

## DATA ACOUISITION IC HANDBOOK



ATELEDYNE SEMICONDUCTOR

## 『゚TELEDYNE SEMICONDUCTOR



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# 1986 Data and Design Manual 

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Ordering Information Package Information

The Device Identification Codes for Device Numbers of TSC8700, TSC9400 and TSC14433 Family are as Follows:


J - Plastic Package
N - Ceramic Package
L - CerDIP
Y - Dice
E - Metal Can (TO-99)
M - Metal Can (TO-18)
EXAMPLE: TSC8701CL Operates Over the Commercial Temperature Range and is a CerDIP Package

## PRODUCT STATUS

Three Classes of Data Sheets are Shown in this Data Book. These are Identified by the Presence or Absence of a "Banner" on the First Page.

| DATA SHEET INDENTIFICATION | PRODUCT STATUS | COMMENTS |
| :--- | :--- | :--- |
| No Identification | Production | Delivery Subject to Product Demand. |
| Preliminary | Initial Production | Data Sheet Electrical Limits <br> Established. Limited Production <br> Quantities Available. Samples <br> Available. |
| Advance Product | In Design | Data Sheet Gives Design Goal, <br> Information |
| Electrical Specifications and Major <br> Product Features. Contact Teledyne <br> Marketing for Samples and Information. |  |  |

Note: Teledyne Semiconductor Reserves the Right to Make Changes at Any Time Without Notice in Order to Improve Performance and Supply.

## Ordering Information

The Device Identification Codes for All Other CMOS Products and All Products in 60 -Pin Flat Packages are as Follows:

## PACKAGED DEVICES

1. TELEDYNE SEMICONDUCTOR DEVICE
2. DEVICE NUMBER
3. ELECTRICAL PERFORMANCE GRADE OPTION (if applicable)

R - Reversed Pin Layout
4. OPERATING TEMPERATURE RANGE

M - Military Temperature Range ( $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ )
I* - Industrial Temperature Range ( $-25^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ )
C - Commercial Temperature Range ( $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ )

*     - May $\mathrm{Be}-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$. Refer to Specific Device Specification

5. PACKAGE TYPE

J - CerDIP Dual-In-Line (non side brazed) O - Plastic "SO' Surface Mount
P - Plastic Dual-In-Line
L - Plastic Leaded Chip Carrier (PLCC)
T - TO-99 Type (round metal can)
B - Plastic Flat Package (formed leads)
S - Plastic Flat Package (unformed (straight) leads)
6. NUMBER OF PACKAGE PINS
A-8
N-18
$Y-8$ (pin 4 connected to case)
D - 14
G-24
Q-60
E-16
I-28
W-44
F-22
L-40
S - 68
7. PROCESSING OPTION

883 - MIL-STD-883B, Class B Processing *
BI $-\mathbf{1 0 0 \%}$ Burn-In at $125^{\circ} \mathrm{C}$ for 160 Hours


EXAMPLE: 303AL Operates Over an Industrial Temperature Range at 15 V and is a CerDIP Package

## Product List - Digital Logic

| 301 | Power NAND Gates Dual 5-Input | 349 | Dual Retriggerable Pulse Stretcher |
| :--- | :--- | :--- | :--- |
| 302 | Power NAND Gates | Quad 2-Input | 350 |
| Multiplexers | -Bit |  |  |
| 303 | Power NAND Gates Quad 2-Input | 351 | Multiplexers Dual 4-Bit |
| 304 | Power NAND Gates Triple 4, 3, 4-Input | 355 | Timer |
| 306 | NOR Gate Quad 2, 2, 3, 3-Input | 361 | Dual 11-16V to 5V Interface Voltage Translator |
| 307 | NOR Gate Quad 2, 2, 3, 3-Input | 362 | $5 V$ to 11-16V Interface Dual Translator |
| 311 | Flip Flops Master/Slave RST | 363 | $5 V$ to 11-16V Interface Quad 2-Input NAND |
| 312 | Flip Flops Dual J-K Edge Triggered | 367 | Schmitt Trigger Quad(Active Pullup) |
| 313 | Flip Flops Dual J-K Master/Slave | 368 | Schmitt Trigger Quad(Open Collector) |
| 321 | NAND Gates Quad 2-Input | 370 | Flip Flop Quad D |
| 322 | NAND Gates Dual 5-Input | 371 | Counters Decade |
| 323 | NAND Gates Quad 2-Input | 372 | Counters Hexadecimal |
| 324 | NAND Gates Quad 2-Input | 373 | Up-Down Counters Decade |
| 325 | NAND Gates 2, 2, 3, 3-Input | 374 | Up-Down Counters Hexadecimal |
| 326 | NAND Gates 2, 2, 3, 3-Input | 375 | Shift Register 4-Bit |
| 331 | Gate Expander Dual 5-Input | 380 | BCD-to-Decade Decoder/Drivers Lamp Driver |
| 332 | Hex Inverter Gates 4-Inverter, 2-NAND | 381 | BCD-to-Decade Decoder/Drivers Logic Driver |
| 333 | Hex Inverter Gates 4-Inverter, 2-NAND | 382 | BCD-to-Decade Decoder/Drivers Gas Tube Driver |
| 334 | Hex Inverter Gates Strobed Hex NAND | 383 | Decoder/Driver BCD-to-7 Segment |
| 335 | Hex Inverter Gates Strobed Hex NAND | 390 | Dual Interface Buffers 4-Input Expandable AND |
| 341 | Multifunction Gates Dual 2-Wide, 2-Input | 391 | Dual Interface Buffers 2-Input AND |
| and/or Invert |  | 392 | Dual Interface Buffers 2-Input NAND |
| 342 | Dual Monostable Multivibrator | 393 | Dual Interface Buffers 2-Input OR |
| 343 | Digital Comparator 4-Bit | 394 | Dual Interface Buffers 2-Input NOR |
| 344 | Multifunction Gates Dual Expandable AND-NOR | 395 | Dual Interface Buffers 4-Input Expandable NAND |
| 347 | Dual Retriggerable Monostable Multivibrator | 396 | Line Driver/Receiver Dual Differential |

Dual Retriggerable Pulse Stretcher
Multiplexers 8-Bit
Multiplexers Dual 4-Bit
Dual 11-16V to 5 V Interface Voltage Translator
5 V to 11-16V interface Dual Translator
Schmitt Trigger Quad(Active Pullup)
Schmitt Trigger Quad(Open Collector)
lip Flop Quad D
Counters Hexadecimal
Up-Down Counters Decade
Up-Down Counters Hexadecimal
Shift Register 4-Bit
(Package \#1)
TO-18 (2-Pin)

(Package \#3) TO-99 (8-Pin)
(Package \#2)
TO-92 (2-Pin)

(Package \#4)
8-PIn Plastic DIP

(Package \#5)
8-Pin CerDIP

(Package \#6) 14-Pin Plastic DIP
(Package \#7) 14-Pin CerDIP

(Package \#8)
16-Pin Plastic DIP
(Package \#9)
16-Pin CerDIP


> (Package \#10)

18-Pin Plastic DIP

(Package \#11) 18-Pin Ceramic DIP
(Package \#12)
24-Pin Plastic DIP
(Package \#13) 24-Pin Ceramic DIP

(Package \#14)
24-Pin CerDIP

(Package \#15) 28-Pin Plastic DIP

(Package \#16)
28-Pin Ceramic DIP
(Package \#17)
40-Pin Plastic DIP
(Package \#18)
40-Pin Ceramic DIP

(Package \#19) 28-Pin CerDIP

(Package \#21)
60-Pin Flat Package
Formed Leads
(Package \#20)
40-Pin CerDIP

(Package \#22) 60-Pin Flat Package Unformed Leads



## (Package \#24) <br> TO-92 (3-Pin)

(Package \#25)
8-Pin Plastic "SO"

bottom view

(Package \#26)
14-Pin Plastic "SO"


Package \#27)
68-Pin Plastic Chip Carrier (PLCC)

(Package \#28)
44-Pin Plastic Chip Carrier (PLCC)
(Package \#29)
28-PIn Plastic Chip Carrier (PLCC)


BOTTOM VIEW 0.137 TYP $\longrightarrow$

0.125 DIA $\times 0.005$ DEEP 4 PLCS (EJECTOR PIN)




Quality Assurance Program

# Teledyne Semiconductor Product Assurance Program 

Teledyne Semiconductor's Product Assurance Program is based on four major blocks:

- Quality Control
- Quality Assurance
- Reliability
- Quality Circles


## Quality Control

The Quality Control function handles continuous monitoring of production, from incoming inspection of raw materials to wafer and assembly processing. This includes surveillance of documentation, calibration, and environmental processing.
The three major areas of Quality Control are:

- Incoming Inspection
- In-Process Control
- Operation Surveillance
- Vendor Qualification


## Quality Assurance

After devices are subjected to $100 \%$ testing in manufacturing, they are formed into lots and submitted to Quality Assurance acceptance testing. Three types of tests are performed on samples: Visual/Mechanical, Parametric, and Functional. The sampling is based on a plan equivalent to a . 07 AQL with a $.5 \%$ AOQL. (All TSC sample plans are in accordance with MIL-M-38510 appendix B or MIL-HDB 105D.) Testing is done at room and elevated temperature. Lower temperature testing is performed when required by the specification, or when a potential problem is known to exist.

The Quality function at TSC is directed at providing a continually improving product that meets or exceeds the customer expectations. This stated goal is being achieved at Teledyne, which is evident in Figure 1 and Figure 2. These show constant improvement both in outgoing percent defective and customer return rate.

## Reliability

The Reliability Group is responsible for the following functions:

- New Process Qualification
- Process Change Qualification
- Process Monitoring
- New Device Qualification
- Device Change Qualification
- Device Monitoring
- New Package Qualification
- Package Change Qualification
- Package Monitoring
- Failure Analysis


## Quality Control Circles

Quality Control Circles are a vital part of the quality loop at Teledyne Semiconductor. The concept allows each employee directly involved in manufacturing to have a voice in how to build a quality product. Volunteers within a group meet weekly to determine and solve problems. Some solutions to problems may be implemented on the job. Others require management support, and to this end, circle members are trained in management presentation. The goal is total employee involvement with an emphasis on building-in quality.

## Product Assurance Program

Figure 1



## Product Assurance Program



## Quality Conformance

A part of the TSC Quality/Reliability program is to assure that all product lines offered meet industry accepted standards. This is done by a periodic submission of product to a conformance test program to collect generic data.

All tests are done in accordance with MIL-STD 883C where applicable. (See pages $3-7 / 3-8$ ) Test listings and results from submissions for a plastic encapsulated device and a CerDIP hermetic sealed device are presented in Table 1 and Table 2.

| Table 1 |  |  |  | Plastic |
| :---: | :---: | :---: | :---: | :---: |
| Test $\quad$ Mil-Std/Test Condition | Sample Size | Qty In Qty Out |  |  |


| Physical Dimension | 883/2010 | $S / S=45$ | 45 | 45 |
| :---: | :---: | :---: | :---: | :---: |
| Salt Atmosphere | 883/1009/A | $S / S=45$ | 45 | 45 |
| Solderability | 883/2003 | $S / S=45$ | 45 | 45 |
| Pressure Cooker | 96 hrs . | $S / S=45$ | 45 | 45 |
| 85/85 ${ }^{\circ} \mathrm{C}$ R H (Bias) | 1.0K hrs. | $S / S=$ | $\mathrm{n} / \mathrm{a}$ | $\mathrm{n} / \mathrm{a}$ |
| SSL | $\mathrm{TA}=125^{\circ} \mathrm{Ct}=1,000 \mathrm{hrs}$. | $S / S=45$ | 45 | 45 |
| Storage | $\mathrm{TS}=150^{\circ} \mathrm{Ct}=1,000 \mathrm{hrs}$. | $S / S=45$ | 45 | 45 |
| Thermal Shock | $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C} 200$ cycle | $S / S=45$ | 45 | 45 |
| Temperature Cycle | $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C} 1000$ cycle | $S / S=45$ | 45 | 45 |
| Group B Test | Table 2 <br> Mil-Std | DIP | y |  |


| SUBGROUP 1 <br> Physical Dimensions | 883/2016 | 2 devices (no failures) | n/a | $\mathrm{n} / \mathrm{a}$ |
| :---: | :---: | :---: | :---: | :---: |
| SUBGROUP 2 |  |  |  |  |
| Resistance to Solvents | 883/2015 | 4 devices (no failures) | 4 | 4 |
| SUBGROUP 3 |  |  |  |  |
| Solderability | 883/2003 | LTPD $=15$ <br> 3 devices min. | 3 | 3 |
| SUBGROUP 4 |  |  |  |  |
| Internal Visual And Mechanical | 883/2014 | 1 device (no failure) | 1 | 1 |
| SUBGROUP 5 |  |  |  |  |
| Bond Strength | 883/2011/D | LTPD = 4 devices | 15 | 15 |
| SUBGROUP 6 |  |  |  |  |
| Internal Water Vapor | 883/1018 | ```3 devices (no failures) 5,000 PPM, 10,000 PPM``` | $n / a$ | $\mathrm{n} / \mathrm{a}$ |

## SUBGROUP 7

Seal
Fine leak
Gross leak 883/1014/C
LTPD $=2$
116
116

## SUBGROUP 8

NA

## Conformance Flow

Generic Data ls generated on a periodic basis for the following test.

| MIL-STD-883C Quality Conformance Tests | Method | Test Condition | LTPD |
| :---: | :---: | :---: | :---: |
| GROUP B |  |  |  |
| SUBGROUP 1 Physical Dimensions | 2016 |  | 2 Devices |
| SUBGROUP 2 |  |  |  |
| SUBGROUP 3 <br> Solderability | 2022 or 2003 |  | 15 |
| SUBGROUP 4 <br> Internal Visual: Mechanical | 2014 |  | 1 Device |
| SUBGROUP 5 Bond Strength | 2011 | Test Condition C or D | 15 |
| SUBGROUP 6 NA |  |  |  |
| $\begin{aligned} & \text { SUBGROUP } 7 \\ & \text { Seal } \\ & \text { Fine } \\ & \text { Gross } \end{aligned}$ | 1014 |  | 5 |
| SUBGROUP 8 <br> NA |  |  |  |
| GROUP C |  |  |  |
| SUBGROUP 1 <br> Steady State Life Test Electrical End Points | 1005 | 1000 hrs. at $125^{\circ} \mathrm{C}$ | 5 |
| SUBGROUP 2 |  |  |  |
| Temperature Cycling Constant Acceleration | $\begin{aligned} & 1010 \\ & 2001 \end{aligned}$ | Test Condition C <br> Test Condition E, Y only | 15 |
| Seal <br> Fine <br> Gross | 1014 |  |  |
| Visual Examination Electrical End Points | 1010 or 1011 |  |  |
| GROUP D |  |  |  |
| SUBGROUP 1 <br> Physical Dimensions | 2016 |  | 15 |
| SUBGROUP 2 <br> Lead Integrity <br> Seal <br> Fine <br> Gross | $\begin{aligned} & 2004 \\ & 1014 \end{aligned}$ | Test Condition B2 | 15 |

## Conformance Flow (Cont.)

## MIL-STD-883C Quality Conformance Tests

Method
Test Condition
LTPD

## GROUP D (Cont.)

| SUBGROUP 3 |  |  |
| :--- | :--- | :--- |
| Thermal Shock | 1011 | Test Condition B, 15 Cycles |
| Temperature Cycling | 1010 | Test Condition C, 100 Cycles |
| Moisture Resistance | 1004 |  |
| Seal | 1014 |  |
| Fine |  |  |
| Gross |  |  |
| Visual Examination |  |  |
| Electrical End Points |  |  |

al End Points
SUBGROUP 4
Mechanical Shock 2002
Vibration Variable Frequency 2007
Constant Acceleration 2001
Seal 1014
Fine
Gross
Visual Examination 1010 or 1011
Electrical End Points
SUBGROUP 5 15
Salt Atmosphere 1009
Seal 1014
Fine
Gross
Visual Examination 1009
SUBGROUP 6
Internal Water-Vapor Content 1018
5,000 PPM - CerDIP only 3 Devices
SUBGROUP 7
Test Condition A

Adhesion of Lead Finish 2025
SUBGROUP 8
Lid Torque 2024
5 Devices

## Quality Assurance Integrated Circuit Screening



## Device Reliability

## Reliability

The work of the Reliability Group at TSC has resulted in a product which should far exceed the reliability needs of any customer. Two important measures of device failure rate are stress testing under elevated temperature and under elevated temperature in conjunction with elevated humidity.

## Steady State Life

Device reliability is often measured by survival rate under high temperature operating conditions. Figure 3 illustrates expected failure rate per 1000 hrs . of operating time over a temperature range from $25^{\circ} \mathrm{C}$ to $175^{\circ} \mathrm{C}$. This graph is for TSC CMOS integrated circuits. The data was derived from results of Dynamic high temperature stress testing at $125^{\circ} \mathrm{C}$ and $150^{\circ} \mathrm{C}$ and calculations based on MIL-HDBK 217D.


Figure 3

## Temperature and Humidity

A major indicator of the reliability of a plastic encapsulated device (commercial class) is its ability to withstand temperature and humidity combined. Elevated temperature and humidity testing is routinely performed by TSC to evaluate the affect of these conditions on device reliability. The industry standard of $85^{\circ} \mathrm{C}$ and $85 \%$ Relative Humidity is used. Teledyne Semiconductor has a policy of using proven state-of-the-art molding compounds in its assembly process. Figure 4 illustrates the improvement this has made in TSC device reliability as measured by the 85/85 stress test.


Figure 4

## I.C. Handling Precautions

## Transportation

Two main concerns to be minimized during transportation are mechanical vibration and shock and Electrostatic Discharge (ESD) damage. While mechanical shock can be minimized by suitable packing and handling, ESD damage requires additional measures including:

- Use containers or jigs which will not induce static electricity as the result of vibration during transportation. It is desirable to use an electrically conductive foam or aluminum foil and static eliminating bags.
- In order to prevent device damage from clothing-induced static electricity, workers should be properly grounded with grounding straps while handling devices. A resistor of about 1 M ohm must be provided to protect from electric shock.
- When transporting the printed circuit boards on which semiconductor devices are mounted suitable preventive measures against static electricity transfer and induction must be taken. Shorting connectors should be placed on open contacts and the board transported in electrically conductive bags.


## Storage

It is preferable to store semiconductor devices in the following ways to prevent deterioration in their electrical characteristics, solderability, and mechanical appearance.

- Store in an ambient temperature of 5 to $30^{\circ} \mathrm{C}$, and in a relative humidity of 40 to $60 \%$.
- Store in a clean air environment, free from dust and active gas.
- Store in a container which does not induce static electricity.
Store without any physical load.
If semiconductor devices are stored for a long time, store them as sent from the factory. If their lead wires are formed beforehand, they may corrode during storage.
If the chips are unsealed, store them in a cool, dry, dark, and dustless place. Assemble them within 5 days after unpacking. Storage in nitrogen gas is desirable. They can be stored for 20 days or less in dry nitrogen gas with a dew point at $-30^{\circ} \mathrm{C}$ or lower. Unpacked chips must not be stored for over 3 months.
Take care not to allow condensation during storage due to rapid temperature changes.


## I.C. Handling Precautions (cont.)


#### Abstract

Testing Avoid ESD, noise or voltage surges when testing ICs. The device is in its least protected state during handling, insertion and testing. Any test equipment that leaks current or is allowed to attain only a few hundred volts of ESD can destroy CMOS ICs. All equipment must be grounded and periodically tested for leakage.


## Soldering

Semiconductor devices should not be left at high temperatures for a long time. Regardless of the soldering method, soldering must be done in a short time and at the lowest possible temperature. Soldering work must meet soldering heat test conditions, namely, $260^{\circ} \mathrm{C}$ for 10 seconds and $350^{\circ} \mathrm{C}$ for 3 seconds at a point 1 to 1.5 mm away from the end of the device package.
Use of a strong alkali or acid flux may corrode the leads, deteriorating reliabilty and device characteristics. The recommended soldering iron is the type that is operated with a secondary voltage supplied by a transformer and grounded to protect from lead current. Solder the leads at the farthest point from the device package.

## Personnel

- All personnel handling or in close proximity to ICs must wear anti-static clothing and shoes.
- Handling personnel must wear grounding straps.
- Work surfaces and straps should be earth grounded through a 1 M ohm resistor.
- Floors and carpets should be treated so as not to generate static electricity.
- Unrelated sources of RF or static electrical fields (e.g., plastic boxes, plastic wrappers) should be kept away from device handling areas.


## Removing Residual Flux

To insure the reliability of electronic systems, residual flux must be removed from circuit boards. Detergent or ultrasonic cleaning is usually applied. If chloric detergent is used for the plastic molded devices, package corrosion may occur. Since cleaning over extended periods or at high temperatures may cause swollen chip coating due to solvent permeation, select the type of detergent and cleaning condition carefully. Do not use trichloroethylene. For ultrasonic cleaning, the following conditions are advisable:

- Frequency: 28 to 29 kHz (to avoid device resonation)
- Ultrasonic output: $15 \mathrm{~W} / \ell$
- Keep the devices out of direct contact with the power generator.
- Cleaning time: Less than 30 seconds
- Clean Freon ${ }^{\text {TM }}$ is recommended if other conditions permit.


Alphanumeric Product List

## Alphanumeric Product List

TSC04/05
TSC170/171
TSC400/401TSC426/427/428TSC429TSC441/442/443TSC444/445/446TSC447TSC450TSC500TSC700ATSC701AMTSC800
TSC805
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Voltage to Frequency Converter (0.01\% Linearity) ..... 9-5
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$31 / 2$ Digit ADC with Multiplexed BCD Output ..... 7-165

Notes


## All TSC Products Cross-Referenced Are Plug-In Replacements

| Part Number | TSC Number | Comments |
| :---: | :---: | :---: |
| ADC-EK10B | TSC8701CJ |  |
| ADC-EK12B | TSC8702CN |  |
| ADC-EK12DC | TSC8750CJ |  |
| ADC-EK12DM | TSC8750BN |  |
| ADC-EK12DR | TSC8750CN |  |
| ADC-EK08B | TSC8700CJ |  |
| ADC-ET10BC | TSC8704CJ |  |
| ADC-ET10BM | TSC8704BN |  |
| ADC-ET10BR | TSC8704CN |  |
| ADC-ET12BC | TSC8705CJ |  |
| ADC-ET12BM | TSC8705BN |  |
| ADC-ET12BR | TSC8705CN |  |
| ADC-ET8BC | TSC8703CJ |  |
| ADC-ET8BM | TSC8703BL |  |
| ADC-ET8BR | TSC8703CL |  |
| CD22104AE | TSC7211AIPL |  |
| CD22105AE | TSC7211AMIPL |  |
| DS0026CJ-8 | TSC4261JA | Pin Compatible, Functional Upgrade |
| DS0026CN-8 | TSC426CPA | Pin Compatible, Functional Upgrade |
| DS0026J-8 | TSC426MJA | Pin Compatible, Functional Upgrade |
| HLCD7211-2 | TSC7211AIPL |  |
| HLCD7211-4 | TSC7211AMIPL |  |
| ICL7106CJL | TSC7106CJL | TSC7106ACPL Has Improved Reference Voltage |
| ICL7106CPL | TSC7106CPL | TSC7106ACPL Offers Improved Reference Tempco |
| ICL7106RCPL | TSC7106RCPL | TSC7106ARCPL Offers Improved Reference Tempco |
| ICL7107CJL | TSC7107CJL | TSC7107ACJL Offers Improved Reference Tempco |
| ICL7107CPL | TSC7107CPL | TSC7107ACPL Offers Improved Reference Tempco |
| ICL7107RCPL | TSC7107RCPL | TSC7107ARCPL Offers Improved Reference Tempco |
| ICL7109CPL | TSC7109CPL | Exact Replacement. TSC7109BCPL For Lower Cost |
| ICL7109IJL | TSC71091JL |  |
| ICL7109MJL | TSC7109MJL |  |
| ICL7116CJL | TSC7116CJL | TSC7116ACJL Offers Improved Reference Tempco |
| ICL7116CPL | TSC7116CPL | TSC7116ACPL Offers Improved Reference Tempco |
| ICL7117CJL | TSC7117CJL | TSC7117ACJL Offers Improved Reference Tempco |
| ICL7117CPL | TSC7117CPL | TSC7117ACPL Offers Improved Reference Tempco |

## CMOS Data Acquisition Cross Reference

All TSC Products Cross-Referenced Are Plug-In Replacements (Cont.)

| Part Number | TSC Number | Comments |
| :---: | :---: | :---: |
| ICL7126CJL | TSC7126CJL | TSC7126ACJL Offers Improved Reterence Tempco |
| ICL7126CPL | TSC7126CPL | TSC7126ACPL Offers Improved Reference Tempco |
| ICL7136CJL | TSC7126CJL | TSC7126CJL and TSC7126ACJL Are Plug-In Replacements |
| ICL7136CPL | TSC7126CPL | TSC7126CPL and TSC7126ACPL Are Plug-In Replacements |
| ICL7650CPA | TSC7650CPA | TSC900ACPA is a Low-Power Plug-In Upgrade |
| ICL7650CPD | TSC7650CPD | TSC900ACPD is a Low-Power Plug-In Upgrade |
| ICL7650IJA | TSC76501JA | TSC900AIJA is a Low-Power Plug-In Upgrade |
| ICL7650IJD | TSC7650IJD | TSC900AIJD is a Low-Power Plug-In Upgrade |
| ICL7660CPA | TSC7660CPA |  |
| ICL7660IJA | TSC76601JA |  |
| ICL7660MJA | TSC7660MJA |  |
| ICL8069CCZR | TSC9491AJ |  |
| ICL8069CMSQ | TSC9491AM |  |
| ICL8069DCZR | TSC9491BJ |  |
| ICL8069DMSQ | TSC9491BM |  |
| ICM7211AIPL | TSC7211AIPL |  |
| ICM7211AMIPL | TSC7211AMIPL |  |
| ICM7212AIJL | TSC7212AIJL | TSC700AIJL is a Higher LED Current Upgrade for "Brighter" Displays |
| ICM7212AIPL | TSC7212AIPL | TSC700AIJL is a Higher LED Current Upgrade for "Brighter" Displays |
| ICM7212AMIJL | TSC7212AMIJL | TSC700AMIJL is a Higher LED Current Upgrade for "Brighter" Displays |
| ICM7212AMIPL | TSC7212AMIPL | TSC701AMIJL is a Higher LED Current Upgrade for "Brighter" Displays |
| MC14433L | TSC14433CL | TSC14433ACL Offers Guaranteed Roll-Over Spec. |
| MC14433P | TSC14433CJ | TSC14433ACJ Offers Guaranteed Roll-Over Spec. |
| MMH0026CP1 | TSC426CPA | Pin Compatible, Functional Upgrade |
| MMH0026CU | TSC426IJA | Pin Compatible, Functional Upgrade |
| MP5531C | TSC9495CJ |  |
| MP5532C | TSC9496CJ |  |
| REF01CP | TSC9495CJ |  |
| REF02CP | TSC9495CJ |  |
| TP4780 | TSC9400CJ |  |
| TP4781 | TSC9401CJ |  |
| VFQ-1C | TSC9400CJ |  |
| VFQ-1R | TSC900CL |  |



## Advance Product Information

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## General Description

The TSC04 (1.2 V Output) and TSC05 (2.5 V Output) bipolar two terminal band-gap voltage references offer precision performance without a premium price. The TSC04/05 do not use thin film resistors. This greatly lowers manufacturing complexity and cost.
A $50 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ output temperature coefficient and $25 \mu \mathrm{~A}$ to 10 mA operating current range make the devices attractive multimeter, data acquisition converter, and telecommunication voltage references

Typical Application
(s)

## Features

- $50 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ Temperature Coefficient
- $25 \mu \mathrm{~A}$ to 10 mA Operating Current Range
- $1 \Omega$ Dynamic Impedance
- Low Cost TO-92 Plastic Package
- 1\% Output Tolerance
- 1.2 V (TSC04) and 2.5 V (TSC05) Output Voltage Option


## Applications

- ADC and DAC Reference
- Current Source Generation
- Threshold Detectors
- Power Supplies
- Multimeters


## Pin Configuration



## Typical 4 1/2 Digit DVM with LCD Display



## General Description

The TSC170/171 bring low power CMOS technology to the current mode switching power supply controller market. Maximum supply current is 3.8 mA . Bipolar current mode control integrated circuits require five times more operating current. Low power supply current eliminates auxiliary power transformers. In off line powering schemes where a simple zener diode circuit provides device supply voltage, power dissipation is greatly reduced. CMOS technology decreases system cost, increases power efficiency, reduces heat generation, and increases total system reliability.
The dual totem pole CMOS outputs drive power MOSFET or bipolar transistors. The 50 ns maximum output rise and fall times with a 1000 pF capacitive load minimize power MOSFET transition power dissipation. Output peak current is 500 mA .

The TSC170/171 contain a full array of system protection circuits. The undervoltage lockout circuit forces outputs OFF if the supply voltage drops below 7.0 V . A soft start feature is also available. The soft start option forces the PWM outputs to initially operate at a minimum duty cycle and low peak output current. The TSC170/171 can be directly turned OFF through a remote shutdown control pin. The shutdown mode can be latched (power must be turned OFF to restart system) or nonlatched. The soft start feature can also be used in system shutdown application. Double output pulse suppression guarantees output drive pulses always alternate from one output driver to the other. Peak current is adjustable by the user.
Current mode control lets users parallel power supply modules. Two or more TSC170/171 controllers can be slaved together for parallel operation. Circuits can operate from a master TSC170/171 internal oscillator or an external system oscillator.
The TSC170/171 operate from an 8 V to 16 V power supply. An internal $2 \% 5.1 \mathrm{~V}$ reference minimizes external component count. The TSC170/171 is pin compatible with the Unitrode UC1846/2846/3846 and UC1847/2847/3847 bipolar controllers.
Other advantages inherent in current mode control include superior line and load regulation and automatic symmetry correction in push-pull converters.

## Ordering Information

| Part No. | Package | Operating <br> Temperature <br> Range |
| :--- | ---: | ---: |
| TSC170CPE | $8-$ Pin <br> Plastic DIP | $0^{\circ} \mathrm{C}$ to $70^{\circ} \mathrm{C}$ |
| TSC170IJE | $8-$ Pin <br> CerDIP | $-25^{\circ} \mathrm{C}$ to $85^{\circ} \mathrm{C}$ |

## Features

- Low Supply Current with CMOS Technology
3.8 mA Maximum
- Current Mode Control
- Internal Reference 5.1 V
- Fast Output Rise/Fall Time ( $\mathrm{C}_{\mathrm{L}}=1000 \mathrm{pF}$ ) ...... 50 ns
- Dual Push-Pull Outputs
- Direct Power MOSFET Drive
- High Totem Pole Output Drive .................. . . 500 mA
- Differential Current Sense Amplifier
- Programmable Current Limit
- Soft start Operation
- Double Pulse Suppression
- Under-Voltage Lockout
- Wide Supply Voltage Operation ................ 8 to 16 V
- High Frequency Operation ..................... 200 kHz
- Plastic and CerDIP Package
- Available with Low (TSC170) or High (TSC171) "OFF" State Outputs
- Low Power, Pin Compatible Replacement for UC3846/3847
Pin Configuration



## Ordering Information Cont.

| Part No. | Package | Operating <br> Temperatur <br> Range |
| :--- | ---: | ---: |
| TSC170MJE | $8-$ Pin <br> CerDIP | $-55^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ |
| TSC171CPE | $8-\mathrm{Pin}$ <br> Plastic DIP | $0^{\circ} \mathrm{C}$ to $70^{\circ} \mathrm{C}$ |
| TSC171IJE | $8-$ Pin <br> CerDIP | $-25^{\circ} \mathrm{C}$ to $85^{\circ} \mathrm{C}$ |
| TSC171MJE | $8-\mathrm{Pin}$ <br> CerDIP | $-55^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ |
| TSC170Y | Chip | - |
| TSC171Y | Chip | - |

# CMOS Current Mode SMPS Controller - 3.8 mA Max. Supply Current - 50 ns Output Rise/Fall Time - 500 mA Output Drive 


input Voltage (Pin 15) ................................... 18 V

Analog (
Lead Temperature (Soldering, 10 Seconds) $\ldots . .+300^{\circ} \mathrm{C}$
Maximum Chip Temperature ...................... $150^{\circ} \mathrm{C}$

CerDIP Package Thermal Resistance:


Electrical Characteristics: $\mathrm{V}_{1 \mathrm{~N}}=16 \mathrm{~V}, \mathrm{RO}_{\mathrm{O}}=24 \mathrm{k} \Omega, \mathrm{CO}_{\mathrm{O}}=1 \mathrm{nF}, \mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ Unless otherwise indicated.

| TYPE | NO. | SYMBOL | PARAMETER | TEST CONDITION | MIN ${ }_{\text {TYP }}^{\text {TSC170/171 }}$ MAX |  |  | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1 | VREF | Output Voltage | IOUT $=1 \mathrm{~mA}$ | 5.0 | 5.1 | 5.2 | V |
| REFERENCE | 2 | - | Line Regulation | V IN $=8 \mathrm{~V}$ to 16 V | - | 5 | 15 | mV |
| VOltage | 3 |  | Load Regulation | IOUT $=1 \mathrm{~mA}$ to 10 mA | - | 3 | 15 | mV |
|  | 4 | VRTC | Temperature Coefficient | Over Operating Temp. Range | - | 0.4 | 0.5 | $\mathrm{mV} /{ }^{\circ} \mathrm{C}$ |
|  | 5 | - | Initial Frequency | - | 38 | 42 | 46 | kHz |
| OSCILLATOR | 6 | - | Voltage Stability | $\mathrm{VIN}=8 \mathrm{~V}$ to 16 V | - | 1.1 | 1.5 | ${ }^{\circ} /{ }^{\circ} \mathrm{V}$ |
|  | 7 | - | Temperature Stability | Over Operating Temp. Range | - | 5 | 10 | \% |
|  | 8 | VEOS | Input Offset Voltage |  | - | - | 20 | mV |
|  | 9 | $\mathrm{I}_{\mathrm{B}}$ | Input Bias Current |  | - | - | 1 | nA |
| ERROR | 10 | VCMRR | Common-Mode Input Voltage | V IN $=8 \mathrm{~V}$ to 16 V | 0 | - | VIN-2 V | V |
| AMPLIFIER | 11 | Avol | Open-Loop Voltage Gain | Vout $=1 \mathrm{~V}$ to 6 V | 70 | - | - | dB |
|  | 12 | BW | Unity Gain Bandwidth |  | - | 1.2 | - | MHz |
|  | 13 | CMRR | Common-Mode Rejection Ratio | $\mathrm{VCMV}=0$ to 14 V | 60 | - | - | dB |
|  | 14 | PSRR | Power Supply Rejection Ratio | V IN $=8 \mathrm{~V}$ to 16 V | 60 | - | - | dB |
|  | 15 | - | Amplifier Gain | Pin $3=0$ to 1.1 V | 2.5 | 3.0 | 3.5 | V/V |
| CURRENT SENSE AMPLIFIER | 16 | - | Maximum Differential Input Signal | VPIN4 - Vpin3 | 1.1 | - | - | V |
|  | 17 |  | Common-Mode Input Voltage |  | 0 | - | VIN -3 V | V |
| CURRENT LIMIT | 18 |  | Current Limit Offset Voltage |  | 0.5 | - | 1 | V |
| ADJUST | 19 |  | Input Bias Current |  | - | - | 1 | nA |
|  | 20 | $V_{\text {TB }}$ | Threshold Voltage |  | 0.3 | 0.35 | 0.4 | V |
| SHUTDOWN | 21 |  | Input Voltage Range |  | 0 | - | VIN | V |
| TERMINAL | 22 |  | Minimum Latching Current at Pin 1 |  | 125 | - | - | $\mu \mathrm{A}$ |
|  | 23 |  | Maximum Non-Latching Current at Pin 1 |  | - | - | 50 | $\mu \mathrm{A}$ |
|  | 24 | VDD | Output Voltage | Pin 13 | - | - | VIN | V |
|  | 25 | VoL | Output Low Level | Isink $=20 \mathrm{~mA}$ | - | - | 0.4 | V |
| OUTPUT | 26 | Vol | Output Low Level | ISINK $=100 \mathrm{~mA}$ | - | - | 2.0 | V |
| STAGE | 27 | VOH | Output High Level | ISOURCE $=20 \mathrm{~mA}$ | VIN -1 V | - | - | V |
|  | 28 | VOH | Output High Level | ISOURCE $=100 \mathrm{~mA}$ | VIN -3.5 V | - | - | V |
|  | 29 | tr | Output Rise Time | $\mathrm{C}_{\mathrm{L}}=1000 \mathrm{pF}$ | - | 50 | 150 | ns |
|  | 30 | tF | Output Fall Time | $\mathrm{C}_{\mathrm{L}}=1000 \mathrm{pF}$ | - | 50 | 150 | ns |
| UNDERVOLTAGE | 31 |  | Start-up | Threshold | - | 7.7 | 8.25 | V |
| LOCKOUT | 32 |  | Threshold Hysteresis |  | 0.5 | 0.75 | 1.0 | V |
| SUPPLY | 33 | Is | Standby Supply Current |  | - | 2.7 | 3.8 | mA |

## CMOS Current Mode <br> SMPS Controller

- 3.8 mA Max. Supply Current
- 50 ns Output Rise/Fall Time
- 500 mA Output Drive

TSC170/171


Block Diagram

## Peak Current Limit Setup

Resistors R1 and R2 at the current limit input (Pin 1) set the TSC170 peak current limit (Figure 1). The potential at Pin 1 is easily calculated:
$V 1=V_{\text {REF }} \frac{R 2}{R 1+R 2}$

R1 should be selected first. The shutdown circuit feature is not latched for (VREF - 0.35)/R1<50 $\mu \mathrm{A}$ and is latched for currents greater than $125 \mu \mathrm{~A}$.
The error amplifier output voltage is clamped from going above V1 through the limit buffer amplifier. Peak current is sensed by RS and amplified by the current amplifier which has a fixed gain of 3.0.
IPCL, the peak current limit, is the current that causes the PWM comparator non-inverting input to exceed V1; the potential at the inverting input. Once the comparator trip point is exceeded both outputs are disabled.

ICPL is easily calculated:

1) $\mathrm{IPCL}=\frac{\mathrm{V} 1-.75 \mathrm{~V}}{3.0(\mathrm{RS})}$
where:
a) $\mathrm{V} 1=\mathrm{REF} \frac{\mathrm{R} 2}{\mathrm{R} 1+\mathrm{R} 2}$
b) $\mathrm{VREF}=$ Internal voltage reference $=5.1 \mathrm{~V}$
c) $3.0 \mathrm{~V}=$ Voltage gain of current sense amplifier
d) $0.75 \mathrm{~V}=$ Current limit offset

Both driver outputs (Pin 11 and Pin 14) are OFF (Iow) when the peak current limit is exceeded. When the sensed current goes below IPCL the circuit operates normally.


Figure 1: R1 and R2 Set Maximum Peak Output Current

## Output Shutdown

The TSC170 outputs can be turned off quickly through the shutdown input (Pin 16). A signal greater than 350 mV at Pin 16 forces the shutdown comparator output high. The PWM latch is held set disabling the outputs.
Q2 is also turned on. If VREF/R1 is greater than $125 \mu \mathrm{~A}$, positive feedback through the lock-up amplifier and Q1 keeps the inverting PWM comparator inverting input below 0.75 V . Q3 remains on even after the shutdown input signal is removed because of the positive feedback. The state can be cleared only through a power-up cycle. Outputs will be disabled whenever the potential at Pin 1 is below 0.75 V .
The shutdown terminal gives a fast, direct way to disable the TSC170 output transistors. System protection and remote shutdown applications are possible.

## Soft Restart from Shutdown

A soft restart can be programmed if non-latched shutdown operation is used.
A capacitor at Pin 1 will cause a gradual increase in potential toward V1. When the voltage at Pin 1 reaches 0.75 V the PWM latch set input is removed and the circuit establishes a regulated output voltage. The soft start operation forces the PWM output drivers to initially operate with minimum duty cycle and low peak currents.

# CMOS Current Mode <br> SMPS Controller 

- 3.8 mA Max. Supply Current
- 50 ns Output Rise/Fall Time
- 500 mA Output Drive


## Soft Start Power-Up

During power-up a capacitor at R1, R2 will initiate a soft start cycle. As the input voltage (Pin 15) exceeds the undervoltage lockout potential (7.5 V), Q4 is turned off ending undervoltage lockout. Whenever the PWM comparator inverting input is below 0.5 V both outputs are disabled.

When the undervoltage lockout level is passed, the capacitor begins to charge. The PWM duty cycle increases until the operating output voltage is reached. Soft start operation forces the PWM output drivers to initially operate with minimum duty cycle and low peak current.

## Current Sense Amplifier

The current sense amplifier operates at a fixed gain of 3.25 . Maximum differential input voltage (VPIN $4-$ VPIN 3) is 1.1 V . Common-mode input voltage range is 0 V to $\mathrm{VIN}-3 \mathrm{~V}$.
Resistive sensing methods are shown In Figure 2. In Figure 2A, a simple RC filter will limit transient voltage spikes at Pin 4 caused by external output transistor collector capacitance. Transformer coupling in Figure 3 offers isolation and better power efficlency but cost and complexity increase.


Figure 2: Resistive Sensing


Figure 3: Transformer Isolated Current Sense

## Undervoltage Lockout

The undervoltage lockout circuit forces the TSC170 outputs OFF (low) if the supply voltage is below 7.7 V . Threshold hysterisis is 0.75 V . Hysterisis guarantees clean, jitter free turn-on and turn-off points. The hysterisis also reduces capacitive filtering requirements at the PWM controller supply input (Pin 15).

## Clrcult Synchronization

Current mode controlied power supplies can be operated in parallel with a common load. Paralleled converters will equally share the load current. Voltage mode controllers unequally share the load current decreasing system reliability.
Two or more TSC170 controllers can be slaved together for parallel operation. Circuits can operate from a master TSC170 internal oscillator with an external driver (Figure 4). Devices can also be slaved to an external oscillator (Figure 5). Disable internal slave device oscillators by grounding Pin 8. Slave controllers derive an oscillator from the bi-directional synchronization output signal at Pin 10.


Figure 4: Master/Slave Parallel Operation


Figure 5: External Clock Synchronization

## Oscillator Frequency and Output Dead TIme

The oscillator frequency for $\mathrm{Ro}=24 \mathrm{k} \Omega$ and $\mathrm{Co}_{0}=1000 \mathrm{pF}$ is:

$$
\mathrm{FO}=\left[\frac{1.27}{\mathrm{ROCO}}-\frac{2800}{R_{\text {2 }} \mathrm{CO}_{0}}\right] \frac{\mathrm{Co}}{\mathrm{Co}+150}
$$

where: Ro $=$ Oscillator Resistor ( $\Omega$ )
Co = Oscillator Capacitor (F)
Fo = Oscillator Frequency ( Hz )
The oscillator resistor Ro can range from $5 \mathrm{k} \Omega$ to $50 \mathrm{k} \Omega$.
Oscillator capacitor Co can range from 250 pF to 1000 pF .
Figure 7 shows typical operation for various resistance and capacitance values.
During transitions between the two outputs simultaneous conduction is prevented. Oscillator fall time controls the output off or dead time (Figure 6).
Delay time is approximately:
$T D \equiv \frac{2000[\mathrm{CO}]}{1-\left(\frac{2.3}{\mathrm{RO}_{\mathrm{O}}}\right)}$
Where: Ro $\equiv$ Oscillator Resistor ( $k \Omega$ )

$$
\begin{aligned}
& C 0=\text { Oscillator Capacitor (F) } \\
& T D=\text { Output Dead Time (sec.) }
\end{aligned}
$$

Maximum possible duty cycle is set by the delay time.


Figure 6: TSC170 Oscillator Circuit

## Typical Characteristic Curves

Output Rise and Fall Time:
$C_{\text {LOAD }}=\mathbf{5 0 0} \mathbf{~ p F}$


Output Rise and Fall TIme: CLOAD $=1000 \mathrm{pF}$


Output Rise and Fall Time: CLOAD $=1800 \mathrm{pF}$

(Figure 7)
Osclilator Frequency vs Osclllator Resistance


# - ${ }^{-1}$ TELEDYNE SEMICONDUCTOR 

## General Description

The CMOS TSC400 16-channel and TSC401 8-channel differential analog multiplexer feature on-chip channel select and control data latches for microprocessor bus interface. The latched channel select address and enable inputs remove the need for external system "glue" logic. The master reset input signal feature clears all latches and turns all switches off. A useful feature during power up initialization. With chip select ( $\overline{\mathrm{CS}}$ ) and write ( $\overline{\mathrm{WR} \text { ) low the datalatches are }}$ transparent.
Operating from dual or single power supplies the low $50 \mu \mathrm{~A}$ supply current minimizes power dissipation. Analog signal range extends to either supply. Switching times guarantee break before make operation.

## Features

- Latched Channel Select Inputs
- Master Reset for Power-Up Initialization
- $50 \mu \mathrm{~A}$ Supply Current
- $\pm 5 \mathrm{~V}$ or +5 V Operation
- Single or Dual Supply Operation
- $500 \Omega$ "ON" Resistance
- 250 ns Write Pulse Operation
- Break Before Make Operation
- CHIP SELECT and WRITE Control Inputs


## Pin Configuration



## General Description

The TSC429 is a single high speed CMOS level translator and driver．Designed specifically to drive highly capacitive power MOSFET gates，the TSC429 features a $2.5 \Omega$ output impe－ dance and 3．5 A peak output current drive．

A 2500 pF capacitive load will be driven 18 V in 25 ns ．Delay time through the device is 25 ns ．The rapid switching times with large capacitive loads minimize power MOSFET transi－ tion power loss．

A TTL／CMOS input logic level is translated into an output voltage swing that equals the supply．The output will swing to within 25 mV of ground or $\mathrm{V}_{\mathrm{S}}^{+}$．Input voltage swing may equal the supply．Logic input current is under $1 \mu \mathrm{~A}$ making direct interface to CMOS／Bipolar switch mode power supply con－ trollers easy．Input＂speed－up＂capacitors are not required．

The CMOS design minimizes quiescent power supply current． With a logic 1 input，power supply current is 5 mA maximum and decreases to 0.5 mA for logic 0 inputs．

For dual devices see the TSC426／427／428 product data sheet．

## Applications

－Switch Mode Power Supplies
－CCD Drivers
－Pulse Transformer Drive
－Class D Switching Amplifiers

## Pin Configuration



NC＝NO INTERNAL CONNECTION

## Features

－Wide Operating Range ．．．．．．．．．．．．．．．．．．．．． 4.5 V to 18 V
－High Impedance CMOS Logic Input
－Logic Input Threshold Independent of Supply Voltage
－Low Supply Current
－ 5 mA Maximum with Logic 1 Input
－ 0.5 mA Maximum with Logic 0 Input
－Output Voltage Swing Within 25 mV of Ground or $\mathrm{V}_{\mathrm{S}}^{+}$．
－Low Delay Time 25 ns
－High Capacitive Load Drive Capability
$-t_{\text {RISE }} t_{\text {fall }}=25 \mathrm{~ns}$ with Cload $=2500 \mathrm{pF}$
－Single +5 V Supply Operation

## Typical Application



# が TELEDYNE SEMICONDUCTOR 

## General Description

The TSC441, TSC442, and TSC443 are quad SPST analog switches with data address latches. The pin out matches the "201" analog switch configuration. Pin 12, which is unused on the 201, is the write enable (WR) input. With $\overline{W R}$ tied low the data address latch is transparent.
The family features single or dual power supply operation with analog input voltage range equal to the supply voltage. Power supply current is a low $300 \mu \mathrm{~A}$.
The TSC441/442 have opposite input logic polarity. The TSC443, with two normally open and two normally closed switches, can be configured as a quad SPST, dual SPDT, DPDT or dual DPST switch.

For devices pin compatible with the AD7590/7591/7592 see the TSC444/445/456 specifications.

## Timing Diagram



## Features

- Data Address Latch On-Chip
- Latch Transparent with $\overline{W R}=0$
- < 250 ns Write Pulse Operation
- < 50 ns Address Hold Time
- Dual $\pm 5 \mathrm{~V}$ or Single +5 to +15 V Supply Operation
- $300 \mu \mathrm{~A}$ Supply Current
- $120 \Omega$ ON Resistance
- 1 nA Analog Input Leakage Current
- Analog Signal Range Equal to Supply Voltage
- TTL/CMOS Compatible, Low Current Logic Input
- TSC441: Pin Compatible to DG221
- "201" Pin Out Compatible (Pin $12=\overline{\text { WRITE ENABLE }})$
- TSC443: SPST, SPDT, DPDT, DPST Configuration


## Truth Table

| AN | WR $^{*}$ | TSC441 <br> Swltch State | TSC442 <br> Switch State | TSC443 <br> Switch State |
| :---: | :---: | :---: | :---: | :---: |
| 0 | 0 | Closed | Open | SW1, SW2, Open <br> SW3, SW4, Closed |
| 1 | 0 | Open | Closed | SW1, SW2, Closed <br> SW3, SW4, Open |
| $\mathbf{X}$ | 1 | Maintains <br> Previous <br> State | Maintains <br> Previous <br> State | Maintains <br> Previous <br> State |

* $\overline{W R}$ Input is Level Sensitive, $\mathrm{X}=$ Don't Care


## Pin Configuration



# *- TELEDYNE SEMICONDUCTOR 

TSC444/445/446
$\mu$-Processor Bus Compatible CMOS Quad Analog Switches Data Latches

- Low Power CMOS - 200 ns Write Pulse Operation


## General Description

The TSC444, TSC445, and TSC446 $\mu$-processor compatible analog switch family combine four analog switches with a data address latch. Quad SPST devices (445/446) and dual SPDT (444) devices feature $120 \Omega$ ON resistance and 1 nA analog input leakage currents. Analog input signal range extends to the power supply rails. A low $300 \mu \mathrm{~A}$ supply current and single or dual supply operation make the family ideal for battery operated systems. Break before make operation is guaranteed. Input logic signals are TTL/CMOS compatible.

## Truth Table

| DISABLE $^{\star}$ | $\overline{\text { WR}^{\star}}$ | A1 or A2 | TSC444 <br> Switch State |
| :---: | :---: | :---: | :---: |
| 0 | X | X | All Switches Open |
| 1 | 0 | 1 | S1 to Out1 Closed <br> S3 to Out2 Closed |
| 1 | 0 | 0 | S2 to Out1 Closed <br> S4 to Out2 Closed |
| 1 | 1 | X | Maintains Previous <br> State |

$\overline{* \overline{W R}}$ and $\overline{\text { DISABLE }}$ Inputs are Level Sensitive, $\mathrm{X}=$ Don't Care

## Truth Table

| AN $^{\prime}$ | WR* | TSC445 <br> Switch <br> State | TSC446 <br> Switch <br> State |
| :---: | :---: | :---: | :---: |
| 0 | 0 | Open | Closed |
| 1 | 0 | Closed | Open |
| $X$ | 1 | Maintains <br> Previous State | Maintains <br> Previous State |

* $\overline{\mathrm{WR}}$ Input is Level Sensitive, $\mathrm{X}=$ Don't Care


## Timing Diagram



## Features

- Data Address Latch On-Chip
- Latch Transparent with $\overline{\mathrm{WR}}=0$
- SPST and SPDT Options
- Dual $\pm 5 \mathrm{~V}$ Supply Operation
- Single +5 V to +15 V Supply Operation
- $300 \mu \mathrm{~A}$ Supply Current
- $120 \Omega$ ON Resistance
- 1 nA Analog Input Leakage Current
- < 250 ns Write Pulse Operation
- < 50 ns Address Hold Time
- TTL/CMOS Compatible, Low Current Logic Input
- Analog Signal Range Equal to Supply Voltage
- TSC445 Pin Compatible to AD7590
- TSC446 Pin Compatible to AD7591
- TSC444 Pin Compatible to AD7592


## Pin Configuration



# - TE TELEDYNE SEMICONDUCTOR 

## General Description

The TSC447 $\mu$-processor compatible analog switch contains four analog switches with a data address latch. Two devices are normally ON and two normally OFF. Analog input signal range extends to the power supply rails. Input leakage current is a low 1 nA . The $300 \mu \mathrm{~A}$ supply current and single or dual supply operation make the TSC447 ideal for battery operated systems. The TSC 447 operates with $+15 \mathrm{~V}, \pm 5 \mathrm{~V}$ or a single +5 V supply.
Break before make operation is guaranteed. The TSC447 can be connected as a latched Quad SPST, Dual SPDT, DPDT or Dual DPST analog switch. Input logic signals are TTL/CMOS compatible.

## Application Configurations



## Features

- Data Address Latch On-Chip
- Latch Transparent with $\overline{W R}=0$
- Two Normally Open and Two Normally Closed Switches
- Dual $\pm 5 \mathrm{~V}$ or +15 V Supply Operation
- Single +5 V to +15 V Supply Operation
- $300 \mu \mathrm{~A}$ Supply Current
- $120 \Omega$ On Resistance
- 1 nA Analog Input Leakage Current
- <250 ns Write Pulse Operation
- $<50$ ns Address Hold Time
- TTL/CMOS Compatible, Low Current Logic Input
- Analog Signal Range Equal to Supply Voltage


## TSC447 Truth Table

| $\mathbf{A N}_{N}$ | WR $^{\star}$ | Switch <br> $\mathbf{1}$ \& 4 <br> State | Switch <br> $\mathbf{2 ~ \& ~ 3 ~ 3 ~}$ <br> State |
| :---: | :---: | :---: | :---: |
| 0 | 0 | Open | Closed |
| 1 | 0 | Closed | Open |
| X | 1 | Maintains <br> Previous <br> State | Maintains <br> Previous <br> State |

$\overline{\overline{\mathrm{WR}}}{ }^{*}$ Input is Level Sensitive

## Pin Configuration



[^0]
## General Description

The TSC827 is a complete integrating analog-to-digital converter with triplex liquid crystal (LCD) display drive. A 101 element LCD bar-graph directly connects to the TSC827.
Two user selected set points can be programmed and displayed. LCD annunciators distinguish between set points. Set point annunciators are activated when a set point has been reached. An input overrange LCD annunciator is also present. Set point and overrange logic outputs are provided for control applications.
A 10-bit serial output with clock allows data to be transmitted at $0.1 \%$ resolution to a remote computer or display.
Operating from $\pm 5 \mathrm{~V}$ supplies, the CMOS TSC827 dissipates only 20 mW . Included on-chip is a precision $75 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ low drift voltage reference. The differential inputs accept 40 mV to 2.0 V input signals. The TSC827 is available in a compact 60 -pin flat package. For a $2.5 \%$ resolution ADC with bargraph output see the TSC826 data sheet.

## Features

- $1 \%$ LCD Bar-Graph Readout
- Triplex LCD Display
- 101 Data Segments
- Overrange and Set Point Annunciators
- Two Selectable Set Points
- Low and High Set Point and Overrange Logic Output Signals
- Differential Analog Input
- Differential Reference for Ratiometric Measurements
- 40 mV to 2.0 V Full-Scale
- 10-Bit Serial Data Output
- $\pm 5 \mathrm{~V}$ Supply Operation
- 20 mW Power Dissipation
- Compact 60-Pin Flat Package


## Block Diagram



TSC829

## General Description

The CMOS TSC829 combines a precision $41 / 2$ digit ADC, and triplex LCD display drive circuit in a single low power CMOS chip. The TSC829 offers several functional enhancements over the first generation ICL7129 converter. An audio frequency continuity buzzer signal is generated on-chip along with the continuity logic output signal. The TSC829 eliminates the external audio signal generator and piezoelectric driver needed in 7129 based systems. More compact and less costly systems result. The 60-pin flat package also allows the complicated dual function 7129 input/output control pins to be replaced by easy to use single function pins.
By using the UP/DOWN, SIGN, X10 and conversion count out logic signals the data can be transferred to a microprocessor.

## Pin Configuration



## Features

- Triplex LCD Display Drive On-Chip
- Control Signals and Data Output for $\mu$-Processor Interface
- Audio Frequency "Buzzer" Signal and Driver for Piezoelectric Continuity Transducer
- On-Chip Low Battery Detector and LCD Annunciator Driver
- On-Chip Continuity Detection and LCD Annunciator Driver
- Easy to Use Single Function DP4, OR, UR, DP3, LATCH and EOC Input/Output Control Pins
- 4 1/2 Digit Resolution
- 10 to 1 Digitally Controlled Full-Scale Range Selection
- Simple 1 V Reference for 200 mV or 2 V Full-Scale Range
- $10 \mu \mathrm{~V}$ Resolution on 200 mV Full-Scale Range


## 4 1/2 Digit Converter Comparison

| FUNCTION | TSC829 | GE/INTERSIL <br> ICL7129 |
| :--- | :---: | :---: |
| On-Chip <br> Audio Frequency Continuity <br> "Buzzer" Drive Signal | Yes | No |
| Simple, Easy to Use | Yes: Each <br> Cocimal Point, Underrange, | No: Control Pins <br> Are Multiplexed <br> And Serve |
| Overrange, Latch and End <br> Of Conversion <br> Input/Output | Input/Output <br> Function Has <br> Control Pins | Dual Functions |

## General Description

The TSC913 is the world's first complete monolithic dual auto-zeroed operational amplifier. The TSC913 sets a new standard for low power precision dual operational amplifiers. Chopper-stabilized or auto-zeroed amplifiers offer low offset voltage errors by periodically sampling offset error and storing correction voltages on capacitors. Previous single amplifier designs required two user supplied external $0.1 \mu \mathrm{~F}$ error storage correction capacitors - much too large for on-chip integration. The unique TSC913 architecture requires smaller capacitors making on-chip integration possible. Microvolt offset levels are achieved and External Capacitors Are Not Required.

The TSC913 system benefits are apparent when contrasted with a 7650 chopper amplifier circuit implementation. A single TSC913 replaces two 7650s and four capacitors. Five components and assembly steps are eliminated.

The TSC913 pinout matches many popular dual operational amplifiers. The OP04, TLC322, LM358, and ICL7621 are typical examples. In many applications operating from dual five volt power supplies or single supplies, the TSC913 offers superior electrical performance and can be a functional, drop-in replacement. Printed circuit board rework is not necessary. The TSC913 low offset voltage error eliminates offset voltage trim potentiometers often needed with bipolar and low accuracy CMOS operational amplifiers.

The TSC913 takes full advantage of Teledyne's proprietary CMOS technology. The TSC913 $650 \mu \mathrm{~A}$ supply current ( $250 \mu \mathrm{~A}$ per amplifier) makes the TSC913 the lowest power, precision dual operational amplifier available. The 250 microampere amplifier supply current does not compromise AC performance. Unity gain bandwidth is 1.5 MHz and slew rate is $2.5 \mathrm{~V} / \mu \mathrm{s}$.

For single and quad operational amplifiers see the TSC911 and TSC914 data sheets.

## Features

- First Monolithic Dual Auto-Zeroed Operational Amplifier
- Chopper Amplifier Performance Without External Capacitors
- $15 \mu \mathrm{~V}$ Vos Maximum
- $0.15 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ Vos Drift Maximum
- Saves Cost/Assembly of Four "Chopper" Capacitors
- Low Supply Current . ............................... $650 \mu \mathrm{~A}$
- Low Input

Voltage Noise ( 0.1 to 10 Hz ) .................. $0.65 \mu \mathrm{VP-P}$

- Wide Common-Mode Voltage Range .... $V_{s}^{-}$to $V_{S}^{+}-2 \mathrm{~V}$
- High Common-Mode Rejection ................. 116 dB
- Dual or Single Supply Operation ......... $\pm 3 \mathrm{~V}$ to $\pm 8 \mathrm{~V}$
+4.5 V to +16 V
- Excellent AC Operating Characteristics
- $2.5 \mathrm{~V} / \mu \mathrm{s}$ Slew Rate
- 1.5 MHz Unity Gain Bandwidth
- Pin Compatible to LM358, OP14, MC1458, ICL7621, TL082, TLC322


## Pin Configuration




| Operating Temp. Range |  |
| :---: | :---: |
| I Device | $-25^{\circ} \mathrm{C}$ to $+85{ }^{\circ} \mathrm{C}$ |
| C Device | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ |
| Package Power Dissipation ( $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ ) |  |
| CerDIP Package | 500 mW |
| Plastic Package | 375 mW |

I Device ............................. $-25^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$
C Device ................................ $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$
Package Power Dissipation ( $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ )
Plastic Package
375 mW

Electrical Characteristics: $\mathrm{V}_{\mathrm{S}}= \pm 5, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ unless otherwise indicated.

| NO. | SYMBOL | PARAMETER | TEST CONDITIONS | MIN | $\begin{gathered} \hline \text { TSC913A } \\ \text { TYP } \end{gathered}$ | MAX | MIN | $\begin{gathered} \text { TSC913E } \\ \text { TYP } \end{gathered}$ | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Vos | Input Offset Voltage | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ | - | 5 | 15 | - | 15 | 30 | $\mu \mathrm{V}$ |
| 2 | Vos/T | Average Temperature Coefficient of Input Offset Voltage | $\begin{aligned} & 0^{\circ} \mathrm{C} \leq \mathrm{T}_{A} \leq 70^{\circ} \mathrm{C} \\ & -25^{\circ} \mathrm{C} \leq \mathrm{T}_{A} \leq 85^{\circ} \mathrm{C} \end{aligned}$ | - | $\begin{aligned} & 0.05 \\ & 0.05 \end{aligned}$ | $\begin{aligned} & 0.15 \\ & 0.15 \end{aligned}$ | - | - | $\begin{aligned} & 0.25 \\ & 0.25 \end{aligned}$ | $\begin{aligned} & \mu \mathrm{V} /{ }^{\circ} \mathrm{C} \\ & \mu \mathrm{~V} /{ }^{\circ} \mathrm{C} \end{aligned}$ |
| 3 | IB | Average Input Bias Current | $\begin{aligned} & T_{A}=25^{\circ} \mathrm{C} \\ & 0^{\circ} \mathrm{C} \leq T_{A} \leq 70^{\circ} \mathrm{C} \\ & -25^{\circ} \mathrm{C} \leq T_{A} \leq 85^{\circ} \mathrm{C} \end{aligned}$ | - | 二 | $\begin{array}{r} 90 \\ 3 \\ 4 \end{array}$ | 二 | - | 120 4 6 | pA nA nA |
| 4 | los | Average Input | Offset Current | - | 5 | 20 | - | 10 | 40 | pA |
| 5 | en | Input Voltage Noise | 0.1 to $1.0 \mathrm{~Hz}, \mathrm{R}_{\mathrm{s}} \leq 100 \Omega$ | - | 0.6 | - | - | 0.6 | - | $\mu \mathrm{V}$ P-P |
| 6 | en | Input Voltage Noise | 0.1 to $10 \mathrm{~Hz}, \mathrm{Rs} \leq 100 \Omega$ | - | 11 | - | - | 11 | - | $\mu \mathrm{VP-P}$ |
| 7 | CMRR | Common-Mode Rejection Ratio | $\mathrm{V}_{S}^{-} \leq \mathrm{VCM} \leq \mathrm{V}_{S}^{+}-2.2 \mathrm{~V}$ | 110 | 116 | - | 100 | 110 | - | dB |
| 8 | CMVR | Common-Mode Voltage Range |  | Vs | - | $\mathrm{V}_{s}^{+}-2.0$ | Vs | - | $\mathrm{V}_{s}^{+}-2.0$ | V |
| 9 | Aol | Open-Loop <br> Voltage Gain | $\mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega, \mathrm{V}_{\mathrm{O}}= \pm 4 \mathrm{~V}$ | 115 | 120 | - | 110 | 120 | - | dB |
| 10 | Vout | Output Voltage Swing | $\mathrm{RL}=10 \mathrm{k} \Omega$ | $\mathrm{Vs}+.3 \mathrm{~V}$ |  | $\mathrm{V}^{+}-.9 \mathrm{~V}$ | $\mathrm{Vs}+.3 \mathrm{~V}$ |  | $\mathrm{V}_{s}^{+}-.9 \mathrm{~V}$ | V |
| 11 | BW | Closed Loop Bandwidth | Closed Loop Gain = +1 | - | 1.5 | - | - | 1.5 | - | MHz |
| 12 | SR | Slew Rate | $\mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega, \mathrm{C}_{\mathrm{L}}=50 \mathrm{pf}$ | - | 2.5 | - | - | 2.5 | - | $\mathrm{V} / \mu \mathrm{s}$ |
| 13 | PSRR | Power Supply Rejection | $\pm 3.3 \leq \mathrm{Vs}^{\leq} \leq 5.5 \mathrm{~V}$ | 110 | - | - | 100 | - | - | dB |
| 14 | Vs | Operating Supply Voltage Range (Note 3) |  | $\pm 3 \mathrm{~V}$ | - | $\pm 8 \mathrm{~V}$ | $\pm 3 \mathrm{~V}$ | - | $\pm 8 \mathrm{~V}$ | V |
| 15 | Is | Quiescent Supply Cur (Both Amplifiers) | $V_{S}= \pm 5 \mathrm{~V}$ | - | 0.65 | 0.85 | - | - | 1.1 | mA |

## Notes:

1. Static Sensitive Device. Unused devices should be stored in conductive material.
2. Stresses above those listed under "Absolute Maximum Ratings" may cause permanent damage to the devices. These are stress ratings only and functional operation of the device at these or any other conditions above those indicated in the operational sections of the specifications is not implied.
3. Single Supply Operation: $\mathrm{V}_{\mathrm{S}}^{+}=+4.5 \mathrm{~V}$ to +16 V .
4. Advance product information.

## General Description

The TSC914 is the world's first complete monolithic quad auto-zeroed operational amplifier. The TSC914 sets a new standard for low power precision quad operational amplifiers. Chopper-stabilized or auto-zeroed amplifiers offer low offset voltage errors by periodically sampling offset error and storing correction voltages on capacitors. Previous single amplifier designs required two user supplied external $0.1 \mu \mathrm{~F}$ error storage correction capacitors - much too large for on-chip integration. The unique TSC914 architecture requires smaller capacitors making on-chip integration possible. Microvolt offset levels are achieved and External Capacitors Are Not Required.

The TSC914 system benefits are apparent when contrasted with a 7650 chopper amplifier circuit implementation. A single TSC914 replaces four 7650s and eight capacitors. Eleven components and assembly steps are eliminated.

The TSC914 pinout matches many popular quad operational amplifiers. The OP11, TLC274, LTC1014, LM348, and ICL7642/ 41 are typical examples. In many applications operating from dual five volt power supplies or single supplies, the TSC914 offers superior electrical performance and can be a functional, drop-in replacement. Printed circuit board rework is not necessary. The TSC914 low offset voltage error eliminates offset voltage trim potentiometers often needed with bipolar and low accuracy CMOS operational amplifiers.

The TSC914 takes full advantage of Teledyne's proprietary CMOS technology. The TSC914 1.5 mA supply current ( 250 $\mu \mathrm{A}$ per amplifier) makes the TSC914 the lowest power, precision quad operational amplifier available. The 250 microampere amplifier supply current does not compromise AC performance. Unity gain bandwidth is 1.5 MHz and slew rate is $2.5 \mathrm{~V} / \mu \mathrm{s}$.

For single and dual operational amplifiers see the TSC911 and TSC913 data sheets.

