classification into a magazine, keeping it properly oriented for subsequent bonding or placement operations. Testing rates range from 200 to 800 ns per piece, depending on the number of parameters.

The chips are untouched by hand from insertion in the machine to placement in the magazine. Readings are taken by precious-metal contacts nested in the equipment.

The machine claims distinct advantages over go-no-go wafer testing units. Testing each chip in a wafer avoids the necessity of breaking up the wafer later to separate the qualified chips from the rejects. The chips are sorted into 9 acceptable categories, according to specs, and rejects. Operation is simple and requires no special skill. A portable laboratory microscope is required for the setup for each different kind of chip to be tested. The machine measures 32 in. square by 36 in. high. A dual version is available to double the production output.

CIRCLE NO. 448

### A-to-D converter digitizes at 40 MHz



*Northern Scientific, Inc., 2551 W. Beltline, Middleton, Wis. Phone: (608) 836-6511. P&A: \$3200 (single converter), \$4200 (dual); 30 days.*

A 40-MHz digitizing rate is achieved by the NS-625 dual analog-to-digital converter. The unit also features a digital-to-zero offset control, two 12-bit address scalars, independent operation for each converter, exclusive circuitry for internal rejection of noncoincident events and overflows, patchcord programing and optional internal logical level interface. The converter uses the peak detection technique. Standard output levels for the data and control signals are  $\pm 0.5$  volt for zero and  $6 \pm 0.5$  volt for one. Coincidence circuitry provides for operation in two-parameter mode with coincidence timing adjustable from 0.5 to 2.5  $\mu$ s. Noncoincident events produce only 3- $\mu$ s dead time.

CIRCLE NO. 449

### Interval counter uses dc level gating

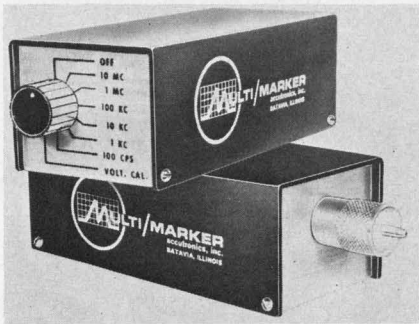


*Anadex Instruments, Inc., 7833 Haskell Ave., Van Nuys, Calif. Phone: (213) 782-9527. Price: \$845.*

Dc level gating is used in this time interval counter. It provides a variety of interval measurements such as pulse length, pulse spacing and time between electrical events. The counter has start/stop dc levels which are adjustable from +30 to -30 V with  $\pm$  slope control. A switch is provided for single-line or two-line gate inputs. Measurements from 10  $\mu$ s to 100,000 s are possible.

CIRCLE NO. 450

## Time mark generator accurate to $\pm 0.007\%$

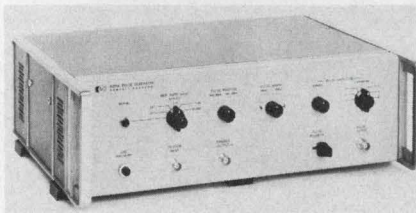


Accutronics, Inc., 12 South Island, Batavia, Ill. Phone: (312) 879-1000. P&A: \$225; stock.

Six crystal-controlled frequencies from 100 Hz to 10 MHz at  $\pm 0.007\%$  accuracy and a 1-V p-p calibrator at better than  $\pm 0.5\%$  are provided by the Multi/marker. Mercury battery powered, it uses silicon planar epitaxial transistors throughout. The unit can be plugged directly into a scope to calibrate the sweep and vertical amplifiers. For field work it can be used as a secondary frequency standard, for calibration of counters or as a trigger source.

CIRCLE NO. 451

## Low-cost pulser has 1-ns rise, fall time



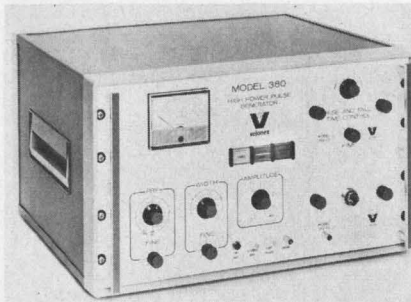
Hewlett-Packard, 1501 Page Mill Rd., Palo Alto, Calif. Phone: (415) 326-7000. P&A: \$990; stock after May 1.

Fast, clean pulses with rise and fall times less than 1 ns are featured in model 8001A pulse generator. Overshoot and ringing on leading edges are less than 3% of pulse amplitude (6% on trailing edges). Pulse tops are flat within 2%. Pulse amplitude is continuously variable from 0.04 V to 10 V across 50  $\Omega$ . Pulse width is also continuously variable from 100 ns to 500 ns.

CIRCLE NO. 452

It's time to renew your subscription to **ELECTRONIC DESIGN**. Return your renewal card today.

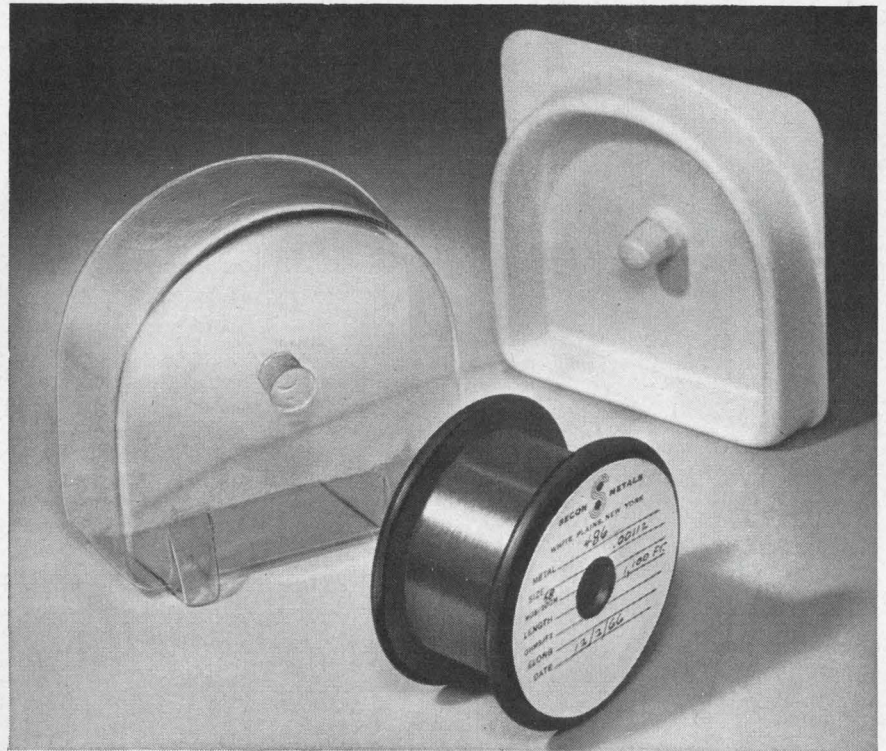
## 5-kW pulser has 10-ns rise time



Velonex, 560 Robert Ave., Santa Clara, Calif. Phone: (408) 244-7370. P&A: \$4200; 30 to 60 days.

A high-power pulse generator has a 10-ns rise time and a 12-ns fall time. A variable rise-fall time control plug-in and high-current and high-voltage plug-ins provide flexibility with output voltages to 1 kV, or output current to 100 A into 0.5  $\Omega$ .

CIRCLE NO. 453



## does your design require precious metal pot wire?

Secon produces high quality, precision — *precious metal* — potentiometer wire. We offer quick delivery for your production requirements, as well as FREE prototype samples.

You get the precious metal alloy wire you need, engineered to meet your exact requirements — from 37 to over 610 ohms/cm; low temperature coefficient of resistance — with excellent roundness and linearity.

This high tensile strength wire is engineered to facilitate uniform winding — available to .0004" diameter. Supplied bare or enameled.

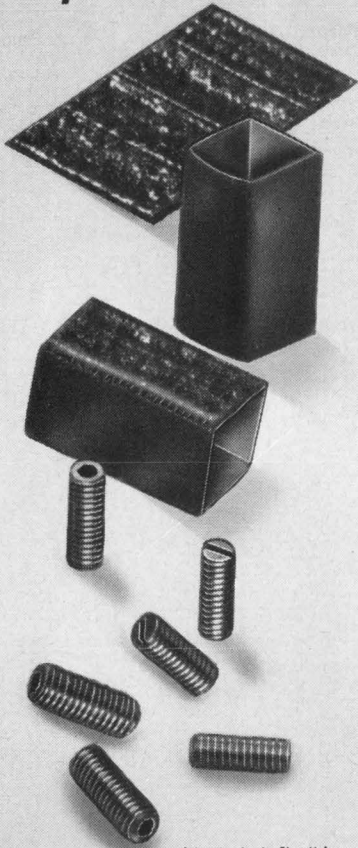
If your requirements are for high quality, fine potentiometer wire you should write for a copy of our comprehensive brochure on wire for the potentiometer industry.