## Features

- First Monolithic Quad Auto-Zeroed Operational Amplifier
- Chopper Amplifier Performance Without External Capacitors
- $15 \mu \mathrm{~V}$ Vos
- $0.15 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ Vos Drift
- High DC Gain ...................................... 110 dB
- Low Supply Current ............................... 1.5 mA
- Wide Common-Mode Voltage Range .... $\mathrm{V}_{S}^{-}$to $\mathrm{V}_{S}^{+}-2 \mathrm{~V}$
- High Common-Mode Rejection ................ 110 dB
- Dual or Single Supply Operation ........ $\pm 3 \mathrm{~V}$ to $\pm 8 \mathrm{~V}$
+4.5 V to +16 V
- Excellent AC Operating Characteristics
$-2.5 \mathrm{~V} / \mu \mathrm{s}$ Slew Rate
- 1.5 MHz Unity Gain Bandwidth
- Pin Compatible to LM348, TLC274, LM324, OP11, ICL7641/42


## Pin Configuration



Absolute Maximum Ratings


```
Operating Temp. Range
    I Device ............................ - - 25 0}\textrm{C}\mathrm{ to +85 0}\textrm{C
    C Device .................................. 0 0}\textrm{C}\mathrm{ to +70 0}\textrm{C
Package Power Dissipation ( }\mp@subsup{T}{A}{}=25\mp@subsup{5}{}{\circ}\textrm{C}
CerDIP Package ...................................... }500\textrm{mW
```



Electrical Characteristics: $V_{S}= \pm 5, T_{A}=25^{\circ} \mathrm{C}$ unless otherwise indicated.

| NO. | SYMBOL | PARAMETER | TEST CONDITIONS | MIN | $\begin{gathered} \text { TSC914A } \\ \text { TYP } \end{gathered}$ | MAX | MIN | $\begin{gathered} \text { TSC9141 } \\ \text { TYP } \end{gathered}$ | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Vos | Input Offset Voltage | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ | - | 5 | 15 | - | 15 | 30 | $\mu \mathrm{V}$ |
| 2 | Vos/T | Average Temperature Coefficient of Input Offset Voltage | $\begin{aligned} & 0^{\circ} \mathrm{C} \leq T_{A} \leq 70^{\circ} \mathrm{C} \\ & -25^{\circ} \mathrm{C} \leq T_{A} \leq 85^{\circ} \mathrm{C} \end{aligned}$ | - | $\begin{aligned} & 0.05 \\ & 0.05 \end{aligned}$ | $\begin{aligned} & 0.15 \\ & 0.15 \end{aligned}$ | - | - | $\begin{aligned} & 0.25 \\ & 0.25 \end{aligned}$ | $\begin{aligned} & \mu \mathrm{V} /{ }^{\circ} \mathrm{C} \\ & \mu \mathrm{~V} /{ }^{\circ} \mathrm{C} \end{aligned}$ |
| 3 | lb | Average Input Bias Current | $\begin{aligned} & T_{A}=25^{\circ} \mathrm{C} \\ & 0^{\circ} \mathrm{C} \leq T_{A} \leq 70^{\circ} \mathrm{C} \\ & -25^{\circ} \mathrm{C} \leq T_{A} \leq 85^{\circ} \mathrm{C} \end{aligned}$ | - | 二 | $\begin{array}{r} 90 \\ 3 \\ 4 \end{array}$ | - | - | 120 4 6 | pA nA nA |
| 4 | los | Average Input | Offset Current | - | 5 | 20 | - | 10 | 40 | DA |
| 5 | en | Input Voltage Noise | 0.1 to $1.0 \mathrm{~Hz}, \mathrm{Rs} \leq 100 \Omega$ | - | 0.6 | - | - | 0.6 | - | $\mu \mathrm{VP-P}$ |
| 6 | en | Input Voltage Noise | 0.1 to $10 \mathrm{~Hz}, \mathrm{Rs} \leq 100 \Omega$ | - | 11 | - | - | 11 | - | $\mu \mathrm{V}$ P-P |
| 7 | CMRR | Common-Mode Rejection Ratio | $\mathrm{V}_{\mathrm{S}}^{-} \leq \mathrm{V}_{C M} \leq \mathrm{V}_{\mathrm{S}}^{+}-2.2 \mathrm{~V}$ | 110 | 116 | - | 100 | 110 | - | dB |
| 8 | CMVR | Common-Mode Voltage Range |  | $V_{s}^{-}$ | - | $\mathrm{V}_{S}^{+}-2.0$ | Vs |  | $\mathrm{V}_{\mathrm{S}}^{+}-2.0$ | V |
| 9 | Aol | Open-Loop Voltage Gain | $\mathrm{RL}_{\mathrm{L}}=10 \mathrm{k} \Omega, \mathrm{V}_{\mathrm{O}}= \pm 4 \mathrm{~V}$ | 115 | 120 | - | 110 | 120 | - | dB |
| 10 | Vout | Output Voltage Swing | $\mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega$ | V - +3 V |  | $\mathrm{V}_{S}^{+}-.9 \mathrm{~V}$ | $\mathrm{Vs}+3 \mathrm{~V}$ |  | $\mathrm{V}_{S}^{+}-.9 \mathrm{~V}$ | V |
| 11 | BW | Closed Loop Bandwidth | Closed Loop Gain $=+1$ | - | 1.5 | - | - | 1.5 | - | MHz |
| 12 | SR | Slew Rate | $\mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega, \mathrm{C}_{\mathrm{L}}=50 \mathrm{pf}$ | - | 2.5 | - | - | 2.5 | - | $\mathrm{V} / \mu \mathrm{s}$ |
| 13 | PSRR | Power Supply Rejection | $\pm 3.3 \leq \mathrm{Vs}^{5} \pm 5.5 \mathrm{~V}$ | 110 | - | - | 100 | - | - | dB |
| 14 | Vs | Operating Supply Voltage Range (Note 3) |  | $\pm 3 \mathrm{~V}$ | - | $\pm 8 \mathrm{~V}$ | $\pm 3 \mathrm{~V}$ | - | $\pm 8 \mathrm{~V}$ | V |
| 15 | Is | Quiescent <br> Supply Current <br> (Four Amplifiers) | $\mathrm{V}_{\mathrm{S}}= \pm 5 \mathrm{~V}$ | - | - | 1.6 | - | - | 2.2 | mA |

## Notes:

1. Static Sensitive Device. Unused devices should be stored in conductive material.
2. Stresses above those listed under "Absolute Maximum Ratings" may cause permanent damage to the devices. These are stress ratings only and functional operation of the device at these or any other conditions above those indicated in the operational sections of the specifications is not implied.
3. Single Supply Operation: $\mathrm{V}_{\mathrm{S}}^{+}=+4.5 \mathrm{~V}$ to +16 V .
4. Advance product information.

## General Description

The TSC4201, TSC4202 and TSC4203 are low leakage, low power CMOS quad SPST analog switches. Pin out matches the " 201 " analog switch configuration.

The TSC4201 and TSC4202 have opposite input logic polarity. The TSC4203, with two normally open and two normally closed switches, can be configured as a quad SPST, dual SPDT, DPDT, or dual DPST switch.

The family features single or dual power supply. Single +5 to +15 V or $\pm 5 \mathrm{~V}$ operation is possible. Analog input voltage range equals the supply voltage. Power supply current is a low $300 \mu \mathrm{~A}$. Leakage currents are a low 1 nA .

For devices with address data latches, see the TSC441, TSC442, and TSC443 product specifications.

## Features

- $300 \mu \mathrm{~A}$ Supply Current
- $120 \Omega$ ON Resistance
- Low Input Leakage Current
- Dual $\pm 5 \mathrm{~V}$ or Single +5 to +15 V Supply Operation
- Analog Signal Range Equal to Supply Voltage
- TTL/CMOS Compatible Low Current Logic Input
- TSC4201: Pin Compatible to DG201
- TSC4202: Pin Compatible to DG202
- TSC4203: SPST, SPDT, DPST Configuration


## Truth Table

| AN | TSC4201 <br> Switch State | TSC4202 <br> Switch State | TSC4203 <br> Switch State |
| :--- | :---: | :---: | :---: |
| 0 | Closed | Open | SW1, SW2, Open <br> SW3, SW4, Closed |
| 1 | Open | Closed | SW1, SW2, Closed <br> SW3, SW4, Open |

## Pin Configuration



AN $=\mathbf{0}, \mathbf{N C}=$ No Internal Connection

# ** TELEDYNE SEMICONDUCTOR 

TSC7129

## 4 1/2 Digit ADC with Triplex

 LCD Display Drive - Single Chip - $10 \mu \mathrm{~V}$ Resolution- Low Battery Detection


## General Description

The TSC7129 4 1/2 digit single chip analog-to-digital converter directly drives multiplexed liquid crystal displays. External LCD drivers for decimal point, low battery, continuity. and polarity annunciators are not required. On-chip low battery detection, analog continuity adn 10 to 1 digital range change circuits eliminate external active components. Underrange and overrange outputs make autorange instruments possible.
Operating form conventional 9 V batteries or the compact VR22 9 V cell supply current is below 1 mA . With twelve external resistors/capacitors, 120 kHz crystal, TSC9491 bandgap reference, and LCD display a precision low cost 0.005\% resolution instrument can be constructed.
For a compact surface mounted single chip 4 1/2 digit ADC see the TSC829 data sheet.

## Pin Configuration



## Features

- Single Chip 4 1/2 Digit ADC
- $\pm 19,999$ Count Resolution
- Triplex LCD Display Drive
- Decimal Point, Low Battery Continuity and Polarity LCD Annunciators
- Low Battery Detection and LCD Annunciator
- Fast Analog Continuity Detection
- Differntial Reference and Signal Input
- 10 mW Power Dissipation
- Overrange/Underrange Outputs
- Digital Range Select
- 200 mV or 2 V Full-Scale
- Direct ICL7129 Replacement


## Typical Configuration



## General Description

The TSC7136A is a low power 3 1/2 Digit LCD display analog-to-digital converter. An improved internal zener reference voltage circuit reduces analog common temperature drift to $35 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ typically. This represents a 2 to 4 times improvement over similar $31 / 2$ digit converters.
An integrator zero cycle eliminates overload recovery hangup. The auto-zero cycle guarantees a zero display reading for zero volt input.

The TSC7136A limits linearity error to less than 1 count on 200 mV or 2 V full-scale ranges. Rollover error (the difference in readings for equal magnitude but opposite polarity input signals) is below 1 count. High impedance differential inputs offer 1 pA leakage currents and a $1012 \Omega$ input impedance. Ratiometric measurements for ohms or bridge transducer measurements are easy with the differential reference input. The low noise performance guarantees a "rock solid" reading.

The TSC7136A dual slope conversion technique rejects interference signals when the converter integration period equals a multiple of the interference signal period. This is especially useful in industrial measurement environments where 50,60 and 400 Hz line frequency signals are present.
The single chip CMOS TSC7136A incorporates all the active devices for a $31 / 2$ digit analog-to-digital converter to directly drive an LCD display. The internal oscillator, precision vol-

## Features

- Fast Recovery from Overrange Input Signals
- Internal Reference With Low

Temperature Drift .................... $35 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ Typical
$75 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ Maximum

- Guaranteed Zero Reading With Zero Input
- Low Noise ......................................... $15 \mu V_{p-p}$
- High Resolution ( $0.05 \%$ ) and Wide Dynamic Range ( 72 dB )
- Low Input Leakage Current ............... 1 pA Typical 10 pA Maximum
- Direct LCD Drive - No External Components
- Precision Null Detection With True Polarity at Zero
- High Impedance Differential Input
- Convenient 9 V Battery Operation With Low Power Dissipation . $900 \mu \mathrm{~W}$ Maximum
- Internal Clock Circuit
- Improved Drop-In Replacement For ICL7136 with Low Analog Common Temperature Coefficient
- Industrial Temperature Range Device Available
- Available in Compact Flat Package
tage reference and display segment/backplane drivers simplify system integration, reduce board space requirements and lower total cost. A low cost, $0.05 \%$ resolution indicating meter requires only a display, four resistors, four capacitors and a 9 V battery. A flat package option eases the mechanical design of low cost, hand held multimeters.

Typical Application
Pin Configuration


Section 7
Display A/D Converters ..... 7-3
TSC500 Analog Processor for Microprocessor-Based A/D Converters ..... 7-5
TSC805 3 1/2 Digit Auto-Ranging A/D Converter ..... 7-7
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TSC14433A Precision 3 1/2 Digit ADC with Multiplexed BCD Output ..... 7-153
TSC14433B Low Cost 3 1/2 Digit ADC with Multiplexed BCD Output ..... 7-159
TSC14433 3 1/2 Digit ADC with Multiplexed BCD Output ..... 7-165

## General Description

The TSC500 allows Microprocessor-Based A/D Converters for Display that offer many more features than an applica-tion-specific ADC can. See page 8-3 for complete details.

## Applications

- The TSC500 Offers Flexibility!
- Under Software Control the User Selects:
- Speed
- Resolution
- Offset Correction
- Transfer Function (Output/Input)
- Leading to End Products Featuring:
- Auto-Ranging
- Auto-Tare (Scales)
- Transducer Linearization
- Complex Functions
- Intelligence


## Features

- 4 Phase Dual Slope Converter Subsystem
- Auto-Zero Phase
- Signal Integrate Phase
- Reference Integrate Phase
- Integrator Zero Phase
- Fast Overload Recovery
- Excellent Linearity 0.005\%
- Low Power .................... 10 mW @ $\pm 5 \mathrm{~V}$ Supplies
- High Input Sensitivity .............................. $100 \mu \mathrm{~V}$
- Differential Analog Input
- Differential Reference Input for Ratiometric Measurement
- Low Input Current ........................... 15 pA Max.


[^1]
## General Description

The TSC805 is a $31 / 2$ digit integrating analog-to-digital converter with triplex LCD display drive and automatic ranging. Input voltage/ohm attenuators ranging from 1 to $1 / 10,000$ are automatically selected. Five full-scale ranges are provided. The CMOS TSC805 contains all the logic and analog switches needed to manufacture an auto-ranging instrument for ohms and voltage measurements. User selected 20 mA and 200 mA current ranges are available. Full-scale range and decimal point LCD annunciators are automatically set in auto-range operation. Auto-range operation is available during ohms (high and low power ohms) and voltage (AC \& DC) measurements. Auto-ranging eliminates expensive range switches in hand-held DMM designs and makes compact meters easier and less costly to design. The auto-range feature may be bypassed allowing decimal point selection and input attenuator selection control through a single line input. Expensive rotary switches are not required.

During manual mode operation resolution is extended to 3000 counts full-scale. The extended range operation is indicated by a flashing 1 MSD. The extended resolution is available during $2000 \mathrm{k} \Omega$ and 2000 V full-scale auto-range operation also.

The memory mode subtracts a reading - up to $\pm 5 \%$ of fullscale - from subsequent measurements. Typical applications involve probe resistance compensation for resistance measurements, tolerance measurements, and tare weight measurement.

The TSC805 includes and AC to DC converter for AC measurements. Only external diodes/resistors/capacitors are required.

A complete LCD annunciator set describes the TSC805 meter function and measurement range during ohms, voltage and current operation. AC measurements are indicated as well as auto-range operation. A low battery detection circuit also sets the low battery display annunciator. The triplex LCD display drive levels may be set and temperature compensation applied via the VoIsp pin.

The "low ohms" measurement option allows in circuit resistance measurements by preventing semiconductor junctions from being forward biased.

A continuity buzzer output is activated with inputs less than $1 \%$ of full-scale. An overrange input signal also enables the buzzer, except during resistance measurements, and flashes the MSD display. Featuring single 9 V battery operation, 10 mW power consumption, a precision internal voltage reference (75 $\mathrm{ppm} /{ }^{\circ} \mathrm{C}$ max. TC) and a compact surface mounted 60 -pin quad flat package, the TSC805 is ideal for portable instruments.

## Features

- Auto-Range Operation for AC \& DC Voltage and Resistance Measurements
- Two User Selected AC/DC Current Ranges 20 \& 200 mA
- 22 Operating Ranges
- 9 DC/AC Voltage
- 4 AC/DC Current
- 9 Resistance and Low Power Ohms
- Low Cost Switches Control Operation
- 3 1/2 Digit Resolution in Auto-Range Mode .... 1/2000
- Extended Resolution in Manual Mode ........ 1/3000
- Memory Mode for Relative Measurements ... $\pm 5 \%$ F.S.
- Internal AC to DC Conversion Op Amp
- Triplex LCD Drive for Decimal Points, Digits and Annunciators
- Continuity Detection and Piezoelectric Transducer Driver
- Compact Surface Mounted 60-Pin Quad Flat Package
- Low Drift Internal Reference ................. $75 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$
- 9 V Battery Operation
- Low Battery Detection and LCD Annunciator
- Low Power CMOS

10 mW

## Ordering Information

| Part. No. | Package | Temp. <br> Range |
| :--- | :--- | ---: |
| TSC805CBQ | 60-Pin Plastic Quad <br> Flat Package <br> Formed Leads | $0^{\circ} \mathrm{C}$ to $70^{\circ} \mathrm{C}$ |
| TSC805CSQ | 60-Pin Plastic Quad <br> Flat Package <br> Straight Leads | $0^{\circ} \mathrm{C}$ to $70^{\circ} \mathrm{C}$ |

Pin Configuration


# 3 1/2 Digit Auto-Ranging Analog-to-Digital Converter - Triplex LCD Drive - Low Power CMOS 

## Absolute Maximum Ratings

| Supply Voltage ( $\mathrm{V}^{+}$to $\mathrm{V}^{-}$) | 15 V | Storage Temperature |
| :---: | :---: | :---: |
| Analog Input Voltage | $\mathrm{V}^{+}$to $\mathrm{V}^{-}$ | Lead Temperature (Soldering, 60 sec.$)$. ........... $300^{\circ} \mathrm{C}$ |
| Reference Input Voltage | $\ldots \mathrm{V}^{+}$to $\mathrm{V}^{-}$ | Stresses above those listed under Absolute Maximum Ratings may |
| Voltage at Pin 43 | GND $\pm 0.7 \mathrm{~V}$ | permanent damage to the device. These are stress ratings only and functional |
| Power Dissipation Plastic Package | 800 mW | operation of the device at these or any other conditions above those indicated in the operational sections of the specifications is not implied. Exposure to |
| Operating Temperature |  | Absolute Maximum Rating Conditions for extended periods may effect device reliability. |

Electrical Characteristics: $V_{S}=9 \mathrm{~V}, T_{A}=25^{\circ} \mathrm{C}$, Figure 1 Test Circuit

| NO. | SYMBOL | PARAMETER | TEST CONDITIONS | MIN | $\begin{gathered} \hline \text { SC805 } \\ \text { TYP } \end{gathered}$ | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 |  | Zero Input Reading | 200 mV Range w/o $10 \mathrm{M} \Omega$ Input Resistor | -0000 | $0000+$ | +0000 | Digital Reading |
|  |  |  | 200 mV Range w/10 M $\Omega$ Input | -0001 | - + | +0001 |  |
|  |  |  | 20 mA and 200 mA Range | -0000 | $0000+$ | +0000 |  |
| 2 | RE | Rollover Error | 200 mV Range $\mathrm{w} / \mathrm{o} 10 \mathrm{M} \Omega$ Input Resistor | - | - | $\pm 1$ | Count |
|  |  |  | 200 mV Range w/10 M $\Omega$ Input | - | - | $\pm 3$ |  |
|  |  |  | 20 mA and 200 mA Range | - | - | $\pm 1$ |  |
| 3 | NL | Linearity Error | Best Case Straight Line | - | - | $\pm 1$ | Count |
| 4 | lin | Input Leakage Current |  | - | - | 10 | pA |
| 5 | En | Input Noise | $\mathrm{BW}=0.1$ to 10 Hz | - | 20 | - | $\mu V_{p-p}$ |
| 6 |  | AC Frequency Response | $\pm 1 \%$ Error | - | 40 to 500 - |  | Hz |
|  |  |  | $\pm 5 \%$ Error | - | 40 to 2000 - |  |  |
| 7 |  | Open Circuit Voltage for OHM Measurements | Excludes $200 \Omega$ Range | - | 570 | 660 | mV |
| 8 |  | Open Circuit Voltage for LO OHM Measurement | Excludes $200 \Omega$ Range | - | 285 | 350 | mV |
| 9 | Vcom | Analog Common Voltage | $\left(\mathrm{V}^{+}-\mathrm{Vcom}\right)$ | 2.5 | 2.6 | 3.3 | V |
| 10 | Vстс | Common Voltage Temperature Coefficient |  | - | - | 50 | ppm $/{ }^{\circ} \mathrm{C}$ |
| 11 |  | Display Multiplex Rate |  | - | 100 | - | Hz |
| 12 | VIL | Low Logic Input | $\overline{20 \mathrm{~mA}}, \overline{\mathrm{AC}}, \mathrm{I}, \overline{\mathrm{LOW} \Omega}$, <br> Range, $-\overline{\mathrm{MEM}}, \overline{\mathrm{OHMS}}$ <br> (Relative to DIG GND Pin 56) | - | - | 1 | V |
| 13 |  | Logic 1 Pull Up Current | $\overline{20 \mathrm{~mA}}, \overline{\mathrm{AC}}, \mathrm{I}, \overline{\text { Low } \Omega}$, Range, - $\overline{\mathrm{MEM}}, \overline{\mathrm{OHMS}}$ (Relative to DIG GND Pin 56) | - | 25 | - | $\mu \mathrm{A}$ |
| 14 |  | Buzzer Drive Frequency |  | - | 4 | - | kHz |
| 15 |  | Low Battery Flag Voltage | Vcc to Vssa | 6.3 | 6.6 | 7.0 | V |
| 16 |  | Operating Supply Current |  | - | 0.8 | 1.5 | mA |

## Note:

1. $200 \Omega$ range open circuit voltage approximately 2.8 V .

## Pin Description and Function Table 1:

| PIN NO. (Quad Flat Package) | SYMBOL | DESCRIPTION |
| :---: | :---: | :---: |
| 1 | $\overline{\mathrm{OHM}}$ | Logic Input. "0" (Digital Ground) for resistance measurement. |
| 2 | $\overline{20 \mathrm{~mA}}$ | Logic Input. "0" (Digital Ground) for 20 mA full-scale current measurement. |
| 3 | $B \cup Z$ | Audio frequency, 4 kHz , output for continuity indication during resistance measurement. A noncontinuous 4 kHz signal is output to indicate an input overrange during voltage or current measurements. |
| 4 | XTAL1 | 32.768 kHz Crystal Connection. |
| 5 | XTAL2 | 32.768 kHz Crystal Connection. |
| 6 | VDISP | Sets peak LCD drive signal: VP = VCC-VDISP. VDISP may also be used to compensate for temperature variation of LCD crystal threshold voltage. |
| 7 | BP1 | LCD Backplane \#1. |
| 8 | BP2 | LCD Backplane \#2. |
| 9 | BP3 | LCD Backplane \#3. |
| 10 | Low $\Omega$ / A | LCD Annunciator segment drive for low ohms resistance measurement and current measurement. |
| 11 | $\Omega / \mathrm{V}$ | LCD Annunciator segment drive for resistance measurement and voltage measurement. |
| 12 | K/m | LCD Annunciator segment drive for k ("kilo-ohms") and m ("milli-amps" and "milli-volts"). |
| 13 | $\begin{gathered} \text { BCPO } \\ \text { (Ones digit). } \end{gathered}$ | LCD segment drive for "b," "c" segments and decimal point of least significant digit (LSD). |
| 14 | AGD0 | LCD segment drive for "a," "g," "d" segments of LSD. |
| 15 | FEO | LCD segment drive for " $f$ " and "e" segments of LSD. |
| 16 | BCP1 | LCD segment drive for "b," "c" segments and decimal point of 2nd LSD. |
| 17 | AGD1 | LCD segment drive for "a," "g," "d" segments of 2nd LSD (Ten's digit). |
| 18 | FE1 | LCD segment drive for "f," and "e" segments of 2nd LSD. |
| 19 | BCP2 | LCD segment drive for "b," "c," and decimal point of 3rd LSD. (Hundreds digit). |
| 20 | AGD2 | LCD segment drive for "a," "g," "d" segments of 3rd LSD. |
| 21 | FE2 | LCD segment drive for "b" and "c" segments of 3rd LSD. |
| 22 | BCP3 | LCD segment drive for "b," "c" segments and decimal point of MSD (Thousand's digit). |
| 23 | AC/-/AUTO | LCD annunciator drive signal for AC measurements, polarity, and auto-range operation. |
| 24 | -MEM/BATT mode. | LCD annunciator drive signal for low battery indication and memory (relative measurement) |
| 25 | VSSD | Negative battery supply connection for internal digital circuits. Connect to negative terminal of battery. |
| 26 | VCC | Positive battery supply connection. |
| 27 | COM | Analog circuit ground reference point. Nominally 2.6 V below VCC. |
| 28 | RMREFH | Ratiometric (Resistance measurement) reference high voltage. |
| 29 | RMREFL | Ratiometric (Resistance measurement) reference low voltage. |
| 30 | CREFL | Reference capacitor negative terminal CREF $=0.1 \mu \mathrm{f}$. |
| 31 | CREFH | Reference capacitor positive terminal CREF $=0.1 \mu \mathrm{f}$. |
| 32 | REFHI | Reference voltage for voltage and current measurement. Nominally 163.85 mV . |
| 33 | תR1 | Standard resistor connection for $200 \Omega$ full-scale. |
| 34 | $\Omega$ R2 | Standard resistor connection for $2000 \Omega$ full-scale. |

## 3 1/2 Digit Auto-Ranging Analog-to-Digital Converter - Triplex LCD Drive <br> - Low Power CMOS

TSC805

## Pin Description and Function Cont.

PIN NO.
(Quad Flat
Package) SYMBOL DESCRIPTION

| 35 | $\Omega$ R3 | Standard resistor connection for $20 \mathrm{k} \Omega$ full-scale range. |
| :---: | :---: | :---: |
| 36 | תR4 | Standard resistor connection for $200 \mathrm{k} \Omega$ full-scale range. |
| 37 | $\Omega$ R5 | Standard resistor connection for $2000 \mathrm{k} \Omega$ full-scale range. |
| 38 | VR3 | Voltage measurement $\div 100$ attenuator. |
| 39 | VR2 | Voltage measurement $\div 10$ attenuator. |
| 40 | VR5 | Voltage measurement $\div 10,000$ attenuator. |
| 41 | VR4 | Voltage measurement $\div 1000$ attenuator. |
| 42 | $V_{1}$ | Unknown voltage input $\div 1$ attenuator. |
| 43 | 11 | Unknown current input. |
| 44 | ACVL | Low output of AC to DC converter. |
| 45 | COMP | Comparator output. |
| 46 | Cl | Integrator capacitor connection. Nominally $0.1 \mu \mathrm{f}$. (Low dielectric absorption. Polypropylene dielectric suggested). |
| 47 | CAZ | Auto-zero capacitor connection. Nominally $0.1 \mu$ f. |
| 48 | Rx | Unknown resistance input. |
| 49 | CFI | Input filter connection. |
| 50 | ADI | Negative input of internal AC to DC operational amplifier. |
| 51 | ADO | Output of internal AC to DC operational amplifier. |
| 52 | R $\Omega$ BUF | Active buffer output for resistance measurement. Integration resistor connection. Integrator resistor nominally $220 \mathrm{k} \Omega$. |
| 53 | RVIBUF | Active buffer output for voltage and current measurement. Integration resistor connection. Integration resistor nominally $150 \mathrm{k} \Omega$. |
| 54 | ACVH | Positive output of AC to DC converter. |
| 55 | VSSA | Negative supply connection for analog circuits. Connect to negative terminal of 9 V battery. |
| 56 | DIG GND | Internal logic digital ground. The logic " 0 " level. Nominally 4.7 V below VCC. |
| 57 | RANGE | Input to set manual operation and change ranges. |
| 58 | MEM | Input to enter memory measurement mode for relative measurements. The two LSD's are stored and subtracted from future measurements. |
| 59 | $\frac{\mathrm{DC} / \overline{\mathrm{AC}}_{1}}{\Omega / \mathrm{LOW} \Omega}$ | Input that selects AC or DC option during voltage/current measurements. For resistance measurements, the ohms or low power (voltage) ohms option can be selected. |
| 60 | T | Input to select current measurement. Set to logic "0" (Digital ground) for current measurement. |



3 1/2 Digit Auto-Ranging
Analog-to-Digital Converter

- Triplex LCD Drive
- Low Power CMOS


Figure 2: TSC805 Analog Section

## 3 1/2 Digit Auto-Ranging Analog-to-Digital Converter - Triplex LCD Drive <br> - Low Power CMOS

causes the TSC805 to return to auto-ranging operation. The "Auto" LCD annunciator driver is active only in the autorange mode.
Table 5 shows typical operation where the manual range selection option is used. Also shown is the extended resolution display format.

## Extended Resolution Manual Operation

The TSC805 extends resolution by $50 \%$ when operated in the manual range select mode for current, voltage, and resistance measurements. Resolution increases to 3000 counts from 2000 counts. The extended resolution feature operates only on the $2000 \mathrm{k} \Omega$ and 2000 V ranges during auto-range operation.
In the extended resolution operating mode readings above 1999 are displayed with a blinking "1" most significant digit. The blinking "1" should be interpreted as the digit 2. The three least significant digits display data normally.

An input overrange condition causes the most significant digit to blink and sets the three least significant digits to display " 000 ". The buzzer output is enabled for input voltage and current signals with readings greater than 2000 counts in both manual and auto-range operation.
For resistance measurements the buzzer signal does not indicate an overrange condition. The buzzer is used to indicate continuity. Continuity is defined as a resistance reading less than 19 counts.

Table 5: Manual Range Operation

| INPUT |  | DC VOLTS |  | AC VOLTS |  | OHM |  | LO OHM |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 23.5 V |  | 18.2 V |  | $18.2 \mathrm{k} \Omega$ |  | $2.35 \mathrm{M} \Omega$ |  |
| POWER-ON <br> AUTO-RANGE OPERATION |  | RANGE | DISPLAY | RANGE | DISPLAY | RANGE | DISPLAY | RANGE | DISPLAY |
|  |  | 200 mV | "1"00.0 mV | 2 V | "1".000 V | $200 \Omega$ | "1"00.0 $\Omega$ | $2 \mathrm{k} \Omega$ | "1".000 k $\Omega$ |
|  |  | 2 V | " 1 ".000 V | 20 V | 18.20 V | $2 \mathrm{k} \Omega$ | "1". $000 \mathrm{k} \Omega$ | $10 \mathrm{k} \Omega$ | " 1 "0.00 k $\Omega$ |
|  |  | 20 V | "1"0.00 V |  |  | $20 \mathrm{k} \Omega$ | $18.20 \mathrm{k} \Omega$ | $200 \mathrm{k} \Omega$ | " 1 "00.0 k $\Omega$ |
|  |  | 200 V | 23.5 V |  |  |  |  | $2000 \mathrm{k} \Omega$ | "1"350 k $\Omega$ |
| \# of RANGE CHANGES 几- |  |  |  |  |  |  |  |  |  |
| $\begin{array}{ll}  & O \\ M & P \\ A & E \\ A & E \\ N & R \\ U & A \\ A & T \\ L & 1 \\ & O \\ & N \end{array}$ | ـ | RANGE | DISPLAY | RANGE | DISPLAY | RANGE | DISPLAY | RANGE | DISPLAY |
|  | 1 | 200 V | 23.5 V | 20 V | 18.20 V | $20 \mathrm{k} \Omega$ | $18.20 \mathrm{k} \Omega$ | $2000 \mathrm{k} \Omega$ | "1"350 k $\Omega$ |
|  | 2 | 200 mV | "1"00.0 mV | 2 V | "1".000 V | $200 \Omega$ | "1"00.0 $\Omega$ | $2 \mathrm{k} \Omega$ | "1".000 k $\Omega$ |
|  | 3 | 2 V | 1.000 V | 20 V | 18.20 V | $2 \mathrm{k} \Omega$ | "1".000 k $\Omega$ | $20 \mathrm{k} \Omega$ | "1"0.00 k $\Omega$ |
|  | 4 | 20 V | "1"3.50 V | 200 V | 18.2 V | $20 \mathrm{k} \Omega$ | $18.20 \mathrm{k} \Omega$ | $200 \mathrm{k} \Omega$ | "1"00.0 k $\Omega$ |
|  | 5 | 200 V | 23.5 V | 600 V | 19 V | $200 \mathrm{k} \Omega$ | $18.2 \mathrm{k} \Omega$ | $2000 \mathrm{k} \Omega$ | "1"350 k |
|  | 6 | 1000 V | 24 V | 2 V | "1".000 V | $2000 \mathrm{k} \Omega$ | $19 \mathrm{k} \Omega$ | $2 \mathrm{k} \Omega$ | " 1 ".000 k $\Omega$ |
|  | 7 | 200 mV | "1"00.0 mV | 20 V | 18.20 V | $200 \Omega$ | "1"'00.0 $\Omega$ | $20 \mathrm{k} \Omega$ | " 1 "0.00 k $\Omega$ |
|  | 8 | 2 V | "1".000 V | 200 V | 18.2 V | $2 \mathrm{k} \Omega$ | "1".000 k $\Omega$ | $200 \mathrm{k} \Omega$ | "1"00.0 k $\Omega$ |

## Notes:

1. A flashing MSD is shown as a "1". A flashing MSD indicates the TSC805 is over-ranged if all other digits are zero.
2. The first manual range selected is the last range in the auto-ranging mode.
3. A flashing MSÚ with a non-zero display indicates the TSC805 has entered the extended resolution operating mode. An additional 1000 counts of resolution is available. This extended operation is avallable only in manual operation for voltage, resistance and current measurements.
4. $\square=$ momentary ground connection.


Example: 200 k $\Omega$ Full-Scale Measurement
(a) $\quad V R=\frac{163.85 \mathrm{k} \Omega}{163.85+220+R X} \times 0.64$
(b) $V X=\frac{R X}{163.85 \mathrm{k} \Omega+220 \Omega} \times 0.64$
(c) "Ramp Up Voltage" = "Ramp Down Voltage"

$$
\therefore \quad \frac{V X}{R_{1} C_{l}} \times T_{1}=\frac{V R}{R_{l} C_{l}} T D E
$$

Where:
$R_{I}=$ Integrating Resistor, $T_{I}=$ Integrate Time
$C_{I}=$ Integrating Capacitor, $T_{D E}=$ Deintegrate Time
(d) $R X=163.85\left(\frac{T_{D E}}{T_{I}}\right)$

Independent of RI, Cl or Internal Voltage Reference
Figure 4: Resistance Measurement Accuracy Set by External Standard Resistor


$$
\begin{aligned}
& \text { External Crystal }=32.768 \mathrm{kHz} \\
& \text { Internal Clock Period }=T p=2 / 32.768=61.04 \mu \mathrm{~s} \\
& \text { Total Conversion Time }=T \text { Tconv }=8000(T p) \\
& =488.3 \mathrm{~ms} \approx 2 \mathrm{CONV} / \mathrm{SEC} \\
& \text { Integration Time }=T_{I}=1638.5(\mathrm{Tp})=100.0 \mathrm{~ms} \\
& \text { Maximum Reference Deintegrate Time } \\
& =T D E=3000(T p)=183.1 \mathrm{~ms} \text { (Manual, Extended Resolution) } \\
& =2000(T p)=122.1 \mathrm{~ms} \text { (Auto-Range) } \\
& \text { Minimum Auto-Zero Time } \\
& =(8000-3000-1638.5) \quad(T p)=205.1 \mathrm{~ms} \text { (Manual, Extended } \\
& =(8000-2000-1638.5) \quad(T p)=266.2 \mathrm{~ms} \text { (Auto-Range) }
\end{aligned}
$$

Figure 5: Basic TSC805 Conversion Timing

## Measurement Options AC to DC Measurements

In voltage and current measurements the TSC805 can be configured for AC measurements. An on chip operational amplifier and external rectifier components perform the AC to DC conversion.
When power is first applied the TSC805 enters the DC measurement mode. For AC measurements (current or voltage), $\overline{\mathrm{AC}} / \mathrm{DC}$ (Pin 59) is momentarily brought low to digital ground potential; the TSC805 sets-up for AC measurements and the $A C$ liquid crystal display annunciator activates. Toggling $\overline{A C} / D C$ low again will return the TSC805 to DC operation.
If the manual operating mode has been selected toggling AC/DC will reset the TSC805 back to the auto-range mode. In manual mode operation AC or DC operation should be selected first and then the desired range selected.

The minimum $A C$ voltage full-scale voltage range is 2 V . The DC full-scale minimum voltage is 200 mV .
AC current measurements are available on the 20 mA and 200 mA full-scale current range.

## Conversion Timing

The TSC805 analog-to-digital converter uses the conventional dual slope integrating conversion technique with an added phase that automatically eliminates zero offset errors. The TSC805 gives a zero reading with a zero volt input.
The TSC805 is designed to operate with a 32.768 kHz crystal. The 32 kHz crystal is low cost and readily available; it serves as a time base oscillator crystal in many digital clocks. (See External Crystal Sources.)
The external clock is divided by two. The internal clock frequency is 16.348 kHz giving a clock period of $61.04 \mu \mathrm{~s}$. The total conversion - auto-zero phase, signal integrate and

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TSC805


Figure 3: Ratiometric Resistance Measurement Functional Diagram

## Voltage Measurement

Resistive dividers are automatically changed to provide in range readings for 200 mV to 2000 V full-scale readings (Figure 2). The input resistance is set by external resistors R14/R13. The divider leg resistors are R9-R12. The divider leg resistors give a 200 mV signal at VI (Pin 42) for full-scale voltages from 200 mV to 2000 V .

For applications which do not require a $10 \mathrm{M} \Omega$ input impedance the divider network impedances may be lowered. This will reduce voltage offset errors induced by switch leakage currents.

## Current Measurement

The TSC805 measures current only under manual range operation. The two user selectable full-scale ranges are: 20 mA and 200 mA . Select the current measurement mode by holding the Tinput (Pin 60) low at digital ground potential

The OHM input (Pin 1) is left floating or tied to the positive supply.
Two ranges are possible. The 20 mA full-scale range is selected by connecting the $\overline{20 \mathrm{~mA}}$ input (Pin 2) to digitai ground. If left floating the 200 mA full-scale range is selected.
External current to voltage conversion resistors are used at the II input (Pin 43). For 20 mA measurements a $10 \Omega$ resistor is used. the 200 mA range needs a $1 \Omega$ resistor. Full-scale is 200 mV .

PC board trace resistance between analog common and R16 (See Figure 1) must be minimized. In the 200 mA range, for example, a $0.05 \Omega$ trace resistance will cause a $5 \%$ current to voltage conversion error at II (Pin 43).

The extended resolution measurement option operates during current measurements.

To minimize rollover error the potential difference between analog common (Pin 27) and system common must be minimized.

## Resistance, Voltage, Current Measurement Selection

The TSC805 is designed to measure voltage, current, and resistance. Auto-ranging is available for resistance and voltage measurements. The $\overline{O H M S}$ (Pin 1) and I (Pin 60) input controls are normally pulled internally to Vcc.
By tying these pins to Digital Ground (Pin 56), the TSC805 is configured internally to measure resistance, voltage, or current. The required signal combinations are shown in Table 2.

Table 2: TSC805 Measurement Selection Logic

| Function Select Pin |  |  |
| :---: | :---: | :--- |
| $\overline{\text { OHM }(\text { Pin 1) }}$ | $\overline{\boldsymbol{T}}($ Pin 60) | Selected Measurement |
| 0 | 0 | Voltage |
| 0 | 1 | Resistance |
| 1 | 0 | Current |
| 1 | 1 | Voltage |

$0=$ Digital Ground
1 = Floating or Tied to Vcc
Notes:

1. $\overline{\mathrm{OHM}} \& T$ are normally pulled internally high to VCC (Pin 26).

This is considered a logic "1."
2. Logic " 0 " is the potential at digital ground (Pin 56).

## Resistance Measurements OHMS \& Low Power OHMS

The TSC805 can be configured to reliably measure in-circuit resistances shunted by semiconductor junctions. The TSC805 low power ohms measurement mode limits the probe open circuit voltage. This prevents semiconductor junctions in the measured system from turning on.
In the resistance measurement mode the $\Omega / \overline{\mathrm{LOW} \Omega}$ (Pin 59) input selects the low power ohms measurement mode. For low power ohms measurements $\Omega / \overline{\text { LOW }}$ (Pin 59) is momentarily brought low to digital ground potential. The TSC805 sets up for a low power ohms measurement with a maximum open circuit probe voltage of 0.35 V above analog common. In the low power ohms mode an LCD display annunciator, LOW $\Omega$, will be activated. On power up the low power ohms mode is not active.
If the manual operating mode has been selected, toggling $\Omega / \overline{L O W} \Omega$ will reset the TSC805 back to the auto-range mode. In manual mode, the decision to make a normal or low power ohms measurement should be made before selecting the desired range.

The low power ohms measurement is not available on the $200 \Omega$ full-scale range. Open circuit voltage on this range is below 2.8 V .

The standard resistance values are listed in Table 3.
Table 3: Ohms Range Ladder Network

| Full-Scale <br> Range | Standard <br> Resistance | Low Power <br> Ohms Mode |
| :--- | :--- | :---: |
| $200 \Omega$ | $163.85 \Omega$ (R1) | NO |
| $2000 \Omega$ | $1638.5 \Omega$ (R2) | YES |
| $20 \mathrm{k} \Omega$ | $16,358 \Omega$ (R3) | YES |
| $200 \mathrm{k} \Omega$ | $163850 \Omega$ (R4) | YES |
| $2,000 \mathrm{k} \Omega$ | $1,638,500 \Omega$ (R5) | YES |

$\mathrm{N} / \mathrm{A}=$ Not available.
R8, a positive temperature coefficient resistor, and the 6.2 V zener, Z1 in Figure 1 provide input voltage protection during ohms measurements.

## Ratiometric Resistance Measurements

The TSC805 measures resistance ratiometrically. Accuracy is set by the external standard resistors connected to Pin 33 through 37. A low-power ohms mode may be selected on all but the $200 \Omega$ full-scale range. The low power ohms mode limits the voltage applied to the measured system. This allows accurate "in-circuit" measurements when a resistor is shunted by semiconductor junctions.
Full auto-ranging is provided. External precision standard resistors are automatically switched to provide the proper range.
Figure 3 shows a detailed block diagram of the TSC805 configured for ratiometric resistance measurements. During the signal integrate phase the reference capacitor charges to a voltage inversely proportional to the measured resistanceRX. Figure 4 shows the conversion accuracy relies on the accuracy of the external standard resistors only.
Normally the required accuracy of the standard resistances will be dictated by the accuracy specifications of the users end product. Table 4 gives the equivalent ohms per count for various full-scale ranges to allow users to judge the required resistor accuracy.

Table 4: Reference Resistors

| Full-Scale <br> Range | Reference <br> Resisior | $\Omega /$ COUNT |
| :--- | :--- | :---: |
| 200 | 163.85 | 0.1 |
| 2 k | 1638.5 | 1 |
| 20 k | 16385 | 10 |
| 200 k | 163850 | 100 |
| 2 M | 1638500 | 1000 |

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Figure 6: Manual Range Selection; Resistance Measurement


Figure 7: Manual Range Selection; Current Measurement

## -MEM Operating Mode

Bringing $\overline{\mathrm{MEM}}$ (Pin 58) momentarily low configures the TSC805 "-MEM" operating mode. The -MEM LCD Annunciator becomes active. In this operating mode subsequent measurements are made relative to the last two digits ( $\leq 99$ ) displayed at the time MEM is low. This represents $5 \%$ of fullscale. The last two significant digits are stored and subtracted from all the following input conversions.

TSC805


Figure 8: Manual Range Selection; Voltage Measurement

A few examples clarify operation:

## Example 1: In Auto-Ranging

$\mathrm{Ri}(\mathrm{N})=18.21 \mathrm{k} \Omega(20 \mathrm{k} \Omega$ Range $)=>$ Display $18.21 \mathrm{k} \Omega$ $\overline{\text { MEM }}$ L- $=>$ Store $0.21 \mathrm{k} \Omega$
$\operatorname{Ri}(\mathrm{N}+1)=19.87 \mathrm{k} \Omega$ ( $20 \mathrm{k} \Omega$ Range) $=>$ Display 19.87-0.21 $=19.66 \mathrm{k} \Omega$
Ri $(\mathrm{N}+2)=22.65 \mathrm{k} \Omega$ ( $200 \mathrm{k} \Omega$ Range) = > Display $22.7 \mathrm{k} \Omega$ \& $\overline{\mathrm{MEM}}$ Disappears
Example 2: In Fixed Range $200.0 \Omega$ Full-Scale
Ri $(N)=18.2 \Omega=>$ Display $18.2 \Omega$
$\overline{\text { MEM }} \sim$ _ $=>$ Store $8.2 \Omega$
$\mathrm{Ri}(\mathrm{N}+1)=36.7 \Omega$
$=>$ Display 36.7-8.2 $=28.5 \Omega$
Ri $(N+2)=5.8 \Omega$

$$
\Rightarrow>\text { Display } 5.8-8.2=-2.4 \Omega^{*}
$$

* Will display minus resistance if following input is less than offset stored at fixed range

Example 3: In Fixed Range 20.00 V Full-Scale
Vi $(\mathrm{N})=0.51 \mathrm{~V}=>$ Display 0.51 V
$\overline{\mathrm{MEM}}$ 几 $=>$ Store 0.51 V
$\mathrm{Vi}(\mathrm{N}+1)=3.68 \mathrm{~V}$
$=>$ Display $3.68-0.51=3.17 \mathrm{~V}$
$\mathrm{Vi}(\mathrm{N}+2)=0.23 \mathrm{~V}$

$$
\Rightarrow>\text { Display } 0.23-0.51=-0.28 \mathrm{~V}
$$

$\mathrm{Vi}(\mathrm{N}+3)=-5.21 \mathrm{~V}$
$=>$ Display $-5.21-0.51=-5.72 \mathrm{~V}$

On Power up the TSC805 "-MEM" mode is not active. Once the "-MEM" is entered bringing $\overline{M E M}$ low again it returns the TSC805 to normal operation.
The "-MEM" mode is also cancelled whenever the measurement type (resistance, voltage, current, $\overline{\mathrm{AC}} / \mathrm{DC}, \Omega / \overline{\mathrm{LOW} \Omega}$ ) or range is changed. The LCD -MEM annunciator will be off in normal operation.
In auto-range operation if the following input signal cannot be converted on the same range as the stored value, the "-MEM" mode is cancelled. The LCD annunciator is turned off.

The "-MEM" operating mode can be very useful in resistance measurements when lead length resistance would cause measurement errors.

## Automatic Range Selection Operation

When power is first applied the TSC805 enters the autorange operating state. The auto-range mode may be entered from manual mode by changing the measurement function (resistance or voltage) or by changing the measurement option ( $\overline{\mathrm{AC}} / \mathrm{DC}, \Omega / \overline{\mathrm{LO} \Omega}$ ).
The automatic voltage range selection begins on the most sensitive scale first: 200 mV for DC or 2.000 V for AC measurements. The voltage range selection flow chart is given in Figure 9.

Internal input protection diodes to VCC (Pin 26) and VSSA (Pin 55) clamp the input voltage. The external $10 \mathrm{M} \Omega$ input resistance (See Figure 1, R14 and R13) limits current safely in an overrange condition.
The voltage range selection is designed to maximize resolution. For input signals less than $9 \%$ of full-scale (count reading $<180$ ) the next most sensitive range is selected.

An overrange voltage input condition is flagged whenever the internal count exceeds 2000 by activating the buzzer output (Pin 3). This 4 kHz signal can directly drive a piezo electric acoustic transducer. An out of range input signal causes the 4 kHz signal to be on for 122 ms , off for 122 ms , on for 122 ms , and off for 610 ms (See Figure 15).
During voltage auto-range operation the extended resolution feature operates on the 2000 V range only (See extended resolution operating mode discussion).

The resistance automatic range selection procedure is shown in Figure 10. The $200 \Omega$ range is the first range selected unless the TSC805 low ohms resistance measurement option is selected. In low ohms operation the first full-scale range tried is $2 \mathrm{k} \Omega$.

The resistance range selected maximizes sensitivity. If the conversion results in a reading less than 180 the next most sensitive full-scale range is tried.
If the conversion is less than 19 in auto-range operation a continuous 4 kHz signal is output at BUZ (Pin 3). An overrange input does not activate the buzzer.

Out of range input conditions are displayed by a blinking most significant digit with the three least significant digits set to "000."
The extended resolution feature operates only on the $2000 \mathrm{k} \Omega$ and 2000 V full-scale range during auto-range operation. A blinking " 1 " most significant digit is interpreted as the digit 2. The three least significant digits display data normally.


Figure 9: Auto-Range Operation; Voltage Measurement


Figure 10: Auto-Range Operation; Resistance Measurement


Figure 11: Low Battery Detector

## Low Battery Detection Circuit

The TSC805 contains a low battery detector. When the 9 V battery supply has been depleted to a 7 V nominal value the LCD display low battery annunciator is activated.
The low battery detector is shown in Figure 11. The low battery annunciator is guaranteed to remain OFF with the battery supply greater than 7.0 V . The annunciator is guaranteed to be ON before the supply battery has reached 6.3 V .

## Triplex Liquid Crystal Drive

The TSC805 directly drives a triplexed liquid crystal display (LCD) using $1 / 3$ bias drive. All data, decimal point, polarity and function annunciator drive signals are developed by the TSC805. A direct connection to a triplex LCD display is possible without external drive electronics. Standard and custom LCD displays are readily available from LCD manufacturers.

The LCDs must be driven with an AC signal having a zero DC component for long display life. The liquid crystal polarization is a function of the RMS voltage appearing across the backplane and segment driver. The peak drive signal applied to the LCD is: VCC-VDISP.
If VDISP, for example, is set at a potential 3 V below VCC the peak drive signal is:

$$
V p=V C C-V D I S P=3 V
$$

An "OFF" LCD segment has an RMS voltage of $\mathrm{Vp} / 3$ across it or 1 volt. An "ON" segment has a 0.63 Vp signal across it or 1.92 V for VCC-VDISP $=3 \mathrm{~V}$.

Since the VDISP pin is available the user may adjust the "ON" and "OFF" LCD levels for various manufacturer's displays by changing Vp. Liquid crystal threshold voltage moves down with temperature.


Figure 12: 1/3 Bias LCD Drive

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"OFF" segments may become visible at high LCD operating temperatures. A voltage with a -5 to $-20 \mathrm{mV} /{ }^{\circ} \mathrm{C}$ temperature coefficient can be applied to VDISP to accommodate the liquid crystal temperature operating characteristics if necessary.
The TSC805 internally generates two intermediate LCD drive potentials ( $\mathrm{V}_{\mathrm{H}} \& \mathrm{~V}_{\mathrm{L}}$ ) from a resistive divider (Figure 12) between VCC (Pin 26) and VDISP (Pin 6). The ladder impedance is approximately $150 \mathrm{k} \Omega$. This drive method is commonly known as $1 / 3$ bias. With VDISP connected to digital ground $V_{P} \approx 5.0 \mathrm{~V}$.
The intermediate levels are needed so that drive signals giving RMS "ON" and "OFF" levels can be generated. Figure 13 shows a typical drive signal and the resulting wave forms for "ON" and "OFF" RMS voltage levels across a selected LCD element.

## LCD Displays

Although most users will design their own custom LCD display, several manufacturers offer standard displays for the TSC805. Figure 14 shows a typical display available from Varitronix.

1. Varitronix Ltd.

9/F Liven House, 61-63, King Yip Street
Kwun Tjong, Hong Kong
Tel: 3-410286
TELEX: 36643 VTRAX HX
Part No.: VIM 309-1 Pin Connector
VIM 309-2 Elastomer Connector
USA OFFICE:
VL Electronics Inc.
2775 Glendower Ave.
Los Angeles, CA 90027
Tel. (213) 661-8883
TELEX: 821554
2. Adamant Kogyo Co., LTD.

16-7, Shinden, 1-Chome, Adachi-Ku, Tokyo, 123, Japan Tel: Tokyo 919-1171


Figure 13: Triplex LCD Drive Waveforms


Flgure 14: Typical LCD Display Configuration TSC805 Triplex

## "Buzzer" Drive Signal

The TSC805 BUZ output (Pin 3) will drive a piezo electric audio transducer. The signal is activated to indicate an input overrange condition for current and voltage measurements or continuity during resistance measurements.
During a resistance measurement a reading less than 19 on any full-scale range causes a continuous 4 kHz signal to be output. This is used as a continuity indication.
A voltage or current input measurement overrange is indicated by a non-continuous 4 kHz signal at the BUZ output. The LCD display MSD also flashes and the three least significant digits are set to display zero. The buzzer drive signal for overrange is shown in Figure 15. The buzzer output is active for any reading over 2000 counts in both manual and autorange operation. The buzzer is activated during an extended resolution measurement.
The BUZ signal swings from VCC (Pin 26) to Digital Ground (Pin 56). The signal is at VCC when not active.
The buz output is also activated for 15 ms whenever a range change is made in auto-range or manual operation. Changing the type of measurement (voltage, current, or resistance) or measurement option ( $\overline{A C} / D C, \Omega / \overline{L O N}$ ) will also activate the buzzer output for 15 ms . A range change during a current measurement will not activate the buzzer output.

| PAD | BP1 | BP2 | 8P3 | PAD | COM1 | COM2 | COM3 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | BP1 | 1 | 1 | 19 | 1 | 1 | 1 |
| 2 | 1 | BP2 | , | 20 | 1 | 1 | 1 |
| 3 | 1 | 1 | BP3 | 21 | 1 | , | 1 |
| 4 | 1 | LOS | A | 22 | , | , | 1 |
| 5 | 1 | $\Omega$ | v | 23 | 1 | 1 | 1 |
| 6 | 1 | k | m | 24 | , | 1 | 1 |
| 7 | b1 | c1 | 1 | 25 | 1 | , | 1 |
| 8 | a1 | 81 | d1 | 26 | , | 1 | 1 |
| 9 | 11 | ${ }^{4} 1$ | , | 27 | , | 1 | 1 |
| 10 | b2 | c2 | P2 | 28 | , | , | 1 |
| 11 | ${ }^{2}$ | 92 | d2 | 29 | , | , | , |
| 12 | 42 | ${ }^{\text {a } 2}$ | 1 | 30 | , | 1 | 1 |
| 13 | b3 | c3 | P3 | 31 | ' | 1 | 1 |
| 14 | a3 | 83 | d3 | 32 | , | 1 | 1 |
| 15 | 13 | e3 | 1 | 33 | 1 | 1 | 1 |
| 16 | b4 | ${ }^{4} 4$ | P4 | 34 | , | / | 1 |
| 17 | AC | $=$ | AUTO | 35 | 1 | 1 | 1 |
| 18 | * | -MEM | 1 | 36 | 1 | 1 | 1 |

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Non-Continuous Buzzer Signal Indicates Input Overrange


Figure 15: TSC805 Timing Waveform for Buzzer Output

## Display Decimal Point Selection

The TSC805 provides a decimal point LCD drive signal. The decimal point position is a function of the selected full-scale range as shown in Table 6.
Table 6: Decimal Point Selection

|  | $\mathbf{1}$ | $\bullet$ | $\mathbf{9}$ | $\bullet$ |
| :--- | :---: | :---: | :---: | :---: |
| $\mathbf{F}$ | $\mathbf{9}$ | $\bullet$ |  |  |
| Full-Scale Range | DP3 | DP2 | DP1 |  |
| $2000 \mathrm{~V}, 2000 \mathrm{k} \Omega$ | OFF | OFF | OFF |  |
| $200.0 \mathrm{~V}, 200.0 \mathrm{k} \Omega$ | OFF | OFF | ON |  |
| $20.00 \mathrm{~V}, 20.00 \mathrm{k} \Omega$ | OFF | ON | OFF |  |
| $2.000 \mathrm{~V}, 2.000 \mathrm{k} \Omega$ | ON | OFF | OFF |  |
| $200.0 \mathrm{mV}, 200.0 \Omega$ | OFF | OFF | ON |  |
| 20.00 mA | OFF | ON | OFF |  |
| 200.0 mA | OFF | OFF | ON |  |

## AC to DC Converter Operational Amplifier

The TSC805 contains an on chip operational amplifier that may be connected as a rectifier for AC to DC voltage and current measurements. Typical operational amplifier characteristics are:

- Slew Rate: $1 \mathrm{~V} / \mu \mathrm{s}$
- Unity Gain Bandwidth: 0.4 MHz
- Open Loop Gain: 44 dB
- Output Voltage Swing (Load $=10 \mathrm{k} \Omega) \pm 1.5 \mathrm{~V}$
(Reference to Analog Common)
When the AC measurement option is selected the input buffer receives an input signal through switch S 14 rather than switch S11 (See Figure 2). With external circuits the AC operating mode can be used to perform other types of functions within the constraints of the internal operational amplifier. External circuits that perform true RMS conversion or a peak hold function are typical examples.


## Component Selection

## Integration Resistor Selection

The TSC805 automatically selects one of two external integration resistors. RVIBUF (Pin 53) is selected for voltage and current measurement. R $\Omega$ BUF (Pin 52) is selected for resistance measurements.

## RVIBUF Selection (PIN 53)

In auto-range operation the TSC805 operates with a 200 mV maximum full-scale potential at VI ( $\operatorname{Pin} 42$ ). Resistive dividers at VR2 (Pin 39), VR3 (Pin 38), VR4 (Pin 41) and VR5 (Pin 40) are automatically switched to maintain the 200 mV full-scale potential.
In manual mode the extended operating mode is activated giving a 300 mV full-scale potential at VI (Pin 42).
The integrator output swing should be maximized but saturations must be avoided. The integrator will swing within 0.45 V of VCC (Pin 26) and 0.5 V of VSSA (Pin 55) without saturating. $\mathrm{A} \pm 2 \mathrm{~V}$ swing is suggested. The value of RVIBUF is easily calculated assuming a worst case extended resolution input signal:

$$
\begin{aligned}
& \mathrm{V}_{\text {INT }}=\text { Integrator Swing }= \pm 2 \mathrm{~V} \\
& \mathrm{~T}_{\mathrm{I}}=\text { Integration Time }=100 \mathrm{~ms} \\
& \mathrm{C}_{\mathrm{I}}=\text { Integration Capacitor }=0.1 \mu \mathrm{f} \\
& \mathrm{~V}_{\text {MAX }}=\text { Maximum Input at } \mathrm{V}_{\mathrm{I}}=300 \mathrm{mV}
\end{aligned}
$$

$$
\text { RVIBUF }=\frac{V_{\text {MAX }}\left(T_{1}\right)}{\operatorname{VINT}^{\left(C_{1}\right)}} \approx 150 \mathrm{k} \Omega
$$

## R $\Omega$ BUF Selection (Pin 52)

In ratiometric resistance measurements the signal at Rx (Pin 48 ) is always positive with respect to analog common. The integrator swings negative.
The worst case integrator swing is for the $200 \Omega$ range with the manual, extended resolution option.
The input voltage VX (Pin 48) is easily calculated (Figure 16).

For a 3.1 V integrator swing the value of $R \Omega$ BUF is easily calculated:

$$
\begin{array}{ll}
V_{\text {INT }} & =\text { Integrator Swing }=3.1 \mathrm{~V} \\
\mathrm{~T}_{1} & =\text { Integration Time }=100 \mathrm{~ms} \\
\mathrm{C}_{1} & =\text { Integration Cap. }=0.1 \mu \mathrm{f} \\
\mathrm{Rx} \text { Max } & =300 \Omega \\
\mathrm{~V} \times \text { Max } & =700 \mathrm{mV} \\
\mathrm{R} \Omega \text { BUF } & =\frac{(\mathrm{V} \times \mathrm{MAX})\left(\mathrm{T}_{1}\right)}{\mathrm{C}_{\mathrm{I}}\left(\mathrm{~V}_{\text {INT }}\right)} \approx 220 \mathrm{k} \Omega
\end{array}
$$

(

Figure 16: R $\Omega B U F$ Calculation ( $200 \Omega$ Manual Operation)

$$
\begin{aligned}
& \mathrm{V}_{\text {ANCOM }}=\text { Potential at Analog Common } \approx 2.7 \mathrm{~V} \\
& \text { R8 } \quad=220 \Omega \\
& R_{1}=163.85 \Omega \\
& \text { Rx } \quad=300 \Omega \\
& \text { Rs } \quad=\text { Internal Switch } 33 \text { Resistance } \approx 600 \Omega \\
& R \Omega B U F=\frac{\left(V C C-V_{A N C O M}\right) R x}{\left(R x+R_{S}+R_{1}+R_{8}\right)}=0.63 V
\end{aligned}
$$

With a low battery voltage of 6.6 V analog common will be approximately 3.6 V above the negative supply terminal. With the integrator swinging down from analog common toward the negative supply a 3.1 V swing will set the integrator output to 0.5 V above the negative supply.

## CINT, CAZ and CREF Capacitors

The integration capacitor, CINT, must have low dielectric absorption. A 0.1 uf polypropylene capacitor is suggested. The auto-zero capacitor, CAZ, and reference capacitor, CREF, should be selected for low leakage and dielectric absorption. Polystyrene capacitors are good choices.

## Reference Voltage Adjustment

The TSC805 contains a low temperature drift internal voltage reference. The analog common potential (Pin 27) is established by this reference. Maximum drift is a low $75 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$. Analog common is designed to be approximately 2.6 V below VCC (Pin 26). A resistive divider (R18/R19, Figure 1) sets the TSC805 reference input voltage (REFHI, Pin 32) to approximately 163.85 mV .
With an input voltage near full-scale on the 200 mV range, R19 is adjusted for the proper reading.

## Flat Package Socket

Sockets suitable for prototype work are available.
A USA source is:
Nepenthe Distribution
2471 East Bayshore
Suite 520
Palo Alto, CA 94303
(415) 856-9332

TWX: 910-373-2060
(a) "BQ" Socket Part No.: IC51-064-042 BQ
(b) "SQ" Socket Part No.: IC51-064-042 SQ

## Resistive Ladder Networks

Resistor attenuator networks for voltage and resistance measurement are available from:
Caddock Electronics
1717 Chicago Avenue
Riverside, CA 92507
TEL: (714) 788-1700
TWX: 910-332-6108

| Attenuator <br> Accuracy | Attenuator <br> Type | Caddock <br> Part Number |
| :---: | :---: | :---: |
| $0.1 \%$ | Voltage | $1776-$ C441 |
| $0.25 \%$ | Voltage | $1776-$ C44 |
| $0.25 \%$ | Resistance | T 1794-204-1 |

## Package Outline



## General Description

The TSC815 is a $31 / 2$ digit integrating analog-to-digital converter with triplex LCD display drive and automatic ranging. A display hold function is on-chip. Input voltage/ohm attenuators ranging from 1 to $1 / 10,000$ are automatically selected. Five full-scale ranges are provided. The CMOS TSC815 contains all the logic and analog switches needed to manufacture an auto-ranging instrument for ohms and voltage measurements. User selected 20 mA and 200 mA current ranges are available. Full-scale range and decimal point LCD annunciators are automatically set in auto-range operation. Auto-range operation is available during ohms (high and low power ohms) and voltage (AC \& DC) measurements. Autoranging eliminates expensive range switches in hand-held DMM designs and makes compact meters easier and less costly to design. The auto-range feature may be bypassed allowing decimal point selection and input attenuator selection control through a single line input. Expensive rotary switches are not required.
During manual mode operation resolution is extended to 3000 counts full-scale. The extended range operation is indicated by a flashing 1 MSD. The extended resolution is available during $2000 \mathrm{k} \Omega$ and 2000 V full-scale auto-range operation also.
The memory mode subtracts a reading - up to $\pm 5 \%$ of fullscale - from subsequent measurements. Typical applications involve probe resistance compensation for resistance measurements, tolerance measurements, and tare weight measurement.
The TSC815 includes and AC to DC converter for AC measurements. Only external diodes/resistors/capacitors are required.
A complete LCD annunciator set describes the TSC815 meter function and measurement range during ohms, voltage and current operation. AC measurements are indicated as well as auto-range operation. A low battery detection circuit also sets the low battery display annunciator. The triplex LCD display drive levels may be set and temperature compensation applied via the VDISP pin. With $\overline{\text { HOLD }}$ low the display is not updated. A HOLD MODE LCD annunciator is activated.
The "low ohms" measurement option allows in circuit resistance measurements by preventing semiconductor junctions from being forward biased.

A continuity buzzer output is activated with inputs less than $1 \%$ of full-scale. An overrange input signal also enables the buzzer, except during resistance measurements, and flashes the MSD display. Featuring single 9 V battery operation, 10 mW power consumption, a precision internal voltage reference ( $75 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ max. TC) and a compact surface mounted 60 -pin quad flat package, the TSC815 is ideal for portable instruments.

## Features

- Auto-Range Operation for AC \& DC Voltage and Resistance Measurements
- Two User Selected AC/DC Current Ranges 20 \& 200 mA
- 22 Operating Ranges
- 9 DC/AC Voltage
- $4 \mathrm{AC} / \mathrm{DC}$ Current
- 9 Resistance and Low Power Ohms
- Display HOLD Function
- 3 1/2 Digit Resolution in Auto-Range Mode .... 1/2000
- Extended Resolution in Manual Mode ....... 1/3000
- Memory Mode for Relative Measurements ... $\pm 5 \%$ F.S.
- Internal AC to DC Conversion Op Amp
- Triplex LCD Drive for Decimal Points, Digits and Annunciators
- Continuity Detection and Piezoelectric Transducer Driver
- Compact Surface Mounted 60-Pin Quad Flat Package
- Low Drift Internal Reference ................ $75 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$
- 9 V Battery Operation .............................. 10 mW
- Low Battery Detection and LCD Annunciator

Ordering Information

| Part. No. | Package | Temp. <br> Range |
| :--- | :--- | ---: |
| TSC815CBQ | 60-Pin Plastic Quad <br> Flat Package <br> Formed Leads | $0^{\circ} \mathrm{C}$ to $70^{\circ} \mathrm{C}$ |
| TSC815CSQ | 60-Pin Plastic Quad <br> Flat Package <br> Straight Leads | $0^{\circ} \mathrm{C}$ to $70^{\circ} \mathrm{C}$ |

## Pin Configuration



# 3 1/2 Digit Auto-Ranging Analog-to-Digital Converter - Triplex LCD Drive <br> - Display Hold Function 

TSC815

## Absolute Maximum Ratings

| Supply Voltage ( ${ }^{+}$to V ) .............................. 15 V |  |
| :---: | :---: |
| Analog Input Voltage | $\mathrm{V}^{+}$to $\mathrm{V}^{-}$ |
| Reference Input Voltage ......................... $\mathrm{V}^{+}$to $\mathrm{V}^{-}$ |  |
| Voltage at Pin 43 | GND $\pm 0.7 \mathrm{~V}$ |
| Power Dissipation |  |
| Plastic Package | 800 mW |
| Operating Temperature |  |
| "C" Devices | C to $+70^{\circ} \mathrm{C}$ |

## Storage Temperature ................... $-65^{\circ} \mathrm{C}$ to $+160^{\circ} \mathrm{C}$ Lead Temperature (Soldering, 60 sec. ) ............. $300^{\circ} \mathrm{C}$

Stresses above those listed under Absolute Maximum Ratings may cause permanent damage to the device. These are stress ratings only and functional operation of the device at these or any other conditions above those indicated in the operational sections of the specifications is not implied. Exposure to Absolute Maximum Rating Conditions for extended periods may effect device reliability

Electrical Characteristics: $\mathrm{V}_{\mathrm{S}}=9 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, Figure 1 Test Circuit

| NO. | SYMBOL | PARAMETER | TEST CONDITIONS | MIN | $\begin{array}{ll} \text { TSC815 } \\ \text { TYP MAX } \end{array}$ | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 |  | Zero Input Reading | 200 mV Range w/o $10 \mathrm{M} \Omega$ Input Resistor | -0000 | $0000+0000$ | Digital Reading |
|  |  |  | 200 mV Range w/10 M $\Omega$ Input | -0001 | +0001 |  |
|  |  |  | 20 mA and 200 mA Range | -0000 | $0000+0000$ |  |
| 2 | RE | Rollover Error | 200 mV Range $\mathrm{w} / \mathrm{o} 10 \mathrm{M} \Omega$ Input Resistor | - | $\pm 1$ | Count |
|  |  |  | 200 mV Range w/10 M $\Omega$ Input | - | $\pm 3$ |  |
|  |  |  | 20 mA and 200 mA Range | - | $\pm 1$ |  |
| 3 | NL | Linearity Error | Best Case Straight Line | - | $\pm 1$ | Count |
| 4 | In | Input Leakage Current |  | - | 10 | pA |
| 5 | $\mathrm{EN}_{\mathrm{N}}$ | Input Noise | $\mathrm{BW}=0.1$ to 10 Hz | - | 20 | $\mu V_{p-p}$ |
| 6 |  | AC Frequency Response | $\pm 1 \%$ Error | - | 40 to 500 - | Hz |
|  |  |  | $\pm 5 \%$ Error | - | 40 to 2000 - |  |
| 7 |  | Open Circuit Voltage for OHM Measurements | Excludes $200 \Omega$ Range | - | 570660 | mV |
| 8 |  | Open Circuit Voltage for LO OHM Measurement | Excludes $200 \Omega$ Range | - | 285350 | mV |
| 9 | VCOM | Analog Common Voltage | $\left(\mathrm{V}^{+}-\mathrm{VCOM}\right)$ | 2.5 | $2.6 \quad 3.3$ | V |
| 10 | Vсtc | Common Voltage Temperature Coefficient |  | - | 50 | ppm $/{ }^{\circ} \mathrm{C}$ |
| 11 |  | Display Multiplex Rate |  | - | 100 | Hz |
| 12 | VIL | Low Logic Input | $\overline{20 \mathrm{~mA}}, \overline{\mathrm{AC}}, \mathrm{I}, \overline{\mathrm{LOW} \Omega}, \overline{\mathrm{HOLD}}$ Range, - $\overline{\mathrm{MEM}}, \overline{\mathrm{OHMS}}$ (Relative to DIG GND Pin 56) | - | - 1 | V |
| 13 |  | Logic 1 Pull Up Current | $\overline{20 \mathrm{~mA}}, \overline{\mathrm{AC}}, \mathrm{I}, \overline{\mathrm{LOW} \Omega}, \overline{\mathrm{HOLD}}$ Range, - $\overline{\mathrm{MEM}}, \overline{\mathrm{OHMS}}$ (Relative to DIG GND Pin 56) | - | 25 - | $\mu \mathrm{A}$ |
| 14 |  | Buzzer Drive Frequency |  | - | 4 | kHz |
| 15 |  | Low Battery Flag Voltage | VCC to VSSA | 6.3 | 6.67 .0 | V |
| 16 |  | Operating Supply Current |  | - | $0.8 \quad 1.5$ | mA |

## Note:

1. $200 \Omega$ range open circuit voltage approximately 2.8 V .

## Pin Description and Function Table 1:

| PIN NO. (Quad Flat Package) | SYMBOL | DESCRIPTION |
| :---: | :---: | :---: |
| 1 | $\overline{\mathrm{OHM}}$ | Logic Input. "0" (Digital Ground) for resistance measurement. |
| 2 | $\overline{20 \mathrm{~mA}}$ | Logic Input. "0" (Digital Ground) for 20 mA full-scale current measurement. |
| 3 | BUZ | Audio frequency, 4 kHz , output for continuity indication during resistance measurement. A noncontinuous 4 kHz signal is output to indicate an input overrange during voltage or current measurements. |
| 4 | XTAL1 | 32.768 kHz Crystal Connection. |
| 5 | XTAL2 | 32.768 kHz Crystal Connection. |
| 6 | VDISP | Sets peak LCD drive signal: VP = VCC-VDISP. VDISP may also be used to compensate for temperature variation of LCD crystal threshold voltage. |
| 7 | BP1 | LCD Backplane \#1. |
| 8 | BP2 | LCD Backplane \#2. |
| 9 | BP3 | LCD Backplane \#3. |
| 10 | Low $\Omega$ / A | LCD Annunciator segment drive for low ohms resistance measurement and current measurement. |
| 11 | $\Omega / \mathrm{V}$ | LCD Annunciator segment drive for resistance measurement and voltage measurement. |
| 12 | K/m/HOLD | LCD Annunciator segment drive for $k$ ("kilo-ohms"), $m$ ("milli-amps" and "milli-volts") and HOLD mode. |
| 13 | BCPO (Ones digit). | LCD segment drive for "b," "c" segments and decimal point of least significant digit (LSD). |
| 14 | AGD0 | LCD segment drive for "a," " g ," " d " segments of LSD. |
| 15 | FEO | LCD segment drive for "f" and "e" segments of LSD. |
| 16 | BCP1 | LCD segment drive for "b," "c" segments and decimal point of 2nd LSD. |
| 17 | AGD1 | LCD segment drive for "a," "g," "d" segments of 2nd LSD (Ten's digit). |
| 18 | FE1 | LCD segment drive for "f," and "e" segments of 2nd LSD. |
| 19 | BCP2 | LCD segment drive for "b," "c," and decimal point of 3rd LSD. (Hundreds digit). |
| 20 | AGD2 | LCD segment drive for "a," "g," "d" segments of 3rd LSD. |
| 21 | FE2 | LCD segment drive for " $b$ " and " $c$ " segments of 3rd LSD. |
| 22 | BCP3 | LCD segment drive for " b ," " $c$ " segments and decimal point of MSD (Thousand's digit). |
| 23 | AC/-/AUTO | LCD annunciator drive signal for AC measurements, polarity, and auto-range operation. |
| 24 | -MEM/BATT mode. | LCD annunciator drive signal for low battery indication and memory (relative measurement) |
| 25 | VSSD | Negative battery supply connection for internal digital circuits. Connect to negative terminal of battery. |
| 26 | VCC | Positive battery supply connection. |
| 27 | COM | Analog circuit ground reference point. Nominally 2.6 V below VCC. |
| 28 | RMREFH | Ratiometric (Resistance measurement) reference high voltage. |
| 29 | RMREFL | Ratiometric (Resistance measurement) reference low voltage. |
| 30 | CREFL | Reference capacitor negative terminal CREF $=0.1 \mu \mathrm{f}$. |
| 31 | CREFH | Reference capacitor positive terminal CREF $=0.1 \mu \mathrm{f}$. |
| 32 | REFHI | Reference voltage for voltage and current measurement. Nominally 163.85 mV . |
| 33 | SR1 | Standard resistor connection for $200 \Omega$ full-scale. |
| 34 | SR2 | Standard resistor connection for 2000 , full-scale. |

## Pin Description and Function Table 1:

| PIN NO. (Quad Flat Package) | SYMBOL | DESCRIPTION |
| :---: | :---: | :---: |
| 35 | תR3 | Standard resistor connection for $20 \mathrm{k} \Omega$ full-scale range. |
| 36 | תR4 | Standard resistor connection for $200 \mathrm{k} \Omega$ full-scale range. |
| 37 | תR5 | Standard resistor connection for $2000 \mathrm{k} \Omega$ full-scale range. |
| 38 | VR3 | Voltage measurement $\div 100$ attenuator. |
| 39 | VR2 | Voltage measurement $\div 10$ attenuator. |
| 40 | VR5 | Voltage measurement $\div 10,000$ attenuator. |
| 41 | VR4 | Voltage measurement $\div 1000$ attenuator. |
| 42 | $V_{1}$ | Unknown voltage input $\div 1$ attenuator. |
| 43 | 11 | Unknown current input. |
| 44 | ACVL | Low output of AC to DC converter. |
| 45 | Cl | Integrator capacitor connection. Nominally $0.1 \mu \mathrm{f}$. (Low dielectric absorption. Polypropylene dielectric suggested). |
| 46 | CAZ | Auto-zero capacitor connection. Nominally $0.1 \mu \mathrm{f}$. |
| 47 | Rx | Unknown resistance input. |
| 48 | CFI | Input filter connection. |
| 49 | ADI | Negative input of internal AC to DC operational amplifier. |
| 50 | ADO | Output of internal AC to DC operational amplifier. |
| 51 | R $\Omega$ BUF | Active buffer output for resistance measurement. Integration resistor connection. Integrator resistor nominally $220 \mathrm{k} \Omega$. |
| 52 | RVIBUF | Active buffer output for voltage and current measurement. Integration resistor connection. Integration resistor nominally $150 \mathrm{k} \Omega$. |
| 53 | ACVH | Positive output of AC to DC converter. |
| 54 | VSSA | Negative supply connection for analog circuits. Connect to negative terminal of 9 V battery. |
| 55 | DIG GND | Internal logic digital ground. The logic "0" level. Nominally 4.7 V below VCC. |
| 56 | RANGE | Input to set manual operation and change ranges. |
| 57 | HOLD | Input to hold display. connect to DIG GND. |
| 58 | $\overline{\mathrm{MEM}}$ | Input to enter memory measurement mode for relative measurements. The two LSD's are stored and subtracted from future measurements. |
| 59 | $\begin{aligned} & \mathrm{DC} / \overline{\mathrm{AC}}, \\ & \Omega / \overline{\mathrm{LOW} \Omega} \end{aligned}$ | Input that selects AC or DC option during voltage/current measurements. For resistance measurements, the ohms or low power (voltage) ohms option can be selected. |
| 60 | T | Input to select current measurement. Set to logic "0" (Digital ground) for current measurement. |



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Figure 2: TSC815 Analog Section

## Resistance, Voltage, Current <br> Measurement Selection

The TSC815 is designed to measure voltage, current, and resistance. Auto-ranging is available for resistance and voltage measurements. The $\overline{O H M S}$ (Pin 1) and $\bar{T}(\operatorname{Pin} 60)$ input controls are normally pulled internally to Vcc.
By tying these pins to Digital Ground (Pin 56), the TSC815 is configured internally to measure resistance, voltage, or current. The required signal combinations are shown in Table 2.

Table 2: TSC815 Measurement Selection Logic

| Function Select Pin |  |  |
| :---: | :---: | :--- |
| OHM (Pin 1) | $\mathbf{I ( P i n} \mathbf{6 0})$ | Selected Measurement |
| 0 | 0 | Voltage |
| 0 | 1 | Resistance |
| 1 | 0 | Current |
| 1 | 1 | Voltage |

$0=$ Digital Ground
1 = Floating or Tied to Vcc

## Notes:

1. $\overline{\mathrm{OHM}} \& \bar{I}$ are normally pulled internally high to VCC (Pin 26).

This is considered a logic " 1. ."
2. Logic " 0 " is the potential at digital ground (Pin 55).

## Resistance Measurements OHMS \& Low Power OHMS

The TSC815 can be configured to reliably measure in-circuit resistances shunted by semiconductor junctions. The TSC815 low power ohms measurement mode limits the probe open circuit voltage. This prevents semiconductor junctions in the measured system from turning on.
In the resistance measurement mode the $\Omega / \overline{\mathrm{LOW} \Omega}$ (Pin 59) input selects the low power ohms measurement mode. For low power ohms measurements $\Omega / \overline{\mathrm{LOW} \Omega}$ (Pin 59) is momentarily brought low to digital ground potential. The TSC815 sets up for a low power ohms measurement with a maximum open circuit probe voltage of 0.35 V above analog common. In the low power ohms mode an LCD display annunciator, $\overline{\text { LOW } \Omega}$, will be activated. On power up the low power ohms mode is not active.

If the manual operating mode has been selected, toggling $\Omega / \overline{\text { LOW }} \Omega$ will reset the TSC815 back to the auto-range mode. In manual mode, the decision to make a normal orlow power ohms measurement should be made before selecting the desired range.

The low power ohms measurement is not available on the $100 \Omega$ full-scale range. Open circuit voltage on this range is below 2.8 V .

The standard resistance values are listed in Table 3.
Table 3: Ohms Range Ladder Network

| Full-Scale <br> Range | Standard <br> Resistance | Low Power <br> Ohms Mode |
| :--- | :--- | :---: |
| $200 \Omega$ | $163.85 \Omega(R 1)$ | NO |
| $2000 \Omega$ | $1638.5 \Omega(R 2)$ | YES |
| $20 \mathrm{k} \Omega$ | $16,358 \Omega(\mathrm{R} 3)$ | YES |
| $200 \mathrm{k} \Omega$ | $163850 \Omega(\mathrm{R} 4)$ | YES |
| $2,000 \mathrm{k} \Omega$ | $1,638,500 \Omega(R 5)$ | YES |

$\mathrm{N} / \mathrm{A}=$ Not available .
R8, a positive temperature coefficient resistor, and the 6.2 V zener, Z1 in Figure 1 provide input voltage protection during ohms measurements.

## Ratiometric Resistance Measurements

The TSC815 measures resistance ratiometrically. Accuracy is set by the external standard resistors connected to Pin 33 through 37. A low-power ohms mode may be selected on all but the $200 \Omega$ full-scale range. The low power ohms mode limits the voltage applied to the measured system. This allows accurate "in-circuit" measurements when a resistor is shunted by semiconductor junctions.

Full auto-ranging is provided. External precision standard resistors are automatically switched to provide the proper range.
Figure 3 shows a detailed block diagram of the TSC815 configured for ratiometric resistance measurements. During the signal integrate phase the reference capacitor charges to a voltage inversely proportional to the measured resistanceRX. Figure 4 shows the conversion accuracy relies on the accuracy of the external standard resistors only.
Normally the required accuracy of the standard resistances will be dictated by the accuracy specifications of the users end product. Table 4 gives the equivalent ohms per count for various full-scale ranges to allow users to judge the required resistor accuracy.

Table 4: Reference Resistors

| Full-Scale <br> Range | Reference <br> Resistor | $\Omega /$ COUNT |
| :--- | :--- | :---: |
| 200 | 163.85 | 0.1 |
| 2 k | 1638.5 | 1 |
| 20 k | 16385 | 10 |
| 200 k | 163850 | 100 |
| 2 M | 1638500 | 1000 |

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Figure 3: Ratiometric Resistance Measurement Functional Diagram

## Voltage Measurement

Resistive dividers are automatically changed to provide in range readings for 200 mV to 2000 V full-scale readings (Figure 2). The input resistance is set by external resistors R14/R13. The divider leg resistors are R9-R12. The divider leg resistors give a 200 mV signal VI (Pin 42) for full-scale voltages from 200 mV to 2000 V .
For applications which do not require a $10 \mathrm{~m} \Omega$ input impedance the divider network impedances may be lowered. This will reduce voltage offset errors induced by switch leakage currents.

## Current Measurement

The TSC815 measures current only under manual range operation. The two user selectable full-scale ranges are: 20 mA and 200 mA . Select the current measurement mode by holding the I input (Pin 60) low at digital ground potential.

The OHM input (Pin 1) is left floating or tied to the positive supply.
Two ranges are possible. The 20 mA full-scale range is selected by connecting the 20 mA input (Pin 2) to digital ground. If left floating the 200 mA full-scale range is selected.
External current to voltage conversion resistors are used at the II input (Pin 43). For 20 mA measurements a $10 \Omega$ resistor is used. the 200 mA range needs a $1 \Omega$ resistor. Full-scale is 200 mV .
PC board trace resistance between analog common and R16 (See Figure 1) must be minimized. In the 200 mA range, for example, a 0.05 trace resistance will cause a $5 \%$ current to voltage conversion error at । (Pin 43).
The extended resolution measurement option operates during current measurements.

To minimize rollover error the potential difference between analog common (Pin 27) and system common must be minimized.


Example: $\mathbf{2 0 0}$ k $\Omega$ Full-Scale Measurement
(a) $\quad V R=\frac{163.85 k \Omega}{163.85+220+R X} \times 0.64$
(b) $\quad V X=\frac{R X}{163.85 \mathrm{k} \Omega+220 \Omega+R X} \times 0.64$
(c) "Ramp Up Voltage" = "Ramp Down Voltage"

$$
\therefore \quad \frac{V X}{R_{1} C_{l}} \times T_{I}=\frac{V R}{R_{I} C_{l}} T_{D E}
$$

Where:
$R_{1}=$ Integrating Resistor, $T_{1}=$ Integrate Time
$C_{I}=$ Integrating Capacitor, $T_{D E}=$ Deintegrate Time
(d) $R X=163.85\left(\frac{T_{D E}}{T_{I}}\right)$

Independent of RI, CI or Internal Voltage Reference
Figure 4: Resistance Measurement Accuracy Set by External Standard Resistor


> External Crystal $=32.768 \mathrm{kHz}$ Internal Clock Period $=T \mathrm{TP}=2 / 32.768=61.04 \mu \mathrm{~s}$ Total Conversion Time $=T \operatorname{coNV}=8000(\mathrm{Tp})$ $=488.3 \mathrm{~ms} \approx 2 \mathrm{CONV} / \mathrm{SEC}$ Integration Time $=T_{1}=1638.5(\mathrm{Tp})=100.0 \mathrm{~ms}$ Maximum Reference Deintegrate Time $=T_{D E}=3000(T \mathrm{~T})=183.1 \mathrm{~ms}$ (Manual, Extended Resolution) $=2000(\mathrm{TP})=122.1 \mathrm{~ms}$ (Auto-Range) Minimum Auto-Zero Time $=(8000-3000-1638.5) \quad(T P)=205.1 \mathrm{~ms}$ (Manual, Extended $=(8000-2000-1.638 .5) \quad(T P)=266.2 \mathrm{~ms}$ (Auto-Range)

Figure 5: Basic TSC815 Conversion Timing

## Measurement Options <br> AC to DC Measurements

In voltage and current measurements the TSC815 can be configured for AC measurements. An on chip operational amplifier and external rectifier components perform the AC to DC conversion.

When power is first applied the TSC815 enters the DC measurement mode. For AC measurements (current or voltage), $\overline{\mathrm{AC}} / \mathrm{DC}(\operatorname{Pin} 59)$ is momentarily brought low to digital ground potential; the TSC815 sets-up for AC measurements and the AC liquid crystal display annunciator activates. Toggling $\overline{A C} / D C$ low again will return the TSC815 to DC operation.
If the manual operating mode has been selected toggling $\overline{A C} / D C$ will reset the TSC815 back to the auto-range mode. In manual mode operation AC or DC operation should be selected first and then the desired range selected.

The minimum $A C$ voltage full-scale voltage range is 2 V . The DC full-scale minimum voltage is 200 mV .
AC current measurements are available on the 20 mA and 100 mA full-scale current range.

## Conversion Timing

The TSC815 analog-to-digital converter uses the conventional dual slope integrating conversion teghnique with an added phase that automatically eliminates zero offset errors. The TSC815 gives a zero reading with a zero volt input.
The TSC815 is designed to operate with a 32.768 kHz crystal. The 32 kHz crystal is low cost and readily available; it serves as a time base oscillator crystal in many digital clocks. (See External Crystal Sources).
The external clock is divided by two. The internal clock frequency is 16.348 kHz giving a clock period of $61.04 \mu \mathrm{~s}$. The total conversion - auto-zero phase, signal integrate and

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reference deintegrate - requires 8000 clock periods or 488.3 ms . There are approximately two complete conversions per second.

The integration time is fixed at 1638.5 clock periods or 100 ms . This gives rejection of $50 / 60 \mathrm{~Hz}$ AC line noise.
The maximum reference deintegrate time, representing a fullscale analog input, is 3000 clock periods or 183.1 ms during manual extended resolution operation. The 3000 counts are available in manual mode, extended resolution operation only. In auto-ranging mode the maximum deintegrate time is 2000 clock periods. The 1000 clock periods are added to the autozero phase. An auto-ranging or manual conversion takes 8000 clock periods. After a zero crossing is detected in the reference deintegrate mode, the auto-zero phase is entered.
Figure 5 shows the basic TSC815 timing relationships.

## Manual Range Selection

The TSC815 voltage and resistance auto-ranging feature can be disabled by momentarily bringing $\overline{\text { RANGE ( }}$ (in 56) to digital ground potential (Pin 55). When the change from auto-to-manual ranging occurs the first manual range selected is the last range in the auto-ranging mode.
The TSC815 power-up circuit selects auto-range operation initially. Once the manual range option is entered, range changes are made my momentarily grounding the RANGE control input. The TSC815 remains in the manual range mode until the measurement function (voltage or resistance) or measurement option (AC/DC, $\Omega / L O \Omega$ ) changes. This
causes the TSC815 to return to auto-ranging operation. The "Auto" LCD annunciator driver is active only in the autorange mode.

Table 5 shows typical operation where the manual range selection option is used. Also shown is the extended resolution display format.

## Extended Resolution Manual Operation

The TSC815 extends resolution by $50 \%$ when operated in the manual range select mode for current, voltage, and resistance measurements. Resolution increases to 3000 counts from 2000 counts. The extended resolution feature operates only on the $2000 \mathrm{k} \Omega$ and 2000 V ranges during auto-range operation.

In the extended resolution operating mode readings above 1999 are displayed with a blinking " 1 " most significant digit. The blinking " 1 " should be interpreted as the digit 2 . The three least significant digits display data normally.
An input overrange condition causes the most significant digit to blink and sets the three least significant digits to display " 000 ". The buzzer output is enabled for input voltage and current signals with readings greater than 2000 counts in both manual and auto-range operation.
For resistance measurements the buzzer signal does not indicate an overrange condition. The buzzer is used to indicate continuity. Continuity is defined as a resistance reading less than 19 counts.

Table 5: Manual Range Operation

| INPUT |  |  |  | AC VOLTS |  |  |  | LO OHM |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 23.5 V |  | 18.2 V |  | $18.2 \mathrm{k} \Omega$ |  | $2.35 \mathrm{M} \Omega$ |  |
| POWER-ON <br> AUTO-RANGE OPERATION |  | RANGE | DISPLAY | RANGE | DISPLAY | RANGE | DISPLAY | RANGE | DISPLAY |
|  |  | 200 mV | "1"00.0 mV | 2 V | "1".000 V | $200 \Omega$ | "1"00.0 $\Omega$ | $2 \mathrm{k} \Omega$ | "1".000 k $\Omega$ |
|  |  | 2 V | "1".000 V | 20 V | 18.20 V | $2 \mathrm{k} \Omega$ | "1". $000 \mathrm{k} \Omega$ | $10 \mathrm{k} \Omega$ | "1"0.00 k $\Omega$ |
|  |  | 20 V | "1"0.00 V |  |  | $20 \mathrm{k} \Omega$ | $18.20 \mathrm{k} \Omega$ | $200 \mathrm{k} \Omega$ | "1"00.0 k $\Omega$ |
|  |  | 200 V | 23.5 V |  |  |  |  | $2000 \mathrm{k} \Omega$ | "1"350 k |
| RANGE CHANGES 乙- |  |  |  |  |  |  |  |  |  |
|  | Lr | RANGE | DISPLAY | RANGE | DISPLAY | RANGE | DISPLAY | RANGE | DISPLAY |
|  | 1 | 200 V | 23.5 V | 20 V | 18.20 V | $20 \mathrm{k} \Omega$ | $18.20 \mathrm{k} \Omega$ | $2000 \mathrm{k} \Omega$ | "1"350 k |
|  | 2 | 200 mV | "1"00.0 mV | 2 V | "1".000 V | $200 \Omega$ | "1"00.0 $\Omega$ | $2 \mathrm{k} \Omega$ | "1".000 k $\Omega$ |
|  | 3 | 2 V | 1.000 V | 20 V | 18.20 V | $2 \mathrm{k} \Omega$ | " 1 ".000 k $\Omega$ | $20 \mathrm{k} \Omega$ | "1"0.00 k $\Omega$ |
|  | 4 | 20 V | "1"3.50 V | 200 V | 18.2 V | $20 \mathrm{k} \Omega$ | $18.20 \mathrm{k} \Omega$ | $200 \mathrm{k} \Omega$ | "1"00.0 k $\Omega$ |
|  | 5 | 200 V | 23.5 V | 600 V | 19 V | $200 \mathrm{k} \Omega$ | $18.2 \mathrm{k} \Omega$ | $2000 \mathrm{k} \Omega$ | "1"350 k |
|  | 6 | 1000 V | 24 V | 2 V | "1".000 V | $2000 \mathrm{k} \Omega$ | $19 \mathrm{k} \Omega$ | $2 \mathrm{k} \Omega$ | "1".000 k $\Omega$ |
|  | 7 | 200 mV | "1"00.0 mV | 20 V | 18.20 V | $200 \Omega$ | "1"'00.0 $\Omega$ | $20 \mathrm{k} \Omega$ | " 1 "0.00 k $\Omega$ |
|  | 8 | 2 V | "1". 000 V | 200 V | 18.2 V | $2 \mathrm{k} \Omega$ | "1".000 k $\Omega$ | $200 \mathrm{k} \Omega$ | "1"00.0 k |

## Notes:

1. A flashing MSD is shown as a " 1 ". A flashing MSD indicates the TSC815 is over-ranged if all other digits are zero.
2. The first manual range selected is the last range in the auto-ranging mode.
3. A flashing MSD with a non-zero display indicates the TSC815 has entered the extended resolution operating mode. An additional 1000 counts of resolution is available. This extended operation is available only in manual operation for voltage, resistance and current measurements.
4. $工=$ momentary ground connection.

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Figure 6: Manual Range Selection;
Resistance Measurement


Figure 7: Manual Range Selection; Current Measurement

## -MEM Operating Mode

Bringing $\overline{M E M}$ (Pin 58) momentarily low configures the TSC815 "-MEM" operating mode. The -MEM LCD Annunciator becomes active. In this operating mode subsequent measurements are made relative to the last two digits ( $\leq 99$ ) displayed at the time MEM is low. This represents $5 \%$ of fullscale. The last two significant digits are stored and subtracted from all the following input conversions.

TSC815


Figure 8: Manual Range Selection; Voltage Measurement

A few examples clarify operation:

## Example 1: In Auto-Ranging

Ri $(\mathrm{N})=18.21 \mathrm{k} \Omega(20 \mathrm{k} \Omega$ Range $)=>$ Display $18.21 \mathrm{k} \Omega$ MEM 工- = > Store $0.21 \mathrm{k} \Omega$
Ri $(N+1)=19.87 \mathrm{k} \Omega(20 \mathrm{k} \Omega$ Range $)$

$$
=>\text { Display } 19.87-0.21=19.66 \mathrm{k} \Omega
$$

Ri $(\mathrm{N}+2)=22.65 \mathrm{k} \Omega$ ( $200 \mathrm{k} \Omega$ Range) $=>$ Display $22.7 \mathrm{k} \Omega \& \overline{\mathrm{MEM}}$ Disappears
Example 2: In Fixed Range $200.0 \Omega$ Full-Scale
Ri $(N)=18.2 \Omega=>$ Display $18.2 \Omega$
$\overline{\mathrm{MEM}}$ —— $=>$ Store $8.2 \Omega$
Ri $(N+1)=36.7 \Omega$
$=>$ Display $36.7-8.2=28.5 \Omega$
$\operatorname{Ri}(N+2)=5.8 \Omega$
$=>$ Display 5.8-8.2 = -2.4 $\Omega^{*}$
*Will display minus resistance if following input is less than offset stored at fixed range

Example 3: In Fixed Range 20.00 V Full-Scale

$$
\begin{aligned}
& \mathrm{Vi}(\mathrm{~N})=0.51 \mathrm{~V}=>\text { Display } 0.51 \mathrm{~V} \\
& \overline{\mathrm{MEM}} \mathrm{~L}^{2}=>\text { Store } 0.51 \mathrm{~V} \\
& \mathrm{Vi}(\mathrm{~N}+1)=3.68 \mathrm{~V} \\
& \quad=>\text { Display } 3.68-0.51=3.17 \mathrm{~V} \\
& \mathrm{Vi}(\mathrm{~N}+2)=0.23 \mathrm{~V} \\
& \quad \Rightarrow>\text { Display } 0.23-0.51=-0.28 \mathrm{~V} \\
& \mathrm{Vi}(\mathrm{~N}+3)=-5.21 \mathrm{~V} \\
& \quad \Rightarrow>\text { Display }-5.21-0.51=-5.72 \mathrm{~V}
\end{aligned}
$$

# 3 1/2 Digit Auto-Ranging Analog-to-Digital Converter - Triplex LCD Drive - Display Hold Function 

On Power up the TSC815 "-MEM" mode is not active. Once the "-MEM" is entered bringing $\overline{M E M}$ low again it returns the TSC815 to normal operation.

The "-MEM" mode is also cancelled whenever the measurement type (resistance, voltage, current, $\overline{\mathrm{AC}} / \mathrm{DC}, \Omega / \overline{\mathrm{LO} \Omega}$ ) or range is changed. The LCD -MEM annunciator will be off in normal operation.

In auto-range operation if the following input signal cannot be converted on the same range as the stored value, the "-MEM" mode is cancelled. The LCD annunciator is turned off.

The "-MEM" operating mode can be very useful in resistance measurements when lead length resistance would cause measurement errors.

## Automatic Range Selection Operation

When power is first applied the TSC815 enters the autorange operating state. The auto-range mode may be entered from manual mode by changing the measurement function (resistance or voltage) or by changing the measurement option ( $\overline{\mathrm{AC}} / \mathrm{DC}, \Omega / \overline{\mathrm{LOS}}$ ).
The automatic voltage range selection begins on the most sensitive scale first: 200 mV for DC or 2.000 V for AC measurements. The voltage range selection flow chart is given in Figure 9.

Internal input protection diodes to VCC (Pin 26) and VSSA (Pin 54) clamp the input voltage. The external $10 \mathrm{M} \Omega$ input resistance (See Figure 1, R14 and R13) limits current safely in an overrange condition.

The voltage range selection is designed to maximize resolution. For input signals less than $9 \%$ of full-scale (count reading $<180$ ) the next most sensitive range is selected.

An overrange voltage input condition is flagged whenever the internal count exceeds 2000 by activating the buzzer output (Pin 3). This 4 kHz signal can directly drive a piezo electric acoustic transducer. An out of range input signal causes the 4 kHz signal to be on for 122 ms , off for 122 ms , on for 122 ms , and off for 610 ms (See Figure 15).

During voltage auto-range operation the extended resolution feature operates on the 2000 V range only (See extended resolution operating mode discussion).
The resistance automatic range selection procedure is shown in Figure 10. The $200 \Omega$ range is the first range selected unless the TSC815 low ohms resistance measurement option is selected. In low ohms operation the first full-scale range tried is $2 \mathrm{k} \Omega$.

The resistance range selected maximizes sensitivity. If the conversion results in a reading less than 180 the next most sensitive full-scale range is tried.

If the conversion is less than 19 in auto-range operation a continuous 4 kHz signal is output at BUZ (Pin 3). An overrange input does not activate the buzzer.

Out of range input conditions are displayed by a blinking most significant digit with the three least significant digits set to "000."
The extended resolution feature operates only on the $2000 \mathrm{k} \Omega$ and 2000 V full-scale range during auto-range operation. A blinking " 1 " most significant digit is interpreted as the digit 2. The three least significant digits display data normally.


Figure 9: Auto-Range Operation; Voltage Measurement


Figure 10: Auto-Range Operation; Resistance Measurement


Figure 11: Low Battery Detector

## Low Battery Detection Circuit

The TSC815 contains a low battery detector. When the 9 V battery supply has been depleted to a 7 V nominal value the LCD display low battery annunciator is activated.
The low battery detector is shown in Figure 11. The low battery annunciator is guaranteed to remain OFF with the battery supply greater than 7.0 V . The annunciator is guaranteed to be ON before the supply battery has reached 6.3 V .

## Triplex Liquid Crystal Drive

The TSC815 directly drives a triplexed liquid crystal display (LCD) using $1 / 3$ bias drive. All data, decimal point, polarity and function annunciator drive signals are developed by the TSC815. A direct connection to a triplex LCD display is possible without external drive electronics. Standard and custom LCD displays are readily available from LCD manu-

The LCDs must be driven with an AC signal having a zero DC component for long display life. The liquid crystal polarization is a function of the RMS voltage appearing across the backplane and segment driver. The peak drive signal applied to the LCD is: VCC-VDISP.
If VDISP, for example, is set at a potential 3 V below $V C C$ the peak drive signal is:

$$
V p=V C C-V D I S P=3 V
$$

An "OFF" LCD segment has an RMS voltage of $V p / 3$ across it or 1 volt. An "ON" segment has a 0.63 Vp signal across it or 1.92 V for $\mathrm{VCC}-\mathrm{VDISP}=3 \mathrm{~V}$.

Since the VDISP pin is available the user may adjust the "ON" and "OFF" LCD levels for various manufacturer's displays by changing Vp. Liquid crystal threshold voltage moves down with temperature.


Figure 12: 1/3 Blas LCD Drive

# 3 1/2 Digit Auto-Ranging Analog-to-Digital Converter - Triplex LCD Drive <br> - Display Hold Function 

"OFF" segments may become visible at high LCD operating temperatures. A voltage with a -5 to $-20 \mathrm{mV} /{ }^{\circ} \mathrm{C}$ temperature coefficient can be applied to VDISP to accommodate the liquid crystal temperature operating characteristics if necessary.
The TSC815 internally generates two intermediate LCD drive potentials ( $\mathrm{V}_{\mathrm{H}} \& \mathrm{~V}_{\mathrm{L}}$ ) from a resistive divider (Figure 12) between VCC (Pin 26) and VDISP (Pin 6). The ladder impedance is approximately $150 \mathrm{k} \Omega$. This drive method is commonly known as $1 / 3$ bias. With VDISP connected to digital ground $V_{P} \approx 5.0 \mathrm{~V}$.
The intermediate levels are needed so that drive signals giving RMS "ON" and "OFF" levels can be generated. Figure 13 shows a typical drive signal and the resulting wave forms for "ON" and "OFF" RMS voltage levels across a selected LCD element.

## LCD Displays

Although most users will design their own custom LCD display, several manufacturers offer standard displays for the TSC815. Figure 14 shows a typical display available from Varitronix.

1. Varitronix Ltd.

9/F Liven House, 61-63, King Yip Street
Kwun Tjong, Hong Kong
Tel: 3-410286
TELEX: 36643 VTRAX HX
Part No.: VIM 310-1 Pin Connector
VIM 310-2 Elastomer Connector
USA OFFICE:
VL Electronics Inc.
2775 Glendower Ave.
Los Angeles, CA 90027
Tel. (213) 661-8883
TELEX: 821554
2. Adamant Kogyo Co., LTD.

16-7, Shinden, 1-Chome, Adachi-Ku, Tokyo, 123, Japan
Tel: Tokyo 919-1171


Waveforms to Generate

## External Crystal

The TSC815 is designed to operate with a $32,768 \mathrm{~Hz}$ crystal. This frequency is internally divided by two to give a $61.04 \mu \mathrm{~s}$ clock period. One conversion takes 8000 clock periods or 488.3 msec ( $\approx 2$ conversions/second). Integration time is 1638.5 clock periods or 100 ms .

The 32 kHz quartz crystal is readily available and inexpensive. The 32 kHz crystal is commonly used in digital clocks and counters.

Several crystal sources exists. A partial listing is:

- Statek Corporation

512 N. Main
Orange, CA 92668
(714) 639-7810

TWX: 910-593-1355
TELEX: 67-8394

- Daiwa Sinku Corporation

1389, Shinzaike - AZA-Kono
Hirakacho, Kakogawa Hyogo, Japan
Tel: 0794-26-3211

- International Piezo LTD

24-26, Sze Shan Street
Yau Ton, Hong Kong
TLX: 35454 XTAL HX
Tel: 3-3501151
Contact manufacturer for full specifications.


Figure 14: Typical LCD Display Configuration TSC815 Triplex

## "Buzzer" Drive Signal

The TSC815 BUZ output (Pin 3) will drive a piezo electric audio transducer. The signal is activated to indicate an input overrange condition for current and voltage measurements or continuity during resistance measurements.
During a resistance measurement a reading less than 19 on any full-scale range causes a continuous 4 kHz signal to be output. This is used as a continuity indication.

A voltage or current input measurement overrange is indicated by a non-continuous 4 kHz signal at the BUZ output. The LCD display MSD also flashes and the three least significant digits are set to display zero. The buzzer drive signal for overrange is shown in Figure 15. The buzzer output is active for any reading over 2000 counts in both manual and autorange operation. The buzzer is activated during an extended resolution measurement.
The BUZ signal swings from VCC (Pin 26) to Digital Ground (Pin 55). The signal is at VCC when not active.
The buz output is also activated for 15 ms whenever a range change is made in auto-range or manual operation. Changing the type of measurement (voltage, current, or resistance) or measurement option ( $\overline{\mathrm{AC}} / \mathrm{DC}, \Omega / \overline{\mathrm{LOS}}$ ) will also activate the buzzer output for 15 ms . A range change during a current measurement will not activate the buzzer output.

| PAD | BP1 | BP2 | BP3 | PAD | COM1 | COM2 | COM3 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | BP1 | 1 | 1 | 19 | 1 | 1 | 1 |
| 2 | 1 | BP2 | $/$ | 20 | 1 | 1 | / |
| 3 | / | / | BP3 | 21 | / | / | 1 |
| 4 | 1 | LOS | A | 22 | 1 | 1 | 1 |
| 5 | 1 | $\Omega$ | V | 23 | 1 | / | 1 |
| 6 | HOLD | k | m | 24 | 1 | / | 1 |
| 7 | b1 | c1 | 1 | 25 | 1 | / | 1 |
| 8 | a1 | $g 1$ | d1 | 26 | 1 | 1 | 1 |
| 9 | $f 1$ | 01 | 1 | 27 | 1 | , | / |
| 10 | b2 | c2 | P2 | 28 | / | 1 | 1 |
| 11 | a2 | $\mathrm{g}^{2}$ | d2 | 29 | 1 | / | 1 |
| 12 | $f 2$ | *2 | 1 | 30 | / | / | / |
| 13 | b3 | c3 | P3 | 31 | 1 | / | / |
| 14 | a3 | g3 | d3 | 32 | 1 | 1 | $/$ |
| 15 | $f 3$ | *3 | 1 | 33 | 1 | 1 | 1 |
| 16 | b4 | c4 | P4 | 34 | 1 | / | 1 |
| 17 | AC | $\square$ | AUTO | 35 | $/$ | 1 | / |
| 18 | - + | -MEM | / | 36 | / | 1 | / |

TSC815


Figure 15: TSC815 Timing Waveform for Buzzer Output

## Display Decimal Point Selection

The TSC815 provides a decimal point LCD drive signal. The decimal point position is a function of the selected full-scale range as shown in Table 6.
Table 6: Decimal Point Selection

|  | $\mathbf{1}$ | $\bullet$ | $\mathbf{9}$ | $\bullet$ |
| :--- | :---: | :---: | :---: | :---: |
| $\mathbf{F}$ | $\mathbf{9}$ | $\bullet$ |  |  |
|  | DP3 | DP2 | DP1 |  |
| $2000 \mathrm{~V}, 2000 \mathrm{k} \Omega$ | OFF | OFF | OFF |  |
| $200.0 \mathrm{~V}, 200.0 \mathrm{k} \Omega$ | OFF | OFF | ON |  |
| $20.00 \mathrm{~V}, 20.00 \mathrm{k} \Omega$ | OFF | ON | OFF |  |
| $2.000 \mathrm{~V}, 2.000 \mathrm{k} \Omega$ | ON | OFF | OFF |  |
| $200.0 \mathrm{mV}, 200.0 \Omega$ | OFF | OFF | ON |  |
| 20.00 mA | OFF | ON | OFF |  |
| 200.0 mA | OFF | OFF | ON |  |

## AC to DC Converter Operational Amplifier

The TSC815 contains an on chip operational amplifier that may be connected as a rectifier for AC to DC voltage and current measurements. Typical operational amplifier characteristics are:

- Slew Rate: $1 \mathrm{~V} / \mu \mathrm{s}$
- Unity Gain Bandwidth: 0.4 MHz
- Open Loop Gain: 44 dB
- Output Voltage Swing (Load $=10 \mathrm{k} \Omega) \pm 1.5 \mathrm{~V}$
(Reference to Analog Common)
When the AC measurement option is selected the input buffer receives an input signal through switch S14 rather than switch S11 (See Figure 2). With external circuits the AC operating mode can be used to perform other types of functions within the constraints of the internal operational amplifier. External circuits that perform true RMS conversion or a peak hold function are typical examples.


## Component Selection

## Integration Resistor Selection

The TSC815 automatically selects one of two external integration resistors. RVIBUF (Pin 52) is selected for voltage and current measurement. RSBUF (Pin 51) is selected for resistance measurements.

## RVIBUF Selection (PIN 52)

In auto-range operation the TSC815 operates with a 200 mV maximum full-scale potential at VI (Pin 42). Resistive dividers at VR2 (Pin 39), VR3 (Pin 38), VR4 (Pin 41) and VR5 (Pin 40) are automatically switched to maintain the 200 mV full-scale potential.
In manual mode the extended operating mode is activated giving a 300 mV full-scale potential at VI (Pin 42).
The integrator output swing should be maximized but saturations must be avoided. The integrator will swing within 0.45 V of VCC (Pin 26) and 0.5 V of VSSA (Pin 54) without saturating. $\mathrm{A} \pm 2 \mathrm{~V}$ swing is suggested. The value of RVIBUF is easily calculated assuming a worst case extended resolution input signal:

$$
\begin{aligned}
& \mathrm{V}_{\text {INT }}=\text { Integrator Swing }= \pm 2 \mathrm{~V} \\
& \mathrm{~T}_{\mathrm{I}}=\text { Integration Time }=100 \mathrm{~ms} \\
& \mathrm{C}_{\mathrm{I}}=\text { Integration Capacitor }=0.1 \mathrm{\mu f} \\
& \mathrm{~V}_{\mathrm{MAX}}=\text { Maximum Input at } \mathrm{V}_{1}=300 \mathrm{mV}
\end{aligned}
$$

$$
\text { RVIBUF }=\frac{\operatorname{V}_{\operatorname{MAX}\left(T_{I}\right)}}{\operatorname{VINT}\left(C_{\mid}\right)} \approx 150 \mathrm{k} \Omega
$$

## R $\Omega$ BUF Selection (Pin 51)

In ratiometric resistance measurements the signal at Rx (Pin 47) is always positive with respect to analog common. The integrator swings negative.
The worst case integrator swing is for the $200 \Omega$ range with the manual, extended resolution option.
The input voltage $V X$ ( $\operatorname{Pin} 47$ ) is easily calculated (Figure 16).
VANCOM $=$ Potential at Analog Common $\approx 2.7 \mathrm{~V}$
R8 $\quad=220 \Omega$
$R_{1}=163.85 \Omega$
$R x \quad=300 \Omega$
Rs $\quad=$ Internal Switch 33 Resistance $\approx 600 \Omega$
$R \Omega B U F=\frac{\left(V C C-V_{A N C O M}\right) R x}{\left(R x+R_{s}+R_{1}+R_{8}\right)}=0.63 \mathrm{~V}$
For a 3.1 V integrator swing the value of R $\Omega B U F$ is easily calculated:

$$
\begin{array}{ll}
\mathrm{V}_{\mathrm{INT}} & =\text { Integrator Swing }=3.1 \mathrm{~V} \\
\mathrm{~T}_{\mathrm{I}} & =\text { Integration Time }=100 \mathrm{~ms} \\
\mathrm{C}_{\mathrm{I}} & =\text { Integration Cap. }=0.1 \mu \mathrm{f} \\
\mathrm{RxMax} & =300 \Omega \\
\mathrm{~V} \times \mathrm{Max} & =700 \mathrm{mV} \\
\mathrm{R} \Omega \mathrm{BUF} & =\frac{(\mathrm{VxMAX})\left(\mathrm{T}_{I}\right)}{\mathrm{C}_{I}\left(\mathrm{VINT}^{\prime}\right)} \approx 220 \mathrm{k} \Omega
\end{array}
$$



Figure 16: R $\Omega B$ UF Calculation ( $200 \Omega$ Manual Operation)

## 3 1/2 Digit Auto-Ranging Analog-to-Digital Converter <br> - Triplex LCD Drive

With a low battery voltage of 6.6 V analog common will be approximately 3.6 V above the negative supply terminal. With the integrator swinging down from analog common toward the negative supply a 3.1 V swing will set the integrator output to 0.5 V above the negative supply.

## CINT, CAZ and CREF Capacitors

The integration capacitor, CINT, must have low dielectric absorption. A 0.1 uf polypropylene capacitor is suggested. The auto-zero capacitor, CAZ, and reference capacitor, CREF, should be selected for low leakage and dielectric absorption. Polystyrene capacitors are good choices.

## Reference Voltage Adjustment

The TSC815 contains a low temperature drift internal voltage reference. The analog common potential (Pin 27) is established by this reference. Maximum drift is a low $75 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$. Analog common is designed to be approximately 2.6 V below VCC (Pin 26). A resistive divider (R18/R19, Figure 1) sets the TSC815 reference input voltage (REFHI, Pin 32) to approximately 163.85 mV .
With an input voltage near full-scale on the 200 mV range, R19 is adjusted for the proper reading.

## Display Hold Feature

The LCD display will not be updated when HOLD (Pin 57) is connected to Ground (Pin 55). Conversions are made but the display is not updated. A HOLD Mode LCD annunciator is activated when HOLD is low.
The LCD HOLD annunciator is activated through the triplex LCD driver signal at Pin 12.

## Flat Package Socket

Sockets suitable for prototype work are available. A USA source is:
Nepenthe Distribution
2471 East Bayshore
Suite 520
Palo Alto, CA 94303
(415) 856-9332

TWX: 910-373-2060
(a) "BQ" Socket Part No.: IC51-064-042 BQ
(b) "SQ" Socket Part No.: IC51-064-042 SQ

## Resistive Ladder Networks

Resistor attenuator networks for voltage and resistance measurement are available from:

Caddock Electronics
1717 Chicago Avenue
Riverside, CA 92507
TEL: (714) 788-1700
TWX: 910-332-6108

| Attenuator <br> Accuracy | Attenuator <br> Type | Caddock <br> Part Number |
| :---: | :---: | :---: |
| $0.1 \%$ | Voltage | $1776-$ C441 |
| $0.25 \%$ | Voltage | $1776-$ C44 |
| $0.25 \%$ | Resistance | T 1794-204-1 |

## Package Outline



## General Description

In many applications a graphical display is preferred over a digital display. Knowing a process or system operates, for example, within design limits is more valuable than a direct system variable readout. A bar or moving dot display supplies information precisely without requiring further interpretation by the viewer.

The TSC826 is a complete analog-to-digital converter with direct liquid crystal (LCD) display drive. The 40 LCD data segments plus zero driver give a $2.5 \%$ resolution bar display. Full-scale differential input voltage range extends from 20 mV to 2 V . The TSC826 sensitivity is $500 \mu \mathrm{~V}$. A low drift $35 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ internal reference, LCD backplane oscillator and driver, input polarity LCD driver, and overrange LCD driver make designs simple and low cost. The CMOS design requires only $125 \mu \mathrm{~A}$ from a 9 V battery. In +5 V systems a TSC7660 DC to DC converter can supply the -5 V supply. The differential analog input leakage is a low 10 pA .

Two display formats are possible. The BAR mode display is like a "thermometer" scale. The LCD segment driver that equals the input plus all below it are on. The DOT mode activates only the segment equal to the input. In either mode the polarity signal is active for negative input signals. An overrange input signal causes the display to flash and activates the overrange annunciator. A hold mode can be selected that freezes the display and prevents updating.

The dual slope integrating conversion method with autozero phase maximizes noise immunity and eliminates zeroscale adjustment potentiometers. Zero-scale drift is a low $5 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$. Conversion rate is typically 5 per second and is adjustable by a single external resistor.

A compact, $0.5^{\prime \prime}$ square, flat package minimizes PC board area. The high pin count LSI package makes multiplexed LCD displays unnecessary. Low cost, direct drive LCD displays offer the widest viewing angle and are readily available. A standard display is available now for TSC826 prototyping work.

## Features

- Bipolar A/D Conversion
- $2.5 \%$ Resolution
- Direct LCD Display Drive
- "Thermometer" Bar or Dot Display
- 40 Data Segments Plus Zero
- Overrange Plus Polarity Indication
- Precision On-Chip Reference .............. $35 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$
- Differential Analog Input
- Low Input Leakage $\qquad$
- Display Flashes on Overrange

10 pA

- Display Hold Mode
- Auto-Zero Cycle Eliminates Zero Adjust Potentiometer
- 9 V Battery Operation
- Low Power Consumption $\qquad$ 1.1 mW
- 20 mV to 2.0 V Full-Scale Operation
- Non-Multiplexed LCD Drive for Maximum Viewing Angle

Ordering Information

| Part No. | Package | Temperature <br> Range |
| :--- | :---: | ---: |
| TSC826CBQ | 60-Pin Plastic <br> Quad Flat Package <br> Formed Leads | $0^{\circ} \mathrm{C}$ to $70^{\circ} \mathrm{C}$ |
| TSC826CSQ | 60-Pin Plastic <br> Quad Flat Package <br> Straight Leads | $0^{\circ} \mathrm{C}$ to $70^{\circ} \mathrm{C}$ |
| TSC826Y | CHIP | $0^{\circ} \mathrm{C}$ to $70^{\circ} \mathrm{C}$ |

## Pin Configuration



# A/D Converter With <br> Bar Graph Display Output - 2.5\% Resolution Direct LCD Drive Bar/Dot Display Format 

## Absolute Maximum Ratings

| Supply Voltage ( $\mathrm{V}^{+}$to $\mathrm{V}^{-}$) | 15 V |
| :---: | :---: |
| Analog Input Voltage (either input) ${ }^{(1)}$ | $\mathrm{V}^{+}$to $\mathrm{V}^{-}$ |
| Package Power Dissipation |  |
| Flat Package (B, S) | 500 mW |

## Operating Temperature

("C" Devices)
$0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$
Storage Temperature .................... $-65^{\circ} \mathrm{C}$ to $+160^{\circ} \mathrm{C}$
Lead Temperature (Soldering, 60 sec ) .............. $300^{\circ} \mathrm{C}$

Electrical Characteristics: $\mathrm{V}_{S}=9 \mathrm{~V}, \mathrm{ROSC}=430 \mathrm{k} \Omega, T A=25^{\circ} \mathrm{C}$, Full-Scale $=20 \mathrm{mV}$ unless otherwise stated.

| NO. | SYMBOL | PARAMETER | TEST <br> CONDITIONS | MIN | TSC826 <br> TYP | MAX |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |

Notes:

1. Input voltages may exceed the supply voltages when the input current is limited to $100 \mu \mathrm{~A}$.
2. Static sensitive device. Unused devices should be stored in conductive material to protect devices from static discharge and static fields.
3. Backplane drive is in phase with segment drive for "off" segment and $180^{\circ} \mathrm{C}$ out of phase for "on" segment. Frequency is 10 times conversion rate.
4. Logic input pins $58,59,60$ should be connected through $1 \mathrm{M} \Omega$ series resistors to $\sqrt{\mathrm{S}}$ for logic 0 .

## A/D Converter With

## Bar Graph Display Output

- 2.5\% Resolution
- Direct LCD Drive
- Bar/Dot Display Format


## Pin Description and Function

| PIN NO. | NAME | DESCRIPTION |
| :---: | :---: | :---: |
| 1 | Analog Common | Establishes the internal analog ground point. Analog common is set to 2.9 V below the positive supply by an internal zener reference circuit. The voltage difference between $\mathrm{V}_{s}^{+}$and analog-common can be used to supply the TSC826 voltage reference input at REF IN (Pin 4). |
| 2 | +IN | Positive analog signal input. |
| 3 | -In | Negative analog signal input. |
| 4 | REF IN | Reference voltage positive input. Measured relative to analog-common. REF $\mathbb{N} \approx$ Full-Scale/2. |
| 5 | Cref + | Reference capacitor connection. |
| 6 | Cref - | Reference capacitor connection. |
| 7 | $\mathrm{V}_{\text {s }}^{+}$ | Positive supply terminal. |
| 8 | VBUF | Buffer output. Integration resistor connection. |
| 9 | CAZ | Negative comparator input. Auto-zero capacitor connection. |
| 10 | VINT | Integrator output. Integration capacitor connection. |
| 11 | $V_{s}^{-}$ | Negative supply terminal. |
| 12 | OSC1 | Oscillator resistor (Rosc) connection. |
| 13 | OSC2 | Oscillator resistor (Rosc) connection. |
| 14 | BP | LCD Backplane driver. |
| 15 | BAR 0 | LCD Segment driver: Bar 0 |
| 16 | 1 | 1 |
| 17 | 2 | 2 |
| 18 | 3 | 3 |
| 19 | 4 | 4 |
| 20 | 5 | 5 |
| 21 | 6 | 6 |
| 22 | 7 | 7 |
| 23 | 8 | 8 |
| 24 | 9 | 9 |
| 25 | 10 | 10 |
| 26 | 11 | 11 |
| 27 | 12 | 12 |
| 28 | 13 | 13 |
| 29 | 14 | 14 |
| 30 | 15 | 15 |
| 31 | 16 | 16 |
| 32 | 17 | 17 |
| 33 | 18 | 18 |
| 34 | 19 | 19 |
| 35 | 20 | 20 |
| 36 | 21 | 21 |
| 37 | 22 | 22 |
| 38 | 23 | 23 |

Pin Description and Function (Cont.)

| PIN NO. | NAME | DESCRIPTION |
| :---: | :---: | :---: |
| 39 | BAR 24 | BAR Segment driver: Bar 24 |
| 40 | 25 | 25 |
| 41 | 26 | 26 |
| 42 | 27 | 27 |
| 43 | 28 | 28 |
| 44 | 29 | 29 |
| 45 | 30 | 30 |
| 46 | 31 | 31 |
| 47 | 32 | 32 |
| 48 | 33 | 33 |
| 49 | 34 | 34 |
| 50 | 35 | 35 |
| 51 | 36 | 36 |
| 52 | 37 | 37 |
| 53 | 38 | 38 |
| 54 | 39 | 39 |
| 55 | 40 | 40 |
| 56 | OR | LCD segment driver that indicates input out-of-range condition. |
| 57 | POL- | LCD segment driver that indicates input signal is negative. |
| 58 | BAR/DOT | Input logic signal that selects bar or dot display format. Normally in bar mode. Connect to $V \bar{s}$ through $1 \mathrm{M} \Omega$ resistor for Dot format. |
| 59 | $\overline{\text { HOLD }}$ | Input logic signal that prevents display from changing. Pulled high internally to inactive state. Connect to Vs through $1 \mathrm{M} \Omega$ series resistor for HOLD mode operation. |
| 60 | $\overline{\text { TEST }}$ | Input logic signal. Sets TSC805 to BAR display mode. Bar 0 to 40, plus OR flash on and off. The POLLCD driver is on. Pulled high internally to inactive state. Connect to $\mathrm{V}_{\mathrm{s}}^{-}$with $1 \mathrm{M} \Omega$ series resistor to activate. |

## A/D Converter With

Bar Graph Display Output

- 2.5\% Resolution
- Direct LCD Drive
- Bar/Dot Display Format

Typical TSC826 Circuit Connection (Figure 1)


## Dual Slope Conversion Principles

The TSC826 is a dual slope, integrating analog-to-digital converter. The conventional dual slope converter measurement cycle has two distinct phases:

- Input Signal Integration
- Reference Voltage Integration (Deintegration)

The input signal being converted is integrated for a fixed time period (Tsı). Time is measured by counting clock pulses. An opposite polarity constant reference voltage is then integrated until the integrator output voltage returns to zero. The reference integration time is directly proportional to the input signal (TRI). (Figure 2).

In a simple dual slope converter a complete conversion requires the integrator output to "ramp-up" and "ramp-down." A simple mathematical equation relates the input signal reference voltage and integration time:
where:

$$
\frac{1}{R C} \int_{0}^{T_{S I}} V_{I N}(t) d t=\frac{V_{R} T_{R I}}{R C}
$$

$V_{R}=$ Reference Voltage
$V_{S I}=$ Signal Integration Time (Fixed)
$T_{R I}=$ Reference Voltage Integration Time (Variable)
For a constant $V_{I N}: \quad V_{I N}=V_{R} \frac{T_{R I}}{T_{S I}}$


Figure 2: Basic Dual Slope Converter

TSC826

The dual slope converter accuracy is unrelated to the integrating resistor and capacitor values as long as they are stable during a measurement cycle. An inherent benefit is noise immunity. Noise spikes are integrated or averaged to zero during the integration periods. Integrating ADCs are immune to the large conversion errors that plague successive approximation converters in high noise environments. interfereing signals with frequency components at multiples of the averaging period will be attenuated. (Figure 3).

The TSC826 converter improves the conventional dual slope conversion technique by incorporating an auto-zero phase. This phase eliminates zero-scale offset errors and drift. A potentiometer is not required to obtain a zero output for zero input.


Figure 3: Normal-Mode Rejection of Dual Slope Converter


Figure 4: TSC826 Analog Section

## A/D Converter With

## Bar Graph Display Output

## - 2.5\% Resolution

- Direct LCD Drive
- Bar/Dot Display Format


## Theory of Operation <br> Analog Section

In addition to the basic signal integrate and deintegrate cycles discussed above the TSC826 incorporates an autozero cycle. This cycle removes buffer amplifier, integrator, and comparator offset voltage error terms from the conversion. A true digital zero reading results without external adjusting potentiometers. A complete conversion consists of three cycles: an auto-zero, signal integrate and reference integrate cycle. See Figure 4 and 5.

## Auto-Zero Cycle

During the auto-zero cycle the differential input signal is disconnected from the circuit by opening internal analog gates. The internal nodes are shorted to analog common (internal analog ground) to establish a zero input condition. Additional analog gates close a feedback loop around the integrator and comparator. This loop permits comparator offset voltage error compensation. The voltage level established on CAZ compensates for device offset voltages.

The auto-zero cycle length is 19 counts minimum. Unused time in the deintegrate cycle is added to the auto-zero cycle.

## Signal Integration Cycle

The auto-zero loop is opened and the internal differential inputs connect to +IN and -IN. The differential input signal is integrated for a fixed time period. The TSC826 signal integra-
tion period is 20 clock periods or counts. The externally set clock frequency is devided by 32 before clocking the internal counters. The integration time period is:

$$
\mathrm{TsI}=\frac{32}{\text { Fosc }} \times 20
$$

Where:

## Fosc = External Clock Frequency

The differential input voltage must be within the device common-mode range when the converter and measured system share the same power supply common (ground). If the converter and measured system do not share the same power supply common, -IN should be tied to analog-common. This is the usual connection for battery operated systems. Polarity is determined at the end of signal integrate signal phase. The sign bit is a true polarity indication in that signals less than 1 LSB are correctly determined. This allows precision null detection limited only by device noise and system noise.

## Reference Integrate Cycle

The final phase is reference integrate or deintegrate. -IN is internally connected to analog common and $+I N$ is connected with the correct polarity to cause the integrator output to return to zero. The time required for the output to return to zero is proportional to the input signal and is between 0 and 40 counts. The digital reading displayed is:

$$
20 \frac{\mathrm{~V}_{\mathrm{IN}}}{\mathrm{~V}_{\mathrm{REF}}}
$$



Figure 5: TSC826 Conversion Has Three Phases

## A/D Converter With Bar Graph Display Output - 2.5\% Resolution - Direct LCD Drive

## System Timing

The oscillator frequency is divided by 32 prior to clocking the internal counters. The three phase measurement cycle takes a total of 80 clock pulses. The 80 count cycle is independent of input signal magnitude.
Each phase of the measurement cycle has the following length:

- Auto-Zero Phase: 19 to 59 Counts

For signals less than full-scale the auto-zero phase is assigned the unused reference integrate time period.

- Signal Integrate: 20 Counts

This time period is fixed. The integration period is:

$$
\mathrm{TSI}_{\mathrm{SI}}=20\left[\frac{32}{\text { FOSC }}\right]
$$

Where Fosc is the externally set clock frequency.

- Reference Integrate: 0 to 41 Counts


## Reference Voltage Selection

A full-scale reading requires the input signal be twice the reference voltage. The reference potential is measured between REF IN (Pin 4) and Analog-Common (Pin 1).

| Required Full-Scale Voltage | V $_{\text {REF }}$ |
| :---: | ---: |
| 20 mV | 10 mV |
| 2 V | 1 V |

The internal voltage reference potential available at analogcommon will normally be used to supply the converters reference. This potential is stable whenever the supply potential is greater than approximately 7 V . In applications where an externally generated reference voltage is desired refer to Figure 6.

The reference voltage is adjusted with a near full-scale input signal. Adjust for proper LCD display readout.


Figure 6: External Reference

## Component Value Selection Integrating Resistor (RINT)

The desired full-scale input voltage and output current capability of the input buffer and integrator amplifier set the integration resistor value. The internal class A output stage amplifiers will supply a $1 \mu \mathrm{~A}$ drive current with minimal linearity error. RINT is easily calculated for a $1 \mu \mathrm{~A}$ full-scale current:

$$
\mathrm{R}_{\mathrm{INT}}=\frac{\text { Full-Scale Input Voltage }(\mathrm{V})}{1 \times 10^{-6}}=\frac{\text { VFS }}{1 \times 10^{-6}}
$$

Where: VFS = Full-Scale Analog Input

## Integrating Capacitor (CINT)

The integrating capacitor should be selected to maximize integrator output swing. The integrator output will swing to within 0.4 V of $\mathrm{V}_{S}^{+}$or $\mathrm{V}_{S}^{-}$without saturating.
The integrating capacitor is easily calculated:


Where: VINT = Integrator Swing
FOSC = Oscillator Frequency
The integrating capacitor should be selected for low dielectric absorption to prevent roll-over errors. Polypropylene capacitors are suggested.

## Auto-Zero Capacitor (CAZ)

CAZ should be 2-3 times larger than the integration capacitor. A polypropylene capacitor is suggested. Typical values from $0.14 \mu \mathrm{f}$ to $0.068 \mu \mathrm{f}$ are satisfactory.

## Reference Capacitor (CREF)

A $1.0 \mu \mathrm{f}$ capacitor is suggested. Low leakage capacitors such as polypropylene are recommended.
Several capacitor/resistor combinations for common fullscale input conditions are given in Table 1.

Table 1: Suggested Component Values

| Component | $2 \mathrm{~V}$ <br> Full-Scale $V_{R E F} \approx 1 \mathrm{~V} V_{R E F}$ | $\begin{aligned} & 200 \mathrm{mV} \\ & \text { Full-Scale } \\ & \approx 100 \mathrm{mV} \end{aligned}$ | $\begin{array}{r} 20 \mathrm{mV} \\ \text { Full-Scale } \\ \mathrm{V}_{\text {REF }} \approx 10 \mathrm{mV} \end{array}$ |
| :---: | :---: | :---: | :---: |
| Rint | $2 \mathrm{M} \Omega$ | $200 \mathrm{k} \Omega$ | $20 \mathrm{k} \Omega$ |
| CINT | $0.033 \mu \mathrm{f}$ | $0.033 \mu \mathrm{f}$ | $0.033 \mu \mathrm{f}$ |
| Cref | $1 \mu \mathrm{f}$ | $1-\mu \mathrm{f}$ | $1 \mu \mathrm{f}$ |
| CAZ | $0.068 \mu \mathrm{f}$ | $0.068 \mu \mathrm{f}$ | $0.14 \mu \mathrm{f}$ |
| Rosc | $430 \mathrm{k} \Omega$ | $430 \mathrm{k} \Omega$ | $430 \mathrm{k} \Omega$ |

[^2]
# A/D Converter With Bar Graph Display Output <br> - 2.5\% Resolution <br> - Direct LCD Drive <br> - Bar/Dot Display Format 

## Differential Signal Inputs (+IN (Pin 2), -IN (Pin 3))

The TSC826 is designed with true differential inputs and accepts input signals within the input stage common-mode voltage range ( VCM ). The typical range is $\mathrm{V}^{+}-1.0$ to $\mathrm{V}^{-}+1 \mathrm{~V}$. Common-mode voltages are removed from the system when the TSC826 operates from a battery or floating power source (Isolated form measured system) and -IN is connected to analog-common ( VCOM ).

In systems where common-mode voltages exist the TSC826 72 dB common-mode rejection ratio minimizes error. Common-mode voltages do, however, affect the integrator output level. Integrator output saturation must be prevented. A worse case condition exists if a large positive VCM exists in conjunction with a full-scale negative differential signal. The negative signal drives the integrator output positive along with $\mathrm{V}_{\mathrm{Cm}}$. For such applications, the integrator output swing can be reduced below the recommended 2.0 V full-scale swing. The integrator output will swing within 0.3 V of $\mathrm{V}_{\mathrm{S}}^{+}$or $\mathrm{V} \overline{\mathrm{s}}$ without increased linearity error.

## Digital Section

The TSC826 contains all the segment drivers necessary to drive a liquid crystal display (LCD). An LCD backplane driver is included. The backplane frequency is the external clock frequency divided by 256. A $430 \mathrm{k} \Omega$ OSC gets the backplane frequency to approximately 55 Hz with a 5 V nominal amplitude. When a segment driver is in phase with the backplane signal the segment is "OFF." An out-of-phase segment drive signal causes the segment to be "ON" or visible. This AC drive configuration results in negligible DC voltage across each LCD segment. This insures long LCD display life. The polarity segment driver, -POL, is "ON" for negative analog inputs. If $+I N$ and $-I N$ are reversed this indicator would reverse. The TSC826 transfer function is shown in Figure 7.


Figure 7: TSC826 Transfer Function

## BAR/DOT Input (Pin 58)

The BAR/ $\overline{D O T}$ input allows the user to select the display format. The TSC826 powers up in the BAR mode. Select the DOT display format by connecting BAR/DOT to the negative supply (Pin 11) through a $1 \mathrm{M} \Omega$ resistor.

## HOLD Input (Pin 59)

The TSC826 data output latches are not updated at the end of each conversion if $\overline{\mathrm{HOLD}}$ is tied to the negative supply (Pin 11) through a $1 \mathrm{M} \Omega$ series resistor. The LCD display continuously displays the previous conversion result.

The HOLD pin is normally pulled high by an internal pull-up.

## TEST Input (Pin 60)

The TSC826 enters a test mode with the TEST input connected to the negative supply (Pin 11). The connection must be made through a $1 \mathrm{M} \Omega$ resistor. The $\overline{T E S T}$ input is normally internally pulled high. A low input sets the output data latch to all ones. The BAR display mode is set. The 41 LCD output segments (zero plus 40 data segments) and overrange annunciator flash on and off at $1 / 4$ the conversion rate. The polarity annunciator (POL-) segment will be on but not flashing.

## Overrange Display Operation (OR, Pin 56)

An out-of-range input signal will be indicated on the LCD display by the OR annunciator driver ( Pin 56 ) becoming active.

In the BAR display formate the 41 bar segments and the overrange annunciator, OR, will flash ON and OFF. The flash rate is one fourth the conversion rate (FOSC/2560).
In the DOT display mode, OR flashes and all other data segment drivers are off.

## Polarity Indication (POL-, Pin 57)

The TSC826 converts and displays data for positive and negative input signals. The POL- LCD segment driver (Pin 57 ) is active for negative signals.

## Oscillator Operation

The TSC826 external oscillator frequency, FOSC, is set by resistor ROSC connected between pins 12 and 13. The oscillator frequency vs resistance curve is shown in Figure 8.

# A/D Converter With Bar Graph Display Output - 2.5\% Resolution 



Figure 8: Oscillator Frequency vs. ROSC
FOSC is divided by 32 to provide an internal system clock, FSYS. Each conversion requires 80 internal clock cycles. The internal system clock is divided by 8 to provide the LCD backplane drive frequency. The display flash rate during an input out-of-range signal is set by dividing FSYS by 320. (See Figure 9)


Figure 9: Internal Oscillator Operation

The internal oscillator may be bypassed by driving OSCl (Pin 12) with an external signal generator. OSC2 (Pin 13) should be left unconnected.

The oscillator should swing from $\mathrm{V}_{\mathrm{S}}^{+}$to $\mathrm{V}_{\mathrm{S}}^{-}$in single supply operation (Figure 10A). In dual supply operation the signal should swing from power supply ground to $\mathrm{V}_{\mathrm{S}}^{+}$.


Figure 10: External Oscillator Connection

## LCD Display Format

The input signal can be displayed in two formats (Figure 11). The BAR/DOT input (Pin 58) selects the format. The TSC826 measurement cycle operates identically for either mode.

## BAR Format

The TSC826 power-ups in the BAR mode. BAR/DOT is pulled high internally. This display format is similar to a thermometer display. All bars/LCD segments, including zero, below the bar/LCD segment equalingd the input signal level are on. A half-scale input signal, for example, would be displayed with BAR 0 to BAR 20 on.