Please write on your letterhead; no obligation of course.



7 INTERVALE STREET, WHITE PLAINS, N.Y. 10606 ■ (914) 949-4757  
ON READER-SERVICE CARD CIRCLE 137

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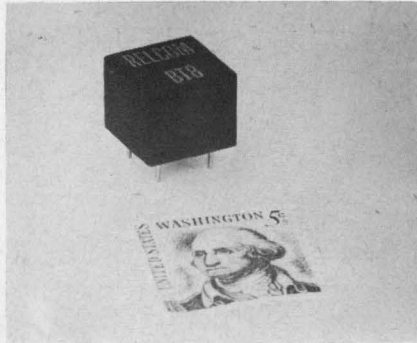
9540 Tully Ave., Oak Lawn, Ill. 60454

Phone: 312-422-3353

ON READER-SERVICE CARD CIRCLE 138

## MICROWAVES

### Balanced transformers cover 50 kHz to 1 GHz

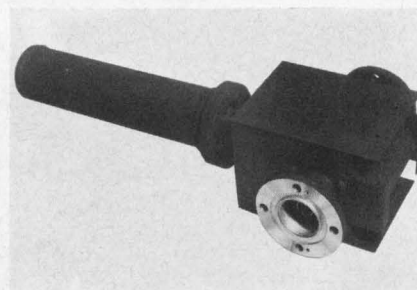


*Relcom, 2164 E. Middlefield Rd., Mountain View, Calif. Phone: (415) 961-6265. P&A: \$11 (over 100); stock.*

Broadband balanced transformers for hybrid junctions, isolated vector addition and division, impedance matching (2:1, 4:1, 8:1, 16:1), balance modulators, phase detectors or phase comparators cover 50 kHz through 1 GHz. Model BT8 features frequency coverage from 1 MHz through 200 MHz with 4:1 impedance matching. Power loss is typically 1 dB, amplitude unbalance is less than 0.1 dB from 1 to 50 MHz and less than 1 dB from 50 to 200 MHz.

CIRCLE NO. 454

### Coax circulator rated at 1.2 kW

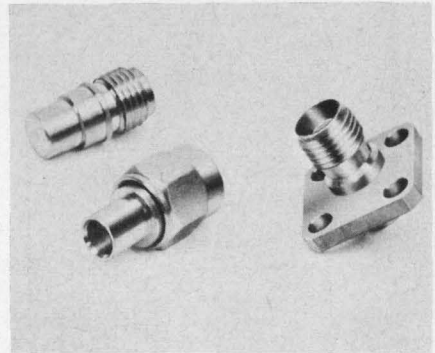


*Litton Industries, Airtron Div., 200 E. Hanover Ave., Morris Plains, N. J. Phone: (201) 539-5500. P&A: about \$1000; 90 days.*

High-power coaxial three-port junction circulators can double as duplexers or low-loss isolators. Model 336265 features an average power of 1.2 kW cw with an insertion loss of 0.4 dB maximum. It covers 1.7 to 2.4 GHz, has an isolation of 20 dB, vswr of 1.2 and has 1-5/8-inch coax connectors.

CIRCLE NO. 455

### Stripline connectors for semirigid cable

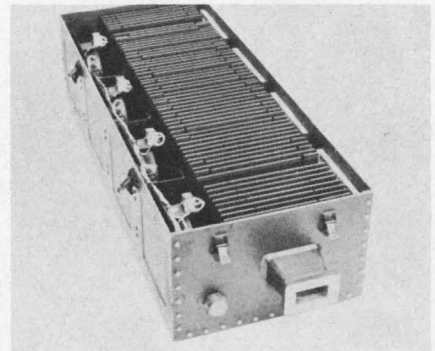


*Elpac, Inc., 3760 Campus Dr., Newport Beach, Calif. Phone: (714) 546-8640.*

Miniature stripline connectors for 0.141-inch semirigid cable mate with OSM, RBM and other standard connectors. Body, flange and coupling nut are of stainless steel. The dielectric is solid Teflon. The heat-treated beryllium copper center contact makes it possible to pre-cut the cable to exact length, and to complete the assembly without tools. The five styles are male and female, male and female square flange and male right angle.

CIRCLE NO. 456

### S-band dummy load convection-cooled

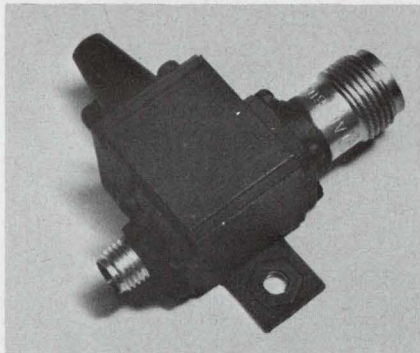


*Microlab/FXR, 10 Microlab Rd., Livingston, N. J. Phone: (201) 992-7700.*

S-band dummy loads are capable of handling fully rated peak power and 20-kW average power without the use of liquid cooling. They feature a built-in forced-air cooling system equipped with an air-flow safety interlock switch. Frequency range is 2.7 to 3.3 GHz and maximum vswr is 1.2.

CIRCLE NO. 457

## Submini circulator weighs 1 ounce

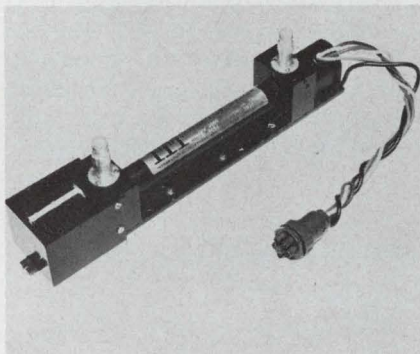


Litton Industries, Airtron Div., 200 E. Hanover Ave., Morris Plains, N. J. Phone: (201) 539-5500. P&A: \$70 to \$100; 30 days.

A subminiature three-port junction coaxial circulator, measuring 5/8 x 3/4 x 3/4 inches and weighing 1 ounce, is available in Y or T configurations. It covers a frequency range of 4.2 to 4.4 GHz. Other models are available in the frequency range of 1 to 10 GHz, covering 5 to 10% bandwidths. Isolation is 20 dB, insertion loss is 0.3 dB and vswr is 1.2.

CIRCLE NO. 458

## Ten-watt TWT weighs 2.5 pounds

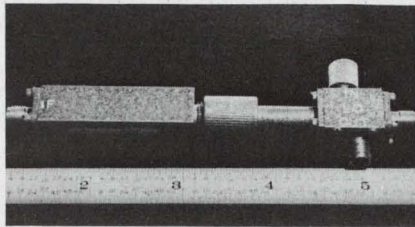


ITT, 320 Park Ave., New York. Phone: (212) 752-6000.

A lightweight 10-watt traveling-wave tube covers the 8-to-12-GHz band. Type F-2094 has 40 dB of gain at rated output. It is of metal-ceramic construction. The tube is ppm focused and forced-air cooling is used. The collector is isolated and can be used at voltages depressed up to 50% below helix-cathode voltage. A dc blocking capacitor is built into the RF output.

CIRCLE NO. 459

## IF mixers cover C through Ku-band

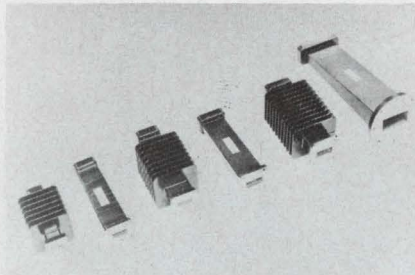


Sage Labs., Inc., 3 Huron Dr., Natick, Mass. Phone: (617) 653-0841. P&A: \$400 to \$600; 45 days.

Four miniature microwave balanced mixers cover high C-band through Ku-band in four signal RF bands: 5 to 7 GHz, 7 to 9.4 GHz, 9.4 to 12 GHz and 12 to 15 GHz. IF is 3 GHz, and the LO frequency is the sum of RF and IF. Conversion loss is 15 dB, signal-to-IF isolation is greater than 40 dB, and LO-to-signal isolation is greater than 8 dB. All models use 1/4-36 connectors.

CIRCLE NO. 460

## Dummy loads handle 25 to 2000 watts



Raytheon Co., Special Microwave Devices Operation, 130 Second Ave., Waltham, Mass. Phone: (617) 899-8400. P&A: from \$150; 30 days.

Twenty-one lightweight air-cooled dummy loads handle high power levels. For example, the LKuM1 weighs 4.8 ounces and handles 25 watts average power, while the LCH100 weighs 3.6 pounds and handles 2000 watts of average power. Available finned or unfinned, the loads operate over uhf, L, S, C, X and K-bands.

CIRCLE NO. 461

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Quality Product of  
**SIGMUND COHN CORP.**

# Platinum Potentiometer Wire Alloy

## No. 479\*

\*Trade Mark/Patented



No. 479 Platinum Alloy Wire is manufactured exclusively in the Sigmund Cohn Corp. plant, specifically for low-noise, precision potentiometers . . . This high tensile strength, long-life potentiometer alloy wire contains 92% Platinum, 8% Tungsten . . . It is exceptionally round . . . linear . . . bright . . . strong and corrosion-resistant. Potentiometers wound with it have very low noise limits — shelf life unlimited . . .