## DOT Format

By connecting BAR/DOT to $V_{S}^{-}$through a $1 \mathrm{M} \Omega$ resistor the DOT mode is selected. Only the BAR LCD segment equalling the input signal is on. The zero segment is on for zero input.
This mode is useful for moving cursor or "needle" applications.

A/D Converter With
Bar Graph Display Output

- 2.5\% Resolution
- Direct LCD Drive
- Bar/Dot Display Format

TSC826
A. BAR MODE

B. DOT MODE


2. $\operatorname{INPUT}=5 \%$ of FULL-SCALE


Figure 11: Display Option Formats

## LCD Displays

Most end products will use a custom LCD display for final production. Custom LCD displays are low cost and available from all manufacturers. The TSC826 interfaces to non-multiplexed LCD displays. A backplane driver is included on chip.

To speed initial evaluation and prototype work a standard TSC826 LCD display is available from Varitronix.
Varitronix Ltd.
9/F Linen House, 61-63, King Yip Street
Kwun Tjong, Hong Kong
Tel: 3-410286
TELEX: 36643 VTRAX HX
USA Office:
VL Electronics Inc.
2775 Glendower Avenue
Los Angeles, CA 900027
Tel: (213) 661-8883
TELEX: 821554

- Part No.: VBG412-1 (Pin Connectors)
- Part No.: VBG412-2 (Elastomer Connectors)

Other standard LCD displays suitable for development work are available in both linear and circular formats. One manufacturer is:

UCE Inc.
24 Fitch Street
Norwalk, Conn. 06855
(203) 838-7509

- Part No. 5040: 50 segment circular display with

3 digit numeric scale.

- Part No. 5020: 50 segment linear display.


## LCD Backplane Driver (Pin 14)

Additional drive electronics is not required to interface the TSC826 to an LCD display. The TSC826 has an on-chip backplane generator and driver. The backplane frequency is:

$$
\mathrm{FBP}=\mathrm{FOSC} / 256
$$

Figure 12 gives typical backplane driver rise/fall time vs backplane capacitance.


Figure 12: Backplane Driver Rise/Fall Time vs Capacitance

## Flat Package Socket

Sockets suitable for prototype work are available. A USA source is:
Nepenthe Distribution
2471 East Bayshore
Suite 520
Palo Alto, California 94303
(415) 856-9332

TWX: 910-373-2060
(a) "BQ" Socket Part No.: IC51-064-042 BQ
(b) "SQ" Socket Part No.: IC51-064-042 SQ

## Package Outline



## General Description

The TSC7106A and TSC7107A $31 / 2$ digit direct display drive analog-to-digital converters allow existing 7106/7107 based systems to be upgraded. Each device offers a precision internal voltage reference featuring a $20 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ typical, $50 \mathrm{ppm}{ }^{\circ} \mathrm{C}$ maximum temperature drift coefficient. This represents a 4 to 7 times improvement over similar 3 1/2 digit converters. Existing 7106 or 7107 based systems may be upgraded without changing external passive component values. The need for a costly, space consuming external reference is removed. The TSC7107A drives common anode light emitting diode (LED) displays directly with an 8 mA drive current per segment. A low cost, high resolution indicating meter requires only a display, four resistors, and tour capacitors. The TSC7106A low power drain and 9 V battery operation make it suitable for portable applications.
The TSC7106A/TSC7107A reduces linearity error to less than 1 count. Rollover error-- the difference in readings for equal magnitude but opposite polarity input signals - is below $\pm 1$ count. High impedance differential inputs offer 1 pA leakage current and a $1012 \Omega$ input impedance. The differential reference input allows ratiometric measurements for ohms or bridge transducer measurements. The $15 \mu \mathrm{Vp}-\mathrm{p}$ noise performance guarantees a "rock solid" reading. The auto-zero cycle guarantees a zero display reading with a zero volt input.
The TSC7106A/TSC7107A dual slope conversion technique


Figure 1: Typical TSC7106A Operating Circuit

## Features

- Internal Reference with Low

$$
\text { Temperature Drift . ................... } 20 \text { ppm } /{ }^{\circ} \mathrm{C} \text { Typical }
$$ $50 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ Maximum

- Drives LCD or LED Displays Directly
- Guaranteed Zero Reading with Zero Input
- Low Noise for Stable Display
- Auto-Zero Cycle Eliminates Need for Zero Adjustment
- True Polarity Indication for Precision Null Applications
- Convenient 9 V Battery Operation (TSC7106A)
- High Impedance CMOS Differential Inputs ..... $1012 \Omega$
- Differential Reference Inputs Simplify Ratiometric Measurements
- Low Power Operation
........................... 10 mW
- Available in 60-Pin Plastic Flat Package
automatically rejects interference signals if the converters integration time is set to a multiple of the interference signal period. This is especially useful in industrial measurement environments where 50,60 and 400 Hz line frequency signals are present.
The TSC7106A/TSC7107A are available in a small 60-pin flat package for compact designs. DIP devices are offered in an industrial temperature range and with burn-in lasting for 160 hours at $+125^{\circ} \mathrm{C}$.
Where long battery life is needed see the TSC7126 or the TSC7126A data sheets.


Figure 2: Typical TSC7107A Operating Circuit

## TSC7106A (LCD Drive) TSC7107A (LED Drive)

## 3 1/2 Digit A/D Converter <br> - Low Drift Internal Reference <br> - Automatic Zero Correction

\section*{Absolute Maximum Ratings TSC7106A <br> 

Stresses above those listed under Absolute Maximum Ratings may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions above those indicated

## TSC7107A

Supply Voltage
$\qquad$
$\mathrm{V}^{-}$......................................................... . . . -9 V

Analog Input Voltage (either input) (Note 1) .... $\mathrm{V}^{+}$to $\mathrm{V}^{-}$
Reference Input Voltage (either input) ........... $\mathrm{V}^{+}$to $\mathrm{V}^{-}$
Clock Input . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . GND to $\mathrm{V}^{+}$
Power Dissipation (Note 2)
CerDIP Package ................................. 1000 mW
Plastic Package .................................... 800 mW
Operating Temperature
"C" Devices ................................... $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$
"I" Devices . . . . . . . . . . . . . . . . . . . . . . . . . . $-25^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$
Storage Temperature .................... $-65^{\circ} \mathrm{C}$ to $+160^{\circ} \mathrm{C}$
Lead Temperature (Soldering, 60 sec ) .............. $300^{\circ} \mathrm{C}$
in the operational sections of the specifications is not implied. Exposure to Absolute Maximum Rating Conditions for extended periods may effect device reliability.

Electrical Characteristics (Note 3)

| CHARACTERISTICS | CONDITIONS | MIN | TYP | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Zero Input Reading | $\begin{aligned} & V_{I N}=0.0 \mathrm{~V} \\ & \text { Full-Scale }=200.0 \mathrm{mV} \end{aligned}$ | -000.0 | $\pm 000.0$ | +000.0 | Digital Reading |
| Ratiometric Reading | $\begin{aligned} & V_{I N}=V_{\text {REF }} \\ & V_{R E F}=100 \mathrm{mV} \end{aligned}$ | 999 | 999/1000 | 1000 | Digital Reading |
| Rollover Error (Difference in Reading for Equal Positive and Negative Reading Near Full-Scale) | $-\mathrm{V}_{\mathrm{IN}}=+\mathrm{V}_{\mathrm{IN}} \simeq 200.0 \mathrm{mV}$ | -1 | $\pm 0.2$ | +1 | Counts |
| Linearity (Max. Deviation From Best Straight Line Fit) | $\begin{aligned} & \text { Full-Scale }=200 \mathrm{mV} \\ & \text { or Full-Scale }=2.000 \mathrm{~V} \end{aligned}$ | -1 | $\pm 0.2$ | +1 | Counts |
| Common-Mode Rejection Ratio (Note 4) | $\begin{aligned} & \text { VCM }= \pm 1 \mathrm{~V}, \mathrm{~V}_{1 N}=0 \mathrm{~V} . \\ & \text { Full-Scale }=200.0 \mathrm{mV} \end{aligned}$ | - | 50 | - | $\mu \mathrm{V} / \mathrm{V}$ |
| Noise (Pk - Pk Value Not Exceeded 95\% of Time) | $\begin{aligned} & \mathrm{VIN}=0 \mathrm{~V} \\ & \text { Full-Scale }=200.0 \mathrm{mV} \end{aligned}$ | - | 15 | - | $\mu \mathrm{V}$ |
| Leakage Current @ Input | $\mathrm{V}_{\mathrm{IN}}=0 \mathrm{~V}$ | - | 1 | 10 | PA |
| Zero Reading Drift | $\begin{aligned} & \text { VIN }=0 \mathrm{~V} \\ & \text { " } \mathrm{C} \text { " Device }=0^{\circ} \mathrm{C} \text { to } 70^{\circ} \mathrm{C} \\ & \mathrm{VIN}=0 \mathrm{~V} \\ & \text { "I" Device }=-25^{\circ} \mathrm{C} \text { to }+85^{\circ} \mathrm{C} \end{aligned}$ | - | 0.2 1.0 | 2 | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
| Scale Factor <br> Temperature Coefficient | $\begin{aligned} & V_{I N}=199.0 \mathrm{mV}, \\ & \text { " } \mathrm{C} \text { " Device }=0^{\circ} \mathrm{C} \text { to } 70^{\circ} \mathrm{C} \\ & \text { (Ext. Ref }=0 \mathrm{ppm} /{ }^{\circ} \mathrm{C} \text { ) } \\ & \text { VIN }=199.0 \mathrm{mV} \\ & \text { "I" Device: }-25^{\circ} \mathrm{C} \text { to }+85^{\circ} \mathrm{C} \end{aligned}$ | - | 1 | 5 20 | $\begin{aligned} & \mathrm{ppm} /{ }^{\circ} \mathrm{C} \\ & \mathrm{ppm} /{ }^{\circ} \mathrm{C} \end{aligned}$ |
| Supply Current (Does Not Include LED Current for TSC7107A) | $\mathrm{V}_{\mathrm{IN}}=0$ | - | 0.8 | 1.8 | mA |
| Analog Common Voltage (With Respect to Pos. Supply) | $25 \mathrm{k} \Omega$ Between Common and Pos. Supply | 2.7 | 3.05 | 3.35 | V |
| Temp. Coeff. of Analog Common (With Respect to Pos. Supply) | $25 \mathrm{k} \Omega$ Between Common and Pos. Supply $0^{\circ} \mathrm{C} \leq T_{A} \leq 70^{\circ} \mathrm{C}$ <br> "C," Commercial Temp. Range Devices | - | 20 | 50 | ppm $/{ }^{\circ} \mathrm{C}$ |
| Temp. Coeff. of Analog Common (with Respect to Pos. Supply) | $25 \mathrm{k} \Omega$ Between Common and Pos. Supply $-25^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq 85^{\circ} \mathrm{C}$ "I," Industrial Temp. Range Devices | - | - | 75 | $\mathrm{ppm} /{ }^{\circ} \mathrm{C}$ |
| $\begin{aligned} & \text { TSC7106A ONLY PK - PK } \\ & \text { Segment Drive Voltage (Note 5) } \end{aligned}$ | $\mathrm{V}^{+}$to $\mathrm{V}^{-}=9 \mathrm{~V}$ | 4 | 5 | 6 | V |

TSC7106A (LCD Drive)
TSC7107A (LED Drive)

Electrical Characteristics (Note 3)

| CHARACTERISTICS | CONDITIONS | MIN | TYP | MAX | UNIT |
| :--- | :--- | :---: | :---: | :---: | :---: |
| TSC7106A ONLY Pk - Pk <br> Backplane Drive Voltage (Note 5) | $\mathrm{V}^{+}$to $\mathrm{V}^{-}=9 \mathrm{~V}$ | 4 | 5 | 6 | V |
| TSC7107A ONLY <br> Segment Sinking Current <br> (Except Pin 19)$\mathrm{V}^{+}=5.0 \mathrm{~V}$ <br> Segment Voltage $=3 \mathrm{~V}$ | 5 | 8.0 | - | mA |  |
| TSC7107A ONLY <br> Segment Sinking Current <br> (Pin 19 Only)$\mathrm{V}^{+}=5.0 \mathrm{~V}$ <br> Segment Voltage $=3 \mathrm{~V}$ | 10 | 16 | - | mA |  |

## NOTES:

1. Input voltages may exceed the supply voltages provided the input current is limited to $\pm 100 \mu \mathrm{~A}$.
2. Dissipation rating assumes device is mounted with all leads soldered to printed circuit board.
3. Unless other wise noted, specifications apply to both the TSC7106A and TSC7107A at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, fCLOCK $=48 \mathrm{kHz}$. TSC 7106 A is tested in the circuit
of Figure 1. TSC7107A is tested in the circuit of Figure 2.
4. Refer to "Differential Input" discussion.
5. Backplane drive is in phase with segment drive for 'off' segment, $180^{\circ}$ out of phase for 'on' segment. Frequency is 20 times conversion rate. Average dc component is less than 50 mV .

## Pin Configuration




## Pin Configuration (Cont.)



## Ordering Information

| Part No. | Package | Pin Layout | Temp. Range | Display Drive |
| :---: | :---: | :---: | :---: | :---: |
| TSC7106ACPL | $\begin{aligned} & \text { 40-Pin } \\ & \text { Plastic Dip } \end{aligned}$ | Normal | $\begin{aligned} & \hline 0^{\circ} \mathrm{C} \text { to } \\ & +70^{\circ} \mathrm{C} \end{aligned}$ | LCD |
| TSC7106ARCPL | $\begin{aligned} & \text { 40-Pin } \\ & \text { Plastic Dip } \end{aligned}$ | Reverse | $\begin{aligned} & 0^{\circ} \mathrm{C} \text { to } \\ & +70^{\circ} \mathrm{C} \end{aligned}$ | LCD |
| TSC7106AIJL | $\begin{aligned} & \text { 40-Pin } \\ & \text { CerDIP } \end{aligned}$ | Normal | $\begin{array}{r} -25^{\circ} \mathrm{C} \text { to } \\ +85^{\circ} \mathrm{C} \end{array}$ | LCD |
| TSC7106ACBQ | 60 -Pin <br> Plastic Flat <br> Package | Formed Leads | $\begin{aligned} & 0^{\circ} \mathrm{C} \text { to } \\ & +70^{\circ} \mathrm{C} \end{aligned}$ | L.CD |
| TSC7106ACSQ | $\begin{aligned} & \text { 60-Pin } \\ & \text { Plastic Flat } \\ & \text { Package } \\ & \hline \end{aligned}$ | Uniormed Leads | $\begin{aligned} & 0^{\circ} \mathrm{C} \text { to } \\ & +70^{\circ} \mathrm{C} \end{aligned}$ | LCD |
| TSC7107ACPL | $\begin{aligned} & \text { 40-Pin } \\ & \text { Plastic Dip } \end{aligned}$ | Normal | $\begin{aligned} & 0^{\circ} \mathrm{C} \text { to } \\ & +70^{\circ} \mathrm{C} \end{aligned}$ | LED |
| TSC7107ARCPL | $\begin{aligned} & \text { 40-Pin } \\ & \text { CerDIP } \end{aligned}$ | Reverse | $\begin{aligned} & 0^{\circ} \mathrm{C} \text { to } \\ & +70^{\circ} \mathrm{C} \end{aligned}$ | LED |


| Part No. | Package | Pin Layout | Temp. Range | Display Drive |
| :---: | :---: | :---: | :---: | :---: |
| TSC7107AIJL | $\begin{aligned} & \text { 40-Pin } \\ & \text { CerDIP } \end{aligned}$ | Normal | $\begin{array}{r} -25^{\circ} \mathrm{C} \text { to } \\ +85^{\circ} \mathrm{C} \end{array}$ | LED |
| TSC7107ACBQ | 60-Pin <br> Plastic Flat <br> Package | Formed Leads | $\begin{aligned} & 0^{\circ} \mathrm{C} \text { to } \\ & +70^{\circ} \mathrm{C} \end{aligned}$ | LED |
| TSC7107ACSQ | $\begin{aligned} & \text { 60-Pin } \\ & \text { Plastic Flat } \\ & \text { Package } \\ & \hline \end{aligned}$ | Unformed Leads | $\begin{aligned} & 0^{\circ} \mathrm{C} \text { to } \\ & +70^{\circ} \mathrm{C} \end{aligned}$ | LED |
| Devices with Burn-In ( 160 Hours at $+125^{\circ} \mathrm{C}$ ) |  |  |  |  |
| TSC7106ACPL/BI | $\begin{aligned} & \text { 40-Pin } \\ & \text { Plastic Dip } \end{aligned}$ | Normal | $\begin{aligned} & 0^{\circ} \mathrm{C} \text { to } \\ & +70^{\circ} \mathrm{C} \end{aligned}$ | LCD |
| TSC7107ACPL/BI | $\begin{aligned} & \text { 40-Pin } \\ & \text { Plastic Dip } \end{aligned}$ | Normal | $\begin{aligned} & 0^{\circ} \mathrm{C} \text { to } \\ & +70^{\circ} \mathrm{C} \end{aligned}$ | LED |
| TSC7107AIJL/B! | $\begin{aligned} & \text { 40-Pin } \\ & \text { CerDIP } \end{aligned}$ | Normal | $\begin{array}{r} -25^{\circ} \mathrm{C} \text { to } \\ +85^{\circ} \mathrm{C} \end{array}$ | LED |

## Pin Description

| 40-Pin DIP <br> Pin Number <br> Normal | (Reverse) | 60-Pin <br> Flat Package <br> Pin Number | Name | Description |
| :--- | :---: | :---: | :---: | :--- |
| 1 | $(40)$ | 13 | $\mathrm{~V}^{+}$ | Positive supply voltage. |
| 2 | $(39)$ | 14 | $\mathrm{D}_{1}$ | Activates the D section of the units display. |
| 3 | $(38)$ | 15 | $\mathrm{C}_{1}$ | Activates the C section of the units display. |
| 4 | $(37)$ | 16 | $\mathrm{~B}_{1}$ | Activates the B section of the units display. |
| 5 | $(36)$ | 17 | $\mathrm{~A}_{1}$ | Activates the A section of the units display. |
| 6 | $(35)$ | 18 | $\mathrm{~F}_{1}$ | Activates the F section of the units display. |
| 7 | $(34)$ | 19 | $\mathrm{G}_{1}$ | Activates the G section of the units display. |
| 8 | $(33)$ | 20 | $\mathrm{E}_{1}$ | Activates the E section of the units display. |
| 9 | $(32)$ | 21 | $\mathrm{D}_{2}$ | Activates the D section of the tens display. |
| T- TELEDYNE SEMICONDUCTOR |  | $7-58$ |  |  |

## Pin Description (Cont.)

| 40-Pin DIP Pin Number Normal | (Reverse) | 60-Pin <br> Flat Package Pin Number | Name | Description |
| :---: | :---: | :---: | :---: | :---: |
| 10 | (31) | 25 | $\mathrm{C}_{2}$ | Activates the C section of the tens display. |
| 11 | (30) | 26 | $\mathrm{B}_{2}$ | Activates the B section of the tens display. |
| 12 | (29) | 27 | $\mathrm{A}_{2}$ | Activates the $A$ section of the tens display. |
| 13 | (28) | 28 | $\mathrm{F}_{2}$ | Activates the F section of the tens display. |
| 14 | (27) | 29 | $E_{2}$ | Activates the E section of the tens display. |
| 15 | (26) | 30 | D | Activates the D section of the hundreds display. |
| 16 | (25) | 31 | B3 | Activates the $B$ section of the hundreds display. |
| 17 | (24) | 32 | F3 | Activates the F section of the hundreds display. |
| 18 | (23) | 33 | $E_{3}$ | Activates the E section of the hundreds display. |
| 19 | (22) | 34 | $\mathrm{AB}_{4}$ | Activates both halves of the 1 in the thousands display. |
| 20 | (21) | 35 | POL | Activates the negative polarity display. |
| 21 | (20) | 36 | $\begin{aligned} & \text { BP } \\ & \text { GND } \end{aligned}$ | TSC7106A: LCD Backplane drive output. TSC7107A: Digital Ground. |
| 22 | (19) | 37 | $\mathrm{G}_{3}$ | Activates the G section of the hundreds display. |
| 23 | (18) | 40 | $A_{3}$ | Activates the A section of the hundreds display. |
| 24 | (17) | 41 | $\mathrm{C}_{3}$ | Activates the C section of the hundreds display. |
| 25 | (16) | 43 | $\mathrm{G}_{2}$ | Activates the G section of the tens display. |
| 26 | (15) | 45 | $\mathrm{V}^{-}$ | Negative power supply voltage. |
| 27 | (14) | 46 | $\mathrm{V}_{\text {INT }}$ | Integrator output. Connection point for integration capacitor. See INTEGRATING CAPACITOR section for additional details. |
| 28 | (13) | 47 | Vbuff | Integration resistor connection. Use a $47 \mathrm{k} \Omega$ for a 200 mV full-scale range and a $470 \mathrm{k} \Omega$ for 2 V full-scale range. |
| 29 | (12) | 49 | $\mathrm{C}_{\text {Az }}$ | The size of the auto-zero capacitor influences the system noise. Use a $0.47 \mu \mathrm{~F}$ capacitor for a 200 mV full-scale, and a $0.047 \mu \mathrm{~F}$ capacitor for a 2 volt full-scale. See paragraph on AUTO-ZERO CAPACITOR for more details. |
| 30 | (11) | 51 | VIN | The analog low input is connected to this pin. |
| 31 | (10) | 55 | $\mathrm{V}_{\text {IN }}^{+}$ | The analog high input signal is connected to this pin. |
| 32 | (9) | 57 | Arıalog Common | This pin is primarily used to set the analog common-mode voltage for battery operation or in systems where the input signal is referenced to the power supply. See paragraph on ANALOG COMMON for more details. It also acts as a reference voltage source. |
| 33 | (8) | 58 | C-EEF | See pin 34. |
| 34 | (7) | 59 | $\mathrm{C}_{\text {Ref }}^{+}$ | A $0.1 \mu \mathrm{~F}$ capacitor is used in most applications. If a large common-mode voltage exists (for example the Vin pin is not at analog common), and a 200 mV scale is used, a $1.0 \mu \mathrm{~F}$ is recommended and will hold the rollover error to 0.5 count. |
| 35 | (6) | 60 | $V_{\text {REF }}^{-}$ | See pin 36. |
| 36 | (5) | 1 | $\mathrm{V}_{\text {+ }}^{+}{ }^{+}$ | The analog input required to generate a full-scale output ( 1,999 counts). Place 100 mV between pins 35 and 36 for 199.9 mV full-scale. Place 1.00 volts between pins 35 and 36 for 2 volts full-scale. See paragraph on REFERENCE VOLTAGE. |
| 37 | (4) | 3 | Test | Lamp test. When pulled high (to $\mathrm{V}^{+}$) all segments will be turned on and the display should read -1888 . It may also be used as a negative supply for externally generated decimal points. See paragraph under TEST for additional information. |
| 38 | (3) | 4 | $\mathrm{OSC}_{3}$ | See pin 40. |
| 39 | (2) | 6 | $\mathrm{OSC}_{2}$ | See pin 40. |
| 40 | (1) | 10 | $\mathrm{OSC}_{1}$ | Pins $40,39,38$ make up the oscillator section. For a 48 kHz clock ( 3 readings per section) connect pin 40 to the junction of a $100 \mathrm{k} \Omega$ resistor and a 100 pF capacitor. The $100 \mathrm{k} \Omega$ resistor is tied to pin 39 and the 100 pF capacitor is tied to pin 38. |

## General Theory of Operation

## Dual Slope Conversion Principles

The TSC7106A and TSC7107A are dual slope, integrating analog-to-digital converters. An understanding of the dual slope conversion technique will aid in following the detailed operation theory.
The conventional dual slope converter measurement cycle has two distinct phases:

- Input Signal Integration
- Reference Voltage Integration (Deintegration)

The input signal being converted is integrated for a fixed time period (Tsı). Time is measured by counting clock pulses. An opposite polarity constant reference voltage is then integrated until the integrator output voltage returns to zero. The reference integration time is directly proportional to the input signal (TRI). (Figure 3A).
In a simple dual slope converter a complete conversion requires the integrator output to "ramp-up" and "ramp-down."


Figure 3A: Basic Dual Slope Converter

A simple mathematical equation relates the input signal, reference voltage and integration time:

$$
\frac{1}{R C} \int_{0}^{V_{I N}(t) d t}=\frac{V_{R} T_{R I}}{R C}
$$

where:
$V_{R}=$ Reference Voltage
$\mathrm{T}_{\mathrm{s}}=$ signal Integration Time (Fixed)
$T_{\text {RI }}=$ Reference Voltage Integration Time (Variable)
For a constant $\mathrm{V}_{\mathrm{IN}}$ :

$$
V_{I N}=V_{R} \frac{T_{R I}}{T_{S I}}
$$

The dual slope converter accuracy is unrelated to the integrating resistor and capacitor values as long as they are stable during a measurement cycle. An inherent benefit is noise immunity. Noise spikes are integrated or averaged to zero during the integration periods. Integrating ADCs are immune to the large conversion errors that plague successive approximation converters in high noise environments. Interfering signals with frequency components at multiples of the averaging period will be attenuated. Integrating ADCs commonly operate with the signal integration period set to a multiple of the $50 / 60 \mathrm{~Hz}$ power line period. (Figure 3B)


Figure 3B: Normal-Mode Rejection of Dual Slope Converter



AN TELEDYNE SEMICONDUCTOR
Figure 7: TSC7107A Block Diagram


| TSC7106A (LCD Drive) |
| :--- |
| TSC7107A (LED Drive) |



## Analog Section

In addition to the basic signal integrate and deintegrate cycles discussed, the circuit incorporates an auto-zero cycle. This cycle removes buffer amplifier, integrator, and comparator offset voltage error terms from the conversion. A true digital zero reading results without external adjusting potentiometers. A complete conversion consists of three cycles: an auto-zero, signal integrate and reference integrate cycle.

## Auto-Zero Cycle

During the auto-zero cycle the differential input signal is disconnected from the circuit by opening internal analog gates. The internal nodes are shorted to analog common (ground) to establish a zero input condition. Additional analog gates close a feedback loop around the integrator and comparator. This loop permits comparator offset voltage error compensation. The voltage level established on $\mathrm{C}_{\mathrm{A}}$ compensates for device offset voltages. The offset error referred to the input is less than $10 \mu \mathrm{~V}$.
The auto-zero cycle length is 1000 to 3000 counts.

## Signal Integrate Cycle

The auto-zero loop is opened, the internal differential inputs connect to $\mathrm{V}_{\mathrm{N}}^{+}$and $\mathrm{V}_{\mathrm{iN}}^{-}$. The differential input signal is integrated for a fixed time period. The signal integration period is 1000 counts. The externally set clock frequency is divided by four before clocking the internal counters. The integration time period is:

$$
T_{S I}=\frac{4}{\text { fosc }} \times 1000
$$

where:

$$
\text { fosc }=\text { External Clock Frequency }
$$

The differential input voltage must be within the device common-mode range ( 1 V of either supply) when the converter and measured system share the same power supply common (ground). If the converter and measured system do not share the same power supply common, Vin should be tied to analog common.
Polarity is determined at the end of signal integrate signal phase. The sign bit is a true polarity indication in that signals less than 1 LSB are correctly determined. This allows precision null detection limited only by device noise and auto-zero residual offsets.

## Reference Integrate Cycle

The final phase is reference integrate or de-integrate. ViN is internally connected to analog common and ViN is connected across the previously charged reference capacitor. Circuitry within the chip ensures that the capacitor will be connected with the correct polarity to cause the integrator output to return to zero. The time required for the output to return to zero is proportional to the input signal and is between 0 and 2000 counts. The digital reading displayed is:

$$
1000 \times \frac{V_{I N}}{V_{R E F}}
$$

## DigItal Section (TSC7106A)

The TSC7106A (Figure 5) contains all the segment drivers necessary to directly drive a $31 / 2$ digit liquid crystal display (LCD). An LCD backplane driver is included. The backplane frequency is the external clock frequency divided by 800 . For three conversions/second the backplane frequency is 60 Hz with a 5 V nominal amplitude. When a segment driver is in phase with the backplane signal the segment is "OFF." An out of phase segment drive signal causes the segment to be "ON" or visible. This AC drive configuration results in negligible $D C$ voltage across each LCD segment. This insures Iong LCD display life. The polarity segment driver is "ON" for negative analog inputs. If $V_{\text {IN }}^{+}$and $V_{\text {IN }}$ are reversed this indicator would reverse.
On the TSC7106A when the test pin is pulled to $\mathrm{V}^{+}$all segments are turned "ON." The display reads -1888 . During this mode the LCD segments have a constant DC voltage impressed. Do not leave the display in this mode for more than several minutes. LCD displays may be destroyed if operated with DC levels for extended periods.
The display FONT and the segment drive assignment are shown in Figure 6.


Figure 6: Display FONT and Segment Assignment

In the TSC7106A an internal digital ground is generated from a 6 volt zener diode and a large $P$ channel source follower. This supply is made stiff to absorb the large capacitive currents when the backplane voltage is switched.

## Digital Section (TSC7107A)

Figure 7 shows the TSC7107A. It is identical to the TSC7106A except that the regulated supply and back plane drive have been eliminated and the segment drive is typically 8 mA . The 1000 output (pin 19) sinks current from two LED segments, and has a 16 mA drive capability. The TSC7107A is designed to drive common anode LEDs.
In both devices, the polarity indication is "on" for negative analog inputs. If $\mathrm{V}^{-1}$ and $\mathrm{V}_{\text {IN }}^{+}$are reversed, this indication can be reversed also, if desired.
The display font is the same as the TSC7106A.

# 3 1/2 Digit A/D Converter <br> - Low Drift Internal Reference - Automatic Zero Correction 

## System Timing

The oscillator frequency is divided by 4 prior to clocking the internal decade counters. The three phase measurement cycle takes a total of 4000 counts or 16000 clock pulses. The 4000 count cycle is independent of input signal magnitude.
Each phase of the measurement cycle has the following length:

- Auto-Zero Phase: 1000 to 3000 Counts
( 4000 to 12000 Clock Pulses)
For signals less than full-scale the auto-zero phase is assigned the unused reference integrate time period.
- Signal Integrate: 1000 Counts
( 4000 Clock Pulses)
This time period is fixed. The integration period is:

$$
\mathrm{Tsı}=4000 \quad\left[\frac{1}{\text { fosc }}\right]
$$

Where fosc is the externally set clock frequency.

- Reference Integrate: 0 to 2000 Counts

$$
\text { ( } 0 \text { to } 8000 \text { Clock Pulses) }
$$

The TSC7106A/7107A are drop replacements for the 7106/ 7107 parts. External component value changes are not required to benefit from the low drift internal reference.

## Clock Circuit

Three clocking methods may be used:

1. An external oscillator connected to pin 40.
2. A crystal between pins 39 and 40.
3. An R-C oscillator using all three pins.


Figure 8: Clock Circuits

## Component Value Selection <br> Auto-Zero Capacitor - CAZ

The CAZ capacitor size has some influence on system noise. A $0.47 \mu \mathrm{~F}$ capacitor is recommended for 200 mV full-scale applications where 1 LSB is $100 \mu \mathrm{~V}$. A $0.047 \mu \mathrm{~F}$ capacitor is adequate for 2.0 V full-scale applications. A mylar type dielectric capacitor is adequate.

## Reference Voltage Capacitor - CREF

The reference voltage used to ramp the integrator output voltage back to zero during the reference integrate cycle is stored on CreF. A $0.1 \mu \mathrm{~F}$ capacitor is acceptable when Vin is tied to analog common. If a large common-mode voltage exists ( $V_{\bar{R} E F} \neq$ analog common) and the application requires a 200 mV full-scale increase $\mathrm{C}_{\text {REF }}$ to $1.0 \mu \mathrm{~F}$. Rollover error will be held to less than 0.5 count. A mylar type dielectric capacitor is adequate.

## Integrating Capacitor - CINT

CINT should be selected to maximize integrator output voltage swing without causing output saturation. Due to the TSC7106A/7107A superior analog common temperature coefficient specification, analog common will normally supply the differential voltage reference. For this case $\mathrm{a} \pm 2 \mathrm{~V}$ full-scale integrator output swing is satisfactory. For 3 readings/second (fosc $=48 \mathrm{kHz}$ ) a $0.22 \mu \mathrm{~F}$ value is suggested. If a different oscillator frequency is used CINT must be changed in inverse proportion to maintain the nominal $\pm 2 \mathrm{~V}$ integrator swing.
An exact expression for CINT is:


Where:
fosc $=$ Clock frequency at Pin 38
$\mathrm{V}_{\mathrm{FS}}=$ Full-scale input voltage
RINT $=$ Integrating resistor
VING $=$ Desired full-scale integrator output swing
CINT must have low dielectric absorption to minimize rollover error. An inexpensive polypropylene capacitor is recommended.

## Integrating Resistor - RINT

The input buffer amplifier and integrator are designed with class A output stages. The output stage idling current is $100 \mu \mathrm{~A}$. The integrator and buffer can supply $20 \mu \mathrm{~A}$ drive currents with negligible linearity errors. RINT is chosen to remain in the output stage linear drive region but not so large that printed circuit board leakage currents induce errors. For a 200 mV full-scale RINT is $47 \mathrm{k} \Omega$. A 2.0 V full-scale requires $470 \mathrm{k} \Omega$.

| Component | Nominal Full-Scale Voltage |  |
| :--- | ---: | ---: |
| Value | 200.0 mV | 2.000 V |
| $\mathrm{C}_{\text {AZ }}$ | $0.47 \mu \mathrm{~F}$ | $0.047 \mu \mathrm{~F}$ |
| RINT $^{\text {Cry }}$ | $47 \mathrm{k} \Omega$ | $470 \mathrm{k} \Omega$ |
| $\mathrm{C}_{\text {INT }}$ | $0.22 \mu \mathrm{~F}$ | $0.22 \mu \mathrm{~F}$ |

Note:

1. $\mathrm{fosc}=48 \mathrm{kHz}$ (3 readings $/ \mathrm{sec}$ )

## 3 1/2 Digit A/D Converter

- Low Drift Internal Reference

TSC7106A (LCD Drive)

- Automatic Zero Correction


## Oscillator Components

Rosc (Pin 40 to Pin 39) should be $100 \mathrm{k} \Omega$. Cosc is selected from the equation:

$$
\text { fosc }=\frac{0.45}{R C}
$$

For fosc of 48 kHz , Cosc is 100 pF nominally.
Note that fosc is divided by four to generate the TSC7106A internal control clock. The backplane drive signal is derived by dividing fosc by 800 .
To achieve maximum rejection of 60 Hz noise pickup, the signal integrate period should be a multiple of 60 Hz . Oscillator frequencies of $240 \mathrm{kHz}, 120 \mathrm{kHz}, 80 \mathrm{kHz}, 60 \mathrm{kHz}, 40 \mathrm{kHz}$, $331 / 3 \mathrm{kHz}$, etc. should be selected. For 50 Hz rejection, oscillator frequencies of $200 \mathrm{kHz}, 100 \mathrm{kHz}, 662 / 3 \mathrm{kHz}, 50 \mathrm{kHz}$, 40 kHz , etc. would be suitable. Note that 40 kHz ( 2.5 readings/ second) will reject both 50 and 60 Hz (also 400 and 440 Hz ).

## Reference Voltage Selection

A full-scale reading ( 2000 counts) requires the input signal be twice the reference voltage.

| Required Full-Scale Voltage ${ }^{*}$ | V $_{\text {REF }}$ |
| :--- | :---: |
| 200.0 mV | 100.0 mV |
| 2.000 V | 1.000 V |
| $* \mathrm{~V}_{\text {FS }}=2 \mathrm{~V}_{\text {REF }}$ |  |

* $V_{F S}=2 V_{\text {REF }}$

In some applications a scale factor other than unity may exist between a transducer output voltage and the required digital reading. Assume, for example, a pressure transducer output is 400 mV for $2000 \mathrm{lb} / \mathrm{in}^{2}$. Rather than dividing the input voltage by two the reference voltage should be set to 200 mV . This permits the transducer input to be used directly.
The differential reference can also be used when a digital zero reading is required when $\mathrm{V}_{\mathrm{IN}}$ is not equal to zero. This is common in temperature measuring instrumentation. A
compensating offset voltage can be applied between analog common and ViN. The transducer output is connected between $\mathrm{V}_{\mathrm{N}}^{+}$and analog common.
The internal voltage reference potential available at analog common will normally be used to supply the converters reference. This potential is stable whenever the supply potential is greater than approximately 7 V . In applications where an externally generated reference voltage is desired refer to Figure 9.


Figure 9: External Reference

## Device Pin Functional Description Differential Signal Inputs <br> ( $\mathrm{V}^{\dagger} \mathrm{N}$ (Pin 31), Vīn (Pin 30))

The TSC7106A/TSC7107A is designed with true differential inputs and accepts input signals within the input stage common mode voltage range ( $\mathrm{V}_{\mathrm{CM}}$ ). The typical range is $\mathrm{V}^{+}$ -1.0 to $\mathrm{V}^{-}+1 \mathrm{~V}$. Common-mode voltages are removed from the system when the TSC7106A/TSC7107A operates from a battery or floating power source (isolated from measured system) and Vin is connected to analog common (Vсом): See Figure 10.


Figure 10: Common-Mode Voltage Removed in Battery Operation with Vin = Analog Common

## Differential Signal Inputs (Cont.)

In systems where common-mode voltages exist the 86 dB common-mode rejection ratio minimizes error. Commonmode voltages do, however, affect the integrator output level. Integrator output saturation must be prevented. A worse case condition exists if a large positive Vсм exists in conjunction with a full-scale negative differential signal. The negative signal drives the integrator output positive along with VCM (Figure 11). For such applications the integrator output swing can be reduced below the recommended 2.0 V full-scale swing. The integrator output will swing within 0.3 V of $\mathrm{V}^{+}$or $\mathrm{V}^{-}$without increasing linearity errors.


Figure 11: Common-Mode Voltage Reduces Available Integrator Swing. (VCOM $\left.\neq \mathrm{VIN}_{\mathrm{I}}\right)$

## Differential Reference

( $\mathrm{V}_{\text {REF }}^{+}$(Pin 36), $\mathrm{V}_{\text {REF }}^{-}(\operatorname{Pin} 39)$ )
The reference voltage can be generated anywhere within the $\mathrm{V}^{+}$to $\mathrm{V}^{-}$power supply range.
To prevent rollover type errors being induced by large common-mode voltages CREF should be large compared to stray node capacitance.
The TSC7106A/TSC7107 A circuits have a significantly lower analog common temperature coefficient. This potential gives a very stable voltage suitable for use as a voltage reference. The temperature coefficient of analog common is $20 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ typically.

## Analog Common (Pin 32)

The analog common pin is set at a voltage potential approximately 3.0 V below $\mathrm{V}^{+}$. The potential is guaranteed to be between 2.7 V and 3.35 V below $\mathrm{V}^{+}$. Analog common is tied internally to an N channeI FET capable of sinking 30 mA . This FET will hold the common line at 3.0 V should an external load attempt to pull the common line toward $\mathrm{V}^{+}$. Analog common source current is limited to $10 \mu \mathrm{~A}$. Analog common is therefore easily pulled to a more negative voltage (i.e., below $\mathrm{V}^{+}-3.0 \mathrm{~V}$ ).

The TSC7106A connects the internal $V_{i N}^{+}$and $V^{-}$iN inputs to analog common during the auto-zero cycle. During the reference integrate phase ViN is connected to analog common. If $\mathrm{V}_{\mathrm{IN}}^{-}$is not externally connected to analog common, a common-mode voltage exists. This is rejected by the converters 86 dB common-mode rejection ratio. In battery operation analog common and ViN are usually connected removing common-mode voltage concerns. In systems where VIN is connected to the power supply ground or to a given voltage, analog common should be connected to ViN.

The analog common pin serves to set the analog section reference or common point. The TSC7106A is specificially designed to operate from a battery or in any measurement system where input signals are not referenced (float) with respect to the TSC7106A power source. The analog common potential of $\mathrm{V}^{+}-3.0 \mathrm{~V}$ gives a 6 V end of battery life voltage. The common potential has a $0.001 \% / \%$ voltage coefficient and $15 \Omega$ output impedance.
With sufficiently high total supply voltage ( $\mathrm{V}^{+}-\mathrm{V}^{-}>7.0 \mathrm{~V}$ ) analog common is a very stable potential with excellent temperature stability - typically $20 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$. This potential can be used to generate the reference voltage. An external voltage reference will be unnecessary in most case because of the $50 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ maximum temperature coefficient. See Internal Voltage Reference discussion.

## Test (Pin 37)

The test pin potential is 5 V less than $\mathrm{V}^{+}$. Test may be used as the negative power supply connection for external CMOS logic. The test pin is tied to the internally generated negative logic supply (Internal Logic Ground) through a $500 \Omega$ resistor in the TSC7106A. The test pin load should be no more than 1 mA .
If test is pulled high to $\mathrm{V}^{+}$all segments plus the minus sign will be activated. Do' not operate in this mode for more than several minutes with the TSC7106A. With Test $=\mathrm{V}^{+}$the LCD Segments are impressed with a DC voltage which will destroy the LCD.
The test pin will sink about 10 mA when pulled to $\mathrm{V}^{+}$.

## Internal Voltage Reference Stability

The analog common voltage termperature stability has been significantly improved (Figure 12). The " $A$ " version of the industry standard circuits allow users to upgrade old systems and design new systems without external voltage references. External R and C values do not need to be changed. Figure 13 shows analog common supplying the necessary voltage reference for the TSC7106A/TSC7107A.

## 3 1/2 Digit A/D Converter

- Low Drift Internal Reference

TSC7106A (LCD Drive)

- Automatic Zero Correction


#### Abstract




Figure 12: Analog Common Temperature Coefficient


SET $V_{\text {REF }}=1 / 2 V_{\text {FULL }}$ SCALE
Figure 13: Internal Voltage Reference Connection

## TSC7107A Power Supplies

The TSC7107A is designed to work from $\pm 5 \mathrm{~V}$ supplies. However, if a negative supply is not available, it can be generated from the clock output with two diodes, two capacitors and an inexpensive IC. Figure 13 shows this application.

In selected applications a negative supply is not required. The conditions to use a single +5 V supply are:

- The input signal can be referenced to the center of the common-mode range of the converter.
- The signal is less than $\pm 1.5$ volts.
- An external reference is used.


Figure 14: Generating Negative Supply From +5 V

The TSC7660 DC to DC converter may also be used to generate -5 V from +5 V (Figure 15).


Figure 15: Negative Power Supply Generation with TSC7660.

## TSC7107 Power Dissipation Reduction

The TSC7107A sinks the LED display current and this causes heat to build up in the IC package. If the internal voltage reference is used, the changing chip temperature can cause the display to change reading. By reducing package power dissipation such variations can be reduced. By reducing the LED common anode voltage the TSC7107A package power dissipation is reduced.
Figure 16 is a photograph of a curve-trace display showing the relationship between output current and output voltage for a typical TSC7107CPL. Since a typical LED has 1.8 volts across it at 7 mA , and its common anode is connected to +5 V , the TSC7107A output is at 3.2 V (point A on Figure 15). Maximum power dissipation is $8.1 \mathrm{~mA} \times 3.2 \mathrm{~V} \times 24$ segments $=$ 622 mW .
Notice, however, that once the TSC7107A output voltage is above two volts, the LED current is essentially constant as output voltage increases. Reducing the output voltage by 0.7 V (point B of Figure 15) results in 7.7 mA of LED current, only a 5 percent reduction. Maximum power dissipation is now only $7.7 \mathrm{~mA} \times 2.5 \mathrm{~V} \times 24=462 \mathrm{~mW}$, a reduction of $26 \%$. An output voltage reduction of 1 volt (point C ) reduces LED current by $10 \%(7.3 \mathrm{~mA})$ but power dissipation by $38 \%$ ! (7.3 mAX 2.2 V X $24=385 \mathrm{~mW}$ ).


Figure 16: TSC7107A Output Current vs Output Voltage

Reduced power dissipation is very easy to obtain. Fig. 17 shows two ways: either a $5.1 \mathrm{ohm}, 1 / 4$ watt resistor or a 1 Amp diode placed in series with the display (but not in series with the TSC7107A). The resistor will reduce the TSC7107A output voltage, when all 24 segments are "ON," to point " C " of Fig. 16. When segments turn off, the output voltage will increase. The diode, on the other hand, will result in a relatively steady output voltage, around point "B."
In addition to limiting maximum power dissipation, the resistor reduces the change in power dissipation as the display changes. This effect is caused by the fact that, as fewer seg-
ments are "ON," each "ON" output drops more voltage and current. For the best case of six segments (a " 111 " display) to worst case (a "1888" display) the resistor will change about 230 mW , while a circuit without the resistor will change about 470 mW . Therefore, the resistor will reduce the effect of display dissipation on reference voltage drift by about 50\%.
The change in LED brightness caused by the resistor is almost unnoticeable as more segments turn off. If display brightness remaining steady is very important to the designer, a diode may be used instead of the resistor.


Figure 17: Diode or Resistor Limits Package Power Dissipation.

## Applications Information Liquid Crystal Display Sources

Several LCD manufacturers supply standard LCD displays to interface with the TSC7106A 3 1/2 digit analog-to-digital converter.

| Manufacturer Address/Phone | Representative <br> Part Numbers ${ }^{1}$ |  |
| :--- | :--- | :--- |
| Crystaloid | 5282 Hudson Dr., <br> Electronics <br> Hudson, OH 44236 <br> 216/655-2429 | C5335, H5535, <br> T5135, SX440 |
| AND | 770 Airport Blvd., <br> Burlingame, CA 94010 <br> 415/347-9916 | FE 0801 |
|  | FE 0203 |  |
| EPSON | 3415 Kashikawa St.,  <br>  Torrance, CA 90505 <br> $213 / 534-0360 ~$ | LD-B709BZ |
|  | LD-H7992AZ |  |
| Hamlin, Inc. | 612 E. Lake St., <br> Lake Mills, WI 53551 <br>  <br>  <br> 414/648-2361 | 3902, 3933, 3903 |

## Note:

1. Contact LCD manufacturer for full product listing/specifications.

## Light Emitting Diode Display Sources

Several LED manufacturers supply seven segment digits with and without decimai point annunciators for the TSC7107A.

| Manufacturer Address | Display <br> Type |  |
| :--- | :--- | :--- |
| Hewlett 640 Page Mill Rd. <br> Packard  <br> Components Palo Alto, CA 94304 | LED |  |
| Litronix, Inc. | 19000 Homestead Rd. <br> Cupertino, CA 94010 | LED |
| And | 770 Airport Blvd. <br> Burlingame, CA 94010 | LED |

## Decimal Point and Annunciator Drive

The test pin is connected to the internally-generated digital logic supply ground through a $500 \Omega$ resistor. The test pin may be used as the negative supply for external CMOS gate segment drivers. LCD display annunciators for decimal points, low battery indication, or function indication may be added without adding an additional supply. No more than 1 mA should be supplied by the test pin. The test pin potential is approximately 5 V below $\mathrm{V}^{+}$.

## Ratiometric Resistance Measurements

The true differential input and differential reference make ratiometric readings possible. Typically in a ratiometric operation, an unknown resistance is measured with respect to a known standard resistance. No accurately defined reference voltage is needed.
The unknown resistance is put in series with a known standard and a current passed through the pair. The voltage developed across the unknown is applied to the input and the voltage across the known resistor applied to the reference input. If the unknown equals the standard, the display will read 1000. The displayed reading can be determined from the following expression:
Displayed Reading $=\frac{\text { R Unknown }}{\text { R Standard }} \times 1000$
The display will overrange for R Unknown $\geq 2 \times R$ Standard.


Figure 18: Decimal Point Drive Using Test as Logic Ground.


Figure 19: Low Parts Count Ratiometric Resistance Measurement

## Application Circults



Figure 20: 3 1/2 Digit True RMS AC DMM


Figure 21: Temperature Sensor


Figure 22: Positive Temperature Coefficient Resistor Temperature Sensor

## 3 1/2 Digit A/D Converter

- Low Drift Internal Reference

TSC7106A (LCD Drive)

- Automatic Zero Correction


## Application Circuits (Cont.)



Figure 23: Integrated Circuit Temperature Sensor


Figure 24: TSC7106A Using the Internal Reference. ( 200 mV Full-Scale, 3 RPS).


Figure 25: TSC7107A Internal Reference ( $\mathbf{2 0 0} \mathbf{~ m V ~ F u l l - ~}$ Scale, 3 RPS, ViN Tied to GND for Single Ended Inputs).

## TSC7106A (LCD Drive)

TSC7107A (LED Drive)
Application Circuits (Cont.)


Figure 26: Circuit for Developing Underrange and Overrange Signals from TSC7106A Outputs.


Figure 28: TSC7107A With a 1.2 V External Band-Gap Reference. Vī Tied to Common).


Figure 27: TSC7106A/TSC7107A: Recommended Component Values for 2.00 V Full-Scale.


Figure 29: TSC7107A Operated from Single +5 V Supply. An External Reference Must Be Used in This Application.

## General Description

The TSC7106 and TSC7107 3-1/2 digit CMOS analog-to-digital converters contain all the active components necessary to construct a $0.05 \%$ resolution measurement system. Seven segment decoders, polarity and digit drivers, voltage reference and clock circuit are integrated on chip. The TSC7106 drives liquid crystal displays (LCD) and includes a backplane driver. The TSC7107 drives common anode light emitting diode (LED) displays directly with an 8 mA drive current per segment.
A low cost, high resolution indicating meter requires only a display, four resistors, and four capicitors. The TSC7106 low power drain and 9 V battery operation make it ideal for portable applications.

The TSC7106/TSC7107 reduces linearity error to less than 1 count. Rollover error - the difference in readings for equal magnitude but opposite polarity input signals-is below $\pm 1$ count. High impedance differential inputs offer 1 pA leakage current and a $1012 \Omega$ input impedance. The differential reference input allows ratiometric measurements for ohms or bridge transducer measurements. The $15 \mu \mathrm{Vp}-\mathrm{p}$ noise performance guarantees a "rock solid" reading. The autozero cycle guarantees a zero display reading with a zero volt input.
The TSC7106/TSC7107 dual slope conversion technique automatically rejects interference signals if the converters


Figure 1: Typical TSC7106 Operating Circuit

## Features

- Drives LCD or LED Displays Directly
- Guaranteed Zero Reading with Zero Input
- Low Noise for Stable Display -2.000 V or 200.0 mV Full-Scale Range
- Auto-Zero Cycle Eliminates Need for Zero Adjustment Potentiometer
- True Polarity Indication for Precision Null Applications
- Convenient 9 V Battery Operation (TSC7106)
- High Impedance CMOS Differential Inputs ..... $1012 \Omega$
- Differential Reference Inputs Simplify Ratiometric Measurements
- Low Power Operation ............................ 10 mW
integration time is set to a multiple of the interference signal period. This is especially useful in industrial measurement environments where 50,60 and 400 Hz line frequency signals are present.
The TSC7106/TSC7107 are available in a small 60-pin flat package for compact designs. Standard devices are offered in an industrial temperature range and with burn-in lasting for 160 hours at $+125^{\circ} \mathrm{C}$.
For applications requiring a more temperature stable internal reference voltage refer to the TSC7106A/7107A data sheets. A display hold feature is available on the TSC7116A and TSC7117A converters.

Figure 2: Typical TSC7107 Operating Circuit


## Absolute Maximum Ratings

TSC7106
Supply Voltage ( $\mathrm{V}^{+}$to $\mathrm{V}^{-}$) .................................. 15 V Analog Input Voltage (either input) (Note 1) .... $\mathrm{V}^{+}$to $\mathrm{V}^{-}$
Reference Input Voltage (either input) $\ldots \ldots . . . \mathrm{V}^{+}$to $\mathrm{V}^{-}$
Clock Input ........................................... Test to $\mathrm{V}^{+}$
Power Dissipation (Note 2)
CerDIP Package ................................. 1000 mW
Plastic Package ................................... 800 mW
Operating Temperature
"C" Devices ................................... $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$
"I" Devices . . . . . . . . . . . . . . . . . . . . . . . . . . . . $-25^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$
Storage Temperature .................... $-65^{\circ} \mathrm{C}$ to $+160^{\circ} \mathrm{C}$
Lead Temperature (Soldering, 60 sec ) .............. $300^{\circ} \mathrm{C}$
Stresses above those listed under Absolute Maximum Ratings may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions above those indicated

## TSC7107

Supply Voltage


Analog input Voltag (e.............. $\mathrm{V}^{-}$
Reference Input Voltage (either input) ........... $\mathrm{V}^{+}$to $\mathrm{V}^{-}$
Clock Input ......................................... GND to $\mathrm{V}^{+}$
Power Dissipation (Note 1)
CerDIP Package .................................. 1000 mW
Plastic Package ........................................... 800 mW
perating Temperature
"C" Devices .................................. $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$

Lead Temperature (Soldering, 60 sec ) .............. $300^{\circ} \mathrm{C}$
in the operational sections of the specifications is not implied. Exposure to reliability.

Electrical Characteristics

| CHARACTERISTICS | CONDITIONS | MIN | TYP | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Zero Input Reading | $\begin{aligned} & \text { Vin }=0.0 \mathrm{~V} \\ & \text { Full-Scale }=200.0 \mathrm{mV} \end{aligned}$ | -000.0 | $\pm 000.0$ | +000.0 | Digital Reading |
| Ratiometric Reading | $\begin{aligned} & V_{I N}=V_{\text {REF }} \\ & V_{\text {REF }}=100 \mathrm{mV} \end{aligned}$ | 999 | 999/1000 | 1000 | Digital Reading |
| Rollover Error (Difference in Reading for Equal Positive and Negative Reading Near Full-Scale) | $-\mathrm{V}_{\mathrm{IN}}=+\mathrm{V}_{\mathrm{IN}} \simeq 200.0 \mathrm{mV}$ | -1 | $\pm 0.2$ | +1 | Counts |
| Linearity (Max. Deviation From Best Straight Line Fit) | Full-Scale $=200 \mathrm{mV}$ or Full-Scale $=2.000 \mathrm{~V}$ | -1 | $\pm 0.2$ | +1 | Counts |
| Common-Mode Rejection Ratio (Note 4) | $\begin{aligned} & \mathrm{VCM}_{\text {C }}= \pm 1 \mathrm{~V}, \mathrm{~V}_{1 \mathrm{~N}}=0 \mathrm{~V} . \\ & \text { Full-Scale }=200.0 \mathrm{mV} \end{aligned}$ | - | 50 | - | $\mu \mathrm{V} / \mathrm{V}$ |
| Noise (Pk - Pk Value Not Exceeded 95\% of Time) | $\begin{aligned} & V_{1 N}=0 \mathrm{~V} \\ & \text { Full-Scale }=200.0 \mathrm{mV} \end{aligned}$ | - | 15 | - | $\mu \mathrm{V}$ |
| Leakage Current @ Input | $\mathrm{VIN}=0 \mathrm{~V}$ | - | 1 | 10 | pA |
| Zero Reading Drift | $\begin{aligned} & \text { VIN }=0 \mathrm{~V} \\ & \text { "C" Device }=0^{\circ} \mathrm{C} \text { to } 70^{\circ} \mathrm{C} \\ & \mathrm{VIN}=0 \mathrm{~V} \\ & \text { "I" Device }=-25^{\circ} \mathrm{C} \text { to }+85^{\circ} \mathrm{C} \end{aligned}$ | - | 0.2 1.0 | 1 2 | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
| Scale Factor <br> Temperature Coefficient | $\begin{aligned} & \text { VIN }=199.0 \mathrm{mV}, \\ & \text { "C" Device }=0^{\circ} \mathrm{C} \text { to } 70^{\circ} \mathrm{C} \\ & \text { (Ext. Ref }=0 \mathrm{ppm} /{ }^{\circ} \mathrm{C} \text { ) } \\ & \text { VIN }=199.0 \mathrm{mV} \\ & \text { "I" Device: }-25^{\circ} \mathrm{C} \text { to }+85^{\circ} \mathrm{C} \end{aligned}$ | - | 1 | 5 20 | $\begin{aligned} & \mathrm{ppm} /{ }^{\circ} \mathrm{C} \\ & \mathrm{ppm} /{ }^{\circ} \mathrm{C} \end{aligned}$ |
| Supply Current (Does Not Include LED Current for 7107) | V IN $=0$ | - | 0.8 | 1.8 | mA |
| Analog Common Voltage (With Respect to Pos. Supply) | $25 \mathrm{k} \Omega$ Between Common and Pos. Supply | 2.4 | 2.8 | 3.2 | V |
| Temp. Coeff. of Analog common (With Respect to Pos. Supply) | $25 \mathrm{k} \Omega$ Between Common and Pos. Supply | - | 80 | - | ppm $/{ }^{\circ} \mathrm{C}$ |
| $\begin{aligned} & \text { TSC7106 ONLY Pk - Pk } \\ & \text { Segment Drive Voltage (Note 5) } \\ & \hline \end{aligned}$ | $\mathrm{V}^{+}$to $\mathrm{V}^{-}=9 \mathrm{~V}$ | 4 | 5 | 6 | V |
| $\begin{aligned} & \text { TSC7106 ONLY PK - Pk } \\ & \text { Backplane Drive Voltage (Note 5) } \end{aligned}$ | $\mathrm{V}^{+}$to $\mathrm{V}^{-}=9 \mathrm{~V}$ | 4 | 5 | 6 | V |

Electrical Characteristics (Note 3) (Continued)

| CHARACTERISTICS | CONDITIONS | MIN | TYP | MAX | UNIT |
| :--- | :--- | :--- | :--- | :--- | :--- |
| TSC7107 ONLY <br> Segment Sinking Current <br> (Except Pin 19) | $\mathrm{V}^{+}=5.0 \mathrm{~V}$ <br> Segment Voltage $=3 \mathrm{~V}$ | 5 | 8.0 | - | mA |
| TSC7107 ONLY <br> Segment Sinking Current <br> (Pin 19 Only) | $\mathrm{V}^{+}=5.0 \mathrm{~V}$ <br> Segment Voltage $=3 \mathrm{~V}$ | 10 | 16 | - | mA |

## NOTES:

1. Input voltages may exceed the supply voltages provided the input current is limited to $\pm 100 \mu \mathrm{~A}$.
2. Dissipation rating assumes device is mounted with all leads soldered to printed circuit board
3. Uniess other wise noted, specifications apply to both the TSC7106 and TSC7107 at $T_{A}=25^{\circ} \mathrm{C}$, fCLOCK $=48 \mathrm{kHz}$. TSC7106 is tested in the circuit of

Figure 1. TSC7107 is tested in the circuit of Figure 2.
4. Refer to "Differential Input" discussion.
5. Backplane drive is in phase with segment drive for 'off' segment, $180^{\circ}$ out of phase for 'on' segment. Frequency is 20 times conversion rate. Average dc component is less than 50 mV .

## 3 1/2 Digit A/D Converter - Direct Display Drive <br> - Automatic Zero Correction

TSC7106 (LCD Drive) TSC7107 (LED Drive)

## Pin Configuration (Continued)



## Ordering Information

| Part No. | Package | Pin Layout | Temp. Range | Display Drive |
| :---: | :---: | :---: | :---: | :---: |
| TSC7106CPL | $\begin{aligned} & \text { 40-Pin } \\ & \text { Plastic Dip } \end{aligned}$ | Normal | $\begin{aligned} & 0^{\circ} \mathrm{C} \text { to } \\ & +70^{\circ} \mathrm{C} \end{aligned}$ | LCD |
| TSC7106RCPL | $\begin{aligned} & \text { 40-Pin } \\ & \text { Plastic Dip } \end{aligned}$ | Reverse | $\begin{aligned} & 0^{\circ} \mathrm{C} \text { to } \\ & +70^{\circ} \mathrm{C} \end{aligned}$ | LCD |
| TSC7106IPL | $\begin{aligned} & \text { 40-Pin } \\ & \text { Plastic Dip } \end{aligned}$ | Normal | $\begin{array}{r} -25^{\circ} \mathrm{C} \text { to } \\ +85^{\circ} \mathrm{C} \end{array}$ | LCD |
| TSC7106CJL | $\begin{aligned} & \text { 40-Pin } \\ & \text { CerDIP } \end{aligned}$ | Normal | $\begin{aligned} & 0^{\circ} \mathrm{C} \text { to } \\ & +70^{\circ} \mathrm{C} \end{aligned}$ | LCD |
| TSC7106IJL | $\begin{aligned} & \text { 40-Pin } \\ & \text { CerDIP } \end{aligned}$ | Normal | $\begin{array}{r} -25^{\circ} \mathrm{C} \text { to } \\ +85^{\circ} \mathrm{C} \\ \hline \end{array}$ | LCD |
| TSC7106CBQ | $\begin{aligned} & \text { 60-Pin } \\ & \text { Plastic Flat } \\ & \text { Package } \\ & \hline \end{aligned}$ | Formed Leads | $\begin{aligned} & 0^{\circ} \mathrm{C} \text { to } \\ & +70^{\circ} \mathrm{C} \end{aligned}$ | LCD |
| TSC7106CSQ | $\begin{aligned} & \text { 60-Pin } \\ & \text { Plastic Flat } \\ & \text { Package } \\ & \hline \end{aligned}$ | Unformed Leads | $\begin{aligned} & 0^{\circ} \mathrm{C} \text { to } \\ & +70^{\circ} \mathrm{C} \end{aligned}$ | LCD |
| TSC7107CPL | $\begin{aligned} & \text { 40-Pin } \\ & \text { Plastic Dip } \end{aligned}$ | Normal | $\begin{aligned} & 0^{\circ} \mathrm{C} \text { to } \\ & +70^{\circ} \mathrm{C} \end{aligned}$ | LED |
| TSC7107RCPL | $\begin{aligned} & \text { 40-Pin } \\ & \text { Plastic Dip } \end{aligned}$ | Reverse | $\begin{aligned} & 0^{\circ} \mathrm{C} \text { to } \\ & +70^{\circ} \mathrm{C} \end{aligned}$ | LED |
| TSC7107IPL | $\begin{aligned} & \text { 40-Pin } \\ & \text { Plastic Dip } \end{aligned}$ | Normal | $\begin{array}{r} -25^{\circ} \mathrm{C} \text { to } \\ +85^{\circ} \mathrm{C} \end{array}$ | LED |
| TSC7107CJL | $\begin{aligned} & \text { 40-Pin } \\ & \text { CerDIP } \end{aligned}$ | Normal | $\begin{aligned} & 0^{\circ} \mathrm{C} \text { to } \\ & +70^{\circ} \mathrm{C} \end{aligned}$ | LED |


| Part No. | Package | Pin <br> Layout | Temp. Range | Display Drive |
| :---: | :---: | :---: | :---: | :---: |
| TSC7107IJL | $\begin{aligned} & \text { 40-Pin } \\ & \text { CerDIP } \end{aligned}$ | Normal | $\begin{array}{r} -25^{\circ} \mathrm{C} \text { to } \\ +85^{\circ} \mathrm{C} \end{array}$ | LED |
| TSC7107CBQ | ```60-Pin Plastic Flat Package``` | Formed Leads | $\begin{aligned} & 0^{\circ} \mathrm{C} \text { to } \\ & +70^{\circ} \mathrm{C} \end{aligned}$ | LED |
| TSC7107CSQ | $\begin{aligned} & \hline \text { 60-Pin } \\ & \text { Plastic Flat } \\ & \text { Package } \\ & \hline \end{aligned}$ | Unformed Leads | $\begin{aligned} & 0^{\circ} \mathrm{C} \text { to } \\ & +70^{\circ} \mathrm{C} \end{aligned}$ | LED |
| Devices with Burn-In (160 Hours at $+125^{\circ} \mathrm{C}$ ) |  |  |  |  |
| TSC7106CPL/BI | $\begin{aligned} & \text { 40-Pin } \\ & \text { Plastic Dip } \end{aligned}$ | Normal | $\begin{aligned} & 0^{\circ} \mathrm{C} \text { to } \\ & +70^{\circ} \mathrm{C} \end{aligned}$ | LCD |
| TSC7106RCPL/BI | $\begin{aligned} & \text { 40-Pin } \\ & \text { Plastic Dip } \end{aligned}$ | Reverse | $\begin{aligned} & 0^{\circ} \mathrm{C} \text { to } \\ & +70^{\circ} \mathrm{C} \end{aligned}$ | LCD |
| TSC7106IJL/BI | $\begin{aligned} & \text { 40-Pin } \\ & \text { CerDIP } \end{aligned}$ | Normal | $\begin{array}{r} -25^{\circ} \mathrm{C} \text { to } \\ +85^{\circ} \mathrm{C} \end{array}$ | LCD |
| TSC7107CPL/BI | $\begin{aligned} & \text { 40-Pin } \\ & \text { Plastic Dip } \end{aligned}$ | Normal | $\begin{aligned} & 0^{\circ} \mathrm{C} \text { to } \\ & +70^{\circ} \mathrm{C} \end{aligned}$ | LED |
| TSC7107RCPL/BI | $\begin{aligned} & \text { 40-Pin } \\ & \text { Plastic Dip } \end{aligned}$ | Reverse | $\begin{aligned} & 0^{\circ} \mathrm{C} \text { to } \\ & +70^{\circ} \mathrm{C} \end{aligned}$ | LED |
| TSC7107IJL/BI | $\begin{aligned} & \text { 40-Pin } \\ & \text { CerDIP } \end{aligned}$ | Normal | $\begin{array}{r} -25^{\circ} \mathrm{C} \text { to } \\ +85^{\circ} \mathrm{C} \end{array}$ | LED |

# 3 1/2 Digit A/D Converter 

- Direct Display Drive

TSC7106 (LCD Drive)

- Automatic Zero Correction TSC7107 (LED Drive)


## Pin Description

| 40-PIn DIP Pin Number Normal | (Reverse) | 60-Pin Flat Package Pin Number | Name | Description |
| :---: | :---: | :---: | :---: | :---: |
| 1 | (40) | 13 | $\mathrm{V}^{+}$ | Positive supply voltage. |
| 2 | (39) | 14 | D1 | Activates the D section of the units display. |
| 3 | (38) | 15 | $\mathrm{C}_{1}$ | Activates the C section of the units display. |
| 4 | (37) | 16 | $\mathrm{B}_{1}$ | Activates the B section of the units display. |
| 5 | (36) | 17 | $\mathrm{A}_{1}$ | Activates the A section of the units display. |
| 6 | (35) | 18 | $F_{1}$ | Activates the $F$ section of the units display. |
| 7 | (34) | 19 | $\mathrm{G}_{1}$ | Activates the G section of the units display. |
| 8 | (33) | 20 | $\mathrm{E}_{1}$ | Activates the E section of the units display. |
| 9 | (32) | 21 | $\mathrm{D}_{2}$ | Activates the D section of the tens display. |
| 10 | (31) | 25 | $\mathrm{C}_{2}$ | Activates the C section of the tens display. |
| 11 | (30) | 26 | $\mathrm{B}_{2}$ | Activates the B section of the tens display. |
| 12 | (29) | 27 | $\mathrm{A}_{2}$ | Activates the $A$ section of the tens display. |
| 13 | (28) | 28 | F2 | Activates the F section of the tens display. |
| 14 | (27) | 29 | E2 | Activates the E section of the tens display. |
| 15 | (26) | 30 | D3 | Activates the D section of the hundreds display. |
| 16 | (25) | 31 | B3 | Activates the B section of the hundreds display. |
| 17 | (24) | 32 | F3 | Activates the F section of the hundreds display. |
| 18 | (23) | 33 | $\mathrm{E}_{3}$ | Activates the E section of the hundreds display. |
| 19 | (22) | 34 | $\mathrm{AB}_{4}$ | Activates both halves of the 1 in the thousands display. |
| 20 | (21) | 35 | POL | Activates the negative polarity display. |
| 21 | (20) | 36 | $\begin{gathered} \mathrm{BP} \\ \text { GND } \end{gathered}$ | TSC7106: LCD Backplane drive output. TSC7107: Digital Ground. |
| 22 | (19) | 37 | G3 | Activates the G section of the hundreds display. |
| 23 | (18) | 40 | $\mathrm{A}_{3}$ | Activates the A section of the hundreds display. |
| 24 | (17) | 41 | $\mathrm{C}_{3}$ | Activates the C section of the hundreds display. |
| 25 | (16) | 43 | $\mathrm{G}_{2}$ | Activates the G section of the tens display. |
| 26 | (15) | 45 | $\mathrm{V}^{-}$ | Negative power supply voltage. |
| 27 | (14) | 46 | VINT | Integrator output. Connection point for integration capacitor. See INTEGRATING CAPACITOR section for additional details. |
| 28 | (13) | 47 | Vbuff | Integration resistor connection. Use a $47 \mathrm{k} \Omega$ for a 200 mV full-scale range and a $470 \mathrm{k} \Omega$ for 2 V full-scale range. |
| 29 | (12) | 49 | $C_{A Z}$ | The size of the auto-zero capacitor influences the system noise. Use a $0.47 \mu \mathrm{~F}$ capacitor for a 200 mV full-scale, and a $0.047 \mu \mathrm{~F}$ capacitor for a 2 volt full-scale. See paragraph on AUTO-ZERO CAPACITOR for more details. |
| 30 | (11) | 51 | VIN | The analog low input is connected to this pin. |
| 31 | (10) | 55 | $\mathrm{V}_{\text {IN }}^{+}$ | The analog high input signal is connected to this pin. |
| 32 | (9) | 57 | Analog Common | This pin is primarily used to set the analog common-mode voltage for battery operation or in systems where the input signal is referenced to the power supply. See paragraph on ANALOG COMMON for more details. It also acts as a reference voltage source. |
| 33 | (8) | 58 | C-̇EF | See pin 34. |
| 34 | (7) | 59 | $\mathrm{C}_{\text {REF }}^{+}$ | A $0.1 \mu \mathrm{~F}$ capacitor is used in most applications. If a large common-mode voltage exists (for example the ViN pin is not at analog common), and a 200 mV scale is used, a $1.0 \mu \mathrm{~F}$ is recommended and will hold the rollover error to 0.5 count. |
| 35 | (6) | 60 | VREF | See pin 36. |

Pin Description (Cont.)

| 40-Pin DIP PIn Number Normal | (Reverse) | 60-Pin Flat Package Pin Number | Name | Description |
| :---: | :---: | :---: | :---: | :---: |
| 36 | (5) | 1 | $\mathrm{V}_{\text {REF }}^{+}$ | The analog input required to generate a full-scale output (1,999 counts). Place 100 mV between pins 35 and 36 for 199.9 mV full-scale. Place 1.00 volts between pins 35 and 36 for 2 volts full-scale. See paragraph on REFERENCE VOLTAGE. |
| 37 | (4) | 3 | Test | Lamp test. When pulled high (to $\mathrm{V}^{+}$) all segments will be turned on and the display should read -1888. It may also be used as a negative supply for externally generated decimal points. See paragraph under TEST for additional information. |
| 38 | (3) | 4 | $\mathrm{OSC}_{3}$ | See pin 40. |
| 39 | (2) | 6 | $\mathrm{OSC}_{2}$ | See pin 40. |
| 40 | (1) | 10 | $\mathrm{OSC}_{1}$ | Pins 40, 39, 38 make up the oscillator section. For a 48 kHz clock ( 3 readings per section) connect pin 40 to the junction of a $100 \mathrm{k} \Omega$ resistor and a 100 pF capacitor. The $100 \mathrm{k} \Omega$ resistor is tied to pin 39 and the 100 pF capacitor is tied to pin 38. |

## Analog Section

Figure 3 shows the Block Diagram of the Analog Section for the TSC7106 and TSC7107. Each measurement cycle is divided into three phases. They are (1) auto-zero (A-Z), (2) signal integrate (INT) and (3) reference (REF).