**SIGMUND COHN CORP.**

121 South Columbus Avenue  
Mount Vernon, N. Y. 10553



Sigmund Cohn Corp. of California, Burbank, Calif.  
Sigmund Cohn-Pyrofuzze, Inc., Dallas, Texas

ON READER-SERVICE CARD CIRCLE 139 ➤

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High purity  
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## APPLICATIONS:

Phosphors  
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Metallurgy  
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Metal Halide Lamps

Like technical data on  
any of the above oxides  
or metals? Write, wire  
or call us about your  
specific interest.

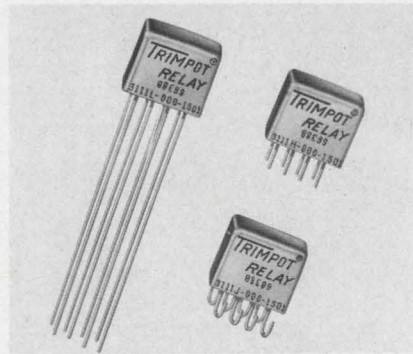
**MICHIGAN  
CHEMICAL  
CORPORATION**



RARE EARTH SALES  
2 North Riverside Plaza  
Chicago, Illinois 60606

## COMPONENTS

### Subminiature relay has 130-mW sensitivity

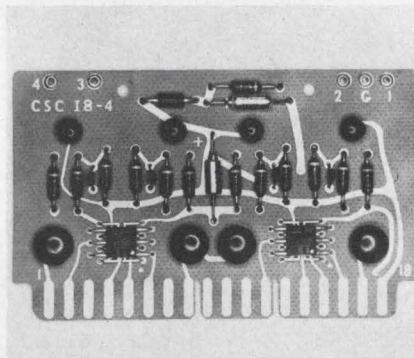


Bourns, Inc., 200 Columbia Ave.,  
Riverside, Calif. Phone: (714) 684-  
1700. P&A: \$21.30 (10 to 24);  
stock.

A dpdt 0.5-A relay, has 0.1-in. pin  
spacing, pick-up sensitivity of 130  
mW and an operating temperature  
range of  $-65^{\circ}$  to  $125^{\circ}$ C. Contact  
material of gold-plated semiprecious  
metal, highly resistant to arcing  
and film formation, provides an op-  
erating life of 150,000 cycles.

CIRCLE NO. 462

### Logic card drives 8 transmission lines

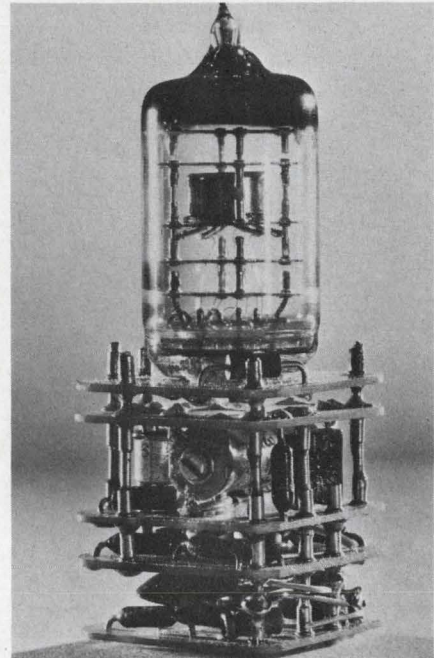


California Systems Components,  
Inc., 9176 Independence Ave., Chats-  
worth, Calif. Phone: (213) 341-  
1050. P&A: \$95; stock.

Four independent gated trans-  
mission line driver circuits are de-  
signed into this logic card. Each  
driver circuit is capable of driving  
up to two  $50\text{-}\Omega$  transmission lines  
in parallel. With a  $25\text{-}\Omega$  max load  
the circuit will have less than 10-ns  
rise and fall times and less than 20-  
ns stretch. The card features DTL  
integrated circuits and silicon dis-  
crete transistors.

CIRCLE NO. 463

### Miniature oscillator accurate to 1 part in $10^8$

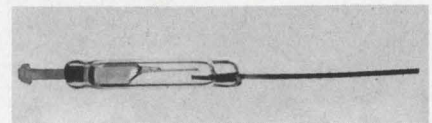


Marconi Co. Ltd., Chelmsford, Es-  
sex, England. Phone: Chelmsford  
53221.

A temperature stabilization tech-  
nique, employing a microelectronic  
circuit, is embodied in a new range  
of miniature master oscillators. The  
oscillators, which have a short term  
stability of 1 part in  $10^8$ , have ap-  
plications in airborne equipment  
and portable man-pack receivers  
employing the most advanced meth-  
ods of radio communication.

CIRCLE NO. 464

### Mercury-wetted reed bounce free

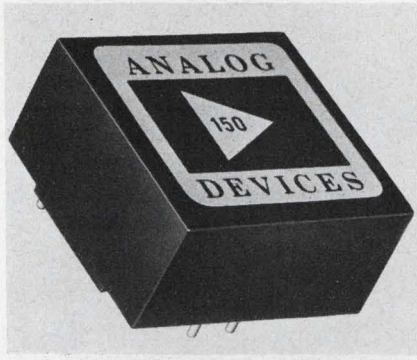


Gordos Corp., 250 Glenwood Ave.,  
Bloomfield, N. J. Phone: (201) 743-  
6800.

Mercury-wetted reed switches,  
available spst-NO, are bounce-free  
and stable in contact resistance and  
pull-in sensitivity. They are capable  
of switching loads of 1 A at 50-Vdc  
for  $50 \times 10^6$  operations. The switch  
has a glass diameter of 0.25 inch,  
glass length of 0.7 inch and over-all  
uncut length of 1.625 inches.

CIRCLE NO. 465

## Op-amp runs 1000 hours from two 3-V cells



Analog Devices, 221 Fifth St., Cambridge, Mass. Phone: (617) 491-1650. P&A: \$30; stock.

This differential dc operational amplifier gives 1000 hours service from a pair of Mallory #TR132R batteries. Besides conventional instrumentation uses, model 150 has applications in upgrading or retrofitting existing instruments and systems. It can operate (with battery pack) thousands of volts above ground, provide isolated measurement for high voltage cables, increase range, sensitivity and input impedance of d'Arsonval meters, turn dc meters into wideband ac instruments, raise input impedance of chart recorders and other apparatus, and operate remotely from solar-powered photovoltaic cells. Output is 1.5 V at 2.5 mA.

CIRCLE NO. 466

## Linear amplifiers from 20 to 80 MHz

Applied Research, Inc., 76 S. Bayles Ave., Port Washington, N. Y. Phone: (516) 767-8707. P&A: \$3500 and \$4500; 45 to 60 days.

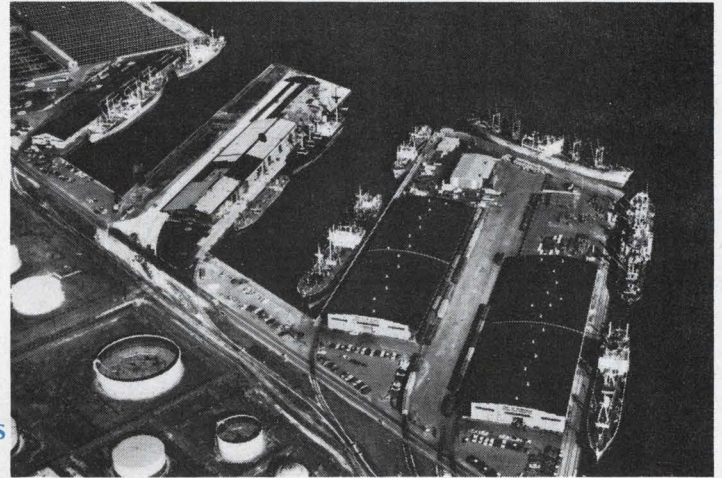
Two solid-state high power RF amplifiers have been developed featuring linear operation, low power drain and high power output. The units are useful in transmission systems, as spectrum analyzers, direction finders and signal sources.

CIRCLE NO. 467

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Did you know that some other city officials actually refer to us as "hustlers"?

We're delighted!

Because when they call us hustlers, they're enviously referring to our extremely well organized, highly developed transport system, unequaled by any other midwestern industrial city. With your plant here, your raw products move *in* fast, your finished products move *out* fast. And all this happens at lower shipping cost than you'd experience elsewhere.

Here's the run-down on our move-out: the best located deep-water world port on the Great Lakes with a natural harbor connecting three navigable rivers. This is fast access to the St. Lawrence Seaway to Europe and ideal for barge transport to the Gulf of Mexico. Rail transport? Five railroads converge on Milwaukee with reciprocal and main line switching in the city. Furthermore, Milwaukee has 62 truck lines in operation with a wide choice of terminal service. Five commercial airline carriers serve us at our rapidly expanding General Mitchell Field, private and corporate aviation is booming at Timmerman Field. Our \$400 million dollar expressway system is being rushed to completion so your product can rush to its destination.

Finally, Milwaukee is "shut-down-proof". No floods, hurricanes or tornadoes. And, an occasional snowstorm is always defeated by the finest equipped force in the nation within a few hours.

Rush a letter to us now! We'll "hustle" the answers you need.

Division of Economic Development  
Dept. ED-4 Office of the Mayor / Room 201, City Hall / Milwaukee, Wisconsin 53202

Gentlemen: Please send free copy of "there's MORE in Milwaukee". Inquiries handled in strict confidence.

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ADDRESS \_\_\_\_\_

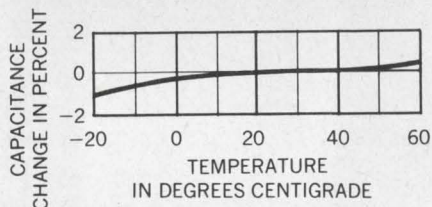
CITY \_\_\_\_\_ STATE \_\_\_\_\_ ZIP \_\_\_\_\_

MILWAUKEE... GREAT FOR BUSINESS, GREAT FOR LIVING, and growing greater

ON READER-SERVICE CARD CIRCLE 141

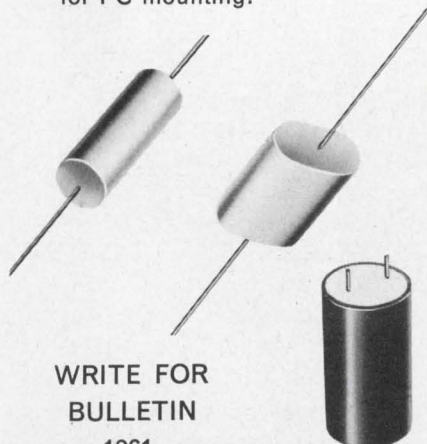


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**Modifilm**<sup>®</sup>  
**CAPACITORS**  
FOR GREATER  
STABILITY IN THE  
ROOM TEMPERATURE  
RANGE



Capacitance change of less than 2% over the temperature range of -20°C to +60°C, plus high insulation resistance ( $10^5$  megohm-microfarads at 25°C), makes this new Modifilm the ideal capacitor for many instrument applications such as integration, long time constant networks, RC circuits, etc.

They are available in many configurations including metal case hermetic sealed, plastic wrap with epoxy fill and in pre-molded phenolic cases for PC mounting.



WRITE FOR  
BULLETIN  
1261.

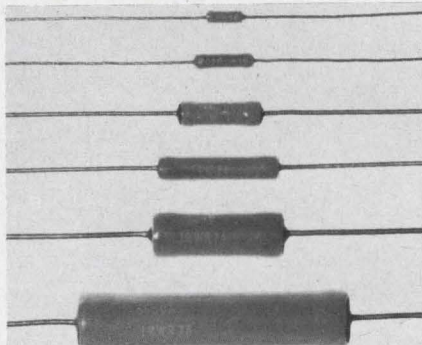
**INDUSTRIAL**  
CONDENSER CORPORATION

3243 No. California Ave.  
Chicago, Illinois 60618

ON READER-SERVICE CARD CIRCLE 142

COMPONENTS

Power resistors for MIL and commercial

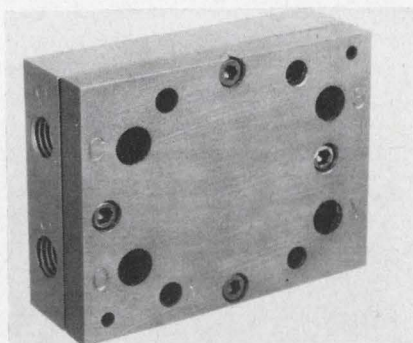


Shallcross Manufacturing Co., Preston Street, Selma, N. C. Phone: (919) 965-2341.

Two precision wirewound power resistors are offered for military and commercial applications. One series of power resistors is produced for established reliability programs requiring documentation and meets MIL-39007. Another series is offered as a general purpose power resistor for MIL-R-26 and commercial applications. Power ratings are 1 to 15 and 1 to 18 W.

CIRCLE NO. 468

Amplifier controls fluid pressures

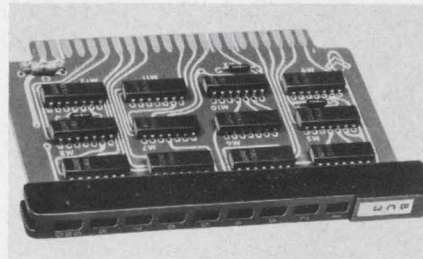


Fluidonics, Div. of Imperial-Eastman Corp., 6300 W. Howard St., Chicago. Phone: (312) 774-1700.

A pressure area amplifier for controlling high fluid pressures by using low pressure sources is offered for use with any filtered noncorrosive fluid, such as air, water, oil or natural gas. The amplifiers are available for use with corrosive fluids. The action of the amplifier is similar to that of a valve as the fluid flow can be proportionately controlled from full flow to shutoff.

CIRCLE NO. 469

12-stage counter card for time-base generators

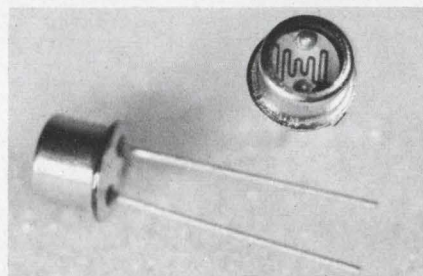


Control Logic, Inc., 3 Strathmore Rd., Natick, Mass. Phone: (617) 655-1170. P&A: \$105.25; stock.

Capable in binary or BCD code, a 12-stage counter card is particularly useful in time base generators and as frequency dividers. The 12 flip-flop stages may be used as a 4-bit to 12-bit binary or as a 1-to-3-digit BCD counter. Two or more cards may be used to construct counters of any length. The counters operate from dc to 1 MHz and have a maximum propagation delay per decade of 120 ns.

CIRCLE NO. 470

CdS photocells measure 1/4 inch across



Sylvania Electric Prod., Inc., Electronic Components Group, Emporium, Pa. Phone: (315) 568-5881.

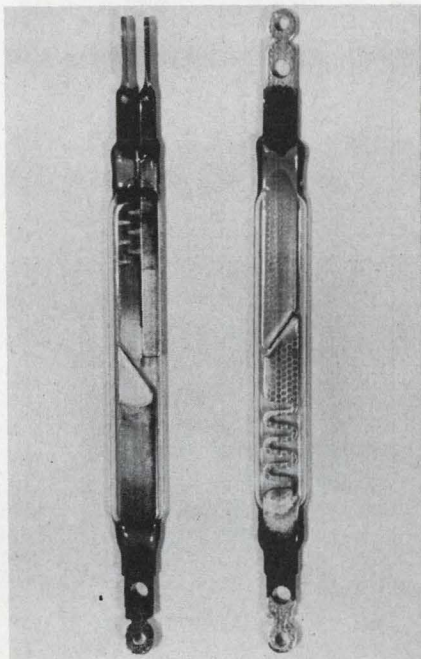
Hermetically sealed photocells, measuring less than 1/4 inch in diameter, are suited for use in high-density photoconductor arrays. The TO-18 photocells are rated for 50-mW power dissipation. They are available in light/resistance ratings ranging from 3000 to 125,000  $\Omega$  (at 2 footcandles), with a dark/light resistance ratio of 100 to 1.

CIRCLE NO. 471

Don't risk missing any issues of **ELECTRONIC DESIGN**. Send in your renewal card today.



**Flat-sealed contacts  
live to be 10 billion**



Tele-Norm Corp, 32-31 57th St., Woodside, N. Y. Phone: (212) 988-1935. P&A: \$5.50 to \$27 (1 to 9); stock.

Flat-sealed contacts (FSC) are less than half the size of usual reed switches but operate at higher speeds for at least 10 billion operations on dry circuit switching. Form A and Form C are the same size and the magnetic latching relay available with Form A needs no holding current. For switching systems and electronic circuitry, the FSC contacts come packaged in 1, 2, 4, 6, 10, 16 and 22-contact relays for panel mounting or for printed circuitry.

CIRCLE NO. 472

**IC logic cards in  
50 configurations**

Wyle Products Division, 133 Center St., El Segundo, Calif. Phone: (213) 322-1763.

A line of IC logic cards includes positive and negative logic, mercury reed relays, input and output level converters, gate expanders and many other functions. Included in the new series is a breadboard blank card with mounting space for eight dual in-line IC packs and discrete components.