## Auto-Zero Phase

Input high and low are disconnected from the pins and internally shorted to analog common. The reference capacitor is charged to the reference voltage. A feedback loop is closed around the system to charge the auto-zero capacitor $\mathrm{C}_{A z}$ to compensate for offset voltages in the buffer amplifier, integrator, and comparator. Since the comparator is included in the loop, the A-Z accuracy is limited only by the noise of the system. The offset referred to the input is less than $10 \mu \mathrm{~V}$.

## Signal Integrate Phase

The auto-zero loop is opened, the internal short is removed, and the internal input high and low are connected to the external pins. The converter then integrates the differential voltage between ViN and ViN for a fixed time. This differential voltage can be within a wide common-mode range; within one volt of either supply. If, on the other hand, the input signal has no return with respect to the converter power supply, Vin can be tied to analog common to establish the correct common-mode voltage. At the end of this phase, the polarity of the integrated signal is determined.

## Reference Integrate Phase

The final phase is reference integrate or de-integrate. Input low is internally connected to analog common and input high is connected across the previously charged reference capacitor. Circuitry within the chip ensures that the capacitor will be connected with the correct polarity to cause the integrator output to return to zero. The time required for the output to return to zero is proportional to the input signal. The digital
reading displayed is:

$$
1000 \times \frac{V_{I N}}{V_{\text {REF }}}
$$

## Differential Reference

The reference voltage can be generated anywhere within the power supply voltage of the converter. The main source of common-mode error is a roll-over voltage caused by the reference capacitor losing or gaining charge to stray capacitance on its nodes. If there is a large common-mode voltage, the reference capacitor can gain charge (increase voltage) when called up to de-integrate a positive signal but lose charge (decrease voltage) when called up to deintegrate a negative input signal. This difference in reference for ( + ) or ( - ) input voltage will give a roll-over error. By selecting the reference capacitor large enough in comparison to the stray capacitance, this error can be held to less than 0.5 count for the worse case condition. (See Component Values Selection.)

## Differential Input

The input can accept differential voltages anywhere within the common-mode range of the input amplifier; or specifically from 1.0 volts below the positive supply to 1.0 volt above the negative supply. In this range the system has a CMRR of 86 dB typical. However, since the integrator also swings with the common-mode voltage, care must be exercised to assure the integrator output does not saturate. A worse case condition would be a large positive common-mode voitage with a near full-scale negative differential input voltage. The negative input signal drives the integrator positive when most of its swing has been used up by the positive common-mode voltage. For these critical applications the integrator swing can be reduced to less than the recommended 2 V full-scale swing with little loss of accuracy. The integrator output can swing within 0.3 volts of either supply without loss of linearity.


Figure 3: Analog Section of TSC7106/TSC7107

## Analog Common

This pin is included primarily to set the common-mode voltage for battery operation (TSC7106) or for any system where the input signals are floating with respect to the power supply. The common pin sets a voltage that is approximately 2.8 volts more negative than the positive supply. This is selected to give a minimum end-of-life battery voltage of about 6 V . However, the analog common has some of the attributes of a reference voltage. When the total supply voltage is large enough to cause the zener to regulate ( $>7 \mathrm{~V}$ ), the common voltage will have a low voltage coefficient ( $0.001 \% / \%$ ), low output impedance ( $\sim 15 \Omega$ ), and a temperature coefficient of $80 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ typically.
An external reference may be added to improve temperature stability or the TSC7106A/TSC7107A devices with lower analog common temperature drift may be used. The circuit is shown in Figure 4.


Figure 4: Using an External Reference

Analog common is also used as the Vin return during autozero and deintegrate. If Vin is different from analog common, a common-mode voltage exists in the system and is taken care of by the excellent CMRR of the converter. However, in some applications Vin will be set at a fixed known voltage (power supply common for instance). In this application, analog common should be tied to the same point, thus removing the common-mode voltage from the converter. The same holds true for the reference voltage. If reference can be conveniently referenced to analog common, it should be since this removes the common-mode voltage from the reference system.
Within the IC, analog common is tied to an N -channel FET that can sink 30 mA or more of current to hold the voltage 2.8 volts below the positive supply (when a load is trying to pull the common line positive). However, there is only $10 \mu \mathrm{~A}$ of source current, so common may easily be tied to a more negative voltage thus over-riding the internal reference.

## Test

The TEST pin serves two functions. On the TSC7107 it is coupled to the internally generated digital supply through a $500 \Omega$ resistor. Thus it can be used as the negative supply for externally generated segment drivers such as decimal points or any other presentation the user may want to include on the LCD display. Figures 5 and 6 show such an application. No more than a 1 mA load should be applied.
The second function is a "lamp test." When TEST is pulled high (to $\mathrm{V}^{+}$) all segments will be turned on and the display should read -1888 . The TEST pin will sink about 10 mA under these conditions.
Caution: On the TSC7106, in the lamp test mode the segments have a constant dc voltage (no square-wave) and may burn the LCD display if left in this mode for several minutes.


Figure 5: Simple Inverter for Fixed Decimal Point


Figure 6: Exclusive 'OR' Gate for Decimal Point Drive


Figure 7: Clock Circults

## Digital Section

Figures 8 and 9 show the digital section for the TSC7106 and TSC7107, respectively. In the TSC7106 (Figure 8), an internal digital ground is generated from a 6 volt Zener diode and a large P channel source follower. This supply is made stiff to absorb the large capacitive currents when the back plane (BP) voltage is switched. The BP frequency is the clock frequency divided by 800 . For three readings/second this is a 60 Hz square wave with a nominal amplitude of 5 volts. The segments are driven at the same frequency and amplitude and are in phase with BP when OFF, but out of phase when ON. In all cases, negligible dc voltage exists across the segments.

Figure 9 is the Digital Section of the TSC7107. It is identical to the TSC7106 except that the regulated supply and back plane drive have been eliminated and the segment drive is typically 8 mA . The 1000 output (pin 19) sinks current from two LED segments, and has a 16 mA drive capability. The TSC7107 is designed to drive common anode LEDs.

In both devices, the polarity indication is "on" for negative analog inputs. If $\mathrm{V}_{\mathrm{N}}^{-}$and $\mathrm{V}_{\mathrm{N}}^{+}$are reversed, this indication can be reversed also, if desired.

## System Timing

Figure 9 shows the clocking method used in the TSC7106 and TSC7107. Three clocking methods may be used:

1. An external oscillator connected to pin 40.
2. A crystal between pins 39 and 40.
3. An RC oscillator using all three pins.

The oscillator frequency is divided by four before it clocks the decade counters. It is then further divided to form the three convert-cycle phases. These are signal integrate (1000 counts), reference de-integrate ( 0 to 2000 counts) and auto-zero ( 1000 to 3000 counts). For signals less than fullscale auto-zero gets the unused portion of reference de-integrate. This makes a complete measure cycle of 4,000 ( 16,000 clock pulses) independent of input voltage. For three readings/second, an oscillator frequency of 48 kHz would be used.
To achieve maximum rejection of 60 Hz pickup, the signal integrate cycle should be a multiple of 60 Hz . Oscillator frequencies of $240 \mathrm{kHz}, 120 \mathrm{kHz}, 80 \mathrm{kHz}, 60 \mathrm{kHz}, 48 \mathrm{kHz}, 40 \mathrm{kHz}$, $33-1 / 3 \mathrm{kHz}$, etc. should be selected. For 50 Hz rejection, oscillator frequencies of $200 \mathrm{kHz}, 100 \mathrm{kHz}, 66-2 / 3 \mathrm{kHz}$, $50 \mathrm{kHz}, 40 \mathrm{kHz}$, etc. would be suitable. Note that $40 \mathrm{kHz}(2.5$ readings/second) will reject both 50 and 60 Hz (also 400 and 440 Hz ).

## Component Value Selection <br> Auto-Zero Capacitor

The size of the auto-zero capacitor has some influence on the noise of the system. For 200 mV full-scale where noise is very important, a $0.47 \mu \mathrm{~F}$ capacitor is recommended. On the 2 volt scale, a $0.047 \mu \mathrm{~F}$ capacitor increase the speed of recovery from overload and is adequate for noise on this scale.

## Reference Capacitor

A $0.1 \mu \mathrm{~F}$ capacitor is acceptable in most applications. However, where a large common-mode voltage exists (i.e. the ViN pin is not at analog common) and a 200 mV scale is used, a large value is required to prevent to roll-over error. Generally $1.0 \mu \mathrm{~F}$ will hold the roll-over error to 0.5 count in this instance.

## Integrating Capacitor

The integrating capacitor should be selected to give the maximum voltage swing that ensures tolerance build-up will not saturate the integrator swing (approx. 0.3 volt from either supply). In the TSC7106 or the TSC7107, when the analog common is used as a reference, a nominal $\pm 2$ volt full-scale integrator swing is acceptable. For the TSC7107 with $\pm 5$ volt supplies and analog common tied to supply ground, $a \pm 3.5$ to


Figure 8: TSC7106 Digital Section


Figure 9: TSC7107 Digital Section
$\pm 4$ volt swing is nominal. For three readings/second ( 48 kHz clock) nominal values for $\mathrm{C}_{\mathrm{INT}}$ are $0.22 \mu 1 \mathrm{~F}$ and $0.10 \mu \mathrm{~F}$, respectively. If different oscillator frequencies are used, these values should be changed in inverse proportion to maintain the output swing.
The integrating capacitor must have low dielectric absorption to prevent roll-over errors. Polypropylene capacitors are recommended for this application.

## Integrating Resistor

Both the buffer amplifier and the integrator have a class $A$ output stage with $100 \mu \mathrm{~A}$ of quiescent current. They can supply $20 \mu \mathrm{~A}$ of drive current with negligible non-linearity. The integrating resistor should be large enough to remain in this very linear region over the input voltage range, but small enough that undue leakage requirements are not placed on the PC board. For 2 volt full-scale, $470 \mathrm{k} \Omega$ is near optimum and similarly a $47 \mathrm{k} \Omega$ for a 200.0 mV scale.

## Oscillator Components

For all ranges of frequency a $100 \mathrm{k} \Omega$ resistor is recommended and the capacitor is selected from the equation $f=\frac{45}{R C}$ For 48 kHz clock (3 readings/second), $C=100 \mathrm{pF}$.

## Reference Voltage

The analog input required to generate full-scale output ( 200 counts) is: $\mathrm{V}_{\text {IN }}=2 \mathrm{~V}_{\text {REF }}$. Thus, for the 200.0 mV and 2.000 volt scale, VREF should equal 100.0 mV and 1.00 volt respectively. However, in many applications where the A/D is connected to a transducer, there will exist a scale factor other than unity between the input voltage and the digital reading. For instance, in a weighing system, the designer might like to have a full-scale reading when the voltage form the transducer is 0.682 V . Instead of dividing the input down to 200.0 mV , the designer should use the input voltage directly and select $V_{\text {REF }}=0.341 \mathrm{~V}$. Suitable values for integrating resistor and capacitor would be $120 \mathrm{k} \Omega$ and $0.22 \mu \mathrm{~F}$. This makes the system slightly quieter and also avoids a divider network on the input. The TSC7107 with $\pm 5 \mathrm{~V}$ supplies can accept input signals up to $\pm 4 \mathrm{~V}$. Another advantage of this system occurs when a digital reading of zero is desired for $\mathrm{V}_{\mathrm{I}}$ $\neq 0$. Temperature and weighing systems with a variable tare are examples. This offset reading can be conveniently generated by connecting the voltage transducer between $\mathrm{V}_{\mathrm{IN}}^{+}$and common and the variable (or fixed) offset voltage between common and ViN.

## TSC7107 Power Supplies

The TSC7107 is designed to work from $\pm 5 \mathrm{~V}$ supplies. However, if a negative supply is not available, it can be generated from the clock output with two diodes, two capacitors and an inexpensive IC. Figure 10 shows this application.
In selected applications no negative supply is required. The conditions to use a single +5 V supply are:

- The input signal can be referenced to the center of the common-mode range of the converter.
- The signal is less than $\pm 1.5$ volts.
- An external reference is used.


Figure 10: Generating Negative Supply From + 5V
Typical Applications


Figure 11: TSC7106 Using the Internal Reference. (200 mV Full-Scale, 3 RPS).


Figure 12: TSC7107 Internal Reference ( 200 mV FullScale, 3 RPS, VinTied to GND for Single Ended Inputs).


Figure 13: CIrcuit for Developing Underrange and Overrange Signals from TSC7106 Outputs.


Figure 14: TSC7107 With a 1.2 V External Band-Gap Reference. Vī Tied to Common).

## Applications Information

The TSC7107 sinks the LED display current and this causes heat to build up in the IC package. If the internal voltage reference is used, the changing chip temperature can cause the display to change reading. By reducing package power dissipation such variations can be reduced. By reducing the LED common anode voltage the TSC7107 package power dissipation is reduced.
Figure 17 is a photograph of a curve-tracer display showing the relationship between output current and output voltage for a typical TSC7107CPL. Since a typical LED has 1.8 volts across it at 8 mA , and its common anode is connected to +5 V , the TSC7107 output is at 3.2 V (point A on Fig. 17). Maximum power dissipation is $8.1 \mathrm{~mA} \times 3.2 \mathrm{~V} \times 24$ segments $=622 \mathrm{~mW}$.


Figure 15: TSC7106/TSC7107: Recommended Component Values for 2.00 V Full-Scale.


Figure 16: TSC7107 Operated from Single +5 V Supply. An External Reference Must Be Used in This Application.

Notice, however, that once the TSC7107 output voltage is above two volts, the LED current is essentially constant as output voltage increases. Reducing the output voltage by 0.7 V (point B of Figure 17) results in 7.7 mA of LED current, only a 5 percent reduction. Maximum power dissipation is now only $7.7 \mathrm{~mA} \times 2.5 \vee \times 24=462 \mathrm{~mW}$, a reduction of $26 \%$. An output voltage reduction of 1 volt (point C) reduces LED current by $10 \%$ ( 7.3 mA ) but power dissipation by 38\%! (7.3 $\mathrm{mA} \times 2.2 \mathrm{VX} 24=385 \mathrm{~mW}$ ).

Reduced power dissipation is very easy to obtain. Fig. 18 shows two ways: either a 5.1 ohm, $1 / 4$ watt resistor or a 1 Amp diode placed in series with the display (but not in series with the TSC7107). The resistor will reduce the TSC7107 output voltage, when all 24 segments are "ON," to point "C" of Fig.

# 3 1/2 Digit A/D Converter <br> - Direct Display Drive <br> - Automatic Zero Correction 

17. When segments turn off, the output voltage will increase. The diode, on the other hand, will result in a relatively steady output voltage, around point "B."
In addition to limiting maximum power dissipation, the resistor reduces the change in power dissipation as the display changes. This effect is caused by the fact that, as fewer segments are "ON," each "ON" output drops more voltage and current. For the best case of six segments (a "111" display) to worst case (a "1888" display) the resistor circuit will


Figure 17: TSC7107 Output Current vs Output Voltage

## Package Information

40-Pin Plastic Dual-In-Line Package
(Package \#17)

change about 230 mW , while a circuit without the resistor will change about 470 mW . Therefore, the resistor will reduce the effect of display dissipation on reference voltage drift by about 50\%.
The change in LED brightness caused by the resistor is almost unnoticeable as more segments turn off. If display brightness remaining steady is very important to the designer, diode may be used instead of the resistor.


Figure 18: Dlode or Resistor Limits Package Power Dissipation

60-PIn Flat Package

(Package \#22)

"BQ" Package - Formed Leads
(Package \#21)

## General Description

The TSC7116A and TSC7117A 3-1/2 digit CMOS analog-todigital converters contain all the active components necessary to construct a $0.05 \%$ resolution measurement system. Seven segment decoders, polarity and digit drivers, voltage reference and clock circuit are integrated on chip. The TSC7116A drives liquid crystal displays (LCD) and includes a backplane driver. The TSC7117A drives common anode light emitting diode (LED) displays directly with an 8 mA drive current per segment.
The TSC7116A/TSC7117A incorporate the display hold (HLDR) function. The displayed reading will remain indefinitely as long as HLDR is held high. Conversions continue but the output data display latches are not updated. The $\mathrm{V}_{\mathrm{REF}}^{-}$ or reference low input is not available as it is with the TSC7 106/TSC7107. V- $\overline{\text { REF }}$ is tied internally to analog common in the TSC7116A/TSC7117A devices.
The TSC7116A/TSC7117A feature a precision low drift internal reference. A low drift external reference voltage is normally not required. Existing 7116/7117 systems may be upgraded without changing external components.
The TSC7116A/TSC7117A reduce linearity error to less than 1 count. Rollover error-the difference in readings for equal magnitude but opposite polarity input signals - is below $\pm 1$ count. High impedance differential inputs offer 1 pA leakage current and a $1012 \Omega$ input impedance. The $15 \mu \mathrm{Vp}-\mathrm{p}$ noise performance guarantees a "rock solid" reading. The


Figure 1: Typical TSC7116A Operating CIrcult

## Features

- Internal Reference with Low

Temperature Drift .................. $20 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ Typical $50 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ Maximum

- Display Hold Function
- Drives LCD or LED Displays Directly
- Guaranteed Zero Reading with Zero Input
- Low Noise for Stable Display -2.000 V or 200.0 mV Full-Scale Range
- Auto-Zero Cycle Eliminates Need for Zero Adjustment Potentiometer
- True Polarity Indication for Precision Null Applications
- Convenient 9 V Battery Operation (TSC7116A)
- High Impedance CMOS Differential Inputs ..... $1012 \Omega$
- Low Power Operation ............................. 10 mW
auto-zero cycle guarantees a zero display reading with a zero volt input.
The TSC7116A/TSC7117A dual slope conversion technique automatically rejects interference signals if the converters integration time is set to a multiple of the interference signal period. This is especially useful in industrial measurement environments where 50,60 and 400 Hz line frequency signals are present.
The TSC7116A/TSC7117A are available in a small 60-pin flat package for compact designs. Standard devices are offered in an industrial temperature range and with burn-in lasting for 160 hours at $+125^{\circ} \mathrm{C}$.


Figure 2: Typical TSC7117A Operating Circult

## 3 1/2 Digit A/D Converter <br> - Low Drift Voltage Reference <br> - Display Hold Function

## Absolute Maximum Ratings

## TSC7116A



Stresses above those listed under Absolute Maximum Ratings may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions above those indicated

## TSC7117A

| Supply Voltage |
| :---: |
| $\mathrm{V}^{+}$.............................................. +6 l V |
| $\mathrm{V}^{-}$. . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . -9 V |
| Analog Input Voltage (either input) (Note 1) .... $\mathrm{V}^{+}$to $\mathrm{V}^{-}$ |
| Reference Input Voltage (either input) ........... $\mathrm{V}^{+}$to $\mathrm{V}^{-}$ |
| Clock Input . .................................. GND to $\mathrm{V}^{+}$ |
| Power Dissipation (Note 1) |
| CerDIP Package ........................... 1000 mW |
| Plastic Package .............................. 800 mW |
| Operating Temperature |
| "C" Devices . . . . . . . . . . . . . . . . . . . . . . . . $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ |
| "I" Devices . . . . . . . . . . . . . . . . . . . . . . . . $-25^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
| Storage Temperature ................. $-65^{\circ} \mathrm{C}$ to $+160^{\circ} \mathrm{C}$ |
| Lead Temperature (Soldering, 60 sec ) ............ $300^{\circ} \mathrm{C}$ |
| in the operational sections of the specifications is not implied. Exposure to Absolute Maximum Rating Conditions for extended periods may effect device reliability. |

Electrical Characteristics (Note 3)

| CHARACTERISTICS | CONDITIONS | MIN | TYP | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Zero Input Reading | $\begin{aligned} & \mathrm{V}_{1 \mathrm{~N}}=0.0 \mathrm{~V} \\ & \text { Full-Scale }=200.0 \mathrm{mV} \end{aligned}$ | -000.0 | $\pm 000.0$ | +000.0 | Digital Reading |
| Ratiometric Reading | $\begin{aligned} & V_{I N}=V_{\text {REF }} \\ & V_{\text {REF }}=100 \mathrm{mV} \end{aligned}$ | 999 | 999/1000 | 1000 | Digital Reading |
| Rollover Error (Difference in Reading for Equal Positive and Negative Reading Near Full-Scale) | $\begin{aligned} & -V_{\text {IN }}=+V_{\text {IN }} \approx 200.0 \mathrm{mV} \\ & \text { or } \approx 2.000 \mathrm{~V} \end{aligned}$ | -1 | $\pm 0.2$ | +1 | Counts |
| Linearity (Max. Deviation From Best Straight Line Fit) | $\begin{aligned} & \text { Full-Scale }=200 \mathrm{mV} \\ & \text { or Full-Scale }=2.000 \mathrm{~V} \end{aligned}$ | -1 | $\pm 0.2$ | +1 | Counts |
| Common-Mode Rejection Ratio (Note 4) | $\begin{aligned} & V_{C M}= \pm 1 \mathrm{~V}, \mathrm{~V}_{1 \mathrm{~N}}=0 \mathrm{~V} . \\ & \text { Full-Scale }=200.0 \mathrm{mV} \end{aligned}$ | - | 50 | - | $\mu \mathrm{V} / \mathrm{V}$ |
| Noise (Pk - Pk Value Not Exceeded 95\% of Time) | $\begin{aligned} & V_{1 \mathrm{~N}}=0 \mathrm{~V} \\ & \text { Full-Scale }=200.0 \mathrm{mV} \end{aligned}$ | - | 15 | - | $\mu \mathrm{V}$ |
| Leakage Current @ Input | $\mathrm{V}_{\mathrm{IN}}=0 \mathrm{~V}$ | - | 1 | 10 | pA |
| Zero Reading Drift | $\begin{aligned} & \mathrm{V}_{\mathrm{IN}}=0 \mathrm{~V} \\ & \text { " } \mathrm{C} \text { " Device }=0^{\circ} \mathrm{C} \text { to } 70^{\circ} \mathrm{C} \\ & \mathrm{VIN}_{\mathrm{IN}}=0 \mathrm{~V} \\ & \text { "I" Device }=-25^{\circ} \mathrm{C} \text { to }+85^{\circ} \mathrm{C} \end{aligned}$ | - | 0.2 1.0 | 1 2 | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
| Scale Factor <br> Temperature Coefficient | $\mathrm{V}_{\mathrm{IN}}=199.0 \mathrm{mV},$ <br> "C" Device $=0^{\circ} \mathrm{C}$ to $70^{\circ} \mathrm{C}$ <br> (Ext. Ref $=0 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ ) <br> $\mathrm{V}_{\mathrm{IN}}=199.0 \mathrm{mV}$ <br> "I" Device: $-25^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | - - | 1 | 5 20 | $\begin{aligned} & \mathrm{ppm} /{ }^{\circ} \mathrm{C} \\ & \mathrm{ppm} /{ }^{\circ} \mathrm{C} \end{aligned}$ |
| Input Resistance, Pin 1 (Note 6) |  | 30 | 70 | - | $\mathrm{k} \Omega$ |
| $\mathrm{V}_{\mathrm{IL}}$, Pin 1 (TSC7116A only) |  | - | - | Test +1.5 | V |
| VIL, Pin 1 (TSC7117A only) |  | - | - | GND +1.5 | V |
| $\mathrm{V}_{\mathrm{IH}, \mathrm{Pin}} 1$ (Both) |  | $\mathrm{V}^{+}-1.5$ | - | - | V |
| Supply Current (Does Not Include LED Current for 7117A) | $\mathrm{V}_{\text {IN }}=0$ | - | 0.8 | 1.8 | mA |
| Analog Common Voltage (With Respect to Pos. Supply) | $25 \mathrm{k} \Omega$ Between Common and Pos. Supply | 2.7 | 3.05 | 3.35 | V |
| Temp. Coeff. of Analog Common (With Respect to Pos. Supply) | " C " Devices: $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ | - | 20 | 50 | ppm $/{ }^{\circ} \mathrm{C}$ |
| Temp. Coeff. of Analog Common (With Respect to Pos. Supply) | $25 \mathrm{k} \Omega$ Between Common and Pos. Supply <br> "I" Devices: $-25^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | - | - | 75 | ppm $/{ }^{\circ} \mathrm{C}$ |

## 3 1/2 Digit A/D Converter <br> - Low Drift Voltage Reference <br> TSC7116A (LCD Drive) <br> - Display Hold Function TSC7117A (LED Drive)

Electrical Characteristics (Cont.)

| CHARACTERISTICS | CONDITIONS | MIN | TYP | MAX | UNIT |
| :--- | :--- | :--- | :--- | :--- | :--- |
| TSC7116A ONLY Pk - Pk <br> Segment Drive Voltage (Note 5) | $\mathrm{V}^{+}$to $\mathrm{V}^{-}=9 \mathrm{~V}$ | 4 | 5 | 6 | V |
| TSC7116A ONLY Pk - Pk <br> Backplane Drive Voltage (Note 5) | $\mathrm{V}^{+}$to $\mathrm{V}^{-}=9 \mathrm{~V}$ | 4 | 5 | 6 | V |
| TSC7117A ONLY <br> Segment Sinking Current <br> (Except Pin 19) | $\mathrm{V}^{+}=5.0 \mathrm{~V}$ <br> Segment Voltage $=3 \mathrm{~V}$ | 5 | 8.0 | - | mA |
| TSC7117A ONLY <br> Segment Sinking Current <br> (Pin 19 Only) | $\mathrm{V}^{+}=5.0 \mathrm{~V}$ <br> Segment Voltage $=3 \mathrm{~V}$ | 10 | 16 | - | mA |

## NOTES:

1. Input voitages may exceed the supply voltages provided the input current is limited to $\pm 100 \mu \mathrm{~A}$.
2. Dissipation rating assumes device is mounted with all leads soldered to printed circuit board.
3. Unless other wise noted, specifications apply to both the TSC7116A and TSC7117A at $T_{A}=25^{\circ} \mathrm{C}, \mathrm{fCLOCK}=48 \mathrm{kHz}$. $\mathrm{T}^{\circ}$ SC7116A is tested in the circuit of Figure 1. TSC7117A is tested in the circuit of Figure 2.
4. Refer to "Differential Input" discussion
5. Backplane drive is in phase with segment drive for 'off' segment, $180^{\circ}$ out of phase for 'on' segment. Frequency is 20 times conversion rate. Average dc component is less than 50 mV .
6. The TSC7116A logic input has an internal pull-down resistor connected from HLDR, Pin 1, to TEST, Pin 37. The TSC7117A logic input has an internal pull-down resistor connected from HLDR, Pin 1 to GROUND, Pin 21.

## Pin Configuration



## Ordering Information

| Part No. | Package | Pin Layout | Temp. Range | Display Drive |
| :---: | :---: | :---: | :---: | :---: |
| TSC7116ACPL | $\begin{aligned} & \text { 40-Pin } \\ & \text { Plastic Dip } \end{aligned}$ | Normal | $\begin{aligned} & 0^{\circ} \mathrm{C} \text { to } \\ & +70^{\circ} \mathrm{C} \end{aligned}$ | LCD |
| TSC7116AIJL | $\begin{aligned} & \text { 40-Pin } \\ & \text { CerDIP } \end{aligned}$ | Normal | $\begin{array}{r} -25^{\circ} \mathrm{C}+0 \\ +85^{\circ} \mathrm{C} \end{array}$ | LCD |
| TSC7116ACBQ | 60 -Pin <br> Plastic Flat <br> Package | Formed Leads | $\begin{aligned} & 0^{\circ} \mathrm{C} \text { to } \\ & +70^{\circ} \mathrm{C} \end{aligned}$ | LCD |
| TSC7116ACSQ | 60-Pin <br> Plastic Flat <br> Package | Unformed Leads | $\begin{aligned} & 0^{\circ} \mathrm{C} \text { to } \\ & +70^{\circ} \mathrm{C} \end{aligned}$ | LCD |
| TSC7117ACPL | $\begin{aligned} & \text { 40-Pin } \\ & \text { Plastic Dip } \\ & \hline \end{aligned}$ | Normal | $\begin{aligned} & 0^{\circ} \mathrm{C} \text { to } \\ & +70^{\circ} \mathrm{C} \end{aligned}$ | LED |


| Part No. | Package | Pln Layout | Temp. Range | Display Drive |
| :---: | :---: | :---: | :---: | :---: |
| TSC7117AIJL | $\begin{aligned} & \text { 40-Pin } \\ & \text { CerDIP } \end{aligned}$ | Normal | $\begin{array}{r} -25^{\circ} \mathrm{C} \text { to } \\ +85^{\circ} \mathrm{C} \end{array}$ | LED |
| TSC7117ACBQ | 60-Pin <br> Plastic Flat <br> Package | Formed Leads | $\begin{aligned} & 0^{\circ} \mathrm{C} \text { to } \\ & +70^{\circ} \mathrm{C} \end{aligned}$ | LED |
| TSC7117ACSQ | 60-Pin <br> Plastic Flat <br> Package | Unformed Leads | $\begin{aligned} & 0^{\circ} \mathrm{C}+{ }^{10} \\ & +70^{\circ} \mathrm{C} \end{aligned}$ | LED |
| Devices with Burn-In (160 Hours at $+125^{\circ} \mathrm{C}$ ) |  |  |  |  |
| TSC7116ACPL/BI | $\begin{aligned} & \hline \text { 40-Pin } \\ & \text { Plastic Dip } \end{aligned}$ | Normal | $\begin{aligned} & 0^{\circ} \mathrm{C}+\mathrm{O} \\ & +70^{\circ} \mathrm{C} \end{aligned}$ | LCD |
| TSC7117ACPL/BI | $\begin{aligned} & \text { 40-Pin } \\ & \text { Plastic Dip } \end{aligned}$ | Normal | $\begin{aligned} & \hline 0^{\circ} \mathrm{C} \text { to } \\ & +70^{\circ} \mathrm{C} \end{aligned}$ | LED |

## Pin Description

| 40-Pin DIP Pin Number Normal | 60-Pin Flat Package Pin Number | Name | Description |
| :---: | :---: | :---: | :---: |
| 1 | 13 | HLDR | Hold Pin, Logic 1 holds present display reading. |
| 2 | 14 | $\mathrm{D}_{1}$ | Activates the D section of the units display. |
| 3 | 15 | $\mathrm{C}_{1}$ | Activates the C section of the units display. |
| 4 | 16 | $\mathrm{B}_{1}$ | Activates the B section of the units display. |
| 5 | 17 | A1 | Activates the A section of the units display. |
| 6 | 18 | $F_{1}$ | Activates the F section of the units display. |
| 7 | 19 | $\mathrm{G}_{1}$ | Activates the G section of the units display. |
| 8 | 20 | $\mathrm{E}_{1}$ | Activates the E section of the units display. |
| 9 | 21 | $\mathrm{D}_{2}$ | Activates the D section of the tens display. |
| 10 | 25 | $\mathrm{C}_{2}$ | Activates the C section of the tens display. |
| 11 | 26 | $\mathrm{B}_{2}$ | Activates the B section of the tens display. |
| 12 | 27 | $\mathrm{A}_{2}$ | Activates the A section of the tens display. |
| 13 | 28 | F2 | Activates the F section of the tens display. |
| 14 | 29 | E2 | Activates the E section of the tens display. |
| 15 | 30 | D | Activates the D section of the hundreds display. |
| 16 | 31 | $\mathrm{B}_{3}$ | Activates the B section of the hundreds display. |
| 17 | 32 | F3 | Activates the F section of the hundreds display. |
| 18 | 33 | $\mathrm{E}_{3}$ | Activates the E section of the hundreds display. |
| 19 | 34 | $\mathrm{AB}_{4}$ | Activates both halves of the 1 in the thousands display. |
| 20 | 35 | POL | Activates the negative polarity display. |
| 21 | 36 | $\begin{aligned} & \text { BP } \\ & \text { GND } \end{aligned}$ | TSC7116A: LCD Backplane drive output. TSC7117A: Digital Ground. |
| 22 | 37 | $\mathrm{G}_{3}$ | Activates the G section of the hundreds display. |
| 23 | 40 | $\mathrm{A}_{3}$ | Activates the A section of the hundreds display. |
| 24 | 41 | $\mathrm{C}_{3}$ | Activates the C section of the hundreds display. |
| 25 | 43 | $\mathrm{G}_{2}$ | Activates the G section of the tens display. |
| 26 | 45 | $\mathrm{V}^{-}$ | Negative power supply voltage. |
| 27 | 46 | VINT | Integrator output. Connection point for integration capacitor. See INTEGRATING CAPACITOR section for additional details. |
| 28 | 47 | Vbuff | Integration resistor connection. Use a $47 \mathrm{k} \Omega$ for a 200 mV full-scale range and a $470 \mathrm{k} \Omega$ for 2 V full-scale range. |


| Pin Description (Cont.) <br> 40-Pin DIP <br> Pin Number <br> Normal <br> 29 | 60-Pin <br> Flat Package <br> Pin Number | Name | Description |
| :---: | :---: | :---: | :---: |

## Analog Section

Figure 3 shows the Block Diagram of the Analog Section for the TSC7116A and TSC7117A. Each measurement cycle is divided into three phases. They are (1) auto-zero (A-Z), (2) signal integrate (INT) and (3) reference (REF).

## Auto-Zero Phase

Input high and low are disconnected from the pins and internally shorted to analog common. The reference capacitor is charged to the reference voltage. A feedback loop is closed around the system to charge the auto-zero capacitor $\mathrm{C}_{A Z}$ to compensate for offset voltages in the buffer amplifier, integrator, and comparator. Since the comparator is included in the loop, the A-Z accuracy is limited only by the noise of the system. The offset referred to the input is less than $10 \mu \mathrm{~V}$.

## Signal Integrate Phase

The auto-zero loop is opened, the internal short is removed, and the internal input high and low are connected to the external pins. The converter then integrates the differential voltage between Vinand $^{+}$ViN $_{\text {IN }}^{-}$for a fixed time. This differential voltage can be within a wide common-mode range; within one volt of either supply. If, on the other hand, the input signal has no return with respect to the converter power supply, Vin can be tied to analog common to establish the correct common-mode voltage. At the end of this phase, the polarity of the integrated signal is determined.

## Reference Integrate Phase

The final phase is reference integrate or de-integrate. Input low is internally connected to analog common and input high is connected across the previously charged reference capacitor. Circuitry within the chip ensures that the capacitor will be connected with the correct polarity to cause the integrator output to return to zero. The time required for the output to return to zero is proportional to the input signal. The digital reading displayed is:

$$
1000 \times \frac{V_{I N}}{V_{\text {REF }}}
$$

## Reference

The positive reference voltage ( $\mathrm{V}_{\mathrm{REF}}^{+}$) is referenced to analog common.

## Differential Input

The input can accept differential voltages anywhere within the common-mode range of the input amplifier; or specifically from 1.0 volts below the positive supply to 1.0 volt above the negative supply. In this range the system has a CMRR of 86 dB typical. However, since the integrator also swings with the common-mode voltage, care must be exercised to assure the integrator output does not saturate. A worse case condition would be a large positive common-mode voltage with a near full-scale negative differential input voltage. The negative input signal drives the integrator positive when most of


Figure 3: Analog Section of TSC7116A/TSC7117A
its swing has been used up by the positive common-mode voltage. For these critical applications the integrator swing can be reduced to less than the recommended 2 V full-scale swing with little loss of accuracy. The integrator output can swing within 0.3 volts of either supply without loss of linearity.

## Analog Common

This pin is included primarily to set the common-mode voltage for battery operation (TSC7116A) or for any system where the input signals are floating with respect to the power supply. The common pin sets a voltage that is approximately 3.0 volts more negative than the positive supply. This is selected to give a minimum end-of-life battery voltage of about 6 V . However, the analog common has some of the attributes of a reference voltage. When the total supply voltage is large enough to cause the zener to regulate ( $>7 \mathrm{~V}$ ), the common voltage will have a low voltage coefficient ( $0.001 \% / \%$ ), iow output impedance ( $\sim 15 \Omega$ ), and a temperature coefficient of $20 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ typically.


Figure 4: Using an External Reference

An external reference may be may be used if necessary. The circuit is shown in Figure 4.

Analog common is also used as the ViN return during autozero and deintegrate. If Vin is different from analog common, a common-mode voltage exists in the system and is taken care of by the excellent CMRR of the converter. However, in some applications Vin will be set at a fixed known voltage (power supply common for instance). In this application, analog common should be tied to the same point, thus removing the common-mode voltage from the converter. The same holds true for the reference voltage. If reference can be conveniently referenced to analog common, it should be since this removes the common-mode voltage from the reference system.

Within the IC, analog common is tied to an N-channel FET that can sink 30 mA or more of current to hold the voltage 3.0 volts below the positive supply (when a load is trying to pull the common line positive). However, there is only $10 \mu \mathrm{~A}$ of source current, so common may easily be tied to a more negative voltage thus over-riding the internal reference.

## Test

The TEST pin serves two functions. On the TSC7117A it is coupled to the internally generated digital supply through a $500 \Omega$ resistor. Thus it can be used as the negative supply for externally generated segment drivers such as decimal points or any other presentation the user may want to include on the LCD display. Figures 5 and 6 show such an application. No more than a 1 mA load should be applied.

The second function is a "lamp test." When TEST is pulled high (to $\mathrm{V}^{+}$) all segments will be turned on and the display should read -1888 . The TEST pin will sink about 10 mA under these conditions.


Figure 5: Simple Inverter for Fixed Decimal Point


Figure 6: Exclusive "OR" Gate for Decimal Point Drive


Figure 7: Clock Circuits

## Digital Section

Figures 8 and 9 show the digital section for the TSC7116A and TSC7117A, respectively. In the TSC7116A (Figure 8), an internal digital ground is generated from a 6 volt Zener diode and a large $P$ channel source follower. This supply is made stiff to absorb the large capacitive currents when the back plane (BP) voltage is switched. The BP frequency is the clock frequency divided by 800 . For three readings/second this is a 60 Hz square wave with a nominal amplitude of 5 volts. The segments are driven at the same frequency and amplitude and are in phase with BP when OFF, but out of phase when ON. In all cases, negligible dc voltage exists across the segments.

Figure 9 is the Digital Section of the TSC7117A. It is identical to the TSC7116A except that the regulated supply and back plane drive have been eliminated and the segment drive is typically 8 mA . The 1000 output (pin 19) sinks current from two LED segments, and has a 16 mA drive capability. The TSC7117A is designed to drive common anode LEDs.
In both devices, the polarity indication is "on" for negative anaiog inputs. If $\mathrm{V}_{\mathrm{N}}^{-}$and $\mathrm{V}_{\mathrm{IN}}^{+}$are reversed, this indication can be reversed also, if desired.

## System Timing

Figure 9 shows the clocking method used in the TSC7116A and TSC7117A. Three clocking methods may be used:

1. An external oscillator connected to pin 40.
2. A crystal between pins 39 and 40.
3. An RC oscillator using all three pins.

The oscillator frequency is divided by four before it clocks the decade counters. It is then further divided to form the three convert-cycle phases. These are signal integrate (1000 counts), reference de-integrate ( 0 to 2000 counts) and autozero (1000 to 3000 counts). For signals less than full-scale auto-zero gets the unused portion of reference de-integrate. This makes a complete measure cycle of 4,000 (16,000 clock puises) independent of input voltage. For three readings/ second, an oscillator frequency of 48 kHz would be used.
To achieve maximum rejection of 60 Hz pickup, the signal integrate cycle should be a multiple of 60 Hz . Oscillator frequencies of $240 \mathrm{kHz}, 120 \mathrm{kHz}, 80 \mathrm{kHz}, 60 \mathrm{kHz}, 48 \mathrm{kHz}, 40 \mathrm{kHz}$, $33-1 / 3 \mathrm{kHz}$, etc. should be selected. For 50 Hz rejection, oscillator frequencies of $200 \mathrm{kHz}, 100 \mathrm{kHz}, 66-2 / 3 \mathrm{kHz}$, $50 \mathrm{kHz}, 40 \mathrm{kHz}$, etc. would be suitable. Note that $40 \mathrm{kHz}(2.5$ readings/second) will reject both 50 and 60 Hz (also 400 and 440 Hz ).

## HOLD Reading Input

When HLDR is at a logic "HI" the latch will not be updated. A/D conversions will continue but will not be updated until the HLDR is returned to "LOW". To continuously update the display connect to TEST (TSC7116A) or GROUND (TSC7117A) or disconnect. This input is CMOS compatible with 70K typical resistance to TEST (TSC7116A) or GROUND (TSC7117A).

## Component Value Selection

## Auto-Zero Capacitor

The size of the auto-zero capacitor has some influence on the noise of the system. For 200 mV full-scale where noise is very important, a $0.47 \mu \mathrm{~F}$ capacitor is recommended. On the 2 volt scale, a $0.047 \mu \mathrm{~F}$ capacitor increase the speed of recovery from overload and is adequate for noise on this scale.

## Reference Capacitor

A $0.1 \mu \mathrm{~F}$ capacitor is acceptable in most applications. However, where a large common-mode voltage exists (i.e. the Vin pin is not at analog common) and a 200 mV scale is used, a large value is required to prevent to roll-over error. Generally $1.0 \mu \mathrm{~F}$ will hold the roll-over error to 0.5 count in this instance.


Figure 8: TSC7116A Digital Section


Figure 9: TSC7117A Digital Section

## Integrating Capacitor

The integrating capacitor should be selected to give the maximum voltage swing that ensures tolerance build-up will not saturate the integrator swing (approx. 0.3 volt from either supply). In the TSC7116A or the TSC7117A, when the analog common is used as a reference, a nominal $\pm 2$ volt full-scale integrator swing is acceptable. For the TSC7117A with $\pm 5$ volt supplies and analog common tied to supply ground, a $\pm 3.5$ to $\pm 4$ volt swing is nominal. For three readings/second ( 48 kHz clock) nominal values for CINT are $0.22 \mu \mathrm{~F}$ and $0.10 \mu \mathrm{~F}$, respectively. If different oscillator frequencies are used, these values should be changed in inverse proportion to maintain the output swing.
The integrating capacitor must have low dielectric absorption to prevent roll-over errors. Polypropylene capacitors are recommended for this application.

## Integrating Resistor

Both the buffer amplifier and the integrator have a class $A$ output stage with $100 \mu \mathrm{~A}$ of quiescent current. They can supply $20 \mu \mathrm{~A}$ of drive current with negligible non-linearity. The integrating resistor should be large enough to remain in this very linear region over the input voltage range, but small enough that undue leakage requirements are not placed on the PC board. For 2 volt full-scale, $470 \mathrm{k} \Omega$ is near optimum and similarly a $47 \mathrm{k} \Omega$ for a 200.0 mV scale.

## Oscillator Components

For all ranges of frequency a $100 \mathrm{k} \Omega$ resistor is recommended and the capacitor is selected from the equation $f=45$. For 48 kHz clock (3 readings/second), $C=100 \mathrm{pF}$. RC

## Reference Voltage

To generate full-scale output (2000 counts) the analog input required is: $\mathrm{V}_{\text {IN }}=2 \mathrm{~V}_{\text {REF }}$. Thus, for the 200.0 mV and 2.000 volt scale, VREF should equal 100.0 mV and 1.00 volt respectively. In many applications where the A/D is connected to a transducer, there will exist a scale factor between the input voltage and the digital reading. For instance, in a measuring system, the designer might like to have a full-scale reading when the voltage from the transducer is 700 mV . Instead of dividing the input down to 200.0 mV , the designer should use the input voltage directly and select $V_{R E F}=350 \mathrm{mV}$. Suitable values for integrating resistor and capacitor would be $120 \mathrm{k} \Omega$ and $0.22 \mu \mathrm{~F}$. This makes the system slightly quieter and also avoids a divider network on the input. The TSC7117A with $\pm 5 \mathrm{~V}$ supplies can accept input signals up to $\pm 4 \mathrm{~V}$. Another advantage of this system occurs when a digital reading of zero is desired for $V_{I N} \neq 0$. Temperature and weighing systems with a variable tare are examples. This offset reading can be conveniently generated by connecting the voltage transducer between $\mathrm{V}_{\mathrm{IN}}^{+}$and common and the variable (or fixed) offset voltage between common and ViN.

## TSC7117A Power Supplies

The TSC7117A is designed to work from $\pm 5 \mathrm{~V}$ supplies. However, if a negative supply is not available, it can be generated from the clock output with two diodes, two capacitors and an inexpensive IC. Figure 10 shows this application.

In selected applications no negative supply is required. The conditions to use a single +5 V supply are:

- The input signal can be referenced to the center of the common-mode range of the converter.
- The signal is less than $\pm 1.5$ volts.
- An external reference is used.


Figure 10: Generating Negative Supply From + 5V
Typical Applications


Figure 11: TSC7116A Using the Internal Reference ( 200 mV Full-Scale, 3 RPS)


Figure 12: TSC7117A Internal Reference ( 200 mV Full-Scale, 3 RPS, Vin Tied to GND for Single Ended Inputs).

## TSC7116A (LCD Drive) TSC7117A (LED Drive)



Figure 13: Clrcult for Developing Underrange and Overrange Signals from TSC7116A Outputs.


Figure 14: TSC7117A WIth a 1.2 V External Band-Gap Reference. Vin Tled to Common).

## Applications Information

The TSC7117A sinks the LED display current and this causes heat to build up in the IC package. If the internal voltage reference is used, the changing chip temperature can cause the display to change reading. By reducing package power dissipation such variations can be reduced. By reducing the LED common anode voltage the TSC7117A package power dissipation is reduced.
Figure 17 is a photograph of a curve-tracer display showing the relationship between output current and output voltage for a typical TSC7117ACPL. Since a typical L.ED has 1.8 volts across it at 8 mA , and its common anode is connected to +5 V , the TSC7117A output is at 3.2 V (point A on Fig. 17). Maximum power dissipation is $8.1 \mathrm{~mA} \times 3.2 \mathrm{VX} 24$ segments $=622 \mathrm{~mW}$


Figure 15: TSC7116A/TSC7117A: Recommended Component Values for 2.00 V Full-Scale.


Figure 16: TSC7117A Operated from Single +5 V Supply. An External Reference Must Ba Used in This Application.

Notice, however, that once the TSC7117A output voltage is above two volts, the LED current is essentially constant as output voltage increases. Reducing the output voltage by 0.7 V (point B of Figure 17) results in 7.7 mA of LED current, only a 5 percent reduction. Maximum power dissipation is now only $7.7 \mathrm{~mA} \times 2.5 \mathrm{~V} \times 24=462 \mathrm{~mW}$, a reduction of $26 \%$. An output voltage reduction of 1 volt (point C) reduces LED current by $10 \%$ ( 7.3 mA ) but power dissipation by $38 \%$ ! (7.3 $\mathrm{mAX} 2.2 \mathrm{~V} \times 24=385 \mathrm{~mW}$ ).

Reduced power dissipation is very easy to obtain. Fig. 18 shows two ways: either a $5.10 \mathrm{hm}, 1 / 4$ watt resistor or a 1 Amp diode placed in series with the display (but not in series with the TSC7117). The resistor will reduce the TSC7117A output voltage, when all 24 segments are "ON," to point " C " of Fig.

## 3 1/2 Digit A/D Converter <br> - Low Drift Voltage Reference <br> TSC7116A (LCD Drive) <br> - Display Hold Function TSC7117A (LED Drive)

17. When segments turn off, the output voltage will increase. The diode, on the other hand, will result in a relatively steady output voltage, around point "B."
In addition to limiting maximum power dissipation, the resistor reduces the change in power dissipation as the display changes. This effect is caused by the fact that, as fewer segments are "ON," each "ON" output drops more voltage and current. For the best case of six segments (a "111" display) to worst case (a "1888" display) the resistor circuit will


Figure 17: TSC7117A Output Current vs. Output Voltage
change about 230 mW , while a circuit without the resistor will change about 470 mW . Therefore, the resistor will reduce the effect of display dissipation on reference voltage drift by about 50\%.

The change in LED brightness caused by the resistor is almost unnoticeable as more segments turn off. If display brightness remaining steady is very important to the designer, diode may be used instead of the resistor.


Figure 18: Dlode or Resistor LImits Package Power Dissipation

## Package Information



## General Description

The TSC7116 and TSC7117 3-1/2 digit CMOS analog-to-digital converters contain all the active components necessary to construct a $0.05 \%$ resolution measurement system. Seven segment decoders, polarity and digit drivers, voltage reference and clock circuit are integrated on chip. The TSC7116 drives liquid crystal displays (LCD) and includes a backplane driver. The TSC7117 drives common anode light emitting diode (LED) displays directly with an 8 mA drive current per segment.
The TSC7116/TSC7117 incorporates the display hold (HLDR) function. the displayed reading will remain indefinitely as long as HLDR is held high. Conversions continue but the output data display latches are not updated. The $V^{-}$REF or reference low input is not available as it is with the TSC7106/TSC7107. $V^{-}$REF is tied internally to analog common in the TSC7116/TSC7117 devices.
A low cost, high resolution indicating meter requires only a display, four resistors, and four capicitors. The TSC7116 low power drain and 9 V battery operation make it ideal for portable applications.
The TSC7116/TSC7117 reduce linearity error to less than 1 count. Rollover error - the difference in readings for equal magnitude but opposite polarity input signals - is below $\pm 1$ count. High impedance differential inputs offer 1 pA leakage current and a $1012 \Omega$ input impedance. The $15 \mu \mathrm{Vp}-\mathrm{p}$ noise performance guarantees a "rock solid" reading. The auto-


Figure 1: Typical TSC7116 Operating Circuit

## Features

- Display Hold Function
- Drives LCD or LED Displays Directly
- Guaranteed Zero Reading with Zero Input
- Low Noise for Stable Display -2.000 V or 200.0 mV Full-Scale Range
- Auto-Zero Cycle Eliminates Need for Zero Adjustment Potentiometer
- True Polarity Indication for Precision Null Applications
- Convenient 9 V Battery Operation (TSC7116)
- High Impedance CMOS Differential Inputs ..... $1012 \Omega$
- Low Power Operation ............................ 10 mW
zero cycle guarantees a zero display reading with a zero volt input.
The TSC7116/TSC7117 dual slope conversion technique automatically rejects interference signals if the converters integration time is set to a multiple of the interference signal period. This is especially useful in industrial measurement environments where 50,60 and 400 Hz line frequency signals are present.
The TSC7116/TSC7117 are available in a small 60-pin flat package for compact designs. Standard devices are offered in an industrial temperature range and with burn-in lasting for 160 hours at $+125^{\circ} \mathrm{C}$.

For applications requiring a more temperature stable internal reference voltage refer to the TSC7116A/7107A data sheets.


Figure 2: Typical TSC7117 Operating Circuit

# 3 1/2 Digit A/D Converter - Direct Display Drive 

 TSC7117 (LED Drive)
## Absolute Maximum Ratings

TSC7116
Supply Voltage ( $\mathrm{V}^{+}$to $\mathrm{V}^{-}$) .................................... 15 V
Analog Input Voltage (either input) (Note 1) $\ldots . . \mathrm{V}^{+}$to $\mathrm{V}^{-}$
Reference Input Voltage (either input) ............ $\mathrm{V}^{+}$to $\mathrm{V}^{-}$
Clock Input ............................................ Test to $\mathrm{V}^{+}$
Power Dissipation (Note 2)
CerDIP Package ....................................................... 800 mW
Plastic Package ....................

| Operating Temperature |  |
| :---: | :---: |
| "C" Devices . . . . . . . . . . . . . . . . . . . . . . . . $0^{\circ} \mathrm{C}$ C to $+70^{\circ} \mathrm{C}$ |  |
| "I" Devices | $-25^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
| Storage Temperature | $-65^{\circ} \mathrm{C}$ to $+160^{\circ} \mathrm{C}$ |
|  | $300^{\circ} \mathrm{C}$ |

Stresses above those listed under Absolute Maximum Ratings may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions above those indicated

## TSC7117

Supply Voltage


Electrical Characteristics (Note 3)

| CHARACTERISTICS | CONDITIONS | MIN | TYP | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Zero Input Reading ${ }^{\prime}$ | $\begin{aligned} & \mathrm{ViN}_{10}=0.0 \mathrm{~V} \\ & \text { Full-Scale }=200.0 \mathrm{mV} \end{aligned}$ | -000.0 | $\pm 000.0$ | +000.0 | Digital Reading |
| Ratiometric Reading | $\begin{aligned} & \mathrm{V}_{\mathrm{IN}}=\mathrm{V}_{\text {REF }} \\ & \mathrm{V}_{\mathrm{REF}}=100 \mathrm{mV} \end{aligned}$ | 999 | 999/1000 | 1000 | Digital Reading |
| Rollover Error (Difference in Reading for Equal Positive and Negative Reading Near Full-Scale) | $-\mathrm{V}_{\text {IN }}=+\mathrm{V}_{\text {IN }} \simeq 200.0 \mathrm{mV}$ | -1 | $\pm 0.2$ | +1 | Counts |
| Linearity (Max. Deviation From Best Straight Line Fit) | $\begin{aligned} & \text { Full-Scale }=200 \mathrm{mV} \\ & \text { or Full-Scale }=2.000 \mathrm{~V} \end{aligned}$ | -1 | $\pm 0.2$ | +1 | Counts |
| Common-Mode <br> Rejection Ratio (Note 4) | $\begin{aligned} & \mathrm{VCM}= \pm 1 \mathrm{~V}, \mathrm{~V}_{\mathrm{IN}}=0 \mathrm{~V} . \\ & \text { Full-Scale }=200.0 \mathrm{mV} \end{aligned}$ | - | 50 | - | $\mu \mathrm{V} / \mathrm{V}$ |
| Noise (Pk - Pk Value Not Exceeded 95\% of Time) | $\begin{aligned} & \hline \mathrm{V}_{\mathrm{N}}=0 \mathrm{~V} \\ & \text { Full-Scale }=200.0 \mathrm{mV} \end{aligned}$ | - | 15 | - | $\mu \mathrm{V}$ |
| Leakage Current @ Input | $\mathrm{VIN}_{\text {I }}=0 \mathrm{~V}$ | - | 1 | 10 | pA |
| Zero Reading Drift | $\begin{aligned} & \text { VIN }=0 \mathrm{~V} \\ & \text { " } \mathrm{C} \text { " Device }=0^{\circ} \mathrm{C} \text { to } 70^{\circ} \mathrm{C} \\ & \mathrm{VIN}=0 \mathrm{~V} \\ & \text { "I" Device }=-25^{\circ} \mathrm{C} \text { to }+85^{\circ} \mathrm{C} \end{aligned}$ | - | 0.2 1.0 | 1 2 | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
| Scale Factor <br> Temperature Coefficient | $\begin{aligned} & \text { VIN }=199.0 \mathrm{mV} \\ & \text { "C Device }=0^{\circ} \mathrm{C} \text { to } 70^{\circ} \mathrm{C} \\ & \text { (Ext. Ref }=0 \mathrm{ppm} /{ }^{\circ} \mathrm{C} \text { ) } \\ & V \text { VI }=199.0 \mathrm{mV} \\ & \text { "I" Device: }-25^{\circ} \mathrm{C} \text { to }+85^{\circ} \mathrm{C} \end{aligned}$ | - | 1 | 5 20 | $\begin{aligned} & \mathrm{ppm} /{ }^{\circ} \mathrm{C} \\ & \mathrm{ppm} /{ }^{\circ} \mathrm{C} \end{aligned}$ |
| Input Resistance, <br> Pin 1 (Note 6) |  | 30 | 70 | - | k $\Omega$ |
| $\mathrm{V}_{\text {IL, Pin }} 1$ (TSC7116 only) |  | - | - | Test +1.5 | V |
| VIL, Pin 1 (TSC7117 only) |  | - | - | GND +1.5 | V |
| $\mathrm{V}_{\mathrm{IH},}$ Pin 1 (Both) |  | $\mathrm{V}^{+}-1.5$ | - | - | V |
| Supply Current (Does Not Include LED Current for 7107) | $\mathrm{V}_{\mathrm{IN}}=0$ | - | 0.8 | 1.8 | mA |
| Analog Common Voltage (With Respect to Pos. Supply) | $25 \mathrm{k} \Omega$ Between Common and Pos. Supply | 2.4 | 2.8 | 3.2 | V |
| Temp. Coeff. of Analog common (With Respect to Pos. Supply) | $25 \mathrm{k} \Omega$ Between Common and Pos. Supply | - | 80 | - | $\mathrm{ppm} /{ }^{\circ} \mathrm{C}$ |
| TSC7116 ONLY Pk - Pk Segment Drive Voltage (Note 5) | $\mathrm{V}^{+}$to $\mathrm{V}^{-}=9 \mathrm{~V}$ | 4 | 5 | 6 | V |

## Electrical Characteristics (Cont.)

| CHARACTERISTICS | CONDITIONS | MIN | TYP | MAX | UNIT |
| :--- | :--- | :---: | :---: | :---: | :---: |
| TSC7116 ONLY PK -Pk <br> Backplane Drive Voltage (Note 5) | $\mathrm{V}^{+}$to $\mathrm{V}^{-}=9 \mathrm{~V}$ | 4 | 5 | 6 | V |
| SSC7117 ONLY <br> Segment Sinking Current <br> (Except Pin 19) | $\mathrm{V}^{+}=5.0 \mathrm{~V}$ <br> Segment Voltage $=3 \mathrm{~V}$ | 5 | 8.0 | - | mA |
| TSC71117 ONLY <br> Segment Sinking Current <br> (Pin 19 Only) | $\mathrm{V}^{+}=5.0 \mathrm{~V}$ <br> Segment Voltage $=3 \mathrm{~V}$ | 10 | 16 | - | mA |

## NOTES:

1. Input voltages may exceed the supply voltages provided the input current is limited to $\pm 100 \mu \mathrm{~A}$.
2. Dissipation rating assumes device is mounted with all leads soldered to printed circuit board.
3. Unless other wise noted, specifications apply to both the TSC7116 and TSC7117 at $T_{A}=25^{\circ} \mathrm{C}$, fCLOCK $=48 \mathrm{kHz}$. TSC7116 is tested in the circuit of Figure 1. TSC7117 is tested in the circuit of Figure 2.
4. Refer to "Differential Input" discussion.
5. Backplane drive is in phase with segment drive for 'off' segment, $180^{\circ}$ out of phase for 'on' segment. Frequency is 20 times conversion rate. Average dc component is less than 50 mV .
6. The TSC7116 logic input has an internal pull-down resistor connected from HLDR, Pin 1, to TEST, Pin 37. The TSC7117 logic input has an internal pulldown resistor connected from HLDR, Pin 1 to GROUND, Pin 21.

## Pin Configuration



## Ordering Information

| Part No. | Package | Pin Layout | Temp. Range | Display Drive |
| :---: | :---: | :---: | :---: | :---: |
| TSC7116CPL | $\begin{aligned} & \text { 40-Pin } \\ & \text { Plastic Dip } \end{aligned}$ | Normal | $\begin{aligned} & 0^{\circ} \mathrm{C} \text { to } \\ & +70^{\circ} \mathrm{C} \end{aligned}$ | LCD |
| TSC7116IPL | $\begin{aligned} & \text { 40-Pin } \\ & \text { Plastic Dip } \end{aligned}$ | Normal | $\begin{array}{r} -25^{\circ} \mathrm{C} \text { to } \\ +85^{\circ} \mathrm{C} \end{array}$ | LCD |
| TSC7116CJL | $\begin{aligned} & \text { 40-Pin } \\ & \text { CerDIP } \end{aligned}$ | Normal | $\begin{aligned} & 0^{\circ} \mathrm{C} \text { to } \\ & +70^{\circ} \mathrm{C} \end{aligned}$ | LCD |
| TSC7116IJL | $\begin{aligned} & \text { 40-Pin } \\ & \text { CerDIP } \end{aligned}$ | Normal | $\begin{array}{r} -25^{\circ} \mathrm{C} \text { to } \\ +85^{\circ} \mathrm{C} \end{array}$ | LCD |
| TSC7116CBQ | 60-Pin <br> Plastic Flat <br> Package | Formed Leads | $\begin{aligned} & 0^{\circ} \mathrm{C} \text { to } \\ & +70^{\circ} \mathrm{C} \end{aligned}$ | LCD |
| TSC7116CSQ | 60-Pin <br> Plastic Flat <br> Package | Unformed Leads | $\begin{aligned} & 0^{\circ} \mathrm{C} \text { to } \\ & +70^{\circ} \end{aligned}$ | LCD |
| TSC7117CPL | $\begin{aligned} & \text { 40-Pin } \\ & \text { Plastic Dip } \end{aligned}$ | Normal | $\begin{aligned} & 0^{\circ} \mathrm{C} \text { to } \\ & +70^{\circ} \mathrm{C} \\ & \hline \end{aligned}$ | LED |
| TSC7117IPL | $\begin{aligned} & \text { 40-Pin } \\ & \text { Plastic Dip } \end{aligned}$ | Normal | $\begin{array}{r} -25^{\circ} \mathrm{C} \text { to } \\ +85^{\circ} \mathrm{C} \end{array}$ | LED |


| Part No. | Package | Pin Layout | Temp. Range | $\begin{gathered} \text { Display } \\ \text { Drive } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: |
| TSC7117CJL | $\begin{aligned} & \text { 40-Pin } \\ & \text { CerDIP } \end{aligned}$ | Normal | $\begin{aligned} & 0^{\circ} \mathrm{C} \text { to } \\ & +70^{\circ} \mathrm{C} \end{aligned}$ | LED |
| TSC7117IJL | $\begin{aligned} & \text { 40-Pin } \\ & \text { CerDIP } \end{aligned}$ | Normal | $\begin{array}{r} -25^{\circ} \mathrm{C} \text { to } \\ +85^{\circ} \mathrm{C} \end{array}$ | LED |
| TSC7117CBQ | 60-Pin <br> Plastic Flat <br> Package | Formed Leads | $\begin{aligned} & 0^{\circ} \mathrm{C} \text { to } \\ & +70^{\circ} \mathrm{C} \end{aligned}$ | LED |
| TSC7117CSQ | $\begin{aligned} & \text { 60-Pin } \\ & \text { Plastic Flat } \\ & \text { Package } \end{aligned}$ | Unformed Leads | $\begin{aligned} & 0^{\circ} \mathrm{C} \text { to } \\ & +70^{\circ} \mathrm{C} \end{aligned}$ | LED |
| Devices with Burn-In ( 160 Hours at $+125^{\circ} \mathrm{C}$ ) |  |  |  |  |
| TSC7116CPL/BI | $\begin{aligned} & \text { 40-Pin } \\ & \text { Plastic Dip } \end{aligned}$ | Normal | $\begin{aligned} & 0^{\circ} \mathrm{C} \text { to } \\ & +70^{\circ} \mathrm{C} \end{aligned}$ | LCD |
| TSC7117CPL/BI | $\begin{aligned} & \text { 40-Pin } \\ & \text { Plastic Dip } \\ & \hline \end{aligned}$ | Normal | $\begin{aligned} & 0^{\circ} \mathrm{C} \text { to } \\ & +70^{\circ} \mathrm{C} \end{aligned}$ | LED |

## Pin Description

| 40-Pin DIP Pin Number | 60-Pin Flat Package Pin Number | Name | Description |
| :---: | :---: | :---: | :---: |
| 1 | 13 | HLDR | Hold Pin, Logic 1 holds present display reading. |
| 2 | 14 | D1 | Activates the D section of the units display. |
| 3 | 15 | $\mathrm{C}_{1}$ | Activates the C section of the units display. |
| 4 | 16 | $\mathrm{B}_{1}$ | Activates the $B$ section of the units display. |
| 5 | 17 | $\mathrm{A}_{1}$ | Activates the A section of the units display. |
| 6 | 18 | $\mathrm{F}_{1}$ | Activates the F section of the units display. |
| 7 | 19 | $\mathrm{G}_{1}$ | Activates the G section of the units display. |
| 8 | 20 | $\mathrm{E}_{1}$ | Activates the E section of the units display. |
| 9 | 21 | $\mathrm{D}_{2}$ | Activates the D section of the tens display. |
| 10 | 25 | $\mathrm{C}_{2}$ | Activates the C section of the tens display. |
| 11 | 26 | $\mathrm{B}_{2}$ | Activates the B section of the tens display. |
| 12 | 27 | $\mathrm{A}_{2}$ | Activates the A section of the tens display. |
| 13 | 28 | F2 | Activates the F section of the tens display. |
| 14 | 29 | E2 | Activates the E section of the tens display. |
| 15 | 30 | $\mathrm{D}_{3}$ | Activates the D section of the hundreds display. |
| 16 | 31 | B3 | Activates the B section of the hundreds display. |
| 17 | 32 | F3 | Activates the F section of the hundreds display. |
| 18 | 33 | $\mathrm{E}_{3}$ | Activates the E section of the hundreds display. |
| 19 | 34 | $\mathrm{AB}_{4}$ | Activates both halves of the 1 in the thousands display. |
| 20 | 35 | POL | Activates the negative polarity display. |
| 21 | 36 | $\begin{gathered} \text { BP } \\ \text { GND } \end{gathered}$ | TSC7116: LCD Backplane drive output. TSC7117: Digital Ground. |
| 22 | 37 | G3 | Activates the G section of the hundreds display. |
| 23 | 40 | A | Activates the A section of the hundreds display. |
| 24 | 41 | $\mathrm{C}_{3}$ | Activates the C section of the hundreds display. |
| 25 | 43 | $\mathrm{G}_{2}$ | Activates the G section of the tens display. |
| 26 | 45 | $\mathrm{V}^{-}$ | Negative power supply voltage. |
| 27 | 46 | VINT | Integrator output. Connection point for integration capacitor. See INTEGRATING CAPACITOR section for additional details. |


| 40-Pin DIP Pin Number Normal | $60-\mathrm{Pin}$ <br> Flat Package Pin Number | Name | Description |
| :---: | :---: | :---: | :---: |
| 28 | 47 | VBuFF | Integration resistor connection. Use a $47 \mathrm{k} \Omega$ for a 200 mV full-scale range and a $470 \mathrm{k} \Omega$ for 2 V full-scale range. |
| 29 | 49 | CAz | The size of the auto-zero capacitor influences the system noise. Use a $0.47 \mu \mathrm{~F}$ capacitor for a 200 mV full-scale, and a $0.047 \mu \mathrm{~F}$ capacitor for a 2 volt full-scale. See paragraph on AUTO-ZERO CAPACITOR for more details. |
| 30 | 51 | VIN | The analog low input is connected to this pin. |
| 31 | 55 | VIN | The analog high input signal is connected to this pin. |
| 32 | 57 | Analog Common | This pin is primarily used to set the analog common-mode voltage for battery operation or in systems where the input signal is referenced to the power supply. See paragraph on ANALOG COMMON for more details. It also acts as a reference voltage source. |
| 33 | 58 | CREF | See pin 34. |
| 34 | 59 | $\mathrm{C}_{\text {+ }}^{+}$ | A $0.1 \mu \mathrm{~F}$ capacitor is used in most applications. If a large common-mode voltage exists (for example the ViN pin is not at analog common), and a 200 mV scale is used, a $1.0 \mu \mathrm{~F}$ is recommended and will hold the rollover error to 0.5 count. |
| 35 | 60 | $\mathrm{V}^{+}$ | Positive Power Supply Voltage. |
| 36 | 1 | $\mathrm{V}_{\text {REF }}^{+}$ | The analog input required to generate a full-scale output (1,999 counts). Place 100 mV between pins 32 and 36 for 199.9 mV full-scale. Place 1.00 volts between pins 32 and 36 for 2 volts full-scale. See paragraph on REFERENCE VOLTAGE. |
| 37 | 3 | Test | Lamp test. When pulled high (to $\mathrm{V}^{+}$) all segments will be turned on and the display should read -1888. It may also be used as a negative supply for externally generated decimal points. See paragraph under TEST for additional information. |
| 38 | 4 | $\mathrm{OSC}_{3}$ | See pin 40. |
| 39 | 6 | $\mathrm{OSC}_{2}$ | See pin 40. |
| 40 | 10 | $\mathrm{OSC}_{1}$ | Pins $40,39,38$ make up the oscillator section. For a 48 kHz clock ( 3 readings per section) connect pin 40 to the junction of a $100 \mathrm{k} \Omega$ resistor and a 100 pF capacitor. The $100 \mathrm{k} \Omega$ resistor is tied to pin 39 and the 100 pF capacitor is tied to pin 38. |

## Analog Section

Figure 3 shows the Block Diagram of the Analog Section for the TSC7116 and TSC7117. Each measurement cycle is divided into three phases. They are (1) auto-zero (A-Z), (2) signal integrate (INT) and (3) reference (REF).

## Auto-Zero Phase

Input high and low are disconnected from the pins and internally shorted to analog common. The reference capacitor is charged to the reference voltage. A feedback loop is closed around the system to charge the auto-zero capacitor $\mathrm{C}_{A Z}$ to compensate for offset voltages in the buffer amplifier, integrator, and comparator. Since the comparator is included in the loop, the A-Z accuracy is limited only by the noise of the system. The offset referred to the input is less than $10 \mu \mathrm{~V}$.

## Signal Integrate Phase

The auto-zero loop is opened, the internal short is removed, and the internal input high and low are connected to the external pins. The converter then integrates the differential voltage between ViNand ViN for a fixed time. This differential voltage can be within a wide common-mode range; within one volt of either supply. If, on the other hand, the input signal has no return with respect to the converter power supply, Vin can be tied to analog common to establish the correct common-mode voltage. At the end of this phase, the polarity of the integrated signal is determined.

## Reference Integrate Phase

The final phase is reference integrate or de-integrate. Input low is internally connected to analog common and input high is connected across the previously charged reference capacitor. Circuitry within the chip ensures that the capacitor will be connected with the correct polarity to cause the integrator output to return to zero. The time required for the output to return to zero is proportional to the input signal. The digital reading displayed is:

$$
1000 \times \frac{V_{\text {IN }}}{V_{\text {REF }}}
$$

## Reference

The positive reference voltage $\left(V_{R E F}^{+}\right)$is referenced to analog common.

## Differential Input

The input can accept differential voltages anywhere within the common-mode range of the input amplifier; or specifically from 1.0 volts below the positive supply to 1.0 volt above the negative supply. In this range the system has a CMRR of 86 dB typical. However, since the integrator also swings with the common-mode voltage, care must be exercised to assure the integrator output does not saturate. A worse case condition would be a large positive common-mode voltage with a near full-scale negative differential input voltage. The negative input signal drives the integrator positive when most of


## Figure 3: Analog Section of TSC7116/TSC7117

its swing has been used up by the positive common-mode voltage. For these critical applications the integrator swing can be reduced to less than the recommended 2 V full-scale swing with little loss of accuracy. The integrator output can swing within 0.3 volts of either supply without loss of linearity.

## Analog Common

This pin is included primarily to set the common-mode voltage for battery operation (TSC7116) or for any system where the input signals are floating with respect to the power supply. The common pin sets a voltage that is approximately 2.8 volts more negative than the positive supply. This is selected to give a minimum end-of-life battery voltage of about 6 V . However, the analog common has some of the attributes of a reference voltage. When the total supply voltage is large enough to cause the zener to regulate ( $>7 \mathrm{~V}$ ), the common voltage will have a low voltage coefficient ( $0.001 \% / \%$ ), low output impedance ( $\sim 15 \Omega$ ), and a temperature coefficient of $80 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ typically.


Figure 4: Using an External Reference

An external reference may be added to improve temperature stability or the TSC7116A/TSC7117A devices with lower analog common temperature drift may be used. The circuit is shown in Figure 4.
Analog common is also used as the Vin return during autozero and deintegrate. If $\mathrm{ViN}^{-1}$ is different from analog common, a common-mode voltage exists in the system and is taken care of by the excellent CMRR of the converter. However, in some applications Vīn will be set at a fixed known voltage (power supply common for instance). In this application, analog common should be tied to the same point, thus removing the cummon-mode voltage from the converter. The same holds true for the reference voltage. If reference can be conveniently referenced to analog common, it should be since this removes the common-mode voltage from the reference system.
Within the IC, analog common is tied to an N -channel FET that can sink 30 mA or more of current to hold the voltage 2.8 volts below the positive supply (when a load is trying to pull the common line positive). However, there is only $10 \mu \mathrm{~A}$ of source current, so common may easily be tied to a more negative voltage thus over-riding the internal reference.

## Test

The TEST pin serves two functions. On the TSC7117 it is coupled to the internally generated digital supply through a $500 \Omega$ resistor. Thus it can be used as the negative supply for externally generated segment drivers such as decimal points or any other presentation the user may want to include on the LCD display. Figures 5 and 6 show such an application. No more than a 1 mA load should be applied.
The second function is a "lamp test." When TEST is pulled high (to $\mathrm{V}^{+}$) all segments will be turned on and the display should read -1888. The TEST pin will sink about 10 mA under these conditions.


Figure 5: Simple Inverter for Fixed Decimal Point


Figure 6: Exclusive "OR" Gate for Decimal Point Drive


Figure 7: Clock Circults

## Digital Section

Figures 8 and 9 show the digital section for the TSC7116 and TSC7117, respectively. In the TSC7116 (Figure 8), an internal digital ground is generated from a 6 volt Zener diode and a large P channel source follower. This supply is made stiff to absorb the large capacitive currents when the back plane (BP) voltage is switched. The BP frequency is the clock frequency divided by 800 . For three readings/second this is a 60 Hz square wave with a nominal amplitude of 5 volts. The segments are driven at the same frequency and amplitude and are in phase with BP when OFF, but out of phase when ON . In all cases, negligible dc voltage exists across the segments.

Figure 9 is the Digital Section of the TSC7117. It is identical to the TSC7116 except that the regulated supply and back plane drive have been eliminated and the segment drive is typically 8 mA . The 1000 output (pin 19) sinks current from two LED segments, and has a 16 mA drive capability. The TSC7117 is designed to drive common anode LEDs.
In both devices, the polarity indication is "on" for negative analog inputs. If $V^{\mathcal{N}}$ and $V_{N N}^{\star}$ are reversed, this indication can be reversed also, if desired.

## System TIming

Figure 9 shows the clocking method used in the TSC7116 and TSC7117. Three clocking methods may be used:

1. An external oscillator connected to pin 40.
2. A crystal between pins 39 and 40 .
3. An RC oscillator using all three pins.

The oscillator frequency is divided by four before it clocks the decade counters. It is then further divided to form the three convert-cycle phases. These are signal integrate (1000 counts), reference de-integrate ( 0 to 2000 counts) and autozero (1000 to 3000 counts). For signals less than full-scale auto-zero gets the unused portion of reference de-integrate. This makes a complete measure cycle of 4,000 ( 16,000 clock pulses) independent of input voltage. For three readings/ second, an oscillator frequency of 48 kHz would be used.
To achieve maximum rejection of 60 Hz pickup, the signal integrate cycle should be a multiple of 60 Hz . Oscillator frequencies of $240 \mathrm{kHz}, 120 \mathrm{kHz}, 80 \mathrm{kHz}, 60 \mathrm{kHz}, 43 \mathrm{kHz}, 40 \mathrm{kHz}$, $33-1 / 3 \mathrm{kHz}$, etc. should be selected. For 50 Hz rejection, oscillator frequencies of $200 \mathrm{kHz}, 100 \mathrm{kHz}, 66-2 / 3 \mathrm{kHz}, \Xi 0 \mathrm{kHz}$, 40 kHz , etc. would be suitable. Note that 40 kHz ( 2.5 readings/ second) will reject both 50 and 60 Hz (also 400 and 440 Hz ).

## HOLD Reading Input

When HLDR is at a logic "HI" the latch will not be upoiated. A/D conversions will continue but will not be updated until the HLDR is returned to "LOW". To continuously update the display connect to TEST (TSC7116) or GROUND (TSC7117) or disconnect. This input is CMOS compatible with 70 K typical resistance to TEST (TSC7116) or GROUND (TSC7117).

## Component Value Selection

## Auto-Zero Capacitor

The size of the auto-zero capacitor has some influence on the noise of the system. For 200 mV full-scale where noise is very important, a $0.47 \mu \mathrm{~F}$ capacitor is recommended. On the 2 volt scale, a $0.047 \mu \mathrm{~F}$ capacitor increase the speed of recovery from overload and is adequate for noise on this scale.

## Reference Capacitor

A $0.1 \mu \mathrm{~F}$ capacitor is acceptable in most applications. However, where a large common-mode voltage exists (i.e. the ViN pin is not at analog common) and a 200 mV scale is used, a large value is required to prevent to roll-over error. Generally $1.0 \mu \mathrm{~F}$ will hold the roll-over error to 0.5 count in this instance.


Figure 8: TSC7116 Digital Section


Figure 9: TSC7117 Digital Section

## Integrating Capacitor

The integrating capacitor should be selected to give the maximum voltage swing that ensures tolerance build-up will not saturate the integrator swing (approx. 0.3 volt from either supply). In the TSC7116 or the TSC7117, when the analog common is used as a reference, a nominal $\pm 2$ volt full-scale integrator swing is acceptable. For the TSC7117 with $\pm 5$ volt supplies and analog common tied to supply ground, $\mathrm{a} \pm 3.5$ to $\pm 4$ volt swing is nominal. For three readings/second ( 48 kHz clock) nominal values for CINT are $0.22 \mu 1 \mathrm{~F}$ and $0.10 \mu \mathrm{~F}$, respectively. If different oscillator frequencies are used, these values should be changed in inverse proportion to maintain the output swing.
The integrating capacitor must have low dielectric absorption to prevent roll-over errors. Polypropylene capacitors are recommended for this application.

## Integrating Resistor

Both the buffer amplifier and the integrator have a class $A$ output stage with $100 \mu \mathrm{~A}$ of quiescent current. They can supply $20 \mu \mathrm{~A}$ of drive current with negligible non-linearity. The integrating resistor should be large enough to remain in this very linear region over the input voltage range, but small enough that undue leakage requirements are not placed on the PC board. For 2 volt full-scale, $470 \mathrm{k} \Omega$ is near optimum and similarly a $47 \mathrm{k} \Omega$ for a 200.0 mV scale.

## Oscillator Components

For all ranges of frequency a $100 \mathrm{k} \Omega$ resistor is recommended and the capacitor is selected from the equation $f=45$. For 48 kHz clock (3 readings/second), $C=100 \mathrm{pF}$. RC

## Reference Voltage

To generate full-scale output (2000 counts) the analog input required is: $\mathrm{V}_{\text {IN }}=2 \mathrm{~V}_{\text {REF }}$. Thus, for the 200.0 mV and 2.000 volt scale, VREF should equal 100.0 mV and 1.00 volt respectively. In many applications where the A/D is connected to a transducer, there will exist a scale factor between the input voltage and the digital reading. For instance, in a measuring system, the designer might like to have a full-scale reading when the voltage from the transducer is 700 mV . Instead of dividing the input down to 200.0 mV , the designer should use the input voltage directly and select $\mathrm{V}_{\text {REF }}=350 \mathrm{mV}$. Suitable values for integrating resistor and capacitor would be $120 \mathrm{k} \Omega$ and $0.22 \mu \mathrm{~F}$. This makes the system slightly quieter and also avoids a divider network on the input. The TSC 7117 with $\pm 5 \mathrm{~V}$ supplies can accept input signals up to $\pm 4 \mathrm{~V}$. Another advantage of this system occurs when a digital reading of zero is desired for $V \mathbb{N} \neq 0$. Temperature and weighing systems with a variable tare are examples. This offset reading can be conveniently generated by connecting the voltage transducer between $\mathrm{V}_{\text {IN }}^{+}$and common and the variable (or fixed) offset voltage between common and ViN.

## TSC7117 Power Supplies

The TSC7117 is designed to work from $\pm 5 \mathrm{~V}$ supplies. However, if a negative supply is not available, it can be generated from the clock output with two diodes, two capacitors and an inexpensive IC. Figure 10 shows this application.

In selected applications no negative supply is required. The conditions to use a single +5 V supply are:

- The input signal can be referenced to the center of the common-mode range of the converter.
- The signal is less than $\pm 1.5$ volts.
- An external reference is used.


Figure 10: Generating Negative Supply From +5 V

## Typical Applications

Figure 11: TSC7116 Using the Internal Reference ( 200 mV Full-Scale, 3 RPS)

Figure 12: TSC7117 Internal Reference ( 200 mV FullScale, 3 RPS, ViN Tied to GND for Single Ended Inputs).



Figure 13: Circuit for Developing Underrange and Overrange Signals from TSC7116 Outputs.


Figure 14: TSC7117 With a 1.2 V External Band-Gap Reference. ViN Tied to Common).

## Applications Information

The TSC7117 sinks the LED display current and this causes heat to build up in the IC package. If the internal voltage reference is used, the changing chip temperature can cause the display to change reading. By reducing package power dissipation such variations can be reduced. By reducing the LED common anode voltage the TSC7117 package power dissipation is reduced.
Figure 17 is a photograph of a curve-tracer display showing the relationship between output current and output voltage for a typical TSC7117CPL. Since a typical LED has 1.8 volts across it at 8 mA , and its common anode is connected to +5 V , the TSC7117 output is at 3.2 V (point A on Fig. 17). Maximum power dissipation is $8.1 \mathrm{~mA} \times 3.2 \mathrm{~V} \times 24$ segments $=622 \mathrm{~mW}$.


Figure 15: TSC7116/TSC7117: Recommended Component Values for 2.00 V Full-Scale.


Figure 16: TSC7117 Operated from Single +5 V Supply. An External Reference Must Be Used in This Application.

Notice, however, that once the TSC7117 output voltage is above two volts, the LED current is essentially constant as output voltage increases. Reducing the output voltage by 0.7 V (point B of Figure 17) results in 7.7 mA of LED current, only a 5 percent reduction. Maximum power dissipation is now only $7.7 \mathrm{~mA} \times 2.5 \vee \times 24=462 \mathrm{~mW}$, a reduction of $26 \%$. An output voltage reduction of 1 volt (point C) reduces LED current by $10 \%(7.3 \mathrm{~mA})$ but power dissipation by $38 \%$ ! 7.3 $\mathrm{mA} \mathrm{X} \mathrm{2.2} \mathrm{~V} \mathrm{X} 24=385 \mathrm{~mW}$ ).
Reduced power dissipation is very easy to obtain. Fig. 18 shows two ways: either a 5.1 ohm, $1 / 4$ watt resistor or a 1 Amp diode placed in series with the display (but not in series with the TSC7117). The resistor will reduce the TSC7117 output voltage, when all 24 segments are "ON," to point "C" of Fig.

## 3 1/2 Digit A/D Converter

- Direct Dlsplay Drive

TSC7116 (LCD Drive)

- Display Hold Function TSC7117 (LED Drive)

17. When segments turn off, the output voltage will increase. The diode, on the other hand, will result in a relatively steady output voltage, around point "B."
In addition to limiting maximum power dissipation, the resistor reduces the change in power dissipation as the display changes. This effect is caused by the fact that, as fewer segments are "ON," each "ON" output drops more voltage and current. For the best case of six segments (a "111" display) to worst case (a "1888" display) the resistor circuit will


Figure 17: TSC7117 Output Current vs Output Voltage
change about 230 mW , while a circuit without the resistor will change about 470 mW . Therefore, the resistor will reduce the effect of display dissipation on reference voltage drift by about 50\%.
The change in LED brightness caused by the resistor is almost unnoticeable as more segments turn off. If display brightness remaining steady is very important to the designer, diode may be used instead of the resistor.


Figure 18: Diode or Resistor Limits Package Power Dissipation

## Package Information



## General Description

The TSC7126A is a low power 3 1/2 Digit LCD display analog to digital converter that allows existing 7126 based systems to be upgraded. An improved internal zener reference voltage circuit maintains the analog common temperature drift to $35 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ typically. A $75 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ maximum limit is guaranteed. This represents a 2 to 4 times improvement over similar 3 1/2 digit converters.
Existing TSC7126 or ICL7126 based systems may be upgraded without changing external passive component values. The costly, space consuming external reference source may be removed. Power dissipation is a low $900 \mu \mathrm{~W}$ maximum. Long battery life is guaranteed; a key design consideration in portable or battery back-up systems.
The TSC7126A limits linearity error to less than 1 count on 200 mV or 2.00 V full-scale ranges. Rollover error - the difference in readings for equal magnitude but opposite polarity input signals - is below $\pm 1$ count. High impedance differential inputs offer 1 pA leakage currents and a $10^{12} \Omega$ input impedance. The differential reference input allows ratiometric measurements for ohms or bridge transducer measurements. The $15 \mu \mathrm{~V}_{\mathrm{p}-\mathrm{p}}$ noise performance guarantees a "rock solid" reading. The auto zero cycle guarantees a zero display readout for a zero volt input.
The single chip CMOS TSC7126A incorporates all the active devices for a $31 / 2$ digit analog to digital converter to directly drive an LCD display. The internal oscillator, precision voltage reference and display segment/backplane drivers simplify system integration, reduce board space requirements and lower total cost. A low cost, high resolution $-0.05 \%$ - indicating meter requires only a display, four resistors, four capacitors and a 9 V battery. The flat package option eases the mechanical design of low cost, hand held multimeters.
The TSC7126A dual slope conversion technique rejects interference signals if the converters integration time is set to a multiple of the interference signal period. This is especially useful in industrial measurement environments where 50, 60 and 400 Hz line frequency signals are present.

## Typical Applications

- Thermometry
- Bridge Readouts (Strain Gauges, Load Cells, Null Detectors)
- Digital Meters
- Voltage/Current/Ohms/Power
- pH
- Capacitance/Inductance
-- Fluid Flow Rate/Viscosity/Level
- Humidity
- Position
- Digital Scales
- Panel Meters
- LVDT Indicators
- Portable instrumentation
- Power Supply Readouts
- Process Monitors
- Gaussometers
- Photometers


## Features

- Internal Reference With Low Temperature Drift .................... $35 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ Typical $75 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ Maximum
- Guaranteed Zero Reading With Zero Input
- Low Noise
- High Resolution ( $0.05 \%$ ) and Wide Dynamic Range ( 72 dB )
- Low Input Leakage Current ............... 1 pA Typical 10 pA Maximum
- Direct LCD Drive - No External Components.
- Precision Null Detection With True Polarity at Zero
- High Impedance Differential Input
- Convenient 9 V Battery Operation With Low

Power Dissipation ....................... $500 \mu \mathrm{~W}$ Typical $900 \mu \mathrm{~W}$ Maximum

- Internal Clock Circuit
- Improved Drop-In Replacement For ICL7126 that offers Low Analog Common Voltage Drift
- Available in Compact Flat Package
- Industrial Temperature Range Device Available


## Ordering Information

| Part No. | Package | Pln Layout | Temp. Range | Reference Temp. Coefficient |
| :---: | :---: | :---: | :---: | :---: |
| TSC7126ACPL | $\begin{aligned} & \text { 40-Pin } \\ & \text { Plastic Dip } \end{aligned}$ | Normal | $\begin{aligned} & 0^{\circ} \mathrm{C} \text { to } \\ & 70^{\circ} \mathrm{C} \end{aligned}$ | $\begin{array}{r} \hline 75 \mathrm{ppm} /{ }^{\circ} \mathrm{C} \\ \mathrm{Max} \\ \hline \end{array}$ |
| TSC7126ARCPL | $\begin{aligned} & \text { 40-Pin } \\ & \text { Plastic Dip } \end{aligned}$ | Reversed | $\begin{gathered} 0^{\circ} \mathrm{C} \text { to } \\ 70^{\circ} \mathrm{C} \end{gathered}$ | $75 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ Max |
| TSC7126AIJL | $\begin{aligned} & \text { 40-Pin } \\ & \text { CerDIP } \end{aligned}$ | Normal | $\begin{array}{r} -25^{\circ} \mathrm{C} \text { to } \\ +85^{\circ} \mathrm{C} \end{array}$ | $100 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ |
| TSC7126ACBQ | $\begin{aligned} & \text { 60-Pin } \\ & \text { Plastic Flat } \end{aligned}$ | Formed Leads | $\begin{aligned} & 0^{\circ} \mathrm{C} \text { to } \\ & 70^{\circ} \mathrm{C} \end{aligned}$ | $\begin{array}{r} 75 \mathrm{ppm} /{ }^{\circ} \mathrm{C} \\ \text { Max } \end{array}$ |
| TSC7126ACSQ | ```60-Pin Plastic Flat``` | Unformed Leads | $\begin{array}{r} 0^{\circ} \mathrm{C} \text { to } \\ 70^{\circ} \mathrm{C} \end{array}$ | $\begin{array}{r} 75 \mathrm{ppm} /{ }^{\circ} \mathrm{C} \\ \mathrm{Max} \end{array}$ |
| Devices with 160 Hour, $+125^{\circ} \mathrm{C}$ Burn-In |  |  |  |  |
| TSC7126ACPL/BI | $\begin{aligned} & \text { 40-Pin } \\ & \text { Plastic Dip } \end{aligned}$ | Normal | $\begin{array}{r} 0^{\circ} \mathrm{C} \text { to } \\ 70^{\circ} \mathrm{C} \end{array}$ | $\begin{array}{r} 75 \mathrm{ppm} /{ }^{\circ} \mathrm{C} \\ \text { Max } \end{array}$ |
| TSC7126AIJL/BI | $\begin{aligned} & \text { 40-Pin } \\ & \text { CerDIP } \end{aligned}$ | Normal | $\begin{array}{r} -25^{\circ} \mathrm{C} \text { to } \\ +85^{\circ} \mathrm{C} \end{array}$ | $100 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ |



Figure 1: Typical Operating Circuit

# 3 1/2 Digit A/D Converter <br> - Low Power Dissipation - $900 \mu \mathrm{~W}$ Max. 

TSC7126A

## Absolute Maximum Ratings



Plastic Package (P)

800 mW

Epoxy Flat Package (B, S)

500 mW
Operating Temperature
("C" Devices) ................................ $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$
("I" Devices) . ................................ $-25^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$
Storage Temperature .................... $-65^{\circ} \mathrm{C}$ to $+160^{\circ} \mathrm{C}$
Lead Temperature (Soldering, 60 sec ) ............ $300^{\circ} \mathrm{C}$

Electrical Characteristics: $V_{s}=9 \mathrm{~V}, \mathrm{f}_{\mathrm{clock}}=16 \mathrm{kHz}$ and $T_{A}=25^{\circ} \mathrm{C}$ unless otherwise noted.

| TYPE | NO. | SYMBOL | PARAMETER | TEST CONDITIONS | MIN | $\begin{gathered} \text { TSC7126A } \\ \text { TYP } \end{gathered}$ | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \mathbf{1} \\ & \mathbf{N} \\ & \mathbf{P} \\ & \mathbf{U} \\ & \mathbf{T} \end{aligned}$ | 1 | - | Zero Input Reading | $\begin{aligned} & \mathrm{V}_{\mathrm{IN}}=0.0 \mathrm{~V} \\ & \text { Full-Scale }=200.0 \mathrm{mV} \end{aligned}$ | -000.0 | $\pm 000.0$ | +000.0 | Digital Reading |
|  | 2 | - | Zero Reading Drift | $\begin{aligned} & V_{I N}=0.0 \mathrm{~V}, \\ & 0^{\circ} \mathrm{C} \leq T_{A} \leq 70^{\circ} \mathrm{C} \end{aligned}$ | - | 0.2 | 1 | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
|  | 3 | - | Ratiometric Reading | $\begin{aligned} & V_{I N}=V_{\text {REF }} \\ & V_{\text {REF }}=100 \mathrm{mV} \end{aligned}$ | 999 | $\frac{999}{1000}$ | 1000 | Digital Reading |
|  | 4 | NL | Linearity Error | Full-Scale $=200 \mathrm{mV}$ or 2.000 V. Max. Deviation from Best Straight Line | -1 | $\pm 0.2$ | +1 | Counts |
|  | 5 | - | Rollover Error | $\begin{aligned} & -V_{\text {IN }}=+V_{\text {IN }} \\ & \approx 200.0 \mathrm{mV} \end{aligned}$ | -1 | $\pm 0.2$ | +1 | Counts |
|  | 6 | En | Noise | $\begin{aligned} & \mathrm{VIN}=0 \mathrm{~V}, \\ & \text { Full-Scale }=200.0 \mathrm{mV} \end{aligned}$ | - | 15 | - | $\mu \mathrm{V}_{\mathrm{p}-\mathrm{p}}$ |
|  | 7 | IL | Input Leakage Current | $\mathrm{V}_{\text {IN }}=0 \mathrm{~V}$ | - | 1 | 10 | pA |
|  | 8 | CMRR | Common-Mode Rejection Ratio | $\begin{aligned} & V_{C M}= \pm 1 \mathrm{~V}, V_{I N}=0 \mathrm{~V} \\ & \text { Full-Scale }=200.0 \mathrm{mV} \end{aligned}$ | - | 50 | - | $\mu \mathrm{V} / \mathrm{V}$ |
|  | 9 | - | Scale Factor Temperature Coefficient | $\begin{aligned} & \mathrm{VIN}=199.0 \mathrm{mV}, \\ & 0^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq 70^{\circ} \mathrm{C} \\ & \text { Ext. Ref. Temp. } \\ & \text { Coeff. }=0 \mathrm{ppm} /{ }^{\circ} \mathrm{C} \end{aligned}$ | - | 1 | 5 | $\mathrm{ppm} /{ }^{\circ} \mathrm{C}$ |
| $\begin{array}{ll} \text { A C } \\ \text { N O } \\ \text { A M } \\ \text { L M } \\ \text { O O } \\ \text { G } \end{array}$ | 10 | Vcto | Analog Common Temperature Coefficient | $250 \mathrm{k} \Omega$ Between Commom and $\mathrm{V}^{+}$ $0^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq 70^{\circ} \mathrm{C}$ <br> "C" Commercial Temp. Range Devices | - | 35 | 75 | $\mathrm{ppm} /{ }^{\circ} \mathrm{C}$ |
|  | 11 | Vctc | Analog Common Temperature Coefficient | $250 \mathrm{k} \Omega$ Between Common and $\mathrm{V}^{+}$ $-25^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq 85^{\circ} \mathrm{C}$ "I" Industrial Temp. Range Devices | - | 35 | 100 | $\mathrm{ppm} /{ }^{\circ} \mathrm{C}$ |
|  | 12 | Vc | Analog Common Voltage | $250 \mathrm{k} \Omega$ Between Common and $\mathrm{V}^{+}$ | 2.7 | 3.05 | 3.35 | V |
| $\begin{gathered} \\ \\ \text { L. } \\ \text { C } \\ \text { D } \\ \text { D } \\ \text { E } \end{gathered}$ | 13 | VSD | LCD Segment Drive Voltage | $\mathrm{V}^{+}$to $\mathrm{V}^{-}=9 \mathrm{~V}$ | 4 | 5 | 6 | $V_{p-p}$ |
|  | 14 | $V_{B D}$ | LCD Backplane Drive Voltage | $\mathrm{V}^{+}$to $\mathrm{V}^{-}=9 \mathrm{~V}$ | 4 | 5 | 6 | $V_{p-p}$ |
| SUPPLY | 15 | Is | Power Supply Current | $\mathrm{V}_{\text {in }}=0 \mathrm{~V}, \mathrm{~V}^{+} \text {to } \mathrm{V}^{-}=9 \mathrm{~V},$ <br> Note 7 | - | 55 | 100 | $\mu \mathrm{A}$ |

## Notes:

1. Input voltages may exceed the supply voltages when the input current is limited to $100 \mu \mathrm{~A}$.
2. Dissipation rating assumes device is mounted with all leads soldered to printed circuit board.
3. Static sensitive device. Unused devices should be stored in conductive material to protect devices from static discharge and static fields.
4. Refer to "Differential Input" discussion.
5. Backplane drive is in phase with segment drive for 'off' segment and $180^{\circ}$ out of phase for 'on' segment. Frequency is 20 times conversion rate. Average $D C$ component is less than 50 mV .
6. See Figure 1.
7. During auto-zero phase, current is $10-20 \mu \mathrm{~A}$ higher. A 48 kHz oscillator, increases current by $8 \mu \mathrm{~A}$ (typ.). Common current not included.

## Pin Configuration




NOTES:

1. NC = NO INTERNAL CONNECTION
2. PINS 8, 23, 38 AND 53 ARE CONNECTED TO THE DIE THE POTENTIAL AT THESE PINS IS APPROXIMATELY $V^{+}$. NO EXTERNAL CONNECTIONS SHOULD BEMADE.

## Pin Description

| 40-Pin DIP <br> Pin Number <br> Normal | (Reverse) | 60-Pin <br> Flat Package <br> Pin Number | Name | Description |
| :---: | :---: | :---: | :---: | :--- |
| 1 | $(40)$ | 13 | $\mathrm{~V}^{+}$ | Positive supply voltage. |
| 2 | $(39)$ | 14 | $\mathrm{D}_{1}$ | Activates the D section of the units display. |
| 3 | $(38)$ | 15 | $\mathrm{C}_{1}$ | Activates the C section of the units display. |
| 4 | $(37)$ | 16 | $\mathrm{~B}_{1}$ | Activates the B section of the units display. |
| 5 | $(36)$ | 17 | $\mathrm{~A}_{1}$ | Activates the A section of the units display. |
| 6 | $(35)$ | 18 | $\mathrm{~F}_{1}$ | Activates the F section of the units display. |
| 7 | $(34)$ | 19 | $\mathrm{G}_{1}$ | Activates the G section of the units display. |
| 8 | $(33)$ | 20 | $\mathrm{E}_{1}$ | Activates the E section of the units display. |
| 9 | $(32)$ | 21 | $\mathrm{D}_{2}$ | Activates the D section of the tens display. |

## Pin Description (Cont.)

| 40-PIn DIP Pin Number Normal | (Reverse) | 60-Pin Flat Package Pin Number | Name | Description |
| :---: | :---: | :---: | :---: | :---: |
| 10 | (31) | 25 | $\mathrm{C}_{2}$ | Activates the C section of the tens display. |
| 11 | (30) | 26 | $\mathrm{B}_{2}$ | Activates the B section of the tens display. |
| 12 | (29) | 27 | $A_{2}$ | Activates the $A$ section of the tens display. |
| 13 | (28) | 28 | F2 | Activates the F section of the tens display. |
| 14 | (27) | 29 | $E_{2}$ | Activates the E section of the tens display. |
| 15 | (26) | 30 | D | Activates the D section of the hundreds display. |
| 16 | (25) | 31 | B3 | Activates the B section of the hundreds display. |
| 17 | (24) | 32 | F3 | Activates the F section of the hundreds display. |
| 18 | (23) | 33 | $\mathrm{E}_{3}$ | Activates the E section of the hundreds display. |
| 19 | (22) | 34 | $\mathrm{AB}_{4}$ | Activates both halves of the 1 in the thousands display. |
| 20 | (21) | 35 | POL | Activates the negative polarity display. |
| 21 | (20) | 36 | BP | Backplane drive output. |
| 22 | (19) | 37 | $\mathrm{G}_{3}$ | Activates the G section of the hundreds display. |
| 23 | (18) | 40 | $\mathrm{A}_{3}$ | Activates the A section of the hundreds display. |
| 24 | (17) | 41 | $\mathrm{C}_{3}$ | Activates the C section of the hundreds display. |
| 25 | (16) | 43 | $\mathrm{G}_{2}$ | Activates the G section of the tens display. |
| 26 | (15) | 45 | $\mathrm{V}^{-}$ | Negative power supply voltage. |
| 27 | (14) | 46 | VINT | The integrating capacitor should be selected to give the maximum voltage swing that ensures component tolerance build up will not allow the integrator output to saturate. When analog common is used as a reference and the conversion rate is 3 readings per second, a $0.047 \mu \mathrm{~F}$ capacitor may be used. The capacitor must have a low dielectric constant to prevent roll-over errors. See INTEGRATING CAPACITOR section for additional details. |
| 28 | (13) | 47 | Vbuff | Integration resistor connection. Use a $180 \mathrm{k} \Omega$ for a 200 mV full-scale range and a $180 \mathrm{M} \Omega$ for 2 V full scale range. |
| 29 | (12) | 49 | $C_{A z}$ | The size of the auto-zero capacitor influences the system noise. Use a $0.33 \mu \mathrm{~F}$ capacitor for a 200 mV full-scale, and a $0.033 \mu \mathrm{~F}$ capacitor for a 2 volt full-scale. See paragraph on AUTO-ZERO CAPACITOR for more details. |
| 30 | (11) | 51 | Vİ | The low input is connected to this pin. |
| 31 | (10) | 55 | ViN | The high input signal is connected to this pin. |
| 32 | (9) | 57 | Analog Common | This pin is primarily used to set the analog common-mode voltage for battery operation or in systems where the input signal is referenced to the power supply. See paragraph on ANALOG COMMON for more details. It also acts as a reference voltage source. |
| 33 | (8) | 58 | Cāef | See pin 34. |
| 34 | (7) | 59 | $\mathrm{C}_{\text {Ref }}^{+}$ | A $0.1 \mu \mathrm{~F}$ capacitor is used in most applications. If a large common mode voltage exists (for example the ViN pin is not at analog common), and a 200 mV scale is used, a $1.0 \mu \mathrm{~F}$ is recommended and will hold the rollover error to 0.5 count. |
| 35 | (6) | 60 | $V_{\text {ReF }}$ | See pin 36. |
| 36 | (5) | 1 | $\mathrm{V}_{\text {REF }}^{+}$ | The analog input required to generate a full-scale output ( 1,999 counts). Place 100 mV between pins 35 and 36 for 199.9 mV full-scale. Place 1.00 volts between pins 35 and 36 for 2 volts full-scale. See paragraph on REFERENCE VOLTAGE. |
| 37 | (4) | 3 | Test | Lamp test. When pulled high (to $\mathrm{V}^{+}$) all segments will be turned on and the display should read $\mathbf{- 1 8 8 8}$. It may also be used as a negative supply for externally generated decimal points. See paragraph under TEST for additional information. |
| 38 | (3) | 4 | $\mathrm{OSC}_{3}$ | See pin 40. |
| 39 | (2) | 6 | $\mathrm{OSC}_{2}$ | See pin 40. |
| 40 | (1) | 10 | $\mathrm{OSC}_{1}$ | Pins $40,39,38$ make up the oscillator section. For a 48 kHz clock ( 3 readings per section) connect pin 40 to the junction of a $180 \mathrm{k} \Omega$ resistor and a 50 pF capacitor. The $180 \mathrm{k} \Omega$ resistor is tied to pin 39 and the 50 pF capacitor is tied to pin 38. |

## 3 1/2 Digit A/D Converter

- Low Power Dissipation - $900 \mu \mathrm{~W}$ Max.
- $35 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ Internal Reference


## General Theory of Operation

## Dual Slope Conversion Principles

The TSC7126A is a dual slope, integrating analog-to-digital converter. An understanding of the dual slope conversion technique will aid in following the detailed TSC7126A operation theory.
The conventional dual slope converter measurement cycle has two distinct phases:

- Input Signal Integration
- Reference Voltage Integration (Deintegration)

The input signal being converted is integrated for a fixed time period (TsI). Time is measured by counting clock pulses. An opposite polarity constant reference voltage is then integrated until the integrator output voltage returns to zero. The reference integration time is directly proportional to the input signal (TRI).
In a simple dual slope converter a complete conversion requires the integrator output to "ramp-up" and "ramp-down."


Figure 2: Basic Dual Slope Converter


Figure 3: Normal-Mode Rejection of Dual Slope Converter

A simple mathematical equation relates the input signal, reference voltage and integration time:

$$
\frac{1}{R C} \int_{0}^{T S I} V_{I N}(t) d t=\frac{V_{R} T_{R I}}{R C}
$$

where:
$V_{R}=$ Reference Voltage
Tsı $=$ Signal Integration Time (Fixed)
$T_{\text {RI }}=$ Reference Voltage Integration Time (Variable)
For a constant Vin:

$$
V_{I N}=V_{R} \frac{T_{R I}}{T_{S I}}
$$

The dual slope converter accuracy is unrelated to the integrating resistor and capacitor values as long as they are stable during a measurement cycle. An inherent benefit is noise immunity. Noise spikes are integrated or averaged to zero during the integration periods. Integrating ADCs are immune to the large conversion errors that plague successive approximation converters in high noise environments. Interfering signals with frequency components at multiples of the averaging period will be attenuated. Integrating ADCs commonly operate with the signal integration period set to a multiple of the $50 / 60 \mathrm{~Hz}$ power line period.

## Analog Section

In addition to the basic signal integrate and deintegrate cycles discussed above the TSC7126A design incorporates an auto-zero cycle. This cycle removes buffer amplifier, integrator, and comparator offset voltage error terms from the conversion. A true digital zero reading results without external adjusting potentiometers. A complete conversion consists of three cycles: an auto-zero, signal integrate and reference integrate cycle.

## Auto-Zero Cycle

During the auto-zero cycle the differential input signal is disconnected from the circuit by opening internal analog gates. The internal nodes are shorted to analog common (ground) to establish a zero input condition. Additional analog gates close a feedback loop around the integrator and comparator. This loop permits comparator offset voltage error compensation. The voltage level established on CAz compensates for device offset voltages. The auto-zero cycle residual is typically $10-15 \mu \mathrm{~V}$.
The auto-zero cycle length is 1000 to 3000 clock periods.

## Signal Integration Cycle

The auto-zero loop is opened and the internal differential inputs connect to $V^{\dagger}$ N and $V_{i n}$. The differential input signal is integrated for a fixed time period. The TSC7126A signal integration period is 1000 clock periods or counts. The externally set clock frequency is divided by four before clocking the internal counters. The intergration time period is:

$$
\mathrm{TSI}_{\mathrm{SI}}=\frac{4}{\mathrm{fosc}} \times 1000
$$

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where:

fosc $=$ External Clock Frequency

The differential input voltage must be within the device common-mode range when the converter and measured system share the same power supply common (ground). If the converter and measured system do not share the same power supply common, Vin should be tied to analog common.
Polarity is determined at the end of signal integrate signal phase. The sign bit is a true polarity indication in that signals less than 1 LSB are correctly determined. This allows precision null detection limited only by device noise and auto-zero residual offsets.

## Reference Integrate Cycle:

The final phase is reference integrate or deintegrate. VīN is internally connected to analog common and $\mathrm{V}_{\mathrm{N}}^{+} \mathrm{is}$ connected across the previously charged reference capacitor. Circuitry within the chip ensures that the capacitor will be connected with the correct polarity to cause the integrator output to return to zero. The time required for the output to return to zero is proportional to the input signal and is between 0 and 2000 internal clock periods. The digital reading displayed is

$$
1000 \frac{V_{I N}}{V_{\text {REF }}}
$$

## Digital Section

The TSC7126A contains all the segment drivers necessary to directly drive a 3-1/2 digit liquid crystal display (LCD). An LCD backplane driver is included. The backplane frequency is the external clock frequency divided by 800 . For three conversions/second the backplane frequency is 60 Hz with a 5 V nominal amplitude. When a segment driver is in phase with the backplane signal the segment is "OFF." An out of phase segment drive signal causes the segment to be "ON" or visible. This AC drive configuration results in negligible DC voltage across each LCD segment. This insures long L.CD display life. The polarity segment driver is "ON" for negative analog inputs. If $V_{I N}{ }^{+}$and $V_{I N}$ are reversed this indicator would reverse.
On the TSC7126A when the test pin is pulled to $\mathrm{V}^{+}$all segments are turned "ON." The display reads -1888 . During this mode the LCD segments have a constant DC voltage impressed. Do not leave the display in this mode for more than several minutes. LCD displays may be destroyed if operated with DC levels for extended periods.
The display FONT and segment drive assignment are shown in Figure 5.


Figure 5: Display FONT and Segment Assignment.

## System Timing

The oscillator frequency is divided by 4 prior to clocking the internal decade counters. The three phase measurement cycle takes a total of 4000 counts or 16000 clock pulses. The 4000 count cycle is independent of input signal magnitude.
Each phase of the measurement cycle has the following length:

- Auto-Zero Phase: 1000 to 3000 Counts
(4000 to 12000 Clock Pulses)
For signals less than full-scale the auto-zero phase is assigned the unused reference integrate time period.
- Signal Integrate: 1000 Counts
(4000 Clock Pulses)
This time period is fixed. The integration period is:

$$
T_{S I}=4000 \quad\left[\frac{1}{f \circ s c}\right]
$$

Where fosc is the externally set clock frequency.

- Reference Integrate: 0 to 2000 Counts
( 0 to 8000 Clock Pulses)
The TSC7126A is a drop in replacement for the TSC7126 and ICL7126 that offers a greatly improved internal reference temperature coefficient. No external component value changes are required to upgrade existing designs.


## Component Value Selection

## Auto-Zero Capacitor - CAZ

The CAZ capacitor size has some influence on system noise. A $0.33 \mu \mathrm{~F}$ capacitor is recommended for 200 mV full-scale applications where 1 LSB is $100 \mu \mathrm{~V}$. A $0.033 \mu \mathrm{~F}$ capacitor is adequate for 2.0 V full-scale applications. A mylar type dielectric capacitor is adequate.

## Reference Voitage Capacitor - Cref

The reference voltage used to ramp the integrator output voltage back to zero during the reference integrate cycle is stored on CREF. A $0.1 \mu \mathrm{~F}$ capacitor is acceptable when Vin is tied to analog common. If a large common-mode voltage exists ( $V_{\bar{R} E F} \neq$ analog common) and the application requires a 200 mV full-scale increase CREF to $1.0 \mu \mathrm{~F}$. Rollover error will be held to less than 0.5 count. A mylar type dielectric capacitor is adequate.

## Integrating Capacitor - CINT

CINT should be selected to maximize integrator output voltage swing without causing output saturation. Due to the TSC7126A superior analog common temperature coefficient specification, analog common will normally supply the differential voltage reference. For this case a $\pm 2 \mathrm{~V}$ full-scale integrator output swing is satisfactory. For 3 readings $/ \mathrm{sec}-$ ond ( $\mathrm{fOSC}=48 \mathrm{kHz}$ ) a 0.047 value is suggested. For one reading per second $0.15 \mu \mathrm{~F}$ is recommended.If a different oscillator frequency is used CINT must be changed in inverse proportion to maintain the nominal $\pm 2 \mathrm{~V}$ integrator swing.
An exact expression for CINT is:

3 1/2 Digit A/D Converter<br>- Low Power Dissipation - $900 \mu$ W Max.<br>- $35 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ Internal Reference



Where:
fosc $=$ Clock frequency at Pin 38
$\mathrm{V}_{\mathrm{FS}}=$ Full-scale input voltage
RINT $=$ Integrating resistor
VINT $=$ Desired full-scale integrator output swing
At three readings per seccond, a $750 \Omega$ resistor should be placed in series with CINT. This increases accuracy by compensating for comparator delay. CINT must have low dielectric absorption to minimize roll-over error. An inexpensive polypropylene capacitor is recommended.

## Integrating Resistor - RINT

The input buffer amplifier and integrator are designed with class A output stages. The output stage idling current is $6 \mu \mathrm{~A}$. The integrator and buffer can supply $1 \mu \mathrm{~A}$ drive currents with negligible linearity errors. Rint is chosen to remain in the output stage linear drive region but not so large that printed circuit board leakage currents induce errors. For a 200 mV full-scale RINt is $180 \mathrm{k} \Omega$. A 2.0 V full-scale requires $1.8 \mathrm{~m} \Omega$.

| Component | Nominal Full-Scale Voltage |  |
| :--- | ---: | ---: |
| Value | 200.0 mV | 2.000 V |
| $\mathrm{C}_{\mathrm{AZ}}$ | $0.33 \mu \mathrm{~F}$ | $0.033 \mu \mathrm{~F}$ |
| $\mathrm{R}_{\text {INT }}$ | $180 \mathrm{k} \Omega$ | $1.8 \mathrm{M} \Omega$ |
| $\mathrm{C}_{\text {INT }}$ | $0.047 \mu \mathrm{~F}$ | $0.047 \mu \mathrm{~F}$ |

Note:

1. $\mathrm{fosc}=48 \mathrm{kHz}$ ( 3 readings $/ \mathrm{sec}$ )

## Oscillator Components

Cosc should be 50 pF . Rosc is selected from the equation:

$$
\text { fosc }=\frac{0.45}{R C}
$$

For a 48 kHz clock ( 3 conversions $/ \mathrm{sec}$ ) $\mathrm{R}=180 \mathrm{k} \Omega$.

Note that fosc is divided by four to generate the TSC7126A internal control clock. The backplane drive signal is derived by dividing fosc by 800 .
To achieve maximum rejection of 60 Hz noise pickup, the signal integrate period should be a multiple of 60 Hz . Oscillator frequencies of $240 \mathrm{kHz}, 120 \mathrm{kHz}, 80 \mathrm{kHz}, 60 \mathrm{kHz}, 40 \mathrm{kHz}$, $331 / 3 \mathrm{kHz}$, etc. should be selected. For 50 Hz rejection, oscillator frequencies of $200 \mathrm{kHz}, 100 \mathrm{kHz}, 662 / 3 \mathrm{kHz}$, $50 \mathrm{kHz}, 40 \mathrm{kHz}$, etc. would be suitable. Note that $40 \mathrm{kHz}(2.5$ readings/second) will reject both 50 and 60 Hz (also 400 and 440 Hz ).

## Reference Voltage Selection

A full-scale reading ( 2000 counts) requires the input signal be twice the reference voltage.

| Required Full-Scale Voltage ${ }^{*}$ | VREF |
| :--- | :---: |
| 200.0 mV | 100.0 mV |
| 2.000 V | 1.000 V |

* $\mathrm{V}_{\mathrm{fs}}=2 \mathrm{~V}_{\mathrm{Ref}}$

In some applications a scale factor other than unity may exist between a transducer output voltage and the required digital reading. Assume, for example, a pressure transducer output is 400 mV for $2000 \mathrm{lb} / \mathrm{in}^{2}$. Rather than dividing the input voltage by two the reference voltage should be set to 200 mV . This permits the transducer input to be used directly.
The differential reference can also be used when a digital zero reading is required when $V_{I N}$ is not equal to zero. This is common in temperature measuring instrumentation. A compensating offset voltage can be applied between analog common and Vin. The transducer output is connected between $\mathrm{V}_{\mathrm{iN}}^{\dagger}$ and analog common.

## Device Pin Functional Description Differential Signal Inputs

(ViN (Pin 31), $\mathrm{V}_{\text {in }}^{-}($Pin 30$)$ )
The TSC7126A is designed with true differential inputs and accepts input signals within the input stage common-mode


Figure 6: Common-Mode Voltage Removed in Battery Operation with ViN = Analog Common
voltage range ( V См) . The typical range is $\mathrm{V}^{+}-1.0$ to $\mathrm{V}^{-}+1 \mathrm{~V}$. Common-mode voltages are removed from the system when the TSC7126A operates from a battery or floating power source (Isolated from measured system) and Vī is connected to analog common (VCOM): See Figure 6.
In systems where common-mode voltages exist the TSC7126A 86 dB common-mode rejection ratio minimizes error. Common-mode voltages do, however, affect the integrator output level. Integrator output saturation must be prevented. A worse case condition exists if a large positive VCM exists in conjunction with a full-scale negative differential signal. The negative signal drives the integrator output positive along with Vcm (Figure 7). For such applications the integrator output swing can be reduced below the recommended 2.0 V full-scale swing. The integrator output will swing within 0.3 V of $\mathrm{V}^{+}$or $\mathrm{V}^{-}$without increased linearity error.


Figure 7: Common-Mode Voltage Reduces Available Integrator Swing. (VCOM $\left.\neq \mathrm{V}_{\mathrm{IN}}\right)$

## Differential Reference

( $\mathrm{V}_{\text {REF }}^{+}$( $\operatorname{Pin} 36$ ), $\mathrm{V}_{\text {REF }}^{-}(\operatorname{Pin} 39)$ )
The reference voltage can be generated anywhere within the $\mathrm{V}^{+}$to $\mathrm{V}^{-}$power supply range.
To prevent rollover type errors being induced by large common-mode voltages CREF should be large compared to stray node capacitance.
The TSC7126A offers a significantly improved analog common temperature coefficient. This potential provides a very stable voltage suitable for use as a voltage reference. The temperature coefficient of analog common is $20 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ typically.

## Analog Common (Pin 32)

The analog common pin is set at a voltage potential approximately 3.0 V below $\mathrm{V}^{+}$. The potential is guaranteed to be between 2.7 V and 3.35 V below $\mathrm{V}^{+}$. Analog common is tied internally to an N channel $\operatorname{FET}$ capable of sinking 30 mA . This FET will hold the common line at 3.0 V should an external load attempt to pull the common line toward $\mathrm{V}^{+}$. Analog common source current is limited to $10 \mu \mathrm{~A}$. Analog common is therefore easily pulled to a more negative voltage (i.e., below $\mathrm{V}^{+}-3.0 \mathrm{~V}$ ).

The TSC7126A connects the internal $\mathrm{V}_{\text {IN }}^{+}$and $\mathrm{V}_{\mathrm{IN}}^{+}$inputs to analog common during the auto-zero cycle. During the reference integrate phase $\mathrm{ViN}_{\text {in }}$ is connected to analog common. If $\mathrm{V}_{\mathrm{IN}}^{-}$is not externally connected to analog common, a common-mode voltage exists. This is rejected by the converters 86 dB common-mode rejection ratio. In battery operation analog common and VIN are usually connected removing common-mode voltage concerns. In systems where Vin is connected to the power supply ground or to a given voltage, analog common should be connected to $\mathrm{ViN}^{-}$.
The analog common pin serves to set the analog section reference or common point. The TSC7126A is specifically designed to operate from a battery or in any measurement system where input signals are not referenced (float) with respect to the TSC7126A power source. The analog common potential of $\mathrm{V}^{+}-3.0 \mathrm{~V}$ gives a 7 V end of battery life voltage. The common potential has a $0.001 \% / \%$ voltage coefficient and a $15 \Omega$ output impedance.
With sufficiently high total supply voltage ( $\mathrm{V}^{+}-\mathrm{V}^{-}>7.0 \mathrm{~V}$ ) analog common is a very stable potential with excellent temperature stability - typically $35 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$. This potential can be used to generate the TSC7126A reference voltage. An external voltage reference will be unnecessary in most cases because of the $35 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ temperature coefficient. See TSC7126A Internal Voltage Reference discussion.

## Test (Pin 37)

The test pin potential is. 5 V less than $\mathrm{V}^{+}$. Test may be used as the negative power supply connection for external CMOS logic. The test pin is tied to the internally generated negative logic supply through a $500 \Omega$ resistor. The test pin load should be no more than 1 mA . See the applications section for additional information on using test as a negative digital logic supply.
If test is pulled high to $\mathrm{V}^{+}$all segments plus the minus sign will be activated. Do not operate in this mode for more than several minutes. With Test $=\mathrm{V}^{+}$the LCD Segments are impressed with a DC voltage which will destroy the LCD.


Figure 8: Analog Common Temperature Coefficient

## TSC7126A Internal Voltage Reference

The TSC7126A analog common voltage temperature stability has been significantly improved (Figure 8). The "A" version of the industry standard 7126 device will allow users to upgrade old systems and design new systems without external voltage references. External R and C values do not need to be changed. Figure 9 shows analog common supplying the necessary voltage reference for the TSC7126A.

## Applications Information Liquid Crystal Display Sources

Several LCD manufacturers supply standard LCD displays to interface with the TSC7126A 3 1/2 digit analog-to-digital converter.

| Manufacturer | Address/Phone | Representative Part Numbers ${ }^{1}$ |
| :---: | :---: | :---: |
| Crystaloid Electronics | 5282 Hudson Dr., Hudson, OH 44236 216/655-2429 | $\begin{aligned} & \text { C5335, H5535, } \\ & \text { T5135, SX440 } \end{aligned}$ |
| AND | 770 Airport Blvd., <br> Burlingame, CA 94010 415/347-9916 | $\begin{aligned} & \text { FE } 0801 \\ & \text { FE } 0203 \end{aligned}$ |
| EPSON | 3415 Kashikawa St., Torrance, CA 90505 213/534-0360 | $\begin{aligned} & \text { LD-B709BZ } \\ & \text { LD-H7992AZ } \end{aligned}$ |
| Hamlin, Inc. | 612 E. Lake St., Lake Mills, WI 53551 414/648-2361 | 3902, 3933, 3903 |

## Note:

1. Contact LCD manufacturer for full product listing/specifications.

## Decimal Point and Annunciator Drive

The test pin is connected to the internally-generated digital logic supply ground through a $500 \Omega$ resistor. The test pin may be used as the negative supply for external CMOS gate segment drivers. LCD display annunciators for decimal points, low battery indication, or function indication may be added without adding an additional supply. No more than 1 mA should be supplied by the test pin. The test pin potential is approximately 5 V below $\mathrm{V}^{+}$.

## Flat Package

The TSC7126A is available in an epoxy 60-pin flat package. The "BQ" device leads are bent while the "SQ" device leads are unformed (straight). A test socket for the TSC7126ACSQ device is available:


Figure 9: TSC7126A Internal Voltage Reference Connection


| Part No.: | IC 51-42 |
| :--- | :--- |
| Manufacturer: | Yamaichi |
| Distribution: | Nepenthe Distribution |
|  | 2471 East Bayshore |
|  | Suite 520 |
|  | Palo Alto, CA 94043 |
|  | (415) 856-9332 |

## 3 1/2 Digit A/D Converter

- Low Power Dissipation - $900 \mu \mathbf{W}$ Max.
- $35 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ Internal Reference


## Ratiometric Resistance Measurements

The TSC7126A true differential input and differential reference make ratiometric readings possible. In ratiometric operation, an unknown resistance is measured with respect to a known standard resistance. No accurately defined reference voltage is needed.
The unknown resistance is put in series with a known standard and a current passed through the pair. The voltage developed across the unknown is applied to the input and the voltage across the known resisior applied to the reference input. If the unknown equals the standard, the display will read 1000. The displayed reading can be determined from the following expression:

$$
\text { Displayed Reading }=\frac{\text { RUnknown }}{\text { R Standard }} \times 1000
$$

The display will overrange for R Unknown $\geq 2 \times R$ Standard.


Figure 10: Low Parts Count Ratiometric Resistance Measurement


Figure 11: Temperature Sensor


Figure 12: Positive Temperature Coefficient Resistor Temperature Sensor


Figure 13: Integrated Circult Temperature Sensor

## Package Information



## General Description

The single chip CMOS TSC7126 incorporates all the active devices for a $31 / 2$ digit analog-to-digital converter to directly drive an LCD display. The internal oscillator, voltage reference and display segment/backplane drivers simplify system integration, reduce board space requirements and lower total cost. A low cost, high resolution - $0.05 \%$ - indicating meter requires only a display, four resistors, four capacitors and a 9 V battery. The flat package option eases the mechanical design of low cost, hand held multimeters and systems.

The TSC7126 dual slope conversion technique rejects interference signals when the integration time is set to a multiple of the interference signal period. This is especially useful in industrial measurement environments where 50,60 and 400 Hz line frequency signals are present.

With an auto-zero error less than $10 \mu \mathrm{~V}$, zero drift less than $1 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$, input bias current of 10 pA max and rollover error of less than one count, the TSC7126 brings exceptional value to the portable battery powered field.

In addition, the differential input and reference allows the measurement on load cells, strain gauges and other bridge type transducers. The low power TSC7126 can be used as a plug-in replacement for the TSC7106 by changing only the values of seven passive components.

For applications needing a low drift internal voltage reference refer to the TSC7126A data sheet.


Figure 1: TSC7126 Clock Frequency 16 kHz (1 reading/sec.)

## Features

- Long Battery Life

8000 Hours Typical

- Auto-Zero Cycle
- Guaranteed Zero Reading With Zero Input
- Low Noise $15 \mu \mathrm{~V}_{\mathrm{p}-\mathrm{p}}$
- High Resolution (0.05\%) and Wide Dynamic Range ( 72 dB )
- Low Input Leakage Current ............... 1 pA Typical 10 pA Maximum
- Direct LCD Display Drive - No External Components.
- Precision Null Detection With True Polarity at Zero
- High Impedance Differential Input
- Convenient 9 V Battery Operation With Low Power Dissipation $500 \mu \mathrm{~W}$ Typical $900 \mu \mathrm{~W}$ Maximum
- Internal Clock Circuit
- Drop-In Replacement for ICL7126
- Available in Compact Flat Package
- Industrial Temperature Range Device


## Typical Applications

- Thermometry
- Bridge Readouts (Strain Gauges, Load Cells, Null Detectors)
- Digital Meters
- Voltage/Current/Ohms/Power
$-\mathrm{pH}$
- Capacitance/Inductance
- Fluid Flow Rate/Viscosity/Level
- Digital Scales
- LVDT Indicators
- Portable Instrumentation
- Power Supply Readouts
- Process Monitors
- Photometers


Figure 2: TSC7126 Clock Frequency 48 kHz (3 readings/sec.)

## Absolute Maximum Ratings*



## Electrical Characteristics ${ }^{3}$

Plastic Package .................................. 800 mW
Operating Temperature
(C Device) ................................. $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$
(I Device) . .............................. . . $-25^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$
Storage Temperature .................... $-65^{\circ} \mathrm{C}$ to $+160^{\circ} \mathrm{C}$
Lead Temperature (Soldering, 60 sec ) .............. $300^{\circ} \mathrm{C}$

| CHARACTERISTICS | CONDITIONS | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Zero Input Reading | $\begin{aligned} & V_{\text {IN }}=0.0 \mathrm{~V} \\ & \text { Full Scale }=200.0 \mathrm{mV} \end{aligned}$ | -000.0 | $\pm 000.0$ | +000.0 | Digital Reading |
| Ratiometric Reading | $\begin{aligned} & V_{\text {IN }}=V_{\text {REF }} \\ & V_{\text {REF }}=100 \mathrm{mV} \end{aligned}$ | 999 | 999/1000 | 1000 | Digita! Reading |
| Rollover Error (Difference in reading for equal positive and negative reading near Full Scale) | $-V_{\text {IN }}=+V_{\text {IN }} \approx 200.0 \mathrm{mV}$ | -1 | $\pm 0.2$ | +1 | Counts |
| Linearity (Max. deviation from best straight line fit) | Full Scale $=200 \mathrm{mV}$ or Full Scale $=2.000 \mathrm{~V}$ | -1 | $\pm 0.2$ | +1 | Counts |
| Common Mode Rejection Ratio ${ }^{(4]}$ | $\begin{aligned} & V_{C M}= \pm 1 \mathrm{~V}, V_{I N}=0 \mathrm{~V} \\ & \text { Full scale }=200.0 \mathrm{mV} \end{aligned}$ | -- | 50 | - | $\mu \mathrm{V} / \mathrm{V}$ |
| Noise (Pk - Pk value not exceeded 95\% of time) | $\begin{aligned} & V_{\text {IN }}=0 \mathrm{~V} \\ & \text { Full Scale }=200.0 \mathrm{mV} \end{aligned}$ | - | 15 | - | $\mu \mathrm{V}$ |
| Leakage Current @ Input | $\mathrm{V}_{1 \mathrm{~N}}=0 \mathrm{~V}$ | - | 1 | 10 | pA |
| Zero Reading Drift | $\begin{aligned} & V_{I N}=0 \\ & 0^{\circ}<T_{A}<70^{\circ} \mathrm{C} \end{aligned}$ | - | 0.2 | 1 | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
| Scale Factor Temperature Coefficient | $\begin{aligned} & V_{I N}=199.0 \mathrm{mV} \\ & 0<\mathrm{T}_{\mathrm{A}}<70^{\circ} \mathrm{C} \\ & \text { (Ext. Ref. } 0 \mathrm{ppm} /{ }^{\circ} \mathrm{C} \text { ) } \end{aligned}$ | - | 1 | 5 | ppm $/{ }^{\circ} \mathrm{C}$ |
| Supply Current (Does not include Common current) | $\begin{aligned} & \mathrm{V}_{\text {IN }}=0 \\ & \text { Note } 6 \end{aligned}$ | - | 50 | 100 | $\mu \mathrm{A}$ |
| Analog Common Vcltage (with respect to positive supply) | 250K』 between Common and positive supply | 2.4 | 2.8 | 3.2 | v |
| Temp. Coeff. of Analog Common (with respect to positive supply) | 250Ks between Common and positive supply | - | 80 | - | $\mathrm{ppm} /{ }^{\circ} \mathrm{C}$ |
| Pk-Pk Segment Drive Voltage (Note 5) | $\mathrm{V}^{+}$to $\mathrm{V}^{--}=9 \mathrm{~V}$ | 4 | 5 | 6 | V |
| Pk-Pk Backplane Drive Voltage (Note 5) | $\mathrm{V}^{+}$to $\mathrm{V}^{-}=9 \mathrm{~V}$ | 4 | 5 | 6 | v |
| Power Dissipation Capacitance | vs. Clock Frequency | - | 40 | - | pF |

## Notes:

1. Input voltages may exceed the supply voltages provided the input current is limited to $\pm 100 \mu \mathrm{~A}$.
2. Dissipation rating assumes device is mounted with all leads soldered to printed circuit board.
3. Unless otherwise noted, specifications apply at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$. fCLOCK $=16 \mathrm{kHz}$ and are tested in the circuit of Figure 1.
4. Refer to "Differential Input" discussion on page 4.
5. Backplane drive is in phase witt: segment drive for 'off' segment, $180^{\circ}$ out of phase for 'on' segment. Frequency is 20 times conversion rate. Average DC component is less than 50 mV .
6. During auto-zero phase, current is $10-20 \mu \mathrm{~A}$ higher. 48 kHz oscillator, Figure 2, increases current by $8 \mu$ a (typ.).

* Stresses above those listed under Absolute Maximum Ratings may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions above those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may effect device reliability.