CIRCLE NO. 473

**You can buy a sample now  
of this new General Electric  
solid state lamp!**



This is the SSL-1, actual size. It's a 2- to 5-volt solid state light source that emits 40 footlamberts of visible light end on @ 50 ma. Turns on and off at the rate of 10,000 cycles per second. Resists shock and vibration better than any filament lamp. Lasts indefinitely with no loss in efficiency!

SSL-1 is a remarkable new development of General Electric Miniature Lamp research. You'll want to consider it in your business, wherever tiny tough lamps are required. As an indicator or photo cell driver, it has hundreds of applications in computers, missiles, telephone equipment and aircraft, to name a few.

**ORDER SAMPLES TODAY**

Perhaps the SSL-1 can help save space, improve performance, reduce maintenance cost in *your* product. It's easy enough to find out: SSL-1 lamps are available now at just \$9.50 each. Order today. Just fill in the coupon and mail it with your check or money order. (Or contact your regular GE lamp representative.) Your calibrated SSL-1 will come to you cradled in styrofoam, protected in a rigid plastic box.

Need more data? Send for free technical bulletin #3-7041. It's yours for the asking.

Miniature Lamp Department



TO: General Electric Company  
Miniature Lamp Department  
P.O. Box 2422, Nela Park, Cleveland, Ohio 44112  
Attn: J. D. McMullen

Please send me \_\_\_\_\_ new GE SSL-1 lamp(s) at \$9.50 ea.

Total enclosed \$ \_\_\_\_\_

Name \_\_\_\_\_

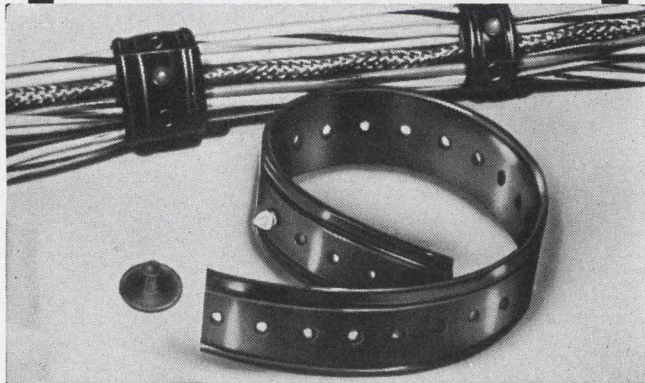
Company \_\_\_\_\_

Address \_\_\_\_\_

City \_\_\_\_\_ State \_\_\_\_\_ Zip \_\_\_\_\_

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## STRAPPING

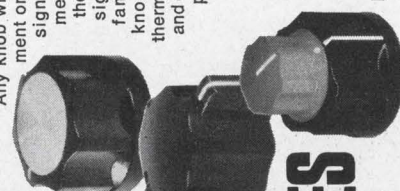
No tools—just 2 components: a nylon stud (like an old time collar button) and PVC strapping... lighter and stronger than metal...yet will not damage wires like lacing or metal clamps. It's the simplest, fastest and least expensive of any tying system that is reusable for "on-the-spot" wiring changes...just strap, snap, snip! And, "feed-out" reels make use and inventory control easy. Available in a variety of colors for identification and coding. Convince yourself. Write for free samples.

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ON READER-SERVICE CARD CIRCLE 144

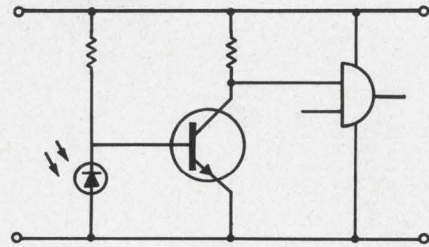
Any knob will turn the equipment on. Kurz-Kasch design-oriented instrument knobs turn on the engineer, the designer, the user. 21 families, 347 stock knobs in a variety of thermosetting materials and colors brighten the products of 3,000 OEM's. You can be 3,001. Write for free catalog and samples! Kurz-Kasch, Inc. Standard Parts Division  
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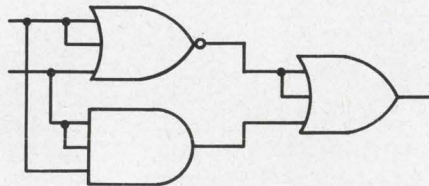
## Application Notes



### Photocell/IC applications

Integrated circuit applications for photocells are fully described in a 6-page brochure. Features are the advantages of silicon photocells, the degree of performance of photovoltaic devices, definitions of modes of operation, application considerations and charts illustrating uses of the cells such as the discrete transistor preamp shown above. Sensor Technology, Inc.

CIRCLE NO. 474



### DTL applications handbook

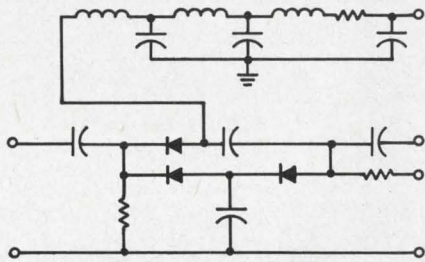
A new, 32-page Applications Handbook gives the system designer complete descriptions of Signetics DTL family. In addition to the text which presents circuit descriptions and characteristics, more than 100 illustrations present design information and detailed application examples, such as the digital comparator above, in the form of schematic and block diagrams. Signetics Corp.

CIRCLE NO. 475

### Reversible counter uses

"Using a Reversible Counter" is a 44-page book surveying some varied applications for reversible counters. There is a treatment of transducers for converting length, angle, flow rate, etc., to electrical signals suitable as inputs to the counter. Transducers covered include laser interferometers, optical gratings, tachometers and several types of flow meters. An extensive list of references completes the manual. Hewlett-Packard.

CIRCLE NO. 476



### Pin diode attenuators

Constant-impedance current-controlled attenuator design is detailed in an 8-page note. The attenuators span 10 MHz to 1 GHz using pin diodes. Design equations, curves and component selection are fully explored. hp Associates.

CIRCLE NO. 477

### Printed motors

The class of servos in which the printed motor has been applied is the intermittent motion, or incrementer system. In these applications, low inertial load is required to be started and stopped rapidly and repeatedly. This 13-page brochure describes the characteristics and applications of such motors. Printed Motors Div. of Photocircuits, Inc.

CIRCLE NO. 478

### SCR control circuits

A set of eight application notes details the design of SCR control circuits for varying devices. Controls for blowers, electric drills, electric fences, dc flashers and alarm circuits are included. Schematics and tables of values aid the discussions. ITT Standard.

CIRCLE NO. 479

### Regulated supply

Use of an IC op-amp as the sense and control element in a power supply regulator is the theme of a 4-page loose-leaf brochure. Text and schematics describe the external circuitry needed for regulated outputs of 20 to 28 Vdc from a 30-V unregulated source. Molecular Electronics Div., Westinghouse.

CIRCLE NO. 480

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The Short mesh p.d.a. 900N and 1300Q extend M-OV's range of C.R.T.s. Ideal for portable oscilloscopes employing solid-state circuitry, their compact rectangular design in no way affects their high performance.

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	1300Q	900N
Scan size	10cm × 6cm	7cm × 5cm
Line width	0.3mm	0.3mm
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Deflection Factor		
D <sub>y</sub>	4 V/cm max.	10 V/cm max.
D <sub>x</sub>	10 V/cm max.	11.5 V/cm max.
Overall length	335mm.	205 mm.

For full technical specification of 1300Q, 900N and the world's first dual-trace mesh PDA tube, the 1300P, write to:

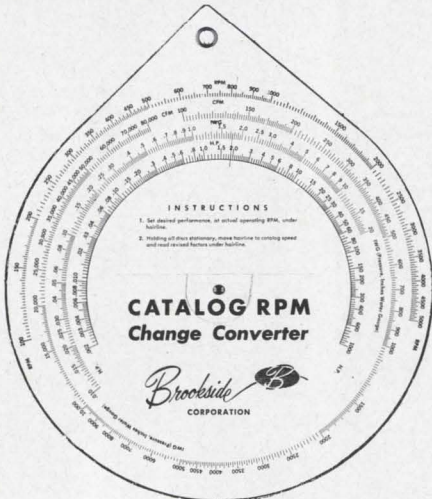
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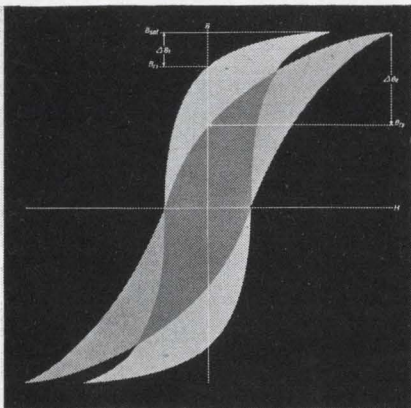
# Design Aids



## Cooling system design rule

Relate actual cooling system, performance with desired system characteristics using this circular slide rule. When the selected fan's catalog performance (including horsepower) and speed are placed under the hairline, actual system performance is determined by moving the hairline to the actual operating speed. Brookside Corp.