## Ordering Information

| Part No. | Package | Pin <br> Layout | Temp. Range | Part No. | Package | Pin Layout | Temp. Range |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TSC7126CPL | 40-Pin <br> Plastic Dip | Normal | $0^{\circ} \mathrm{C}$ to $70^{\circ} \mathrm{C}$ | TSC7126CSQ | $\begin{aligned} & \text { 60-Pin } \\ & \text { Plastic Fiat } \end{aligned}$ | Unformed Leads | $\begin{array}{r} 0^{\circ} \mathrm{C} \text { to } \\ 70^{\circ} \mathrm{C} \end{array}$ |
| TSC7126RCPL | $\begin{aligned} & \text { 40-Pin } \\ & \text { Plastic Dip } \end{aligned}$ | Reversed | $\begin{array}{r} 0^{\circ} \mathrm{C} \\ 70^{\circ} \mathrm{C} \end{array}$ | Devices with 160 Hour, $+125^{\circ} \mathrm{C}$ Burn-in |  |  |  |
|  |  |  |  | TSC7126CPL/BI | 40-Pin |  | $0^{\circ} \mathrm{C}$ to |
| TSC7126IJL | $\begin{aligned} & \text { 40-Pin } \\ & \text { CerDIP } \end{aligned}$ | Normal | $\begin{array}{r} -25^{\circ} \mathrm{C} \text { to } \\ +85^{\circ} \mathrm{C} \\ \hline \end{array}$ |  | Plastic Dip | Normal | $70^{\circ} \mathrm{C}$ |
| TSC7126CBQ | 60-Pin <br> Plastic Flat | Formed Leads | $0^{\circ} \mathrm{C}$ to $70^{\circ} \mathrm{C}$ | TSC7126IJL/BI | 40-Pin <br> CerDIP | Normal | $\begin{array}{r} -25^{\circ} \mathrm{C} \text { to } \\ +85^{\circ} \mathrm{C} \end{array}$ |

## Pin Configuration



## Pin Description

| 40-Pin DIP <br> Pin Number <br> Normal | (Reverse) | 60-Pin <br> Flat Package <br> Pin Number | Name | Description |
| :---: | :---: | :---: | :---: | :--- |
| 1 | $(40)$ | 13 | $\mathrm{~V}^{+}$ | Positive supply voltage. |
| 2 | $(39)$ | 14 | $\mathrm{D}_{1}$ | Activates the D section of the units display. |
| 3 | $(38)$ | 15 | $\mathrm{C}_{1}$ | Activates the C section of the units display. |
| 4 | $(37)$ | 16 | $\mathrm{~B}_{1}$ | Activates the B section of the units display. |
| 5 | $(36)$ | 17 | $\mathrm{~A}_{1}$ | Activates the A section of the units display. |
| 6 | $(35)$ | 18 | $\mathrm{~F}_{1}$ | Activates the F section of the units display. |
| 7 | $(34)$ | 19 | $\mathrm{G}_{1}$ | Activates the G section of the units display. |
| 8 | $(33)$ | 20 | $\mathrm{E}_{1}$ | Activates the E section of the units display. |

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## Pin Description (Cont.)

| 40-Pin DIP Pin Number Normal | (Reverse) | 60-Pin Flat Package Pin Number | Name | Description |
| :---: | :---: | :---: | :---: | :---: |
| 9 | (32) | 21 | $\mathrm{D}_{2}$ | Activates the D section of the tens display. |
| 10 | (31) | 25 | $\mathrm{C}_{2}$ | Activates the C section of the tens display. |
| 11 | (30) | 26 | $\mathrm{B}_{2}$ | Activates the $B$ section of the tens display. |
| 12 | (29) | 27 | $\mathrm{A}_{2}$ | Activates the $A$ section of the tens display. |
| 13 | (28) | 28 | $\mathrm{F}_{2}$ | Activates the F section of the tens display. |
| 14 | (27) | 29 | $\mathrm{E}_{2}$ | Activates the E section of the tens display. |
| 15 | (26) | 30 | D3 | Activates the D section of the hundreds display. |
| 16 | (25) | 31 | B3 | Activates the B section of the hundreds display. |
| 17 | (24) | 32 | F3 | Activates the F section of the hundreds display. |
| 18 | (23) | 33 | $E_{3}$ | Activates the E section of the hundreds display. |
| 19 | (22) | 34 | $\mathrm{AB}_{4}$ | Activates both halves of the 1 in the thousands display. |
| 20 | (21) | 35 | POL | Activates the negative polarity display. |
| 21 | (20) | 36 | BP | Backplane drive output. |
| 22 | (19) | 37 | G3 | Activates the G section of the hundreds display. |
| 23 | (18) | 40 | $\mathrm{A}_{3}$ | Activates the A section of the hundreds display. |
| 24 | (17) | 41 | $\mathrm{C}_{3}$ | Activates the C section of the hundreds display. |
| 25 | (16) | 43 | $\mathrm{G}_{2}$ | Activates the G section of the tens display. |
| 26 | (15) | 45 | $\mathrm{V}^{-}$ | Negative power supply voltage. |
| 27 | (14) | 46 | VINT | The integrating capacitor should be selected to give the maximum voltage swing that ensures component tolerance build up will not allow the integrator output to saturate. When analog common is used as a reference and the conversion rate is 3 readings per second, a $0.047 \mu \mathrm{~F}$ capacitor may be used. The capacitor must have a low dielectric constant to prevent roll-over errors. See INTEGRATING CAPACITOR section for additional details. |
| 28 | (13) | 47 | Vbuff | Integration resistor connection. Use a $180 \mathrm{k} \Omega$ for a 200 mV full-scale range and a 1.80 $\mathrm{M} \Omega$ for 2 V full-scale range. |
| 29 | (12) | 49 | Caz | The size of the auto-zero capacitor influences the system noise. Use a $0.33 \mu \mathrm{~F}$ capacitor for a 200 mV full-scale, and a $0.033 \mu \mathrm{~F}$ capacitor for a 2 volt full-scale. See paragraph on AUTO-ZERO CAPACITOR for more details. |
| 30 | (11) | 51 | VIN | The low input is connected to this pin. |
| 31 | (10) | 55 | $\mathrm{V}_{\text {IN }}^{+}$ | The high input signal is connected to this pin. |
| 32 | (9) | 57 | Analog Common | This pin is primarily used to set the analog common-mode voltage for battery operation or in systems where the input signal is referenced to the power supply. See paragraph on ANALOG COMMON for more details. It also acts as a reference voltage source. |
| 33 | (8) | 58 | $\mathrm{C}_{\text {ReF }}^{\text {- }}$ | See pin 34. |
| 34 | (7) | 59 | $\mathrm{C}_{\text {REF }}^{+}$ | A $0.1 \mu \mathrm{~F}$ capacitor is used in most applications. If a large common mode voltage exists (for example the VIN pin is not at analog common), and a 200 mV scale is used, a $1.0 \mu \mathrm{~F}$ is recommended and will hold the rollover error to 0.5 count. |
| 35 | (6) | 60 | $\mathrm{V}_{\text {REF }}$ | See pin 36. |
| 36 | (5) | 1 | $\mathrm{V}_{\text {REF }}^{+}$ | The analog input required to generate a full-scale output ( 1,999 counts). Place 100 mV between pins 35 and 36 for 199.9 mV full-scale. Place 1.00 volts between pins 35 and 36 for 2 volts fuli-scale. See paragraph on REFERENCE VOLTAGE. |
| 37 | (4) | 3 | Test | Lamp test. When pulled high (to $\mathrm{V}^{+}$) all segments will be turned on and the display should read -1888. It may also be used as a negative supply for externally generated decimal points. See paragraph under TEST for additional information. |
| 38 | (3) | 4 | $\mathrm{OSC}_{3}$ | See pin 40. |
| 39 | (2) | 6 | $\mathrm{OSC}_{2}$ | See pin 40. |
| 40 | (1) | 10 | $\mathrm{OSC}_{1}$ | Pins 40, 39, 38 make up the oscillator section. For a 48 kHz clock ( 3 readings per section) connect pin 40 to the junction of a $180 \mathrm{k} \Omega$ resistor and a 50 pF capacitor. The $180 \mathrm{k} \Omega$ resistor is tied to pin 39 and the 50 pF capacitor is tied to pin 38. |

## Detailed Description

## ANALOG SECTION

Figure 3 shows the Block Diagram of the Analog Section for the 7126. Each measurement cycle is divided into three phases. They are (1) auto-zero (A-Z), (2) signal integrate (INT) and ( 3 ) de-integrate, (DE).

## 1. Auto-zero phase

Input high and low are disconnected from the pins and internally shorted to analog COMMON. The reference capacitor is charged to the reference voltage. A feedback loop is closed around the system to charge the auto-zero capacitor $C_{A Z}$ to compensate for offset voltages in the buffer amplifier, integrator, and comparator. Since the comparator is included in the loop, the A-Z accuracy is limited only by the noise of the system. The offset referred to the input is less than $10 \mu \mathrm{~V}$.

## 2. Signal Integrate phase

The auto-zero loop is opened, the internal short is removed, and the internal input high and low are connected to the external pins. The converter then integrates the differential voltage between IN Hr and IN LO for a fixed time. This differential voltage can be within a wide common mode range; within one volt of either supply. If, on the other hand, the input signal has no return with respect to the converter power supply, IN LO can be tied to analog COMMON to establish the correct common-mode voltage. At the end of this phase, the polarity of the integrated signal is determined.

## 3. De-integrate Phase

The final phase is reference integrate or de-integrate. Input low is internally connected to analog common and input high is connected across the previously charged
reference capacitor. Circuitry within the chip ensures that the capacitor will be connected with the correct polarity to cause the integrator output to return to zero. The time required for the output to return to zero is proportional to the input signal. The digital reading displayed is $1000 \times \frac{V_{\text {IN }}}{V_{\text {REF }}}$

## Differential Reference

The reference voltage can be generated anywhere within the power supply voltage of the converter. The main source of common mode error is a roll-over voltage caused by the reference capacitor losing or gaining charge to stray capacity on its nodes. If there is a large common mode voltage, the reference capacitor can gain charge (increase voltage) when called up to de-integrate a positive signal but lose charge (decrease voltage) when called up to deintegrate a negative input signal. This difference in reference for $(+)$ or $(-)$ input voltage will give a roll-over error. However, by selecting the reference capacitor large enough in comparison to the stray capacitance, this error can be held to less than 0.5 count for the worst case condition. See Component Values Selection.

## Differential Input

The input can accept differential voltages anywhere within the common mode range of the input amplifier; or specifically from 1.0 volts below the positive supply to 1.0 volt above the negative supply. In this range the system has a CMRR of 86 dB typical. However, since the integrator also swings with the common mode voltage, care must be exercised to assure the integrator output does not saturate. A worst case condition would be a large positive commonmode voltage with a near full-scale negative differential input voltage. The negative input signal drives the integrator


Figure 3: Analog Section of TSC7126.

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positive when most of its swing has been used up by the positive common mode voltage. For these critical applications the integrator swing can be reduced to less than the recommended 2 V full scale swing with little loss of accuracy. The integrator output can swing within 0.3 volts of either supply without loss of linearity.

## Analog Common

This pin is included primarily to set the common mode voltage for battery operation or for any system where the input signals are floating with respect to the power supply. The common pin sets a voltage that is approximately 2.8 volts more negative than the positive supply. This is selected to give a minimum end-of-life battery voltage of about 6 V . However, the analog common has some of the attributes of a reference voltage. When the total supply voltage is large enough to cause the zener to regulate ( $>7 \mathrm{~V}$ ), the common voltage will have a low voltage coefficient $(0.001 \% / \%)$, low output impedance $(\sim 15 \Omega)$, and a temperature coefficient typically less than $80 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$.
An external reference may be added to improve temperature stability. The circuit is shown in Figure 4.


Figure 4: Using an External Reference
Analog common is also used as the IN LO return during auto-zero and de-integrate. If IN LO is different from analog COMMON, a common mode voltage exists in the system and is taken care of by the excellent CMRR of the converter. However, in some applications IN LO will be set at a fixed known voltage (power supply common for instance). In this application, analog COMMON should be tied to the same point, thus removing the common mode voltage from the converter. The same holds true for the reference voltage. If reference can be conveniently referenced to analog COMMON, it should be since this removes the common mode voltage from the reference system.

Within the IC analog COMMON is tied to an N -channel FET that can sink $100 \mu \mathrm{~A}$ or more of current to hold the voltage 2.8 volts below the positive supply (when a load is trying to pull the common line positive). However, there is only $1 \mu \mathrm{~A}$ of source current, so COMMON may easily be tied to a more negative voltage thus over-riding the internal reference.

## Test

The TEST pin serves two functions. It is coupled to the internally generated digital supply through a $500 \Omega$ resistor. Thus it can be used as the negative supply for externally generated segment drivers such as decimal points or any other presentation the user may want to include on the LCD display. No more than a 1 mA load should be applied. Figures 5 and 6 show such an application.

The second function is a "lamp test". When TEST is pulled high (to $\mathrm{V}^{+}$) all segments will be turned on and the display should read - 1888. The TEST pin will sink about 10 mA under these conditions

Caution: In the lamp test mode, the segments have a constant $d-c$ voltage (no square-wave) and may burn the LCD display if left in this mode for several minutes.


Figure 5: Simple Inverter for Fixed Decimal Poir:


Figure 6: Exclusive 'OR' Gate for Decimal Point Drive

## DIGITAL SECTION

Figure 8 shows the digital section for the 7126. An internal digital ground is generated from a 6 volt Zener diode and a large $P$ channel source follower. This supply is made stiff to absorb the relative large capacitive currents when the backplane (BP) voltage is switched. The BP frequency is the clock frequency divided by 800 . For three readings/second this is a 60 Hz square wave with a nominal amplitude of 5 volts. The segments are driven at the same frequency and amplitude and are in phase with

BP when OFF, but out of phase when ON. In all cases, negligible d-c voltage exists across the segments. The polarity indication is "ON" for negative analog inputs. If IN LO and IN HI are reversed, this indication can be reversed also, if desired.

## System Timing

Three clocking methods may be used: (Figure 7)

1. An external oscillator connected to pin 40.
2. A crystal between pins 39 and 40.
3. An R-C oscillator using all three pins.

The oscillator frequency is divided by four before it clocks the decade counters. It is then further divided to form the three convert-cycle phases. These are signal integrate ( 1000 counts), reference de-integrate ( 0 to 2000 counts) and autozero (1000 to 3000 counts). For signals less than full scale, auto-zero gets the unused portion of reference integrate. This makes a complete measure cycle of 4,000 (16,000 clock pulses) independent of input voltage. For three readings/ second, an oscillator frequency of 48 kHz would be used.

To achieve maximum rejection of 60 Hz pickup, the signal integrate cycle should be a multiple of 60 Hz . Oscillator frequencies of $60 \mathrm{kHz}, 48 \mathrm{kHz}, 40 \mathrm{kHz}, 33-1 / 3$ kHz , etc. should be selected. For 50 Hz rejection, Oscillator frequencies of $66-2 / 3 \mathrm{kHz}, 50 \mathrm{kHz}, 40 \mathrm{kHz}$, etc. would be suitable. Note that 40 kHz ( 2.5 readings/second) will reject both 50 and 60 Hz (also 400 and 440 Hz ).


Figure 7: Clock Circuits


Figure 8: Digital Section

## Component Value Selection

## 1. Auto-zero Capacitor

The size of the auto-zero capacitor has some influence on the noise of the system. For 200 mV full scale where noise is very important, a $0.33 \mu \mathrm{~F}$ capacitor is recommended. On the 2 volt scale, a $0.033 \mu \mathrm{~F}$ capacitor increases the speed of recovery from overload and is adequate for noise on this scale.

## 2. Reference Capacitor

A $0.1 \mu \mathrm{~F}$ capacitor is acceptable in most applications. However, where a large common mode voltage exists (i.e. the REF LO pin is not at analog COMMON and a 200 mV scale is used, a larger value is required to prevent roll-over error. Generally $1.0 \mu \mathrm{~F}$ will hold the roll-over error to 0.5 count in this instance.

## 3. Integrating Capacitor

The integrating capacitor should be selected to give the maximum voltage swing that ensures tolerance build-up will not saturate the integrator swing (approx. 0.3 volt from either supply). When the analog COMMON is used as a reference, a nominal $\pm 2$ volt full scale integrator swing is acceptable). For three readings/second ( 48 kHz clock) nominal value for $\mathrm{C}_{\text {INT }}$ is $0.047 \mu \mathrm{~F}$, for one reading per second ( 16 kHz ) use $0.15 \mu \mathrm{~F}$.
If different oscillator frequencies are used, these values should be changed in inverse proportion to maintain the output swing.
The integrating capacitor must have low dielectric absorption to prevent roll-over errors. Polypropylene capacitors are recommended for this application.
At three readings/sec., a $750 \Omega$ resistor should be placed in series with the integrating capacitor, to compensate for comparator delay.

## 4. Integrating Resistor

Both the buffer amplifier and the integrator have a class $A$ output stage with $6 \mu \mathrm{~A}$ of quiescent current. They can supply $\sim 1 \mu A$ of drive current with negligible non-linearity. The integrating resistor should be large enough to remain in this very linear region over the input voltage range, but small enough that undue leakage requirements are not placed on the PC board. For 2 volt full scale, $1.8 \mathrm{M} \Omega$ is near optimum and similarly $180 \mathrm{~K} \Omega$ for a 200.0 mV scale.

## 5. Oscillator Components

For all ranges of frequency a 50 pF capacitor is recommended and the resistor is selected from the approximate equation $f \sim \frac{45}{R C}$. For 48 kHz clock ( 3 readings/second), $R=180 \mathrm{~K} \Omega$.

## 6. Reference Voltage

The analog input required to generate full-scale output ( 2000 counts) is: VIN $=2 \mathrm{~V}_{\text {REF }}$. Thus, for the 200.0 mV and 2.000 volt scale, VREFF should equal 100.0 mV and 1.000 volt, respectively. However, in many applications where the A/D is connected to a transducer, there will exist a scale factor other than unity between the input voltage and the digital reading. For instance, in a weighing system, the designer might like to have a full scale reading when the voltage from the transducer is 0.682 V . Instead of dividing the input down to 200.0 mV , the designer should use the input voltage directly and select $\mathrm{V}_{\text {Ref }}=0.341 \mathrm{~V}$. A suitable value for integrating resistor would be $330 \mathrm{~K} \Omega$. This makes the system slightly quieter and also avoids the necessity of a divider network on the input. Another advantage of this system occurs when a digital reading of zero is desired for $V_{I N} \neq 0$. Temperature and weighing systems with a variable tare are examples. This offset reading can be conveniently generated by connecting the voltage transducer between N HI and COMMON and the variable or fixed offset voltage between COMMON and IN LO.

## Typical Applications



Figure 9: AC to DC Converter with TSC7126. Test is Used as a Common Mode Reference Level to Ensure Compatibility with Most Op-amps.

## 3 1/2 Digit A/D Converter

 - Low Power Dissipation - $900 \mu$ W Max.
## Typical Applications (Cont.)



Figure 10: Recommended Values for 2.000 V FullScale, Three Readings Per Second.


Figure 11: TSC7126 with Zener Diode Reference.


Figure 12: TSC7126 Using the Internal Reference. 200.0 mV Full-Scale, Three Readings Per Second, Floating Supply Voltage (9 V Battery).


Figure 13: TSC7126 Operated From Single +5 V Supply. An External Reference Must Be Used.

## Typical Applications (Cont.)



Figure 14: TSC7126 Measuring Ratiometric Values of Quad Load Cell. The Resistor Values Within the Bridge are Determined by the Desired Sensitivity.


Figure 15: TSC7126 With an External Band-Gap Reference ( 1.2 V Typ) IN LO Is Tied to Common. Values Shown are for One Reading Per Second.


Figure 16: TSC7126 Used as a Digital Centigrade Thermometer. A Silicon Diode-Connected Transistor Has a Temperature Coefficient of About $2 \mathrm{mV} /{ }^{\circ} \mathrm{C}$.


Figure 17: Circuit for Developing Underrange and Overrange Signals from TSC7126 Outputs.

## Typical Applications (Cont.)



Figure 18: Recommended Component Values for 2.00 V Full-Scale, One Reading Per Second.

## Package Information



Notes

## General Description

The TSC7135 $41 / 2$ digit analog converter offers 50 ppm (1 part in 20,000 ) resolution with a maximum linearity error of 1 count. An auto-zero cycle reduces the zero error to below $10 \mu \mathrm{~V}$ and zero drift to $0.5 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$. Source impedance error sources are minimized by a 10 pA maximum input current. Rollover error is limited to $\pm 1$ count.

By combining the TSC7135 with a TSC7211A (LCD), TSC7212A (LED) or TSC700A (High LED Segment Current) driver a $41 / 2$ digit display DVM or DPM can be constructed. Overrange and underrange signals support automatic range switching and special display blanking/flashing applications.

Micro-processor based measurement systems are supported by the TSC7135 Busy, Strobe and Run/HOLD control signals. Remote data acquisition systems with data transfer via UARTs are also possible. The additional control pins and multiplexed BCD outputs make the TSC7135 the ideal converter for display or $\mu$-processor based measurement systems.

## Ordering Information

| Part No. | Package | Temperature <br> Range |
| :--- | :--- | ---: |
| TSC7135CJI | 28-Pin CerDIP | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ |
| TSC7135CPI | 28-Pin Plastic | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ |
| TSC7135CBQ | 60-Pin Plastic <br> Flat Package $\mathrm{w} /$ <br> Formed Leads | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ |
| TSC7135CSQ | 60-Pin Plastic <br> Flat Package $\mathrm{w} /$ <br> Unformed Leads | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ |

## Features

- Low Rollover Error ............... $\pm 1$ Count Maximum
- Guaranteed $\pm 1$ Count Maximum Error
- Guaranteed Zero Reading for 0 V Input
- True Polarity Indication at Zero for Null Detection
- Multiplexed BCD Data Output
- TTL Compatible Outputs
- Differential Input
- Control Signals Permit Interface to UARTS and $\mu$-Processors
- Auto-ranging Supported with Over and Underrange Signals
- Blinking Display Visually Indicates Overrange Condition
- Low Input Current
- Low Zero Reading Drift $\ldots \ldots . . . . . . . . . . . . . .{ }^{2}{ }^{2} \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$
- Interface to TSC7211A, TSC7212A, and TSC700A Display Drivers


## Pin Configuration



Typical 4 1/2 Digit DVM with LCD Display


## Absolute Maximum Ratings (Note 1)

| Positive Supply Voltage ................................ . +6 V <br> Negative Supply voltage . . . . . . . . . . . . . . . . . . . . . . . . . . -9 V <br> Analog Input Voltage (Pin 9 or 10) $\ldots . . \mathrm{V}^{+}$to $\mathrm{V}^{-}$(Note 2) <br> Reference Input Voltage (Pin 2) .................... $\mathrm{V}^{+}$to $\mathrm{V}^{-}$ |
| :---: |
|  |  |
|  |  |
|  |  |


| Operating Temperature Range .............. $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ |
| :---: |
| Soldering Lead Temperature ( 10 Seconds) ....... $300^{\circ} \mathrm{C}$ |
| CerDIP(J) Package Power Dissipation ................ 1 W |
| Plastic(P) Package Power Dissipation .............. 0.8 W |

Electrical Specifications: $T_{A}=25^{\circ} \mathrm{C}$, fclock $=120 \mathrm{kHz}, \mathrm{V}^{+}=5.0 \mathrm{~V}, \mathrm{~V}^{-}=-5 \mathrm{~V}$

| TYPE | NO. | SYMBOL | PARAMETER | TEST CONDITIONS | MIN | TSC7135 TYP | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A$\mathbf{N}$ALOG | 1 |  | Display Reading with Zero Volt Input | Note 3,4 | -0.0000 | $\pm 0.0000$ | +0.0000 | Display Reading |
|  | 2 | TCz | Zero Reading <br> Temperature Coefficient | $V_{I N}=0 V$ <br> Note 5 | - | 0.5 | 2 | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
|  | 3 | TCFs | Full Scale Temperature Coefficient | $\begin{aligned} & \mathrm{V}_{\mathrm{IN}}=2 \mathrm{~V} \\ & \text { Notes 5,6 } \end{aligned}$ | - | - | 5 | $\mathrm{ppm} /{ }^{\circ} \mathrm{C}$ |
| $\begin{aligned} & \mathbf{S} \\ & \mathbf{E} \\ & \mathbf{C} \\ & \mathbf{T} \\ & \mathbf{I} \\ & \mathbf{O} \\ & \mathbf{N} \end{aligned}$ | 4 | NL | Nonlinearity Error | Note 7 | - | 0.5 | 1 | count |
|  | 5 | DNL | Differential Linearity Error | Note 7 | - | 0.01 | - | LSB |
|  | 6 |  | Display Reading In Ratiometric Operation | $V_{I N}=V_{\text {REF }}$ <br> Note 3 | +0.9998 | +0.9999 | +1.0000 | Display Reading |
|  | 7 | $\pm$ FSE | $\pm$ Full Scale Symmetry Error (Rollover Error) | $-V_{\text {IN }}=+V_{\text {IN }}$ <br> Note 8 | - | 0.5 | 1 | count |
|  | 8 | IIN | Input Leakage Current | Note 4 | - | 1 | 10 | pA |
|  | 9 | $\mathrm{V}_{\mathrm{N}}$ | Noise | Peak-to-Peak <br> Value not exceed 95\% of time | - | 15 | - | $\mu \vee \mathrm{p}$-p |
| $\begin{aligned} & \text { D S } \\ & I E \\ & \text { G C } \\ & 1 \\ & T \\ & \text { T I } \\ & \text { A O } \\ & \text { L N } \end{aligned}$ | 10 | INL | Input Low Current | $\mathrm{V}_{\text {IN }}=0 \mathrm{~V}$ | - | 10 | 100 | $\mu \mathrm{A}$ |
|  | 11 | INH | Input High Current | $\mathrm{V}_{\text {IN }}=+5 \mathrm{~V}$ | - | 0.08 | 10 | $\mu \mathrm{A}$ |
|  | 12 | VoL | Output Low Voltage | $\mathrm{IOL}=1.6 \mathrm{~mA}$ | - | 0.20 | 0.40 | V |
|  | 13 | VOH | Output High Voltage $\left(B_{1}, B_{2}, B_{4}, B_{8}, D_{1}-D_{5}\right)$ | $1 \mathrm{OH}=1 \mathrm{~mA}$ | 2.4 | 4.4 | 5.0 | V |
|  | 14 | VOH | Output High Voltage (Busy, Polarity, Overrange, Underrange, Strobe) | $\mathrm{IOH}=10 \mu \mathrm{~A}$ | 4.9 | 4.99 | 5.0 | V |
|  | 15 | fclk | Clock Frequency | Note 11 | 0 | 100 | 1200 | kHz |
| $\begin{aligned} & P_{U}^{S} \\ & Q_{P}^{P} \\ & W_{P}^{P} \\ & E_{Y}^{L} \end{aligned}$ | 16 | $\mathrm{V}^{+}$ | Positive Supply Voltage |  | 4 | 5 | 6 | V |
|  | 17 | $\mathrm{V}^{-}$ | Negative Supply Voltage |  | -3 | -5 | -8 | V |
|  | 18 | $1^{+}$ | Positive Supply Current | $\mathrm{fCLK}=0 \mathrm{~Hz}$ | - | 1.0 | 3.0 | mA |
|  | 19 | $\mathrm{I}^{-}$ | Negative Supply Current | $\mathrm{fCLK}=0 \mathrm{~Hz}$ | - | 0.7 | 3.0 | mA |
|  | 20 | Pd | Power Dissipation | fCLK $=0 \mathrm{~Hz}$ | - | 8.5 | 30 | mW |

[^3]7. $-2 \mathrm{~V} \leq \mathrm{V}_{\mathrm{IN}} \leq+2 \mathrm{~V}$. Error of reading from best fit straight line.
8. $|\mathrm{V}| \mathbb{N} \mid=1.9959$.
9. Test Circuit shown in Figure 1.
10. Static Sensitive Device. Unused devices must be stored in conductive material to protect devices form static discharge and static fields.
11. Specification related to clock frequency range over which the TSC7135 correctly performs its various functions. Increased errors result at higher operating frequencies.

## Test Circults



Figure 1: TSC7135 Test Circuit


Figure 2: TSC7135 Digital Logic Input


Figure 3A: TSC7135 Analog Circult Function Dlagram


Figure 3B: TSC7135 System Zero Phase


Figure 3C: TSC7135 Input Signal Integration Phase


Figure 3D: Reference Voltage Integration Cycle


FIgure 3E: TSC7135 Integrator Output Zero Phase

## General Theory of Operation Dual Slope Conversion Principles

The TSC7135 is a dual slope, integrating analog to digital converter. An understanding of the dual slope conversion technique will aid in following the detailed TSC7135 operation theory.
The conventional dual slope converter measurement cycle has two distinct phases:

- Input Signal Integration
- Reference Voltage Integration (Deintegration)

The input signal being converted is integrated for a fixed time period. Time is measured by counting clock pulses. An opposite polarity constant reference voltage is then integrated until the integrator output voltage returns to zero. The reference integration time is directly proportional to the input signal.
In a simple dual slope converter a complete conversion requires the integrator output to "ramp-up" and "ramp-down."


Figure 3: Basic Dual Slope Converter

A simple mathematical equation relates the input signal, reference voltage and integration time:

$$
\frac{1}{R C} \int_{0}^{T S I} V_{I N}(t) d t \quad=\frac{V_{R} T_{R I}}{R C}
$$

where:

$$
\begin{aligned}
& V_{R}=\text { Reference Voltage } \\
& \mathrm{TSI}^{=} \text {Signal Integration Time (Fixed) } \\
& \mathrm{T}_{\mathrm{RI}}=\text { Reference Voltage Integration Time (Variable) }
\end{aligned}
$$

For a constant VIN:

$$
V_{I N}=V_{R}\left[\frac{T_{R I}}{T_{S I}}\right]
$$

The dual slope converter accuracy is unrelated to the integrating resistor and capacitor values as long as they are stable during a measurement cycle. An inherent benefit is noise immunity. Noise spikes are integrated or averaged to zero during the integration periods. Integrating ADCs are immune to the large conversion errors that plague successive approximation converters in high noise environments.

## TSC7135 Operation Theory

The TSC7135 incorporates a system zero and integrator output voltage zero phase to the normal two phase dual slope measurement cycle. Reduced system errors, fewer calibration steps and a shorter overrange recovery time result.
The TSC7135 measurement cycle contains four phases:

- System Zero
- Analog Input Signal Integration
- Reference Voltage Integration
- Integrator Output Zero

Internal analog gate status is shown in Table 1 for each phase.

Table 1: Internal Analog Gate Status

| Conversion Cycle Phase | Internal Analog Gate Status |  |  |  |  |  |  | Reference Schematic |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | SWI | SW ${ }_{\text {RI }}^{+}$ | SW可 | SWz | SWR | SW1 | SWIZ |  |
| System Zero |  |  |  | Closed | Closed | Closed |  | 3 A |
| Input Signal Integration | Closed |  |  |  |  |  |  | 3 B |
| Reference Voltage Integration |  | Closed* |  |  |  | Closed |  | 3 C |
| Integrator Output Zero |  |  |  |  |  | Closed | Closed | 3 D |

[^4]
## System Zero Phase (Figure 3B)

During this phase errors due to buffer, integrator and comparator offset voltages are compensated for by charging CAZ (auto-zero capacitor) with a compensating error voltage. With a zero input voltage the integrator output will remain at zero.

The external input signal is disconnected from the internal circuitry by opening the two SWI switches. The internal input points connect to analog common. The reference capacitor charges to the reference voltage potential through SWR. A feedback loop, closed around the integrator and comparator, charges the CAZ capacitor with a voltage to compensate for buffer amplifier, integrator and comparator offset voltages.

## Analog Input Signal Integration Phase

(Figure 3C)
The TSC7135 integrates the differential voltage between the + Input and - Input. The differential voltage must be within the device common-mode range; -1 V from either supply rail typically.
The input signal polarity is determined at the end of this phase.

## Reference Voltage Integration (Figure 3D)

The previously charged reference capacitor is connected with the proper polarity to ramp the integrator output back to zero. The digital reading displayed is:

$$
\text { Reading }=10,000\left[\frac{\text { Differential Input }}{V_{\text {REF }}}\right]
$$

## Integrator Output Zero (Figure 3E)

This phase guarantees the integrator output is at zero volts when the system zero phase is entered and that the true system offset voltages are compensated for. This phase normally lasts 100 to 200 clock cycles. If an overrange condition exists the phase is extended to 6200 clock cycles.

## Analog Pin Functional Description

Differential Inputs (+ Input (Pin 10) and -Input (Pin 9))
The TSC7135 operates with differential voltages within the input amplifier common-mode range. The input amplifier common-mode range extends from 0.5 V below the positive supply to 1.0 V above the negative supply. Within this com-mon-mode voltage range an 86 dB common-mode rejection ratio is typical.

The integrator output also follows the common-mode voltage. The integrator output must not be allowed to saturate. A worst case condition exists, for example, when a large positive common-mode voltage with a near full scale negative differential input voltage is applied. The negative input signal drives the integrator positive when most of its swing has been used up by the positive common-mode voltage. For these critical applications the integrator swing can be reduced to less than the recommended 4 V full scale swing with some loss of accuracy. The integrator output can swing within 0.3 volts of either supply without loss of linearity.

## Analog Common (Pin 3)

Analog COMMON is used as the - Input return during autozero and de-integrate. If -Input is different from analog COMMON, a common-mode voltage exists in the system. This signal is rejected by the excellent CMRR of the converter. In most applications - Input will be set at a fixed known voltage (power supply common for instance). In this application, analog COMMON should be tied to the same point, thus removing the common-mode voltage from the converter. The reference voltage is referenced to analog COMMON.

## Reference Voltage (REF IN (Pin 2))

The REF IN reference voltage input must be a positive voltage with respect to analog COMMON. Two reference voltage circuits are shown in Figure 4.


Figure 4: Using an External Reference
The TSC7135 digital section is shown in Figure 5. Timing relationships are shown in Figure 6.

## Pin Configuration



## 4 1/2 Digit Precision Analog-to-Digital Converter



Figure 5: TSC7135 Digital Section Function Diagram


Figure 6: Timing Dlagrams for Outputs

## TSC7135 Digital Section Functional Description

The major digital subsystems within the TSC7135 are illustrated in Figure 5 with timing relationships shown in Figure 6. The multiplexed BCD output data can be displayed on LCD or LED displays with the TSC700A (LED), TSC7211A (LCD), or TSC7212A (LED) four digit display drivers.
The digital section is best described through a discussion of the control signals and data outputs.

## Run/Hold Input (Pin 25)

When left open this pin assumes a logic 1 level. With $R / H=1$ the TSC7135 performs conversions continuously with a new measurement cycle beginning every 40,002 clock pulses.
When R/H changes to a logic 0 the measurement cycle in progress will be completed and data held and displayed as long as the logic 0 condition exists.

A positive pulse ( $>300 \mathrm{~ns}$ ) at $\mathrm{R} / \mathrm{H}$ will initiate a new measurement cycle. The measurement cycle in progress when $\mathrm{R} / \mathrm{H}$ initially assumed the logic " 0 " state must be completed before the positive pulse can be recognized as a single conversion run command.
The new measurement cycle begins with a 10,001 count auto-zero phase. At the end of this phase the busy signal goes high.

## Strobe Output (Pin 26)

During the measurement cycle the STROBE control line is pulsed low five times. The five low pulses occur in the center of the digit drive signals ( $\mathrm{D}_{1}, \mathrm{D}_{2}, \mathrm{D}_{3}, \mathrm{D}_{5}$ ). (Figure 7)
$D_{5}$ (MSD) goes high for 201 counts when the measurement cycles end. In the center of the D5 pulse, 101 clock pulses after the end of the measurement cycle, the first STROBE occurs for one-half clock pulse. After the $\mathrm{D}_{5}$ digit strobe, $\mathrm{D}_{4}$ goes high for 200 clock pulses. The STROBE goes low 100 clock pulses after $D_{4}$ goes high. This continues through the $\mathrm{D}_{1}$ digit drive pulse.
The digit cirive signals will continue to permit display scanning. STROBE pulses are not repeated until a new measurement is completed. The digit drive signals will not continue if the previous signal resulted in an overrange condition.
The active low $\overline{S T R O B E}$ pulses aid BCD data transfer to UARTs, processors and external latches. See Application Note AN16.


Figure 7: Strobe Signal Pulses Low 5 Times Per Conversion.

## Busy Output (Pin 21)

At the beginning of the signal integration phase BUSY goes high and remains high until the first clock pulse after the integrator zero crossing. BUSY returns to the logic " 0 " state after the measurement cycle ends in a overrange condition. The internal display latches are loaded during the first clock pulse after busy and are latched at the ciock pulse end. The busy signal does not go high at the beginning of the measurement cycle which starts with the auto-zero cycle.

## Overrange Output (Pin 27)

If the input signal causes the reference voltage integration time to exceed 20,000 clock pulses the overrange output is set to a logic 1. The overrange output register is set when BUSY goes low and is reset at the beginning of the next reference integration phase.

## TSC7135 Digital Section Functiorial Description (Cont.) <br> Underrange Output (Pin 28)

If the output count is $9 \%$ of full scale or less ( $\leq 1800$ counts) the underrange register bit is set at the end of BUSY. The bit is set low at the next signal integration phase.

## Polarity Output (Pin 23)

A positive input is registered by a logic 1 polarity signal. The polarity bit is valid at the beginning of reference integrate and remains valid until determined during the next conversion. The polarity bit is valid even for a zero reading. Signals less than the converters LSB will have the signal polarity determined correctly. This is useful in null applications.

Digit Drive Outputs (Pins 12, 17, 18, 19 \& 20)
Digit drive signals are positive going signals. The scan sequence is $\mathrm{D}_{5}$ to $\mathrm{D}_{1}$. All positive pulses are 200 clock pulses wide except $D_{5}$ which is 201 clock pulses wide.
All five digits are scanned continuously unless an overrange condition occurs. In an overrange condition all digit drives are held low from the final STROBE pulse until the beginning of the next reference integrate phase. The scainning sequence is then repeated. This provides a blinking visual display indication.

## BCD Data Outputs (Pins 13, 14, 15 and 16)

The binary coded decimal bits $\mathrm{B}_{8}, \mathrm{~B}_{4}, \mathrm{~B}_{2}, \mathrm{~B}_{1}$ are positive true logic signals. The data bits become active simultaneously with the digit drive signals. In an overrange condition all data bits are at a logic " 0 " state.

## Applications Information

## Component Value Selection

The integrating resistor is determined by the full scale input voltage and the output current of the buffer used to charge the integrator capacitor. Both the buffer amplifier and the integrator have a class A output stage with $100 \mu \mathrm{~A}$ of quiescent current. A $20 \mu \mathrm{~A}$ drive current gives negligible linearity errors. Values of 5 to $40 \mu \mathrm{~A}$ give good results. The exact value of integrating resistor for a $20 \mu \mathrm{~A}$ current is easily calculated.

$$
\text { RiNT }=\frac{\text { full-scale voltage }}{20 \mu \mathrm{~A}}
$$

## Integrating Capacitor

The product of integrating resistor and capacitor should be selected to give the maximum voltage swing which ensures that the tolerance build-up will not saturate the integrator swing (approx. 0.3 volt from either supply). For $\pm 5$ volt supplies and analog COMMON tied to supply ground, $a \pm 3.5$ to $\pm 4$ volt full scale integrator swing is adequate. $\mathrm{A} 0.10 \mu \mathrm{~F}$ to $0.47 \mu \mathrm{~F}$ is recommended. In general, the value of CINT is given by:

$$
\begin{aligned}
\mathrm{CINT} & =\frac{[10,000 \times \text { clock period }] \times \text { linT }}{\text { Integrator output voltage swing }} \\
& =\frac{(10,000)(\text { clock period })(20 \mu \mathrm{~A})}{\text { Integrator output voltage swing }}
\end{aligned}
$$

A very important characteristic of the integrating capacitor is that it has low dielectric absorption to prevent roll-over or ratiometric errors. A good test for dielectric absorption is to use the capacitor with the input tied to the reference. This ratiometric condition should read half scale 0.9999. Any deviation is probably due to dielectric absorption. Polypropylene capacitors give undetectable errors at reasonable cost. Polystyrene and polycarbonate capacitors may also be used in less critical applications.

## Auto-Zero and Reference Capacitor

The size of the auto-zero capacitor has some influence on the noise of the system. A large capacitor reduces the noise. The reference capacitor should be large enough such that stray capacitance to ground from its nodes is negligible.
The dielectric absorption of the reference cap and auto-zero cap are only important at power-on or when the circuit is recovering from an overload. Smaller or cheaper caps can be used if accurate readings are not required for the first few seconds of recovery.

## Reference Voltage

The analog input required to generate a full-scale output is $\mathrm{V}_{\mathrm{IN}}=2 \mathrm{~V}_{\text {REF }}$.
The stability of the reference voltage is a major factor in the overall absolute accuracy of the converter. For this reason, it is recommended that a high quality reference be used where high-accuracy absolute measurements are being made. Suitable references are:

| Part Type | Manufacturer |
| :--- | :--- |
| TSC9491 | Teledyne Semiconductor |
| MC1400U2 | Motorola |

## Conversion Timing Line Frequency Rejection

A signal integration period at a multiple of the 60 Hz line frequency will maximize 60 Hz "line noise" rejection.
A 100 kHz clock frequency will reject both $50 \mathrm{~Hz}, 60 \mathrm{~Hz}$ and 400 Hz noise. This corresponds to 2.5 readings per second.

| Oscillator Frequency | Frequency Rejected |
| :---: | :---: |
| $300 \mathrm{kHz}, 200 \mathrm{kHz}$, <br> $150 \mathrm{kHz}, 120 \mathrm{kHz}, 100 \mathrm{kHz}$, $40 \mathrm{kHz}, 331 / 3 \mathrm{kHz}$ | 60 Hz |
| $250 \mathrm{kHz}, 1662 / 3 \mathrm{kHz}$, <br> $125 \mathrm{kHz}, 100 \mathrm{kHz}$ | 50 Hz |
| 100 kHz | $50 \mathrm{~Hz}, 60 \mathrm{~Hz}, 400 \mathrm{~Hz}$ |

Conversion Rate vs Clock Frequency

| Oscillator <br> Frequency <br> (kHz) | Conversion <br> Rate (Conv/Sec) |
| :---: | :---: |
| 100 | 2.5 |
| 120 | 3 |
| 200 | 5 |
| 300 | 7.5 |
| 400 | 10 |
| 800 | 20 |
| 1,200 | 30 |

## Power Supplies and Grounds

## Power Supplies

The TSC7135 is designed to work from $\pm 5 \mathrm{~V}$ supplies. The conditions to use a single +5 V supply are:

- The input signal is referenced to the center of the common mode range of the converter.
- The signal is less than $\pm 1.5$ volts.


## Grounding

Systems should use separate digital and analog ground systems to avoid loss of accuracy.

## Displays and Driver Circuits

Teledyne Semiconductor manufactures three display decoder/driver circuits to interface the TSC7135 to LCD or LED displays. Each driver has 28 outputs for driving four seven segment digit displays. The TSC700A features increased LED segment drive current for greater display brightness.

| Device | Package | Description |
| :--- | :--- | :--- | :--- |
| TSC7211AIPL 40 Pin Epoxy | 4 Digit LCD Driver/Decoder |  |
| TSC7212AIPL 40 Pin Epoxy | 4 Digit LED Driver/Decoder |  |
| TSC700AIJL | 40 Pin CerDIP | 4 Digit LED Driver/Decoder <br> with high LED Segment <br> Current (ISEG $\geq 11 \mathrm{~mA})$ |
| Several sources exist for LCD and LED displays: |  |  |

## High Speed Operation

The maximum conversion rate of most dual-slope A/D converters is limited by the frequency response of the comparator. The comparator in this circuit follows the integrator ramp with a $3 \mu \mathrm{~s}$ delay, and at a clock frequency of $160 \mathrm{kHz}(6 \mu \mathrm{~s}$ period) half of the first reference integrate clock period is lost in delay. This means that the meter reading will change from 0 to 1 with a $50 \mu \mathrm{~V}$ input, 1 to 2 with $150 \mu \mathrm{~V}, 2$ to 3 at $250 \mu \mathrm{~V}$, etc. This transition at mid-point is considered desirable by most users; however, if the clock frequency is increased appreciably above 160 kHz , the instrument will flash " 1 " on noise peaks even when the input is shorted.

For many-dedicated applications where the input signal is always of one polarity, the delay of the comparator need not be a limitation. Since the non-linearity and noise do not increase substantially with frequency, clock rates of up to $\sim 1$ MHz may be used. For a fixed clock frequency, the extra count or counts caused by comparator delay will be a constant and can be subtracted out digitally.
The clock frequency may be extended above 160 kHz without this error, however, by using a low value resistor in series with the integrating capacitor. The effect of the resistor is to introduce a small pedestal voltage on to the integrator output at the beginning of the reference integrate phase. By careful selection of the ratio between this resistor and the integrating resistor (a few tens of ohms in the recommended circuit), the comparator delay can be compensated and the maximum clock frequency extended by approximately a factor of 3. At higher frequencies, ringing and second order breaks will cause significant non-linearities in the first few counts of the instrument.

The minimum clock frequency is established by leakage on the auto-zero and reference caps. With most devices, measurement cycles as long as 10 seconds give no measurable leakage error.

The clock used should be free from significant phase or frequency jitter. Several suitable low-cost oscillators are shown in the Applications section. The multiplexed output means that if the display takes significant current from the logic supply, the clock should have good PSRR.

## Zero-Crossing Flip-Flop

The flip-flop interrogates the data once every clock pulse after the transients of the previous clock pulse and half-clock pulse have died down. False zero-crossings caused by clock pulses are not recognized. Of course, the flip-flop delays the true zero-crossing by up to one count in every instance, and if a correction were not made, the display would always be one count too high. Therefore, the counter is disabled for one clock pulse at the beginning of the reference integrate (deintegrate) phase. This one-count delay compensates for the delay of the zero-crossing flip-flop, and allows the correct number to be latched into the display. Similarly, a one-count delay at the beginning of auto-zero gives an overload display of 0000 instead of 0001 . No delay occurs during signal integrate, so that true ratiometric readings result.

## Application Circults



Figure A: R/C Oscillator


Figure B: Comparator Clock Circuit

## 4 1/2 Digit ADC with Multiplexed Common Anode LED Display



## 4 1/2 Digit ADC Interfaced to LCD Display with Digit Blanking on Overrange



## 4 1/2 Digit ADC with Multiplexed Common Cathode LED Display



## Four Channel Data Acquisition System



Negative Supply Voltage Generator


## Output Voltage vs Output Current

A negative voltage can be generated from the positive supply by using a hex inverter as a free running oscillator to drive a voltage doubler. The five inverters are paralleled to provide a low output impedance. Since the 4049 is a standard 4000 CMOS part, the circuit can be operated from 3 to 15 volts. The $10 \mu \mathrm{~F}$ capacitors were used in order to minimize output ripple at low $\mathrm{V}+$ voltages. When higher input voltages ( $\mathrm{V}+$ )
are available the $10 \mu \mathrm{~F}$ capacitors can be lowered to 1 or 0.1 $\mu \mathrm{F}$ depending on the output loading. If this circuit generates more voltage than is needed, one half of the diodes and capacitors can be eliminated to reduce cost. The output voltage will then beone-half of that shown in the graph and is available on the negative side of the $10 \mu \mathrm{~F}$ capacitor connected to ground.

## Package Outlines



## General Description

The Teledyne Semiconductor TSC8750 is a $31 / 2$ digit monolithic CMOS analog-to-digital converter. Fully self-contained in a single 24-pin dual in-line package, the converter requires only passive support components, voltage or current reference and power supplies.
Conversion is performed by an incremental charge balancing technique which has inherently high accuracy, linearity and noise immunity. An amplifier integrates the sum of the unknown analog current and pulses of a reference current. The number of pulses (charge increments) needed to maintain the amplifier summing junction near zero are counted. At the end of conversion the total count is latched into the digital outputs in a $31 / 2$ digit parallel BCD digital format.

Ordering Information

| Part No. | Package | Temperature <br> Range |
| :--- | :--- | ---: |
| TSC8750CJ | $24-$ Pin <br> Plastic Dip | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ |
| TSC8750CN | $24-$ Pin <br> Ceramic | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
| TSC8750BN | $24-$ Pin <br> Ceramic | $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |

## Pin Configuration



## Features

- High Accuracy - 3 1/2 Digit Resolution With $< \pm 0.025 \%$ Error
- Military Temperature Range Devices
- Monotonic Performance - No Missing Codes
- Monolithic CMOS Construction Gives Low Power Dissipation - 20 mW Typical
- Contains All Required Active Elements - Needs only Passive Support Components, Reference Voltage and Dual Power Supply
- High Stability Over Full Temperature Range
- Gain Temperature Coefficient Typically $<25 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$
- Zero Drift Typically $<30 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$
- Differential Non-Linearity Drift Typically $<2.5 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$
- Latched Parallel BCD Outputs
- LPTTL and CMOS Compatible Outputs and Control Inputs
- Strobed or Free Running Conversion
- Infinite Input Range - Any Positive Voltage Can Be Applied Via a Scaling Resistor


## Absolute Maximum Ratings

Storage Temperature .................... $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ Operating Temperature


VDD -VSS ...................................................... 18 V
Iin ....................................................... . . $\pm 10 \mathrm{~mA}$
IREF .................................................... $\pm 10 \mathrm{~mA}$
Digital Input Voltage .................. -0.3 to VDD +0.3 V
Operating VDD and VSs Range ................ 3.5 V to 7 V
Package Dissipation ................................ . 500 mW
Lead Temperature ......................................... $300^{\circ} \mathrm{C}$
(Soldering, 10 seconds)

## HANDLING PRECAUTIONS

CMOS devices must be handled correctly to prevent damage. Package and store only in conductive foam, anti-static tubes or other conductive material. Use proper anti-static handling procedures. Do not connect in circuits under "power on" conditions, as high transients may cause permanent damage.

Electrical Characteristics Unless otherwise specified, $\mathrm{V}_{\mathrm{DD}}=+5 \mathrm{~V}, \mathrm{~V}_{S S}=-5 \mathrm{~V}, \mathrm{~V}_{\mathrm{GND}}=0, \mathrm{~V}_{\text {REF }}=-6.4 \mathrm{~V}, \mathrm{R}_{B I A S}=100 \mathrm{k} \Omega$ test circuit shown. $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ unless Full Temperature Range is specified. $\left(-55^{\circ} \mathrm{C}\right.$ to $+125^{\circ} \mathrm{C}$ for $\mathrm{BN},-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ for CN package, $0^{\circ}$ to $70^{\circ} \mathrm{C}$ for CJ package.)

| PARAMETER | DEFINITION | CONDITIONS | MIN | TYP | CJ/CL MAX | $\begin{array}{r} \text { BL } \\ \text { MAX } \end{array}$ | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Accuracy |  |  |  |  |  |  |  |
| Resolution Accuracy | BCD Word Length Of Digital Output |  | $\begin{array}{r} 31 / 2 \\ (1999 \\ \text { (190nts) } \end{array}$ | - | - | - | Digits |
| Relative Accuracy | Output Deviation From Straight Line Between Normalized Zero and Full-Scale Input |  | - | - | 0.025 | 0.025 | \% |
| Differential Non-Linearity | Deviation From 1 LSB <br> Between Transition Points |  | - | - | - | 0.025 | 0.025\% |
| Differential <br> Non-Linearity <br> Temperature Drift | Variation in Differential Non-Linearity Due To Temperature Change | Full <br> Temperature <br> Range | - | $\pm 2.5$ | $\pm 5$ | $\pm 5$ | ppm $/{ }^{\circ} \mathrm{C}$ |
| Gain Variance | Variation From Exact (Compensate By Trimming Rin or RREF) |  | - | $\pm 2$ | $\pm 5$ | $\pm 5$ | \% of Nominal |
| Gain <br> Temperature Drift | Variation $\ln \mathrm{A}$ <br> Due To <br> Temperature Change | Full <br> Temperature Range | - | $\pm 25$ | $\pm 75$ | $\pm 80$ | ppm $/{ }^{\circ} \mathrm{C}$ |
| Zero Offset | Correction at Zero Adjust to Give Zero Output When Input Is Zero | $\mathrm{l} \mathrm{IN}^{\text {= }} 0$ | - | $\pm 10$ | $\pm 50$ | $\pm 50$ | mV |
| Zero Temperature Drift | Variation in Zero Offest Due to Temperature Change | Full Temperature Range | - | $\pm 3$ | $\pm 5$ | $\pm 8$ | $\mathrm{ppm} /{ }^{\circ} \mathrm{C}$ |
| Analog Inputs Iin Full-Scale | Full-Scale Analog Input Current To Achieve Specified Accuracy |  | - | 10 | - | - | $\mu \mathrm{A}$ |
| I ReF (Note 1) | Reference Current Input To Achieve Specified Accuracy |  | - | -20 | - | - | $\mu \mathrm{A}$ |
| Digital Inputs $V_{1 N}{ }^{(1)}$ | Logical "1" Input Threshold For Initiate Conversion Input | Full Temperature Range | 3.5 | - | - | - | V |
| VIN ${ }^{(0)}$ | Logical "0" Input Threshold For Initiate Conversion Input | Full Temperature Range | - | - | 1.5 | 1.5 | V |
| Digital Outputs Vout ${ }^{(1)}$ | Logical "1" Output Voltage For Digits Out, Busy, and Data Valid Outputs | Full Temp. Range lout $=-10 \mu \mathrm{~A}$ IOUT $=-500 \mu \mathrm{~A}$ | 4.5 | - | - | - | V |
| Vout ${ }^{(0)}$ | Logical "0" Output Voltage For Digits Out, Busy, and Data Valid Outputs | Full Temp. Range <br> $V_{D D}=4.75 \mathrm{~V}$ <br> lout $=500 \mu \mathrm{~A}$ | - | - | 0.4 | 0.4 | V |
| Dynamic <br> Conversion Time | Time Required to Perform One Complete A/D Conversion | Full Temp. Range | - | 10 | 12 | 12 | ms |
| Conversion <br> Rate in <br> Free-Run Mode |  | VINT CONV $=+5 \mathrm{~V}$ | 84 | 100 | - | - | Conv'ns per <br> Second |
| Minimum Pulse Width for Initiate Conversion |  | Full Temp. Range | 500 | - | - | - | ns |

## 3 1/2 Digit ADC <br> w/Parallel BCD Output <br> - 10 mS Conversion Time <br> - Latched Outputs

TSC8750
Electrical Characteristics Unless otherwise specified, $V_{D D}=+5 \mathrm{~V}, \mathrm{~V}_{S S}=-5 \mathrm{~V}, \mathrm{~V}_{G N D}=0, \mathrm{~V}_{\text {REF }}=-6.4 \mathrm{~V}, \mathrm{R}_{\mathrm{BIAS}}=100 \mathrm{k} \Omega$, test circuit shown. $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ unless Full Temperature Range is specified. $\left(-55^{\circ} \mathrm{C}\right.$ to $+125^{\circ} \mathrm{C}$ for $\mathrm{BN},-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ for CN package, $0^{\circ}$ to $70^{\circ} \mathrm{C}$ for CJ package.)

| PARAMETER | DEFINITION | CONDITIONS | MIN | TYP | CJ/CL MAX | $\begin{array}{r} \text { BL } \\ \text { MAX } \end{array}$ | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Supply Current IDD Quiescent (N Package) (J Package) | Current Required From Positive Supply During Operation | Full Temp. Range VINT CONV = OV | - | $\begin{aligned} & 1.4 \\ & 1.4 \end{aligned}$ | 2.5 5.0 | 3.5 | mA mA |
| Iss Quiescent (N Package) <br> (J Package) | Current Required From Negative Supply During Operation | Full Temp. Range <br> VINIT CONV = OV | - | $\begin{aligned} & -1.6 \\ & -1.6 \end{aligned}$ | $\begin{aligned} & -2.5 \\ & -5.0 \end{aligned}$ | -3.5 | $\begin{gathered} \mathrm{mA} \\ \mathrm{~mA} \end{gathered}$ |
| Supply Sensitivity | Change in Full-Scale Gain vs Supply Voltage Change | $V_{D D} \pm 1 \mathrm{~V}, \mathrm{~V}_{S S} \pm 1 \mathrm{~V}$ | - | $\pm 0.5$ | $\pm 1.0$ | $\pm 1.0$ | \%/V |
| $\left\|\mathrm{V}_{\text {DD }}\right\|=\left\|\mathrm{V}_{S S}\right\|=5 \mathrm{~V} \pm 1 \mathrm{~V}$ | Change in Full-Scale Gain vs Sup Voltage Change for Tracking Sup |  | $\pm 0.05$ | $\pm 0.1$ | $\pm 0.1$ | $\pm 0.1$ | \%/V |

## NOTE:

lin and Iref pins connect to the summing junction of an operational amplifier.
Voltage sources cannot be attached directly but must be buffered by external
resistors. See Test Circuit.

## Test Circuit



## Circuit Description

During conversion the sum of a continuous current lin and pulses of a reference current IREF is integrated for a fixed number of clock periods. $\operatorname{lin}$ is proportional to the analog input voltage; I ReF is switched in for exactly one clock period just frequently enough to maintain the summing input of the integrator near zero. Thus, the charge from the continuous lin current is balanced against the pulses of Iref current. The total number of IREF pulses needed during the
conversion period to maintain the charge balance is counted, and the result (in BCD) is latched into the outputs at the end of conversion.
The converter contains two counters and a clock in addition to an operational amplifier, comparator, latching output buffers and housekeeping logic. One counter is a clock counter which (after a reset pulse) starts counting clock pulses; when the required count is reached, the clock counter generates a pulse to start the end-of-conversion routine.

The other counter is a data counter, which is reset synchronously with the clock counter and counts the number of times the IREF current is switched into the summing input of the amplifier during the period defined by the clock counter.

When the Initiate Conversion input is strobed with a positive signal, the busy line latches high and a $10 \mu \mathrm{~s}$ (times given are approximate) start up cycle begins. The integrating capacitor is discharged and both counters are reset during this start up period. Conversion begins at the end of the reset pulse and ends with a pulse generated either by the clock
counter or by an overflow condition in the data counter. This pulse disables further inputs into both counters and triggers a $10 \mu \mathrm{~s}$ shutdown cycle. During the shutdown cycle Data Valid goes low for $5 \mu \mathrm{~s}$. This binary sequence is shown in the timing diagrams. Busy is true high, and when the circuit is busy, Initiate conversion has no effect and may be high or low. Data Valid is also true high. The data from a conversion remain valid for as long as power is applied to the circuit or until Data Valid falls at the end of a subsequent conversion, at which time the output data are updated to reflect the latest conversion.

Timing Diagrams (Rise, fall times $=200 \mathrm{~ns}$ typ., $\mathrm{C}_{\mathrm{L}}=50 \mathrm{pF}$ )


## Pin Functions

## Initiate Conversion Input

Accepts CMOS and most 5 V logic inputs. Applying a logic " 1 " to the Initiate Conversion pin initiates the A/D conversion cycle. Once conversion has been initiated, the cycle cannot be interrupted, and the Initiate Conversion pin is disabled until conversion is complete. Two modes of operation are permitted, clocked or free-running. For clocked operation the Initiate Conversion input is held at logic " 0 " for standby and taken to logic " 1 " when a conversion is desired. For freerunning operation the Initiate Conversion pin is connected to VDD or similar permanent logic " 1 " voltage.

## Busy Output

A digital status output which is compatible with CMOS logic and low power TTL (can sink and source $500 \mu \mathrm{~A}$ ). A logic "1" output on the Busy pin indicates a conversion cycle is in process. A logic " 1 " to logic " 0 " transition indicates that conversion is complete and the result has been latched at the Digits Out pins. A logic " 0 " to logic " 1 " transition indicates a
new conversion cycle has been initiated. If the device is operating in the free-running mode, the Busy output will remain low for approximately $2.5 \mu \mathrm{~s}$, marking the completion and initiation of consecutive conversion cycles.

## Data Valid Output

A digital status which is compatible with CMOS logic and low power TTL (can sink and source $50 \mu \mathrm{~A}$ ). A logic " 1 " output at the Data Valid pin indicates that the Digits Out pins are latched with the result of the last conversion cycle. The Data Valid output goes to logic " 0 " approximately $5 \mu$ s before the completion of a conversion cycle. During this $5 \mu \mathrm{~s}$ interval new data is being transferred to the Digits Out pins, and the Digits Out are not valid.

## Digits Out

(ones, tens, hundreds and thousand)
The BCD digit outputs which are the result of the A/D conversion. These outputs are CMOS logic and low power TTL compatible.

## Applications Information <br> Input/Output Relationships

The analog input voltage $\left(\mathrm{V}_{\mathrm{IN}}\right)$ is related to the output by the transfer equation:

$$
\begin{aligned}
\text { Digital Counts } & =\frac{V_{I N} \cdot A \cdot R_{\text {REF }}}{R_{I N} \cdot V_{\text {REF }}} \\
A & =4128
\end{aligned}
$$

where Digital Counts is the value of the BCD output word presented at Digits Out pins in response to Vin.

The digital output code format is as follows:

| Analog <br> Input | Digltal <br> Output |
| :---: | :--- |
| VIN $\leq$ Full-Scale | 1100110011001 |
| $=$ Full-Scale -1 LSB | 1100110011001 |
| $=1$ LSB | $0 \ldots 000 \ldots 1$ |
| $\leq 0$ | $0 \ldots . . .000 . .0$ |

## External Component Selection

Obtaining a high accuraccy conversion system depends on the voltage regulation of VREF and the thermal stability of RIN and Rref. The exact dependence is given by the transfer function. System accuracy also depends, to a lesser degree, on the voltage regulation of VDD and VSS. The supply connections VDD and VSS should have bypass capacitors of value $0.1 \mu \mathrm{~F}$ or larger right at the device pins.

## Rin, Ref

Values of these components are chosen to give a full-scale input current of approximately $10 \mu \mathrm{~A}$ and a reference current of approximately $-20 \mu \mathrm{~A}$.

$$
R_{I N} \cong \frac{V_{I N} \text { Full-Scale }}{10 \mu \mathrm{~A}} \quad \mathrm{R}_{\mathrm{REF}} \cong \frac{\mathrm{~V}_{\text {REF }}}{-20 \mu \mathrm{~A}}
$$

Examples:

$$
\mathrm{R}_{\mathbb{N}} \cong \frac{10 \mathrm{~V}}{10 \mu \mathrm{~A}}=1 \mathrm{M} \Omega \quad \mathrm{R}_{\mathrm{REF}} \cong \frac{-6.4 \mathrm{~V}}{-20 \mu \mathrm{~A}}=320 \mathrm{k} \Omega
$$

Note that these values are approximations, and the exact relationships are defined by the transfer equation. In practice, the value of RIN typically would be trimmed using the optional gain adjust circuit to obtain full-scale output at $V_{\mathbb{N}}$ Full-Scale (see adjustment procedure). Metal film resistors with $1 \%$ tolerance or better are recommended for high accuracy applications because of their thermal stability and low noise generation.

## RBIAS

Specifications for the TSC8750 are based on RBIAS $=100 \mathrm{k} \Omega$ $\pm 10 \%$ unless otherwise noted. However, there are instances when the designer may want to change this resistor in order
to affect the conversion time and the supply current. By decreasing RBIAS the A/D will convert much faster and the supply current will be higher. (For example: When Rbias is 20 k the conversion time is reduced by $1 / 3$, and the supply current will increase from 2 mA to 7 mA .) Likewise, if the RBIAS is increased the conversion time will be longer and the supply current will be much lower. (For example: When RBIAS $=1 \mathrm{~m} \Omega$ the conversion time will be six times longer, and the supply current is now reduced to .5 mA ). For details of this relationship refer to AN-9 typical performance curves.

## Rdamp

Exact value not critical but should have a nominal value of $100 \Omega \pm 10 \%$. Locate close to pin 14.

## CDamp

Exact value not critical but should have a nominal value of $270 \mathrm{pF} \pm 20 \%$. Locate close to pin 14.

## Cint

Exact value not critical but should have a nominal value of $68 \mathrm{pF} \pm 10 \%$. Low leakage types are recommended, although mica or ceramic devices can be used in applications where their temperature limits are not exceeded. Locate as close as possible to pins $14,15$.

## $V_{\text {REF }}$

A negative reference voltage must be supplied. This may be obtained from a constant current source circuit or from the negative supply.

## VDD, Vss

Power supplies of $\pm 5 \mathrm{~V}$ are recommended, with $0.05 \%$ line and load regulation and $0.1 \mu \mathrm{~F}$ decoupling capacitors.

## Adjustment Procedure

The test circuit diagram shows optional circuits for trimming the zero location and full-scale gain. Because the digital outputs remain constant outside of the normal operating range (i.e. below zero and above full-scale), it is recommended that transition points be used in setting the zero and full-scale values. Recommended procedure is as follows:

- Set the initiate conversion control high to provide free-run operation and verify that converter is operating.
- Set VIN to $+1 / 2$ LSB and trim the zero adjust circuit to obtain a $000 \ldots 000 \ldots$ to $000 \ldots 001$ transition. This will correctly locate the zero end.
- For full-scale adjustment, set VIN to the full-scale value less 1 1/2 LSB and trim the gain adjust circuit for a 1100110011000 to 1100110011001 transition.
If adjustments are performed in this order, there should be no interaction and they should not have to be repeated.


## Application/Design Circuits

## 3 1/2 Digit A/D with LCD Display



## Bipolar Operation (+ and - inputs)



## 3 1/2 Digit ADC

w/Parallel BCD Output

- 10 mS Conversion Time
- Lat ed Outputs

TSC8750

## Microprocessor-Based ADC System



## Package Information



## General Description

The TSC14433A is a monolithic CMOS $31 / 2$ digit A/D converter which features improved performance over the industry standard TSC14433. Rollover, which is the measurement of an idencital positive and negative signal is guaranteed to have the same reading within one count. The output drive current is increased and is fully compatible to drive TTL loads and conforms to standard B-Series CMOS. The power consumption at 4 mW is approximately one-half of the TSC14433. The TSC14433A combines both analog and digital circuits on a single IC, thus minimizing the number of external components. This dual slope A/D converter provides automatic polarity and zero correction with the addition of two external resistors and two capacitors. The full-scale voltage range of this ratiometric IC extends from 199.9 millivolts to 1.999 volts. The TSC14433A can operate over a wide range of power supply voltages including batteries and standard 5 volt supplies.

The TSC14433A will interface with the TSC7211A (LCD), TSC7212A (LED) and TSC700A (high LED current drive) display drivers.

HANDLING PRECAUTIONS: These devices are CMOS and must be handled correctly to prevent damage. Package and store only in conductive foam, anti-static handling procedures. Do not connect in circuits under "power on" conditions, as high transients may cause permanent damage.

## Features

- Rollover: $\pm 1$ Count
- Standard B-Series CMOS Outputs - Drives One Standard TTL Load
- Low Power Consumption: 4 mW Typical @ $\pm 5.0 \mathrm{~V}$
- Overrange and Underrange Signals Available
- Operates in Auto Ranging Circuits
- Accuracy: $\pm 0.05 \%$ of Reading $\pm 1$ Count
- Two Voltage Ranges: 1.999 V and 199.9 mV
- Up to 25 Conversions Per Second
- ZIN > 1000 M Ohm
- Auto-Polarity and Auto-Zero
- Single Positive Voltage Reference
- Uses On-chip System Clock or External Clock
- Wide Supply Range: e.g., $\pm 4.5 \mathrm{~V}$ to $\pm 8.0 \mathrm{~V}$
- Operates With LED and LCD Displays
- Low External Component Count


## Applications

- Portable Instruments
- Digital Voltmeters
- Digital Panel Meters
- Digital Scales
- Digital Thermometers
- Remote A/D Sensing Systems
- MPU Systems
- See Application Notes 19 and 21


## Block Diagram



## Absolute Maximum Ratings

| RATING | SYMBOL | VALUE | UNIT |
| :---: | :---: | :---: | :---: |
| DC Supply Voltage | VDD to VEE | $\begin{array}{r} -0.5 \text { to } \\ +18 \mathrm{Vdc} \end{array}$ | Vdc |
| Voltage, Any Pin, Referenced Vee | V | $\begin{array}{r} -0.5 \text { to } \\ \text { VDD }+0.5 \end{array}$ | Vdc |
| DC Current Drain Per Pin | 1 | 10 | mAdc |
| Operating Temperature Range | TA | -40 to +85 | ${ }^{\circ} \mathrm{C}$ |
| Storage Temperature Range | Tstg | -65 to +150 | ${ }^{\circ} \mathrm{C}$ |

Recommended Operating Conditions
( $\mathrm{V}_{S S}=0$ or $\mathrm{V}_{\mathrm{EE}}$ )

| PARAMETER | SYMBOL | VALUE | UNIT |
| :--- | :--- | ---: | ---: |
| DC Supply Voltage |  |  |  |
| VDD to Analog Ground | VDD | +5.0 to +8.0 | Vdc |
| VEE to Analog Ground | VEE | -2.8 to -8.0 |  |
| Clock Frequency | fCLK | 32 to 400 | kHz |
| Zero Offset | $0.1 \pm 20 \%$ | $\mu \mathrm{~F}$ |  |

Note: This device contains circuitry to protect the inputs against damage due to high static voltages or electric fields; however, it is advised that normal precautions be taken to avoid application of any voltage higher than maximum rated voltages to this high impedance circuit. For proper operation it is recommended that $V_{\text {IN }}$ and $V_{\text {OUT }}$ be constrained to the range $V_{E E} \leq$ ( $V_{\text {IN }}$ or $\left.V_{\text {OUT }}\right)$ $\leq \mathrm{VDD}$.

Electrical Characteristics: $\left(C_{I}=0.1 \mu \mathrm{~F}\right.$ mylar, $\mathrm{R}_{I}=470 \mathrm{k} \Omega @ \mathrm{~V}_{\text {REF }}=2.000 \mathrm{~V}, \mathrm{R}_{\mathrm{I}}=27 \mathrm{k} \Omega @ \mathrm{~V}_{\text {REF }}=200.0 \mathrm{mV} . C_{0}=0.1 \mu \mathrm{~F}$, $\mathrm{Rc}=300 \mathrm{k} \Omega$; all voltages referenced to Analog Ground, pin 1.)


## Note:

1. Accuracy - The accuracy of the meter at full-scale is the accuracy of the setting of the reference voltage. Zero is recalculated during each conversion cycle. The meaningful specification is linearity. In other words, the deviation from correct reading for all inputs other than positive fuli-scale and
zero is defined as the linearity specification.
2. Three LSD stability for 200 mV scale is defined as the range that the LSD will occupy $95 \%$ of the time.
3. Pin numbers refer to 24 -Pin DIP.