CIRCLE NO. 481



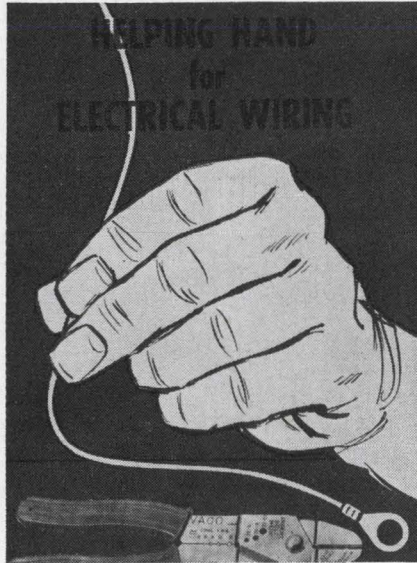
Pulse Engineering, Inc.

Miniature Pulse Transformers: Selection, Specification & Testing

## Miniature pulse transformers

A 12-page brochure completely details pulse transformer selection, specification and measurement. A pair of nomograms relates resistance, pulse length, droop and inductance; and inductance, voltage, pulse length and current. Applications information and methods of measurement are fully covered. Pulse Engineering, Inc.

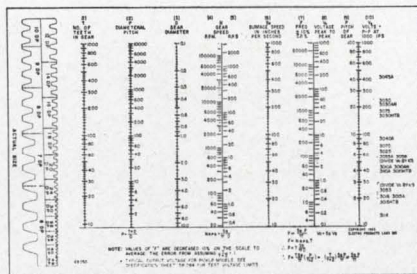
CIRCLE NO. 482



## Production line 'how to'

Two pocket-sized guidebooks, "How to Use Screwdriver" and "Helping Hand for Electrical Wiring," present "how to" facts, illustrations and pointers. "Helping Hand" details techniques in electrical connections and splices. It covers a discussion of basic electricity complete with diagrams to illustrate wiring methods, tools and accessories. Sections show assembly line applications in control panels, transformers, relays and motors. The booklet includes wire size and decimal equivalent charts, an "automatic" terminal selector and a glossary. Vaco Products Co.

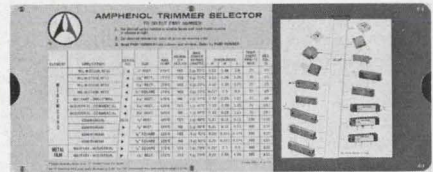
CIRCLE NO. 483



## Magnetic pickup handbook

Magnetic pickups are completely defined in a handy 6-page fold-out booklet. A set of charts and the nomogram shown above aid in calculations. The nomogram relates the number of gear teeth, diametral pitch, gear diameter, gear speed, surface speed, frequency, peak-to-peak voltage, gear pitch and peak-to-peak voltage at 1000 inches per second. Electro Products Laboratories, Inc.

CIRCLE NO. 484



## Trimmer selector

Amphenol Controls' entire line of wirewound and metal film trimmers is presented in slide rule form for easy selection. The desired series number, by application and size, is set in one window and the model number is read opposite a photo of the trimmer at the right. By turning the rule over and setting the desired resistance value, part number and per cent resolution are given. Ordering may then be done by noting Amphenol prices and comparing them with those of Bourns, Dale, Spectrol, IRC, Daystrom and Helipot which are given in a handy table. Amphenol Controls Div.

CIRCLE NO. 485

## DECIMAL EQUIVALENT CHART

1/32	0.015625	17/32	0.53125
1/16	0.03125	9/16	0.5625
3/32	0.046875	19/32	0.59375
1/8	0.0625	5/8	0.625
5/32	0.078125	11/16	0.6875
3/16	0.09375	7/8	0.875
1/4	0.109375	1/2	0.5
9/64	0.125	13/16	0.8125
5/32	0.140625	23/32	0.71875
11/32	0.15625	3/4	0.75
7/16	0.171875	25/32	0.78125
13/16	0.1875	27/32	0.84375
3/8	0.203125	11/8	1.375
19/32	0.21875	13/8	1.625
5/8	0.234375	7/4	1.75
17/16	0.25	9/4	2.25
9/8	0.265625	5/2	2.5
19/16	0.28125	3	3.0
23/16	0.296875	4	4.0
5/4	0.3125	5	5.0
11/4	0.328125	6	6.0
3/2	0.34375	7	7.0
7/2	0.359375	8	8.0
13/2	0.375	9	9.0
15/2	0.390625	10	10.0
17/2	0.40625	11	11.0
19/2	0.421875	12	12.0
21/2	0.4375	13	13.0
23/2	0.453125	14	14.0
25/2	0.46875	15	15.0
27/2	0.484375	16	16.0
29/2	0.5	17	17.0
31/2		18	18.0
33/2		19	19.0
35/2		20	20.0
37/2		21	21.0
39/2		22	22.0
41/2		23	23.0
43/2		24	24.0
45/2		25	25.0
47/2		26	26.0
49/2		27	27.0
51/2		28	28.0
53/2		29	29.0
55/2		30	30.0
57/2		31	31.0
59/2		32	32.0
61/2		33	33.0
63/2		34	34.0
65/2		35	35.0
67/2		36	36.0
69/2		37	37.0
71/2		38	38.0
73/2		39	39.0
75/2		40	40.0
77/2		41	41.0
79/2		42	42.0
81/2		43	43.0
83/2		44	44.0
85/2		45	45.0
87/2		46	46.0
89/2		47	47.0
91/2		48	48.0
93/2		49	49.0
95/2		50	50.0

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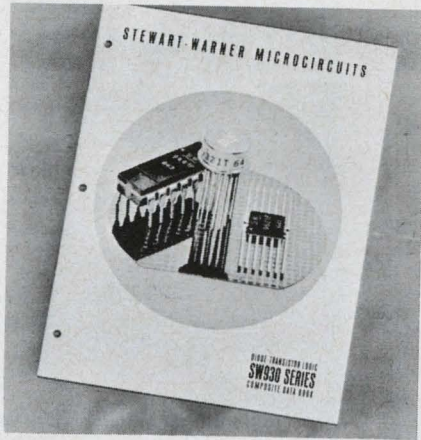
## Decimal equivalent wall chart

This 16 x 10-1/2-in. wall chart converts frequently used fractions to decimals at a glance. Decimals are carried to 6 places for accuracy. Accompanying the wall chart is the latest Product Data Bulletin from the manufacturer covering electrical insulation products. Inmanco, Inc.

CIRCLE NO. 486

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## New Literature



### DTL data book

A 20-page data book details the DTL930 series of compatible monolithic integrated logic circuits. Circuits are shown for all data presented, specifically defining how data was derived, and circuits, logic and pin layouts, diagrams and package dimensions are presented along with details of product reliability programs. A glossary of terms defines parameters used. Descriptions are given of test techniques. Stewart-Warner Corp.

CIRCLE NO. 487

### Switch uses unlimited

"Uses Unlimited" describes a dozen switch applications in solving industrial problems. One of the illustrated features describes an application in which inspection is accomplished on an eight-dimension steel stamping. Another feature deals with minimizing the effects of radio frequency interference. Other switch applications describe flow-actuated proximity, explosion-proof and mercury switches in unusual installations. Micro Switch, Div. of Honeywell.

CIRCLE NO. 488

### 360-page products catalog

A 360-page volume features product listings from 113 manufacturers, with pricing up-to-date. An accurate index provides specific assistance in finding the desired product. Complete line catalogs from 21 manufacturers are available.

Available on company letterhead from Esco Electronics, 3130 Valleywood Drive, Dayton, Ohio.

# RCL power wire wound resistors

- Standard Temperature Coefficient  $\pm 10$  PPM
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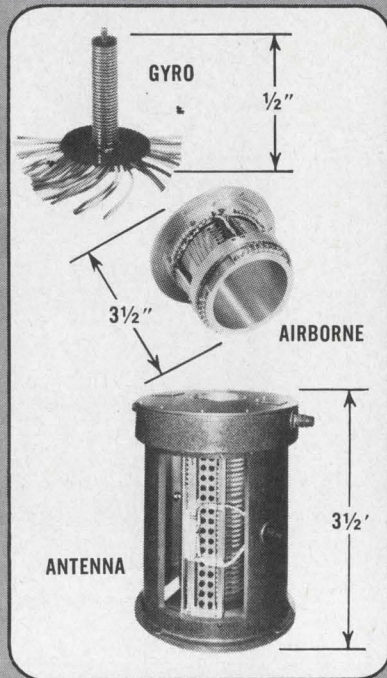
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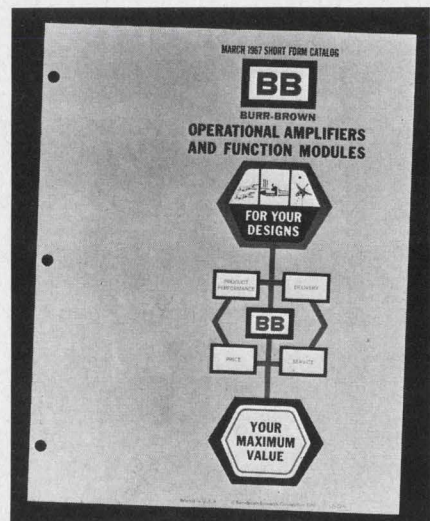
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## NEW LITERATURE



### Op-amp and function modules

This 16-page illustrated catalog describes analog and hybrid plug-in modules along with twenty-two op-amps, a line of instrumentation amps, seven function modules, a line of active filters and eleven power supplies. It includes 50 op-amps which are available in various package styles. The instrumentation amp line includes transducer amps, preamps, and galvanometer amps. The epoxy-encapsulated line of function modules includes squaring modules, a quarter-square multiplier, a noise generator, logarithmic amps, an analog comparator and electronic switch modules. Burr-Brown Research Corp.

CIRCLE NO. 489

### 82-page instruments catalog

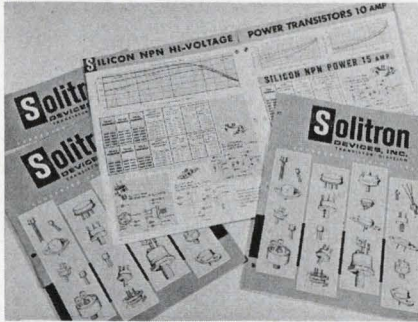
An 82-page catalog entitled "Modular Instruments" is available. It contains specifications on modular nuclear instruments. Also included is a guide to assist the user in selecting the proper combination of modules for a specific application. A separate section describing input and output accessories which are used to complete the modular system is contained. Nuclear-Chicago Corp.

CIRCLE NO. 490

### CO<sub>2</sub> laser applications

"On the significance and use of CO<sub>2</sub> lasers" is an 8-page report covering theory and applications. A complete rundown on lab experiments is included. Seed Electronics Corp.

CIRCLE NO. 491



### Power transistor selection

A 28-page book covers silicon and germanium transistors for military, industrial and commercial applications. Each family of transistors is presented in a separate section and includes typical  $h_{FE}$ ,  $V_{BE}$  and  $V_{CE}$  curves, along with specification charts and outline dimension drawings. Suggested applications are included. Solitron Devices.

CIRCLE NO. 492

### Wire marking brochure

A 12-page brochure describes a line of wire/cable harnessing, marking and accessory products. Included in the booklet are three types of harnesses, adjustable P-clips, three types of markers and grommet strip. Illustrations with dimensional drawings and tables providing physical properties, chemical properties, applications, ordering data and specifications are included. Electrovert, Inc.

CIRCLE NO. 493

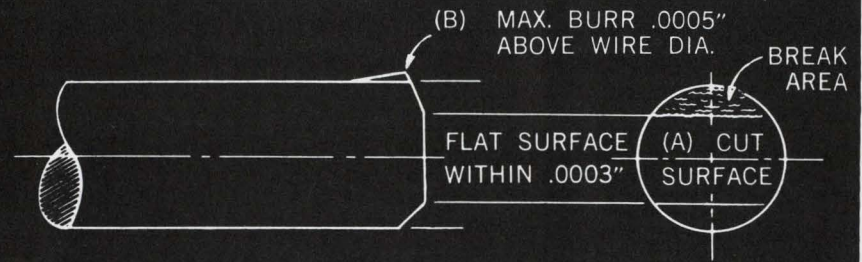
### Coaxial switches

A 12-page technical discussion completely covers coaxial switches. Included are principles of operation, descriptions of basic design types and relative merits, contact arrangements and switching actions, operational differences, definitions of terms and performance characteristics, drive methods, trade-off characteristics and a guide to specification. The discussion includes a comparison of the merits of electromechanical switches vs solid-state switches. Sage Labs.

CIRCLE NO. 494

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## How far can you go when you specify square cut leads?



Straightening and cutting wire isn't as simple as it looks. Especially when you need a surface on which to weld or solder. Here's what we've developed on a typical .018 diameter lead.

- Cut Surface — 80% minimum cut (See "A" above)
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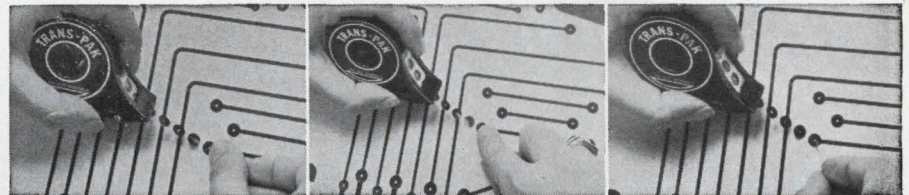
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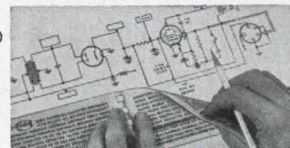


Chart-Pak Inc. A subsidiary of Avery Products Corp. 344 River Rd., Leeds, Mass. 01053

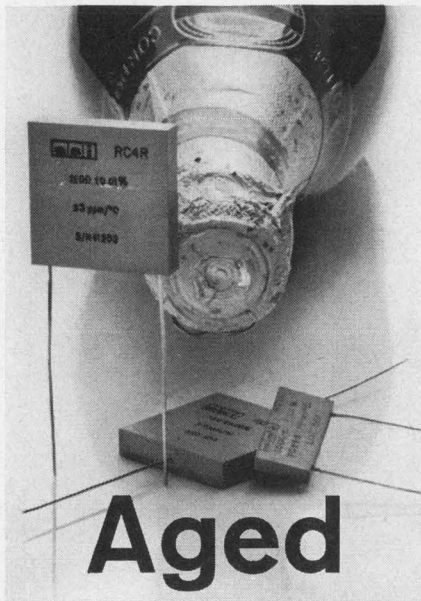


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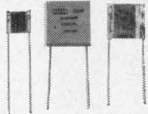


**Aged**

Our precision resistors are aged to improve reliability, and we guard the process like a vintage champagne maker. Ageing is just one of many extra steps that make our precision components the most reliable you can specify. A few of our components are described briefly below.

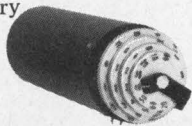
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### 2. Dekastat® Decade Resistors

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### 3. Dekapot® Resistive Voltage Dividers

These rapid-setting potentiometers have a terminal linearity up to 0.002%. Kelvin-Varley circuitry provides constant input impedance.



### 4. Dekatran Transformer Voltage Divider

The patented coaxial dial is easy to read and adjust. Accuracy of 0.001% and long-term stability are achieved through gapless toroidal cores of very high permeability.



**esi**

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Union Carbide Electronics, Mountain View, California has just placed the largest exclusive advertising campaign in magazine publishing history.

Their objective: To become an even greater factor in the fast-paced twenty-one billion dollar electronics industry.

Their campaign: 138 pages over the next 12 months.

Their magazine: **Electronic Design.**

Union Carbide Electronics and their agency, Hal Lawrence, Inc., decided the best return on their advertising investment would be achieved by concentrating in the magazine read by the greatest number of their prime customers and prospects.

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138 pages over the next 12 months . . . that's **impact.**



## Electronic Design

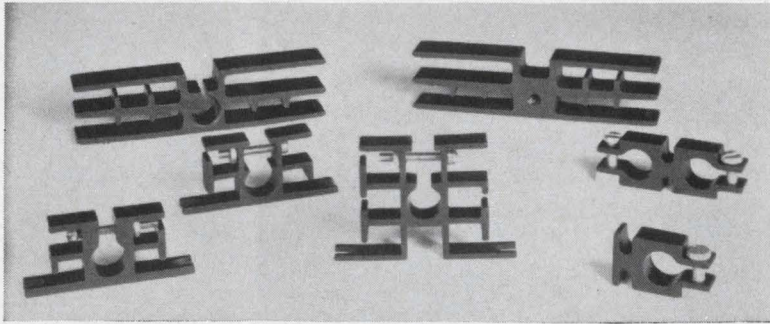
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The black-anodized aluminum units are available from stock. Technical data and price information will be sent on request.



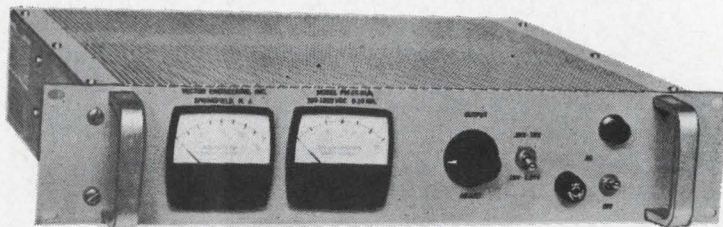
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ON READER-SERVICE CARD CIRCLE 153

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Operate PHOTOMULTIPLIER and MICROWAVE tubes  
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provides a highly regulated stable source of D.C. Power. Either output terminal may be grounded thus providing a plus or minus output voltage.

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Guaranteed to operate continuously in an ambient temperature of 0 to 50°C. A pair of 2% accuracy (full scale) meters are mounted on the front panel to monitor both voltage and output current.

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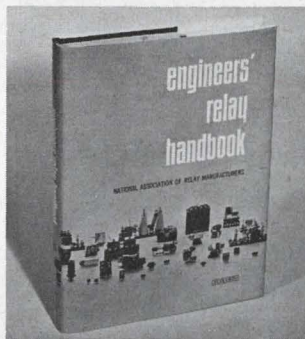
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# 178

## Engineers' Relay Handbook



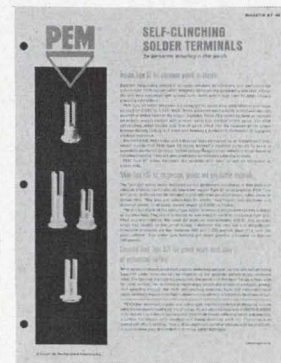
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# 179

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Bulletin ST-166 describes a complete line of PEM self-clinching solder terminals for permanent mounting on thin panels. Information discloses data on PEM spline and concealed head types as well as the regular type ST. These solder terminals provide permanent electrical connections, resistant to vibrations and environmental disturbances and are electroplated with tin and stearic acid wax for ease of soldering and resistance to oxide development during storage. Bulletin ST-166 includes dimensions, installation suggestions and design limitations.

### Penn Engineering & Manufacturing Corp.

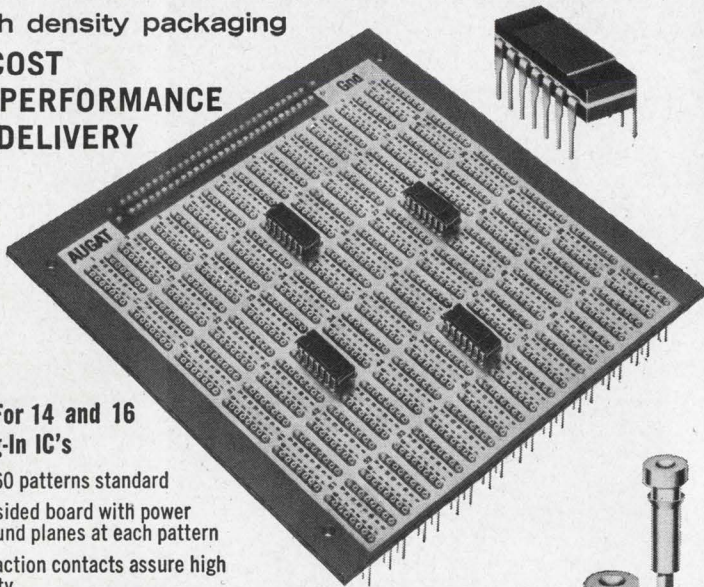
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# 180

# IC PACKAGING PANELS

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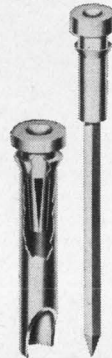
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# Designer's Datebook

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JUNE						
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11	12	13	14	15	16	17
18	19	20	21	22	23	24
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## May 1-3

**Commercial Utilization of Space Meeting** (Dallas) Sponsor: American Astronautical Society; P. O. Box 1415, Grand Prairie, Tex. 75050.

CIRCLE NO. 495

## May 3-5

**Electronic Components Technical Conference** (Washington, D.C.) Sponsors: IEEE, EIA; W. S. Hepner, Jr., Electronic Ind. Assoc., 2001 Eye St., Wash., D. C. 20006.

CIRCLE NO. 496

## May 4-5

**American Society of Naval Engineers Meeting** (Washington, D.C.) Sponsor: ASNE; Miss R. Leonard, ASNE, Suite 507, 1012 14 St., N.W., Washington, D. C. 20005.

CIRCLE NO. 497

## May 9-11

**Frontiers of Energy Conversion—IEEE Region 6 Conference** (Albuquerque, N. M.) Sponsor: Region 6 IEEE; B. D. Trembly, Barnhill Assoc., Albuquerque, N. M. 87101.

CIRCLE NO. 498

## May 16-18

**National Telemetry Conference** (San Francisco) Sponsors: IEEE, AIAA, ISA; Lewis Winner, 152 W. 42 St., New York, N. Y. 10036.

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## May 18-19

**Midwest Symposium on Circuit Theory** (Lafayette, Ind.) Sponsors: IEEE, Purdue University; G. F. Lee, Purdue University, Lafayette, Ind. 47907.

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# new disciplines in DC



## take the NEWEST CONCEPT in Bench DC Power Supplies

Advanced fabrication techniques result in higher quality at lower cost

### Two Compact Models Available

0-25V @ 0-400 MA ... 0-50V @ 0-200 MA • 0.01% Regulation

Two extremely compact, well-regulated DC power supplies designed especially for bench use have just been added to the hp power supply line. New fabrication techniques have been employed for these supplies to minimize manufacturing costs while retaining component and circuit quality. Reliable, yet low cost, these "hand-size" battery substitutes have over-all performance features ideal for circuit development, component evaluation, and other laboratory applications.

The all-silicon circuit uses an input differential amplifier to compare the output voltage with a reference voltage derived from a temperature-compensated zener diode. These stable input and reference circuits are combined with a high gain feedback amplifier to achieve low noise, drift-free performance. Output voltage is fully adjustable **down to zero**. Special design precautions prevent output overshoot during turn-on or turn-off, or when AC power is suddenly removed.

The front panel meter can be switched to monitor output voltage or current. Constant Voltage/Current Limiting insures short-circuit-proof operation, and permits series and parallel connection of two or more supplies when greater voltage or current is desired.

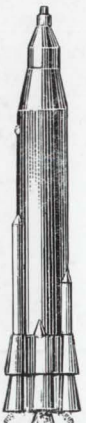
The molded, impact-resistant case includes an interlocking feature for stacking several units vertically, thus minimizing bench space required for multiple supplies. Alternatively, up to three units can be mounted side by side on a standard 3½" H x 19" W rack panel.

DC Output:	Model 6215A, 0-25V at 0-400 MA Model 6217A, 0-50V at 0-200 MA
Either positive or negative output terminal may be grounded, or the supply may be operated "floating" up to 300V off ground.	
AC Input:	105-125 VAC*, 50-400 Hz
Load Regulation:	0.01% + 1 MV
Line Regulation:	0.01% + 4 MV
Ripple & Noise:	<200 $\mu$ V RMS
Temperature Coefficient:	<0.02% + 1 MV/° C
Stability for Eight Hours After 30 Minutes Warm-up:	<0.1% + 5 MV
Transient Recovery Time:	<50 $\mu$ s for output recovery to within 10 MV following a full load change
Output Impedance:	<0.03 ohms from DC to 1 KHz <.5 ohms from 1 KHz to 100 KHz <3 ohms from 100 KHz to 1 MHz
Maximum Ambient Operating Temperature:	+ 55°C
Size:	3¼" (8.26 cm) H x 5¼" (13.34 cm) W x 7" (17.78 cm) D
Weight:	5¼ lbs (2,38 kilograms)
Price—Model 6215A:	\$90.00
Model 6217A:	\$90.00

\*210-250 VAC input also available

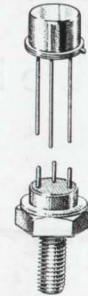
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# From RCA "overlay" first high-reliability RF-power transistors available off-the-shelf

RATINGS FOR RF SERVICE				
	40305	40306	40307	Units
V <sub>CB0</sub> (max)	65	65	65	Volts
V <sub>CEV</sub> (max)	65	65	65	Volts
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I <sub>C</sub> (max)	1.0	1.5	3.0	Amperes
P <sub>OUT</sub> (min)	2.5W @ 175 MHz	7.5W @ 100 MHz	13.5W @ 175 MHz	



RCA, originator of the revolutionary "overlay" technique, introduces another new concept in rf-power transistors... high-reliability units *available off-the-shelf*. Designed primarily for critical aerospace and military high-frequency applications, RCA 40305, 40306, and 40307 transistors go beyond the high standard of reliability established by RCA "overlay" to assure a new level of confidence... confidence for those designs where device failure cannot be tolerated.

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Electrically similar to RCA types 2N3553, 2N3375, and 2N3632, these hi-rel devices are designed to

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- Fine Leak, 1 x 10<sup>-8</sup> cc/sec/max.
- Gross Leak, 70 psig, 16 hours min.
- Acceleration Test (2006 of MIL-STD-750, 10,000 G, Y<sub>1</sub> axis)
- Temperature Cycling (MIL-STD-202)
- Power Age (168 hours)
- X-ray Inspection, RCA Spec 1750326

For more information on RCA's "overlay" high-reliability capability, consult your RCA Representative. For technical data on 40305, 40306, and 40307, write: RCA Commercial Engineering, Section 1G4-4, Harrison, N.J. 07029.

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