## Pin Description

| $\begin{gathered} \text { PIN NO. } \\ 60-\mathrm{Pin} \\ \text { FP } \end{gathered}$ | $\begin{gathered} \text { PIN NO. } \\ \text { 24-Pin } \\ \text { DIP } \end{gathered}$ | SYMBOL | DESCRIPTION |
| :---: | :---: | :---: | :---: |
| 7 | 1 | $V_{\text {AG }}$ | This is the Analog Ground. It has a high input impedance. This pin determines the reference level for the unknown input voltage ( $V \mathrm{~V}$ ) and the reference voltage ( $\mathrm{V}_{\mathrm{REF}}$ ). |
| 10 | 2 | Vref | Reference voltage. Full-scale output is equal to the voltage applied to VreF. Therefore, full-scale voltage of 1.999 V requires 2.000 V reference and 199.9 mV full-scale requires a 200 mV reference. VREF functions as system reset, also. When switched to $V_{E E}$ the system is reset to the beginning of the conversion cycle. |
| 12 | 3 | $V_{x}$ | The Unknown Input Voltage ( V x ) is measured as a ratio of the reference voltage (VREF) in a ratio-metric $A / D$ conversion. |
| $\begin{aligned} & 19 \\ & 22 \\ & 24 \end{aligned}$ | $\begin{aligned} & 4 \\ & 5 \\ & 6 \end{aligned}$ | $\begin{gathered} \mathrm{R}_{1} \\ \mathrm{R}_{1} / \mathrm{C}_{1} \\ \mathrm{C}_{1} \end{gathered}$ | These pins are for external components used for the integration function in the dual slope conversion. Typical values are $0.1 \mu \mathrm{~F}$ (mylar) capacitor for $\mathrm{C}_{1}$. <br> $\mathrm{R}_{1}=470 \mathrm{k} \Omega$ (resistor) for 2.0 V full-scale. <br> $\mathrm{R}_{1}=27 \mathrm{k} \Omega$ (resistor) for 200 mV full-scale. <br> Clock frequency of 66 kHz gives 250 ms conversion time. See equation below for calculation of integrator component values. |
| $\begin{aligned} & 25 \\ & 26 \end{aligned}$ | $\begin{aligned} & 7 \\ & 8 \end{aligned}$ | $\begin{aligned} & \mathrm{CO}_{1} \\ & \mathrm{CO} \end{aligned}$ | These pins are used for connecting the offset correction capacitor. The recommended value is $0.1 \mu \mathrm{~F}$. |
| 27 | 9 | DU | Display Update input pin. When DU is connected to the EOC output every conversion is displayed. <br> New data will be strobed into the output latches during the conversion cycle if a positive edge is received on DU prior to the ramp-down cycle. When this pin is driven from an external source, the voltage should be referenced to VSs. |
| 34 36 | 10 11 | CLK CLK | Clock input pins. The TSC14433 has its own oscillator system clock. Connecting a single resistor between CLK ${ }_{1}$ and CLK 0 sets the clock frequency. A crystal or LC circuit may be inserted in lieu of a resistor for improved stability. CLK 1 , the clock input, can be driven from an external clock source, which need only have standard CMOS output drive. This pin is referenced to VEE for external clock inputs. A $300 \mathrm{k} \Omega$ resistor yields a clock frequency of about 66 kHz . (See typical characteristic curves). (See Figure 9 for alternate circuits). |
| 37 | 12 | Vee | Negative Power Supply. Connection pin for the most negative supply. Please note the current for the output drive circuit is returned through Vss. Typical supply current is 0.8 mA . |
| 39 | 13 | Vss | Negative Power Supply for Output Circuitry. This pin sets the low voltage level for the output pins (BCD, Digit Selects, EOC, OR). When connected to analog ground, the output voltage is from analog ground to $V_{D D}$. If connected to $V_{E E}$, the output swing is from VEE to $V_{D D}$. The recommended operating range for $V_{S S}$ is between VDD -3.0 volts and $V_{E E}$. |
| 40 | 14 | EOC | End of Conversion output generates a pulse at the end of each conversion cycle. This generated pulse width is equal to one half the period of the system clock. |
| 41 | 15 | OR | Overrange pin. Normally this pin is set high. When Vx exceeds $V_{\text {ref }}$ the OR pin is low. |
| 49 | 16 | DS4 | Digit Select pins. The digit select output goes high when the respective digit is selected. The MSD ( $1 / 2$ digit) turns on immediately after an EOC pulse. |
| 51 | 17 | DS3 | The remaining digits turn on in sequence from MSD to LSD. |
| 52 | 18 | DS2 | To ensure that the BCD data has settled, an inter-digit blanking time of two clock periods is included. |
| 54 | 19 | DS 1 | Clock frequency divided by 80 equals multiplex rate. For example a system clock of 66 kHz gives a multiplex rate of 0.8 kHz . |
| 5 | 20 | Qo | See Figure 12 for Digit Select Timing Diagram. |
| 4 | 21 | Q1 | BCD Data Output pins. Multiplexed BCD outputs contain 3 full digits of information during digit select DS2, 3, 4 . |
| $\begin{aligned} & 57 \\ & 55 \end{aligned}$ | $\begin{aligned} & 22 \\ & 23 \end{aligned}$ | $\begin{aligned} & Q_{2} \\ & Q_{3} \end{aligned}$ | During DS1, the $1 / 2$ digit, overrange, underrange and polarity information is available. Refer to Truth Table. |
| 6 | 24 | VDD | Positive Power Supply. This is the most positive power supply pin. |

## Ordering Information

| Part No. | Package | Temperature <br> Range |  |  | Part No. | Package |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |

## Pin Configuration

$$
\begin{aligned}
& R_{1}=\frac{V_{x}(\max )}{C_{1}} \times \frac{T}{\Delta V} \\
& \Delta V=V_{D D}-V_{X}(\max )-0.5 \\
& T=4000 \times \frac{1}{\text { fCLK }}
\end{aligned}
$$

Where
$R_{1}$ is in $k \Omega$
$V_{D D}$ is the voltage at pin 24 referenced to $V_{A G}$
$V_{x}$ is the voltage at pin 3 referenced

NOTES

1. NC = NO INTERNAL CONNECTION
2. PINS 8, 23, 38 AND 53 ARE CONNECTED TO THE DIE SUBSTRATE. THE POTENTIAL AT THESE PINS IS APPROXIMATELY $V^{+}$. NO EXTERNAL CONNECTIONS SHOULD BE MADE.




## Typical Applications

TSC7212A Interface to TSC14433A 3 1/2 Diglt ADC.


## Package Information



## General Description

The TSC14433B is a monolithic CMOS $31 / 2$ digit A/D converter. This low cost electrical version is ideal in systems where optimum rollover performance is not required. The TSC14433B combines both analog and digital circuits on a single IC, thus minimizing the number of external components. This dual slope A/D converter provides automatic polarity and zero correction with the addition of two external resistors and two capacitors. The full scale voltage range of this ratiometric IC extends from 199.9 millivolts to 1.999 volts. The TSC14433B can operate over a wide range of power supply voltages including batteries and standard 5 volt supplies.
The TSC14433B will interface with the TSC7211A (LCD), TSC7212A (LED) and TSC700A (high LED current drive) display drivers.

HANDLING PRECAUTIONS: These devices are CMOS and must be handled correctly to prevent damage. Package and store only in conductive foam, anti-static handling procedures. Do not connect in circuits under "power on" conditions, as high transients may cause permanent damage.

## Features

- Low Cost
- Available in Compact Flat Package
- Rollover: $\pm 4$ Count
- Low Power Consumption: 4 mW Typical @ $\pm 5.0 \mathrm{~V}$
- Overrange and Underrange Signals Available
- Operates in Auto Ranging Circuits
- Accuracy: $\pm 0.05 \%$ of Reading $\pm 1$ Count
- Two Voltage Ranges: 1.999 V and 199.9 mV
- Up to 25 Conversions Per Second
- $Z_{\text {IN }}>1000 \mathrm{M}$ Ohm
- Auto-Polarity and Auto-Zero
- Uses On-chip System Clock or External Clock
- Wide Supply Range: e.g., $\pm 4.5 \mathrm{~V}$ to $\pm 8.0 \mathrm{~V}$
- Operates With LED, LCD, Vacuum Fluorescent Displays


## Applications

- Portable Instruments
- Digital Voltmeters
- Digital Panel Meters
- Digital Scales
- Digital Thermometers
- Remote A/D Sensing Systems
- MPU Systems
- See Application Notes 19 and 21


## Block Diagram



# 3 1/2 Digit CMOS Low Cost - Multiplexed BCD Data - $\pm 4$ Count Rollover Error 

| Rating | SYMBOL | VALUE | VIT |
| :---: | :---: | :---: | :---: |
| DC Supply Voltage | $\begin{aligned} & \mathrm{V}_{\text {DD }} \mathrm{V}_{\text {VEE }} \end{aligned}$ | $\begin{array}{r} -0.5 \text { to } \\ +188 d c \end{array}$ | Vdc |
| Voltage, Any Pin, Referenced $\mathrm{V}_{\mathrm{EE}}$ | $v$ | $v_{00}^{-0.5+0.5}$ | Vdc |
| DC Current Drain Per Pin | 1 | 10 | Adc |
| Operating Temperature Range | TA | -40 to +85 |  |
| Storage Temperature Range | Tstg | -65 to +150 | ${ }^{\circ} \mathrm{C}$ |


| Recommended Operating Conditions (VSS $=0$ or VEE) |  |  |  |
| :---: | :---: | :---: | :---: |
| PARAMETER | SYMBOL | VALUE | UNIT |
| DC Supply Voltage VDD to Analog Ground | VDD | +5.0 to +8.0 | Vdc |
| $V_{\text {EE }}$ to Analog Ground | Vee | -2.8 to -8.0 |  |
| Clock Frequency | folk | 32 to 400 | kHz |
| Zero Offset Correction Capacitor | Co | $0.1 \pm 20 \%$ | $\mu \mathrm{F}$ |

Note: This device contains circuitry to protect the inputs against damage due to high static voltages or electric fields; however, it is advised that normal precautions be taken to avoid application of any voltage higher than maximum rated voltages to this high impedance circuit. For proper operation it is recommended that $\mathrm{V}_{\text {IN }}$ and VOUT be constrained to the range $\mathrm{V}_{\text {EE }} \leq$ (VIN or VOUT) $\leq$ VDD.
Electrical Characteristics: (CI=0.1 $\mu \mathrm{F}$ mylar, $\mathrm{R}_{\mathrm{I}}=470 \mathrm{k} \Omega @ \mathrm{~V}_{\mathrm{REF}}=2.000 \mathrm{~V}, \mathrm{R}_{\mathrm{I}}=27 \mathrm{k} \Omega @ \mathrm{~V}_{\mathrm{REF}}=200.0 \mathrm{mV} . \mathrm{Co}_{0}=0.1 \mu \mathrm{~F}$, Rc $=300 \mathrm{k} \Omega$; all voltages referenced to Analog Ground, pin 1.)

| CHARACTERISTIC | SYMBOL | $\begin{aligned} & \mathrm{V}_{\mathrm{DD}} \\ & \mathrm{~V}_{\mathrm{dc}} \end{aligned}$ | $\begin{aligned} & \mathrm{V}_{\mathrm{EE}} \\ & \mathrm{~V}_{\mathrm{dc}} \end{aligned}$ | $-40^{\circ} \mathrm{C}$ |  | $25^{\circ} \mathrm{C}$ |  |  | $85^{\circ} \mathrm{C}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | MIN | MAX | MIN | TYP | MAX | MIN | MAX | UNIT |
| Rollover Error (Difference in reading for equal positive and negative reading near Full-Scale) <br> $-\mathrm{VIN}_{\mathrm{IN}}=+\mathrm{V}_{\text {IN }} 200 \mathrm{mV}$ Full-Scale | - |  |  | - | - | -4 | - | +4 | - | - | counts |
| $\begin{aligned} & \text { Output Current - Pins } 14 \text { to } 23 \\ & \left(V_{s s}=0 \mathrm{~V}\right) \end{aligned}$ |  |  |  |  |  |  |  |  |  |  |  |
| $(\mathrm{VOH}=4.6 \mathrm{~V})$ Source | IOH | 5.0 | -5.0 | -0.25 | - | -0.2 | -0.36 | - | -0.16 | - | mA |
| ( $\mathrm{VOL}=0.4 \mathrm{~V}$ ) Sink | IOL | 5.0 | -5.0 | 0.64 | - | 0.51 | 0.88 | - | 0.36 | - | mA |
| $(\mathrm{Vss}=-5.0 \mathrm{~V})$ |  |  |  |  |  |  |  |  |  |  |  |
| ( $\mathrm{VOH}=4.5 \mathrm{~V}$ ) Source <br> ( V OL $=-4.5 \mathrm{~V}$ ) Sink | $\begin{aligned} & \mathrm{IOH} \\ & \mathrm{IOL} \end{aligned}$ | $\begin{aligned} & 5.0 \\ & 5.0 \end{aligned}$ | $\begin{aligned} & -5.0 \\ & -5.0 \end{aligned}$ | $\begin{array}{r} -0.52 \\ 1.3 \end{array}$ | - | $\begin{array}{r} -0.5 \\ 1.3 \end{array}$ | $\begin{aligned} & -0.9 \\ & 2.25 \end{aligned}$ | - | $\begin{array}{r} -0.35 \\ 0.9 \end{array}$ | - | $\begin{aligned} & \mathrm{mA} \\ & \mathrm{~mA} \end{aligned}$ |
| Linearity Output Reading (Note 1) $\left(\mathrm{V}_{\mathrm{REF}}=2.000 \mathrm{~V}\right)$ <br> ( $\mathrm{V}_{\text {REF }}=200.0 \mathrm{mV}$ ) | - | $\begin{aligned} & 5.0 \\ & 5.0 \end{aligned}$ | $\begin{aligned} & -5.0 \\ & -5.0 \end{aligned}$ | - | - | $\begin{array}{r} -0.05- \\ 1 \mathrm{cnt} \end{array}$ | $\pm 0.05$ | $\begin{array}{r} +0.05+ \\ 1 \mathrm{cnt} \end{array}$ | - | - | \%rdg <br> \%rdg |
| $\begin{aligned} & \text { Stability Output Reading (Note 2) } \\ & \left(V x=1.990 \mathrm{~V}, V_{\text {REF }}=2.000 \mathrm{~V}\right) \\ & (V x=199.0 \mathrm{mV}, \\ & \left.V_{\text {REF }}=200.0 \mathrm{mV}\right) \end{aligned}$ | - | 5.0 5.0 | -5.0 -5.0 | - | - | - | - | 3 | - | - | LSD LSD |
| Zero Output Reading $\left(V_{X}=0 \mathrm{~V}, V_{R E F}=2.000 \mathrm{~V}\right)$ | - | 5.0 | -5.0 | - | - | - | 0 | 0 | - | - | LSD |
| Bias Current - |  |  |  |  |  |  |  |  |  |  |  |
| Analog Input | - | 5.0 | -5.0 | - | - | - | $\pm 20$ | $\pm 100$ | - | - | pA |
| Reference Input |  | 5.0 | -5.0 | - | - | - | $\pm 20$ | $\pm 100$ | - | - | pA |
| Analog Ground |  | 5.0 | -5.0 | - | - | - | $\pm 20$ | $\pm 500$ | - | - | pA |
| $\begin{aligned} & \text { Common-Mode Rejection } \\ & \text { (Vx }=1.4 \mathrm{~V}, \mathrm{~V} \text { REF }=2.000 \mathrm{~V}, \\ & \text { foc }=32 \mathrm{kHz}) \end{aligned}$ |  | 5.0 | -5.0 | - | - | - | 65 | - | - | - | dB |
| Output Voltage - Pins 14 to 23 |  |  |  |  |  |  |  |  |  |  |  |
| (1" Level | VOH | 5.0 | -5.0 | 4.95 | - | 4.95 | 5.0 | - | 4.95 | - | V |
| (Vss $=-5.0 \mathrm{~V}$ ) "0" Level | VoL | 5.0 | -5.0 | - | -4.95 | - | -5.0 | -4.95 | - | -4.95 | V |
| "1" Level | VOH | 5.0 | -5.0 | 4.95 | - | 4.95 | 5.0 | - | 4.95 | - | V |
| Clock Frequency (Rc $=300 \mathrm{k}$ ) | fCLK | 5.0 | -5.0 | - | - | - | 66 | - | - | - | kHz |
| Input Current - DU | IDU | 5.0 | -5.0 | - | $\pm 0.3$ |  | . 00001 | $\pm 0.3$ | - | $\pm 1.0$ | $\mu \mathrm{A}$ |
| Quiescent Current (VDD to Vee, Iss =0) | 10 | $\begin{aligned} & 5.0 \\ & 8.0 \end{aligned}$ | $\begin{aligned} & \hline-5.0 \\ & -8.0 \\ & \hline \end{aligned}$ | - | $\begin{aligned} & 3.7 \\ & 7.4 \end{aligned}$ | - | 0.4 1.4 | $\begin{aligned} & 2.0 \\ & 4.0 \end{aligned}$ | - | $\begin{aligned} & 1.6 \\ & 3.2 \end{aligned}$ | $\begin{aligned} & \mathrm{mA} \\ & \mathrm{~mA} \end{aligned}$ |
| Supply Rejection (VDD to VEE, ISS $=0$, $\mathrm{V}_{\text {REF }}=2.000 \mathrm{~V}$ ) | - | 5.0 | -5.0 | - | - | - | 0.5 | - | - | - | mV/V |
| Note: <br> 1. Accuracy - The accuracy of the meter at full-scale is the accuracy of the setting of the reference voltage. Zero is recalculated during each conversion cycle. The meaningful specification is linearity. In other words, the |  |  |  |  | deviation from correct reading for all inputs other than positive full-scale and zero is defined as the linearity specification. <br> 2. Three LSD stability for 200 mV scale is defined as the range that the LSD will occupy $95 \%$ of the time. |  |  |  |  |  |  |

TN TELEDYNE SEMICONDUCTOR

## Pin Description

| $\begin{aligned} & \text { PIN NO. } \\ & \text { 60-Pin } \\ & \text { FP } \end{aligned}$ | $\begin{aligned} & \text { PIN NO. } \\ & \text { 24-PIn } \\ & \text { DIP } \end{aligned}$ | SYMBOL | DESCRIPTION |
| :---: | :---: | :---: | :---: |
| 7 | 1 | VAG | This is the Analog Ground. It has a high input impedance. This pin determines the reference level for the unknown input voltage ( $V_{x}$ ) and the reference voltage (VREF). |
| 10 | 2 | Vref | Reference voltage. Full-scale output is equal to the voltage applied to VreF. Therefore, full-scale voltage of 1.999 V requires 2.000 V reference and 199.9 mV full-scale requires a 200 mV reference. VREF functions as system reset, also. When switched to Vee the system is reset to the beginning of the conversion cycle. |
| 12 | 3 | $\mathrm{V}_{\mathrm{x}}$ | The Unknown Input Voltage $\left(V_{x}\right)$ is measured as a ratio of the reference voltage (VREF) in a ratio-metric A/D conversion. |
| 19 | 4 | $\mathrm{R}_{1}$ | These pins are for external components used for the integration function in the dual slope conversion. Typical values are $0.1 \mu \mathrm{~F}$ (mylar) capacitor for $\mathrm{C}_{1}$. |
| $\begin{aligned} & 22 \\ & 24 \end{aligned}$ | $\begin{aligned} & 5 \\ & 6 \end{aligned}$ | $\begin{gathered} \mathrm{R}_{1} / \mathrm{C}_{1} \\ \mathrm{C}_{1} \end{gathered}$ | $R_{1}=470 \mathrm{k} \Omega$ (resistor) for 2.0 V full-scale. <br> $\mathrm{R}_{1}=27 \mathrm{k} \Omega$ (resistor) for 200 mV full-scale. <br> Clock frequency of 66 kHz gives 250 ms conversion time. See equation below for calculation of integrator component values. |
| $\begin{aligned} & 25 \\ & 26 \end{aligned}$ | $\begin{aligned} & 7 \\ & 8 \end{aligned}$ | $\begin{aligned} & \mathrm{CO}_{1} \\ & \mathrm{CO} 2 \end{aligned}$ | These pins are used for connecting the offset correction capacitor. The recommended value is $0.1 \mu \mathrm{~F}$. |
| 27 | 9 | DU | Display Update input pin. When DU is connected to the EOC output every conversion is displayed. <br> New data will be strobed into the output latches during the conversion cycle if a positive edge is received on DU prior to the ramp-down cycle. When this pin is driven from an external source, the voltage should be referenced to VSs. |
| 34 | 10 | CLK ${ }_{1}$ | Clock input pins. The TSC14433 has its own oscillator system clock. Connecting a single resistor between CLK ${ }_{1}$ and CLK $\mathrm{K}_{0}$ sets the clock frequency. |
| 36 | 11 | CLKo | A crystal or LC circuit may be inserted in lieu of a resistor for improved stability. CLK $_{1}$, the clock input, can be driven from an external clock source, which need only have standard CMOS output drive. This pin is referenced to $V_{E E}$ for external clock inputs. A $300 \mathrm{k} \Omega$ resistor yields a clock frequency of about 66 kHz . (See typical characteristic curves). (See Figure 9 for alternate circuits). |
| 37 | 12 | Vee | Negative Power Supply. Connection pin for the most negative supply. Please note the current for the output drive circuit is returned through Vss. Typical supply current is 0.8 mA . |
| 39 | 13 | Vss | Negative Power Supply for Output Circuitry. This pin sets the low voltage level for the output pins (BCD, Digit Selects, EOC, OR). When connected to analog ground, the output voltage is from analog ground to $V_{D D}$. If connected to $V_{E E}$, the output swing is from VEE to $V_{D D}$. The recommended operating range for $V_{S S}$ is between VDD -3.0 volts and $V_{E E}$. |
| 40 | 14 | EOC | End of Conversion output generates a pulse at the end of each conversion cycle. This generated pulse width is equal to one half the period of the system clock. |
| 41 | 15 | OR | Overrange pin. Normally this pin is set high. When Vx exceeds Vref the OR pin is low. |
| 49 | 16 | DS4 | Digit Select pins. The digit select output goes high when the respective digit is selected. The MSD ( $1 / 2$ digit) turns on immediately after an EOC pulse. |
| 51 | 17 | DS3 | The remaining digits turn on in sequence from MSD to LSD. |
| 52 | 18 | DS2 | To ensure that the BCD data has settled, an inter-digit blanking time of two clock periods is included. |
| 54 | 19 | DS1 | Clock frequency divided by 80 equals multiplex rate. For example a system clock of 66 kHz gives a multiplex rate of 0.8 kHz . |
| 5 | 20 | Qo | See Figure 12 for Digit Select Timing Diagram. |
| 4 | 21 | Q1 | BCD Data Output pins. Multiplexed BCD outputs contain 3 full digits of information during digit select DS2, 3, 4 . |
| $\begin{aligned} & 57 \\ & 55 \end{aligned}$ | $\begin{aligned} & 22 \\ & 23 \end{aligned}$ | $\begin{aligned} & Q_{2} \\ & Q_{3} \end{aligned}$ | During DS1, the $1 / 2$ digit, overrange, underrange and polarity information is available. Refer to Truth Table. |
| 6 | 24 | VDD | Positive Power Supply. This is the most positive power supply pin. |

## Ordering Information

| Part No. | Package | Temperature <br> Range |
| :--- | :--- | ---: |
| TSC14433BCL | 24-pin CerDIP | -40 to $+85^{\circ} \mathrm{C}$ |
| TSC14433BCJ | 24-pin Plastic Dip | -40 to $+85^{\circ} \mathrm{C}$ |
| TSC14433BCBQ | 60-Pin Plastic <br> Flat Package: <br> Formed Leads | -40 to $+85^{\circ} \mathrm{C}$ |


| Part No. | Package | Temperature <br> Range |
| :--- | :--- | ---: |
| TSC14433BCSQ | 60-Pin Plastic <br> Flat Package: <br> Unformed Leads | -40 to $+85^{\circ} \mathrm{C}$ |

## Pin Configuration

|  $\begin{aligned} R_{1} & =\frac{V_{x}(\text { max })}{C_{1}} \times \frac{T}{\Delta V} \\ \Delta V & =V_{D D}-V_{x}(\text { max })-0.5 \\ T & =4000 \times \frac{1}{\text { fCLK }} \end{aligned}$ <br> Where <br> $R_{1}$ is in $k \Omega$ <br> $V_{D D}$ is the voltage at pin 24 referenced to $V_{A G}$ <br> $V_{x}$ is the voltage at pin 3 referenced to $V_{A G}$ <br> folk is the clock frequency at pin 10 in kHz |  |
| :---: | :---: |

## 3 1/2 Digit CMOS

- Low Cost
- Multiplexed BCD Data


## Typical Applications

TSC7212A Interface to TSC14433B 3 1/2 Digit ADC.


## Package Information



## General Description

The TSC14433 is a low power, high-performance, monolithic CMOS $31 / 2$ digit A/D converter. The TSC14433 combines both analog and digital circuits on a single IC, thus minimizing the number of external components. This dual slope A/D converter provides automatic polarity and zero correction with the addition of two external resistors and two capacitors. The full-scale voltage range of this ratiometric IC extends from 199.9 millivolts to 1.999 volts. The TSC14433B can operate over a wide range of power supply voltages including batteries and standard 5 volt supplies.
The high impedance MOS analog inputs are well suited for applications using current, resistance or voltmeters. The output drive is compatible with low power Schottky TTL loads and conforms to standard B-series CMOS.

The TSC14433 will interface with the TSC7211A (LCD), TSC7212A (LED) and TSC700A (high LED current drive) display drivers.

HANDLING PRECAUTIONS: These devices are CMOS and must be handled correctly to prevent damage. Package and store only in conductive foam, anti-static handling procedures. Do not connect in circuits under "power on" conditions, as high transients may cause permanent damage.

## Features

- Accuracy: $\pm 0.05 \%$ of Reading $\pm 1$ Count
- Two Voltage Ranges: 1.999 V and 199.9 mV
- Up to 25 Conversions Per Second
- $Z_{\text {IN }}>1000 \mathrm{M} \mathrm{Ohm}$
- Single Positive Voltage Reference
- Standard B-Series CMOS Outputs - Drives One Low Power Schottky load
- Uses On-chip System Clock, or External Clock
- Low Power Consumption: 8.0 mW Typical @ $\pm 5.0 \mathrm{~V}$
- Wide Supply Range: e.g., $\pm 4.5 \mathrm{~V}$ to $\pm 8.0 \mathrm{~V}$
- Overrange and Underrange Signals Available
- Operates in Auto Ranging Circuits
- Operates With LED and LCD Displays
- Low External Component Count
- Available in Compact Flat Package


## Applications

- Portable Instruments
- Digital Voltmeters
- Digital Panel Meters
- Digital Scales
- Digital Thermometers
- Remote A/D Sensing Systems
- MPU Systems
- See Application Notes 19 and 21

Block Diagram


TSC14433

Absolute Maximum Ratings

| RATING | SYMBOL | VALUE | UNIT |
| :--- | :--- | ---: | ---: |
| DC Supply Voltage | VDD to | -0.5 to | Vdc |
| Voltage, Any Pin, <br> Referenced to VEE | V | -0.5 to | Vdc |
| DC Current | V | $\mathrm{VDD}^{+0.5}$ | Va |
| Drain Per Pin | mAdc |  |  |
| Operating Tempera- <br> ture Range | $\mathrm{TA}_{\mathrm{A}}$ | -40 to +85 | ${ }^{\circ} \mathrm{C}$ |
| Storage Tempera- <br> ture Range | TSTG | -65 to +150 | ${ }^{\circ} \mathrm{C}$ |

Recommended Operating Conditions
(VSS = 0 or $\mathrm{V}_{\mathrm{EE}}$ )

| PARAMETER | SYMBOL | VALUE | UNIT |
| :---: | :---: | :---: | :---: |
| DC Supply Voltage - |  |  |  |
| VDD to Analog Ground | VDD | +5.0 to +8.0 | Vdc |
| $V_{\text {EE }}$ to Analog Ground | Vee | -2.8 to -8.0 |  |
| Clock Frequency | fclk | 32 to 400 | kHz |
| Zero Offset Correction Capacitor | Co | $0.1 \pm 20 \%$ | $\mu \mathrm{F}$ |

Note: This device contains circuitry to protect the inputs against damage due to high static voltages or electric fields; however, it is advised that normal precautions be taken to avoid application of any voltage higher than maximum rated voltages to this high impedance circuit. For proper operation it is recommended that $\mathrm{V}_{\text {IN }}$ and $\mathrm{V}_{\text {OUT }}$ be constrained to the range $\mathrm{V}_{\mathrm{EE}} \leq$ (VIN or $\mathrm{V}_{\text {OUT }}$ ) $\leq$ VDD.

Electrical Characteristics: ( $C_{I}=0.1 \mu \mathrm{~F}$ mylar, $\mathrm{R}_{I}=470 \mathrm{k} \Omega @ \mathrm{~V}_{\text {REF }}=2.000 \mathrm{~V}, \mathrm{R}_{\mathrm{I}}=27 \mathrm{k} \Omega @ \mathrm{~V}_{\text {REF }}=200.0 \mathrm{mV}, C_{0}=0.1 \mu \mathrm{~F}$, $\mathrm{Rc}=300 \mathrm{k} \Omega$; all voltages referenced to Analog Ground, pin 1.)

| CHARACTERISTIC | SYMBOL | $\begin{aligned} & \mathrm{V}_{\mathrm{DD}} \\ & \mathrm{~V}_{\mathrm{dc}} \end{aligned}$ | $\begin{aligned} & \mathrm{V}_{\mathrm{EE}} \\ & \mathrm{~V}_{\mathrm{dc}} \end{aligned}$ | $-40^{\circ} \mathrm{C}$ |  | $25^{\circ} \mathrm{C}$ |  |  | $85^{\circ} \mathrm{C}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | MIN | MAX | MIN | TYP | MAX | MIN | MAX | UNIT |
| $\begin{aligned} & \text { Linearity Output Reading (Note 1) } \\ & (\text { VREF }=2.000 \mathrm{~V}) \\ & \left(\text { VREF }^{2}=200.0 \mathrm{mV}\right) \end{aligned}$ | - | 5.0 5.0 | -5.0 -5.0 | - | - | -0.05 count | +0.05 | $\begin{aligned} & +0.05 \\ & \text { count } \end{aligned}$ | - | - | \%rdg |
| $\begin{aligned} & \hline \text { Stability Output Reading (Note 2) } \\ & \left(V x=1.990 \mathrm{~V}, V_{\text {REF }}=2.000 \mathrm{~V}\right) \\ & \left(V_{x}=199.0 \mathrm{mV},\right. \\ & \left.V_{\text {REF }}=200.0 \mathrm{mV}\right) \end{aligned}$ | - | 5.0 5.0 | -5.0 -5.0 | - | - | - | - | 3 | - | - | $\begin{aligned} & \text { LSD } \\ & \text { LSD } \end{aligned}$ |
| Zero Output Reading $\left(V_{x}=0 \mathrm{~V}, V_{\text {REF }}=2.000 \mathrm{~V}\right)$ | - | 5.0 | -5.0 | - | - | - | 0 | 0 | - | - | LSD |
| Bias Current - |  |  | $\begin{aligned} & -5.0 \\ & -5.0 \\ & -5.0 \end{aligned}$ |  |  |  |  |  |  |  |  |
| Analog Input | - | $\begin{aligned} & 5.0 \\ & 5.0 \\ & 5.0 \\ & \hline \end{aligned}$ |  | 二 | - | - | $\begin{aligned} & \pm 20 \\ & \pm 20 \\ & \pm 20 \\ & \hline \end{aligned}$ | $\begin{aligned} & \pm 100 \\ & \pm 100 \\ & \pm 500 \end{aligned}$ | - | - | pApApA |
| Reference Input |  |  |  |  |  | - |  |  | - |  |  |
| Analog Ground |  |  |  | - | - | - |  |  | - |  |  |
| $\begin{aligned} & \text { Common-Mode Rejection } \\ & (\mathrm{Vx}=1.4 \mathrm{~V}, \mathrm{VREF}=2.000 \mathrm{~V}, \\ & \text { foc }=32 \mathrm{kHz} \text {, } \end{aligned}$ |  | 5.0 | -5.0 | - | - | - | 65 | - | - | - | dB |
| Output Voltage - Pins 14 to 23 |  |  |  |  |  |  |  |  |  |  |  |
| (1) "1" Level | Vor | 5.0 | -5.0 | 4.95 | , | 4.95 | 5.0 | - | 4.95 | - | V |
| (Vss =-5.0 V) "0" Level | VoL | 5.0 | -5.0 | - | -4.95 | - | -5.0 | -4.95 | - | -4.95 | V |
| "1" Level | VOH | 5.0 | -5.0 | 4.95 | - | 4.95 | 5.0 | - | 4.95 | - | V |
| $\begin{aligned} & \text { Output Current — Pins } 14 \text { to } 23 \\ & (\text { Vss }=0 \mathrm{~V}) \end{aligned}$ |  |  |  |  |  |  |  |  |  |  |  |
| ( $\mathrm{VOH}=4.6 \mathrm{~V}$ ) Source | IOH | 5.0 | -5.0 | -0.25 | - | -0.2 | -0.36 | - | -0.14 | - | mA |
| ( $\mathrm{VOL}=0.4 \mathrm{~V}$ ) Sink | loL | 5.0 | -5.0 | 0.64 | - | 0.51 | 0.88 | - | 0.36 | - | mA |
| (Vss $=-5.0 \mathrm{~V}$ ) $\mathrm{V}^{\text {(V) }}$ |  |  |  |  |  |  |  |  |  |  |  |
| $(\mathrm{VOH}=4.5 \mathrm{~V})$ Source | ${ }^{\mathrm{IOH}}$ | 5.0 | -5.0 | -0.62 | - | -0.5 | -0.9 | - | -0.35 | - | $\begin{aligned} & \mathrm{mA} \\ & \mathrm{~mA} \end{aligned}$ |
| ( $\mathrm{VOL}=-4.5 \mathrm{~V}$ ) Sink | 10 | 5.0 | -5.0 | 1.6 | - | 1.3 | 2.25 | - | 0.9 | - |  |
| Clock Frequency ( $\mathrm{Rc}=300 \mathrm{k} \Omega$ ) | fCLK | 5.0 | -5.0 | - | - | - | 66 | - | - | - | kHz |
| Input Current - DU | IDU | 5.0 | -5.0 | - | $\pm 0.3$ |  | 0.00001 | $\pm 0.3$ | - | $\pm 1.0$ | $\mu \mathrm{A}$ |
| Quiescent Current | 10 | 5.0 | -5.0 | - | 3.7 | - | 0.9 | 2.0 | - | 1.6 | mA |
| ( $\mathrm{V}_{\mathrm{DD}}$ to $\mathrm{V}_{\text {EE, }}$ Iss $=0$ ) |  | 8.0 | -8.0 | - | 7.4 | - | 1.8 | 4.0 | - | 3.2 | mA |
| $\begin{aligned} & \text { Supply Rejection } \\ & \text { (VDD to } V_{\text {EE }} \text { Iss }=0, \\ & V_{\text {REF }}=2.000 \mathrm{~V} \text { ) } \\ & \hline \end{aligned}$ | - | 5.0 | -5.0 | - | - | - | 0.5 | - | - | - | mV/V |

## Note:

1. Accuracy - The accuracy of the meter at full-scale is the accuracy of the setting of the reference voltage. Zero is recalculated during each conversion cycle. The meaningful specification is linearity. In other words, the deviation from correct reading for all inputs other than positive full-scale and
zero is defined as the linearity specification
2. Three LSD stability for 200 mV scale is defined as the range that the LSD will occupy $95 \%$ of the time
3. Pin numbers refer to 24 -pin DIP.

| $\begin{gathered} \hline \text { PIN NO. } \\ 60-\mathrm{Pin} \\ \text { FP } \end{gathered}$ | $\begin{gathered} \text { PIN NO. } \\ \text { 24-Pin } \\ \text { DIP } \end{gathered}$ | SYMBOL | DESCRIPTION |
| :---: | :---: | :---: | :---: |
| 7 | 1 | $V_{\text {AG }}$ | This is the Analog Ground. It has a high input impedance. This pin determines the reference level for the unknown input voltage $\left(V_{x}\right)$ and the reference voltage (VREF). |
| 10 | 2 | VREF | Reference voltage. Full-sca!e output is equal to the voltage applied to Vref. Thereiore, full-scale voltage of 1.999 V requires 2.000 V reference and 199.9 mV full-scale requires a 200 mV reference. VREF functions as system reset, also. When switched to VEE the system is reset to the beginning of the conversion cycle. |
| 12 | 3 | Vx | The Unknown Input Voltage ( $\mathrm{V} x$ ) is measured as a ratio of the reference voltage ('/REF) in a ratio-metric A/D conversion. |
| 19 | 4 | $\mathrm{R}_{1}$ | These pins are for external components used for the integration function in the dual slope conversion. Typical values are $0.1 \mu \mathrm{~F}$ (mylar) capacitor for $\mathrm{C}_{1}$. |
| $\begin{aligned} & 22 \\ & 24 \end{aligned}$ | $\begin{aligned} & 5 \\ & 6 \end{aligned}$ | $\begin{gathered} \mathrm{R}_{1} / \mathrm{C}_{1} \\ \mathrm{C}_{1} \end{gathered}$ | $\mathrm{R}_{1}=470 \mathrm{k} \Omega$ (resistor) for 2.0 V full-scale. <br> $\mathrm{R}_{1}=27 \mathrm{k} \Omega$ (resistor) for 200 mV full-scale. <br> Clock frequency of 66 kHz gives 250 ms conversion time. See equation below for calculation of integrator component values. |
| $\begin{aligned} & 25 \\ & 26 \end{aligned}$ | $\begin{aligned} & 7 \\ & 8 \end{aligned}$ | $\begin{aligned} & \mathrm{CO}_{1} \\ & \mathrm{CO}_{2} \end{aligned}$ | These pins are used for connecting the offset correction capacitor. The recommended value is $0.1 \mu \mathrm{~F}$. |
| 27 | 9 | DU | Display Update input pin. When DU is connected to the EOC output every conversion is displayed. <br> New data will be strobed into the output latches during the conversion cycle if a positive edge is received on DU prior to the ram-down cycle. When this pin is driven from an external source, the voltage should be referenced to Vss. |
| 34 | 10 | CLK ${ }_{1}$ | Clock input pins. The TSC14433 has its own oscillator system clock. Connecting a single resistor between CLK ${ }_{1}$ and CLK 0 sets the clock frequency. |
| 36 | 11 | CLKo | A crystal or LC circuit may be inserted in lieu of a resistor for improved stability. CLK 1 , the clock input, can be driven from an external clock source, which need only have standard CMOS outpui drive. This pin is referenced to $V_{E E}$ for external clock inputs. A $300 \mathrm{k} \Omega$ resistor yields a clock frequency of about 66 kHz . (See typical chacacteristic curves). (See Figure 9 for alternate circuits). |
| 37 | 12 | Vee | Negative Power Supply. Comnection pin for the most negative supply. Please note the current for the output drive circuit is returned through Vss. Typical supply current is 0.8 mA . |
| 39 | 13 | Vss | Negative Power Supply for Jutput Circuitry. This pin sets the low voltage level for the output pins (BCD, Digit Selects, EOC, OR). When connected to analog ground, the ou put voltage is from analog grourid to $V_{D D}$. If connected to $V_{E E}$, the output swing is fron $V_{E E}$ to $V_{D D}$. The recommended operating range for $V_{S S}$ is between VDD -3.0 volts and $V_{E E}$. |
| 40 | 14 | EOC | End of Conversion output generates a pulse at the end of each conversion cycle This generated pulse width is equal to one half the perind of the system clock. |
| 41 | 15 | OR | Overrange pin. Normally this pin is set high. When Vx exceeds Vref the OR pin is low. |
| 49 | 16 | $\mathrm{DS}_{4}$ | Digit Select pins. The digit select output goes high when the respective digit is selected. The MSD ( $1 / 2 \mathrm{digit}$ ) turns on immediately after an EOC pulse. |
| 51 | 17 | DS3 | The remaining digits turn on in sequence from MSD to LSD. |
| 52 | 18 | DS2 | To ensure that the BCD data has settled, an inter-digit blanking time of two clock periods is included. |
| 54 | 19 | DS 1 | Clock frequency divided by 80 equals multiplex rate. For example a system clock of 66 kHz gives a multiplex rate of 0.8 kHz . |
| 5 | 20 | Qo | See Figure 12 for Digit Select Timing Diagram. |
| 4 | 21 | Q1 | BCD Data Output pins. Multiplexed BCD outputs contain 3 full digits of information during digit select DS2, 3, 4 . |
| $\begin{aligned} & 57 \\ & 55 \end{aligned}$ | $\begin{aligned} & 22 \\ & 23 \end{aligned}$ | $\begin{aligned} & Q_{2} \\ & Q_{3} \end{aligned}$ | During DS1, the $1 / 2$ digit, overrange, underrange and polarity information is availabie. Refer to Truth Table. |
| 6 | 24 | VDD | Positive Power Supply. This is the most positive power supply pin. |

Negative Power Supply for Jutput Circuitry. This pin sets the low voltage level for the output pins (BCD, Digit Selects, EOC, OR). When connected to analog ground, the output


End of Conversion output generates a pulse at the end of each conversion cycle This generated pulse width is equal to one half the perind of the system clock.
Overrange pin. Normally this pin is set high. When $V_{x}$ exceeds $V_{r e f}$ the OR pin is low.
Digit Select pins. The digit select output goes high when the respective digit is selected.
The MSD ( $1 / 2$ digit) turns on immediately after an EOC pulse.
The remaining digits turn on in sequence from MSD to LSU.
To ensure that the BCD data has settled, an inter-digit blanking time of two clock periods is
Clock frequency divided by 80 equals multiplex rate. For example a system clock of 66 kHz gives a multiplex rate of 0.8 kHz .

Figure 12 for Digit Select Timing Diagram. during digit select DS2, 3, 4.
During DS1, the $1 / 2$ digit, overrange, underrange and polarity information is available. Positive Power Supply. This is the most positive power supply pin.

## Ordering Information

| Part No. | Package | Temperature <br> Range |
| :--- | :--- | ---: |
| TSC14433CJ | 24-pin Plastic Dip | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
| TSC14433CL | 24-pin CerDIP | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
| TSC14433CBQ | 60-Pin Plastic <br> Flat Package: <br> Formed Leads | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |


| Part No. | Package | Temperature <br> Range |
| :--- | :--- | :--- |
| TSC14433CSQ | 60-Pin Plastic <br> Flat Package: <br> Unformed Leads | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
| Devices with 160, Hour, $+125^{\circ} \mathrm{C}$ Burn-In |  |  |
| TSC14433CJ/BI | 24-Pin Plastic Dip | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
| TSC14433CL/BI | 24-Pin CerDIP | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |

## Pin Configuration



## Typical Characteristics



Figure 1: Typical Rollover Error vs. Power Supply Skew.


Figure 2: Typical Quiescent Power Supply Current vs. Temperature.

## Typical Characteristics (Cont.)



Figure 3: Typical N-Channel Sink Current at VDD-VSS $=5$ Volts.


Figure 5: Typical Clock Frequency vs. Resistor (Rc).


Figure 4: Typical P-Channel Source Current at VDD $-V_{S S}=5$ Volts.


Figure 6: Typical \% Change of Clock Frequency vs. Temperature.

| CONVERSION RATE $=\frac{\text { CLOCK FREQUENCY }}{16,400} \pm 1.5 \%$ |
| :--- |
| MULTIPLEX RATE $=\frac{\text { CLOCK FREQUENCY }}{80}$ |

## Circuit Description

The TSC14433 CMOS IC becomes a modified dual slope A/D with a minimum of external components. This IC has the customary CMOS digital logic circuitry as well as the CMOS analog circuitry. It provides the user with digital functions (Such as counters, latches, multiplexers ) and analog functions (such as operational amplifiers and comparators) on a single chip.
Features of this sytem include auto-zero, high input impedances and autopolarity. Low power consumption and a
wide range of power supply voltages are also advantages of this CMOS device. The system's auto-zero function compensates for the offset voltage of the internal amplifiers and comparators. In this "ratiometric system," the output reading is the ratio of the unknown voltage to the reference voltage where a ratio of 1 equal to the maximum count of 1999. It takes approximately 16,000 clock periods to complete one conversion cycle. Each conversion cycle may be divided into six segements. Figure 7 shows the conversion cycle in 6 segments for both positive and negative inputs.
Segment 1 - The offset capacitor (Co), which compensates


Figure 7: Integrator Waveforms at Pin 6.
for the input offset voltages of the buffer and integrator amplifiers, is charged during this period. However, the integrator capacitor is shorted. This segment requires 4000 clock periods.
During Segment 2 - The integrator output decreases to the comparator threshold voltage. At this time a number of counts equivalent to the input offset voltage of the comparator is stored in the offset latches for later use in the auto-zero process. The time for this segment is variable, and less than 800 clock periods.
Segment 3 - This segment of the conversion cycle is the same as Segment 1.


Figure 8: Equivalent Circuit Diagrams of the Analog Section During Segment 4 of the Timing Cycle.

Segment 4 - Segment 7 is an up-going ramp cycle with the unknown input voltage $(\mathrm{Vx})$ as the input to the integrator. Figure 8 shows the equivalent configuration of the analog section of the TSC14433. The actual configuration of the analog section is dependent upon the polarity of the input voltage during the previous conversion cycle.

Segment 5 - this segment is a down-going ramp period with the reference voltage as the input to the integrator. Segment 5 of the conversion cycle has a time equal to the number of counts stored in the offset storage latches during Segment 2. As a result, the system zeros automatically.
Segment 6 - This is an extension of Segment 5. The time period for this portion is 4000 clock periods. The results of the A/D conversion cycle are determined in this portion of the conversion cycle.


Figure 9: Alternate Oscillator Circuits.

## Applications Information

Figure 10 is an example of a $31 / 2$ digit voltmeter using the TSC14433 with common-anode displays. This system require a 2.5 V reference. Full-scale may be adjusted to 1.999 V or 199.9 mV . Input overrange is indicated by flashing a display:

This display uses LEDs with common anode digit lines. Power supply for this system is shown as a dual $\pm 5 \mathrm{~V}$ supply; however, the TSC14433 will operate over a wide voltage range (see recommended operating conditions, page 3).

## 3 1/2 Digit ADC

- Multiplexed BCD Data
- Low Power


Figure 10: 3 1/2 Digit Voltmeter-Common Anode Displays, Flashing Overrange


Figure 11: 3 1/2 Digit Voltmeter with LCD Display.


Figure 12: Digit Select Timing Diagram

The circuit in Figure 11 shows a $31 / 2$ digit LCD voltmeter. The 14024B provides the low frequency square wave signal drive to the LCD backplane. Dual power supplies are shown here, however, one supply may be used when Vss is connected to $\mathrm{V}_{\mathrm{Ee}}$. In this case $\mathrm{V}_{\mathrm{Ag}}$ must be at least 2.8 V above VEE.
When only segment $b$ and $c$ of the decoder are connected to the $1 / 2$ digit of the display, $4,0,7$ and 3 appear as 1 .

The overrange indication ( $\mathrm{Q} 3=0$ and $\mathrm{Q} 0=1$ ) occurs when the count is greater than 1999, e.g., 1.999 V for a reference of 2.000 V . The underrange indication, useful for autoranging circuits, occurs when the count is less than 180, e.g., 0.180 V for a reference of 2.000 V .

CAUTION: If the most significant digit is connected to a display other than a " 1 " only; such as a full digit display, segments other than $b$ and $c$ must be disconnected. The BCD to seven segment decoder must blank on BCD inputs 1010 to 1111.

TRUTH TABLE

| CODED CONDITION <br> OF MSD | Q3 | Q2 | Q1 | Q0 | BCD TO 7 SEGMENT <br> DECODING |
| :---: | :---: | :---: | :---: | :---: | :---: |
| +0 | 1 | 1 | 1 | 0 | Blank |
| -0 | 1 | 0 | 1 | 0 | Blank |
| +0 UR | 1 | 1 | 1 | 1 | Blank |
| -0 UR | 1 | 0 | 1 | 1 | Blank |
| +1 | 0 | 1 | 0 | 0 | $4 \rightarrow 1$ |
| -1 | 0 | 0 | 0 | 0 | $0 \rightarrow 1$ |
| Hook Up |  |  |  |  |  |
| +1 OR | 0 | 1 | 1 | 1 | $7 \rightarrow 1$ |
| only seg b |  |  |  |  |  |
| -1 and c to |  |  |  |  |  |
| -10 | 0 | 1 | 1 | $3 \rightarrow 1$ | MSD |

## Notes for Truth Table

Q3 - $1 / 2$ digit, low for " 1 ", high for " 0 "
Q2 - Polarity: " 1 " = positive, " 0 " = negative
Q0 - Out of range condition exists if $Q 0=1$. When used in conjunction with Q3 the type of out of range condition is indicated, i.e., Q3 $=0 \mapsto \mathrm{OR}$ or Q3 $=1 \rightarrow$ UR


Figure 13: Demultiplexing for TSC14433 BCD Data.


Figure 14: 3 1/2 Digit Voltmeter with Low Component Count using Common Cathode Displays.


Figure 15: TSC7212A Interface to TSC14433 3 1/2 Digit ADC.

Figure 14 is an example of a $3 \Upsilon / 2$ digit LED voltmeter with a minimum of external components (only 11 additional components). In this circuit the 14511B provides the segment drive and the 75492 or 1413 provides sink for digit current Display is blanked during the ovarrange condition.

## 3 1/2 Digit ADC

- Multiplexed BCD Data
- Low Power


## Package Information



Notes


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## General Description

The CMOS TSC500 contains all the analog circuits needed to construct an integrating analog-to-digital converter. The analog input buffer, integrator, analog switches, comparator and phase control logic are all on chip. Resolution to $41 / 2$ digits (1 part in 20,000) is possible.
The dual slope converter uses time to quantize the analog input signal. A microprocessor and software routine perform the digital function of "counting clocks" for the dual slope integrating converter process. The user can control resolution and conversion speed through software. The TSC500 analog building block can be used to construct an 8-bit or high resolution 14-bit converter by modifying software routines.
A microprocessor controls the TSC500 through the A and B logic input signals. Four TSC500 phases are possible: autozero, signal integrate, reference integrate (deintegrate), and integrator zero output.
The TSC500 comparator output provides polarity and integrator zero crossing information. The comparator output always makes a high to low transition when the integrator crosses zero. This signals the end of a conversion to the processor.
A precision dual slope integrating converter with automatic zero scale offset voltage and drift correction requires only a reference, two capacitors, a resistor and a microprocessor

## Features

- Differential Analog Input
- Differential Reference
- Low Linearity Error ................................. . . . $0.005 \%$
- Fast Zero-Crossing Comparator ..................... $4 \mu \mathrm{~s}$
- Low Power Dissipation ............................ 10 mW
- Auto-Zero Cycle Eliminates Zero-Scale Error \& Drift
- Zero Integrator Phase Speeds Recovery From Over-range Input Signals
- Automatic Internal Polarity Detection
- Low Input Current

15 pA Max

- Wide Analog Input Voltage
... . $\pm 4.2 \mathrm{~V}$
- Microprocessor Control of Dual Slope ADC Conversion
controller. The TSC500 contains the analog circuits needed to construct a dual slope integrating converter with an auto-zero phase. A zero-integrator output phase can be selected to eliminate errors caused by out-of-range input signals. The zero integrator phase makes the next conversion after an out-of-range conversion accurate.
The CMOS TSC500 operates from $\pm 5 \mathrm{~V}$ supplies. Power dissipation is only 10 mW . Leakage currents at the differential inputs are a low 10 pA . The TSC500 differential reference inputs allow easy ratiometric measurements.

Functional Diagram

Absolute Maximum Ratings
Supply ( $V_{s}^{+}$to $V_{\bar{s}}^{-}$) ..... 18 V
Positive Supply Voltage ( $\mathrm{V}_{s}^{+}$to Gnd ) ..... 12 V
Negative Supply Voltage ( $V_{s}^{-}$to $\operatorname{Gnd}$ ) ..... $-12 \mathrm{~V}$
Analog Input Voltage ( $\mathrm{V}^{+}$or $\mathrm{ViN}^{-}$)$\ldots \ldots . . . . . . V_{s}^{+}$to $V s$
$V_{s}^{+}+0.3 V$ to ${ }^{-}$nd $-0.3 V$

Package Power Dissipation
Ambient Operating Temperature Range
CerDIP Package ( $\qquad$ $-25^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$
Plastic Package (C) ........................ $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$
Storage Temperature ....................... $-55^{\circ} \mathrm{C}$ to $150^{\circ} \mathrm{C}$ Lead Soldering Temperature ( 60 seconds) ........ $+300^{\circ} \mathrm{C}$

Electrical Specifications: $T_{A}=25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{S}}= \pm 5 \mathrm{~V}$ unless otherwise specified. $\mathrm{C}_{\mathrm{AZ}}=\mathrm{C}_{\text {REF }}=1.0 \mu \mathrm{f}$.


Electrical Specifications: $T_{A}=25^{\circ} \mathrm{C}, \mathrm{V}_{S}= \pm 5 \mathrm{~V}$ unless otherwise specified. $C_{A Z}=C_{R E F}=1.0 \mu$. (Cont.)

| TYPE | NO. | SYMBOL | PARAMETER | TEST CONDITIONS | MIN | $\begin{gathered} \text { TSC500 } \\ \text { TYP } \end{gathered}$ | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} P \\ O \\ \mathbf{W} \\ \mathbf{E} \\ \mathbf{R} \end{gathered}$ | 23 | Is | Supply Current | $\mathrm{V}_{\mathrm{S}}= \pm 5 \mathrm{~V}, \mathrm{~A}=0, \mathrm{~B}=1$ | - | 1.0 | 1.5 | mA |
|  | 24 | PD | Power Dissipation | $\mathrm{V}_{\mathrm{S}}= \pm 5 \mathrm{~V}$ | - | - | 15 | mW |
|  | 25 | $\mathrm{V}_{s}^{+}$ | Positive Supply Operating Voltage Range |  | 4 | - | 10 | V |
|  | 26 | $v_{s}^{-}$ | Negative Supply Operating Voltage Range |  | -3 | - | -8 | V |
|  | 27 | $V_{s}^{+}-V_{s}^{-}$ | Supply Operating Voltage Range |  | 7 | - | 15 | V |

## Notes:

1.) Integrate time $=10,000 T_{p}$, Auto-Zero Time $=10,000 T_{p}$, Full-Scale Deintegrate Time $=20,000 \mathrm{Tp}, \mathrm{TP}_{\mathrm{P}}=8.3 \mu \mathrm{~s}$ (3.0 Conversions/Second) $\mathrm{V}_{\mathrm{FS}}=2.0 \mathrm{~V}$, $\mathrm{CINT}=0.33 \mu \mathrm{f}$, RINT $=125 \mathrm{k} \Omega$

## Ordering Information

| Part No. | Package | Temperature <br> Range | System <br> Resolution |
| :--- | :--- | :--- | ---: |
| TSC500CPE | $16-P i n$ <br> Plastic Dip | $0^{\circ} \mathrm{C}$ to $70^{\circ} \mathrm{C}$ | 4$4 / 2$ Digits <br> $(50 \mathrm{ppm})$ |
| TSC500IJE | $16-$ Pin <br> CerDIP | $-25^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | $41 / 2$ Digits <br> $(50 \mathrm{ppm})$ |

## TSC500 Operation Theory

The TSC500 incorporates a system zero and integrator output voltage zero phase to the normal two phase dual slope measurement cycle. Reduced system errors, fewer calibration steps and a shorter over-range recovery time result.
The TSC500 measurement cycle can use all four phases if desired.

- System Zero
- Analog Input Signal Integration
- Reference Voltage Integration (Deintegrate Phase)
- Integrator Output Zero

Internal analog gate status is shown in Table 1 for each phase.
Table 1: Internal Analog Gate Status
Conversion


> Output Zero $(A=B=0)$

Note: *Assumes a positive polarity input signal. SW ${ }_{R}^{-}$I would be closed for a negative input signal.
2.) End Point Linearity at, $\pm 1 / 4, \pm 1 / 2, \pm 3 / 4$ FS after Full-Scale Adjustment.

## Pin Configuration



## System Zero Phase

During this phase errors due to buffer, integrator and comparator offset voltages are compensated for by charging CAZ (auto-zero capacitor) with a compensating error voltage. With a zero input voltage the integrator output will remain at zero.
The external input signal is disconnected from the internal circuitry by opening the two SW, switches. The internal input points connect to analog common. The reference capacitor charges to the reference voltage potential through SWR. A feedback loop, closed around the integrator and comparator, charges the CAZ capacitor with a voltage to compensate for buffer amplifier, integrator and comparator offset voltages.

## Analog Input Signal Integration Phase

The TSC500 integrates the differential voltage between the + Input and - Input. The differential voltage must be within the device common-mode range.
The input signal polarity is normally checked via software at the end of this phase.

## Reference Voltage Deintegration

The previously charged reference capacitor is connected with the proper polarity to ramp the integrator output back to zero.

## Integrator Output Zero

This phase guarantees the integrator output is at zero volts when the system zero phase is entered and that the true system offset voltages are compensated. It is normally used when the input has been over-ranged. The phase is not necessary for operation if over-range inputs do not occur or recovery time is not a system consideration.

## TSC500 Analog Section

## Differential Inputs (ViN [Pin 11], Vī [Pin 10])

The TSC500 operates with differential voltages within the input amplifier common-mode range. The input amplifier common-mode range extends from 0.8 V below the positive supply to 0.8 V above the negative supply. Within this common-mode voltage range a common-mode rejection ratio is typically 80 dB . Full accuracy is maintained, however, when the inputs are no more than 1.5 V from either supply.

The integrator output also follows the common-mode voltage. The integrator output must not be allowed to saturate. A worst case condition exists, for example, when a large positive common-mode voltage with a near full-scale negative differential input voltage is applied. The negative input signal drives the integrator positive when most of its swing has been used up by the positive common-mode voltage. For these critical applications the integrator swing can be reduced. The integrator output can swing within 0.9 volts of either supply without loss of linearity.

## Analog Common (Pin 5)

Analog common is used as the Vin return during system-zero and reference deintegrate. If ViN is different from analog common, a common-mode voltage exists in the system. This signal is rejected by the excellent CMRR of the converter. In most applications, Vin will be set at a fixed known voltage (power supply common, for instance). A common-mode voltage will exist when Vin is not connected to analog common.

## Differential Reference (REFHIPin 9, REFLOPin 8)

The reference voltage can be generated anywhere within the power supply voltage of the converter. Roll-over error is caused by the reference capacitor losing or gaining charge due to stray capacitance on its nodes. The difference in reference for ( + ) or ( - ) input voltages will cause a roll-over error. This error can be minimized by using a large reference capacitor in comparison to the stray capacitance. A $1 \mu f$ capacitor is suitable.

## Phase Control Inputs (A [Pin 12], B[Pin 13])

The $A, B$ unlatched logic inputs select the TSC500 operating phase. The A, B inputs are normally driven by a microprocessor I/O port or peripheral input/output chip.

## Comparator Output

By monitoring the comparator output during the fixed signal integrate time the input signal polarity can be determined by the microprocessor controlling the conversion. The comparator output is high for positive signals and low for negative signals during the signal integrate phase (Figure 2).

During the variable reference deintegrate phase the comparator output will make a high to low transition as the integrator output ramp crosses zero. This indicates the conversion is complete. The transition can be used to interrupt the processor controlling the conversion.
The internal comparator delay is $4 \mu \mathrm{sec}$ typically.
Figure 2 shows the comparator output for large positive and negative signal inputs. For signal inputs at or near zero volts, however, the integrator swing is nonexistent. If commonmode noise is present, the comparator can switch several times during the signal integrate period. To ensure that the polarity reading is correct, the comparator output should be read and stored at the end of Signal Integrate.

## TSC500 Comparator Output

| Input <br> Signal | Operating <br> Phase | Comparator <br> Output |
| :--- | ---: | ---: |
| Positive | Signal <br> Integrate | Logic 1 |
| Negative | Signal <br> Integrate | Logic 0 |
| Positive | Reference <br> Deintegrate | Logic 1 to 0 <br> Transition At <br> Zero-Crossing |
| Negative | Reference <br> Deintegrate | Logic 1 to 0 <br> Transition At <br> Zero-Crossing |



Figure 2: Comparator Output

## Integrating Converter <br> Analog Processor

- Automatic Zero Adjust
- $\mu$ Processor Controlled


## Component Value Selection Integrating Resistor (Rint)

The desired full-scale input voltage and output current capability of the input buffer and integrator amplifier set the integration resistor value. The internal class A output stage amplifiers will supply a $20 \mu \mathrm{~A}$ drive current with minimal linearity error. RINT is easily calculated for a $20 \mu \mathrm{~A}$ full-scale current:

RINT $(M \Omega)=$ $\qquad$ 20

## Reference Capacitor (Cref)

A $1.0 \mu \mathrm{~F}$ capacitor is suggested. Larger values may be used to limit roll-over errors. Low leakage capacitors such as polypropylene are suggested.

## Auto Zero Capacitor ( $\mathrm{C}_{\text {az }}$ )

A $1.0 \mu \mathrm{~F}$ polypropylene capacitor is suggested.

## Integrating Capacitor (Cint)

The integrating capacitor should be selected to maximize integrator output swing. The integrator output will swing to within 0.8 V of $\mathrm{V}_{S}^{+}$or $\mathrm{V}_{\mathrm{S}}^{-}$without saturating.

Using the suggested $20 \mu \mathrm{~A}$ full-scale buffer output current, the integrating capacitor is easily calculated:

$$
\mathrm{C}_{\mathrm{INT}}=\frac{(\mathrm{T})\left(\mathrm{V}_{\mathrm{FS}}\right)}{\text { Integrator Output Voltage Swing (RINT) }}
$$

Where $T=$ Integration Period
$V_{F S}=$ Full-Scale Input Voltage

A very important integrating capacitor characteristic is dielectric absorption. Polypropylene capacitors give undetectable errors at reasonable cost. Polystyrene and polycarbonate capacitors may also be used in less critical applications.

## General Theory of Operation Dual Slope Conversion Principles

The TSC500 is an integrating analog-to-digital converter building block. An understanding of the dual slope conversion technique will aid in following the detailed TSC500 operation theory.

The conventional dual slope converter measurement cycle has two distinct phases:

- Input Signal Integration
- Reference Voltage Integration (Deintegration)

The input signal being converted is integrated for a fixed time period. Time is measured by counting clock pulses. An opposite polarity constant reference voltage is then integrated until the integrator output voltage returns to zero. The TSC500 automatically switches in the proper polarity reference signal. The reference integration time is directly proportional to the input signal. (Figure 3)

In a simple dual slope converter a complete conversion requires the integrator output to "ramp-up" and "ramp-down." The TSC500 comparator zero-crossing interrupts the processor to indicate the deintegrate cycle is complete.


Figure 3: Basic Dual Slope Converter with TSC500

A simple mathematical equation relates the input signal, reference voltage and integration time:

$$
\frac{1}{R C} \int_{0}^{T S I} V_{I N(t)}^{T} d t=\frac{V_{R} T_{R I}}{R C}
$$

Where:

| $V_{R}$ | $=$ Reference Voltage |
| :--- | :--- |
| $\mathrm{T}_{\mathrm{Si}}$ | $=$ Signal Integration Time (Fixed) |
| $\mathrm{T}_{\mathrm{RI}}$ | $=$ Reference Voltage Integration Time (Variable) |

For a constant $\mathrm{V}_{\mathrm{IN}}$ :

$$
V_{I N}=V_{R} \quad\left[\frac{T_{R I}}{T_{S I}}\right]
$$

The dual slope converter accuracy is unrelated to the integrating resistor and capacitor values as long as they are stable during a measurement cycle.
An inherent benefit is noise immunity. Input noise spikes are integrated or averaged to zero during the integration periods. Integrating ADCs are immune to the large conversion errors that plague successive approximation converters in high noise environments.
Integrating converters provide noise rejection automatically with at least a $20 \mathrm{~dB} / \mathrm{decade}$ attenuation rate. Interference signals with frequencies at integral multiples of the integration period are theoretically completely removed. This intuitively makes sense, since the average value of a sine wave of frequency $1 / T$ averaged over a period $T$ is zero.
Integrating converters often establish the integration period to reject $50 / 60 \mathrm{~Hz}$ line frequency interference signals. The ability to reject such signals is shown by a normal mode rejection plot (Figure 4). Normal mode rejection is practically set to $50-65 \mathrm{~dB}$, since the line frequency can deviate by a few tenths of a percent (Figure 5).


Figure 4: Normal Mode Rejection vs. Input Frequency


Figure 5: Integrating Converter Normal Mode Rejection vs. 60 Hz Line Frequency Variations.

## Integrating Converter

Analog Processor

- Automatic Zero Adjust
- $\mu$ Processor Controlled

Test Set Up


TSC500 to 6522 Peripheral I/0 Chip


Package Information


## General Description

The TSC800 is a 15 -bit plus sign integrating analog to digital converter. The TSC800 improves the conventional two cycle dual slope conversion cycle by incorporating system zero and integrator output zero phases. Offset error sources are automatically zeroed and overrange recovery time is reduced. The integrating conversion technique is immune to the noise spikes that introduce conversion errors in successive approximation converters.

The externally adjustable clock allows integration periods . which are integral multiples of 50 Hz or 60 Hz for maximum power-line noise rejection. By using the 2.4576 MHz crystal oscillator mode (2.5 CONV/SEC) 50,60 and 400 Hz signals are rejected.
Micro-processor interface signals support single byte (16bit) or two byte (8-bit) parallel data transfers. A "handshake" operating mode supports serial data transmission via a UART. A serial count output is derivable by gating the clock signal with data valid (DVD). The count output pulses may be used in serial fiber optic transmission systems.
The high impedance differential inputs, 5 pA input leakage current, 16 -bit dynamic range and interface control signals make the high resolution TSC800 the ideal analog to digital converter for process control, data logging and "intelligent" measurement systems.

## Features

- 15 Bit Resolution Plus Sign Bit
- 96 dB Dynamic Range
- Integrating Dual Slope Converter
- Monotonic
- Eliminate $50 / 60 \mathrm{~Hz}$ "Line" Interference
- High Noise Immunity
- Auto Zero Cycle Eliminates Trimming
- Incorporates Integrator Zero Cycle for Fast Overload Recovery
- Three State Data Bit/Sign Outputs
- 8 or 16 Bit Parallel Data Transfer to $\mu$-Processor Bus
- UART Control Signals
- Serial Data Transmission
- "Handshake" Data Transfer
- Distributed Control Systems
- Fiber Optic Transmission Systems
- Easy Conversion Cycle Monitoring and Control
- Data Valid Output Signal
- Continuous or Convert on Command Operation
- High Impedance Differential Input
- 15 pA Maximum input Current
- Low Input Noise
$-15 \mu V_{p-p}$
- On Chip Crystal Oscillator for 2.5 Conversions/Sec.
$-f_{x \text { tal }}=2.4576 \mathrm{MHz}$
- 100 mSEC Integration Period Rejects $50,60,400 \mathrm{~Hz}$ Interference Signals
- Convenient $\pm 5 \mathrm{~V}$ Supply Operation
- Low Power Dissipation
- Static Discharge Protected Inputs
- Available in 60-Pin Flat Package

Functional Diagram


## Absolute Maximum Ratings ${ }^{2}$

Positive Supply Voltage (Vs๋ to Gnd)
+6.2 V
Negative Supply Voltage (Vs̄ to Gnd) ................ . 9.0 V
Analog Input Voltage ( $\mathrm{V}^{+} \mathbb{N}_{\mathrm{N}}$ or $\left.\mathrm{V}_{\mathrm{IN}}\right)$................ $\mathrm{V}^{+}$to $\mathrm{V}_{\mathrm{S}}^{-}$
Voltage Reference Input (VREF) .................. VS to Vs
Logic Input Voltage ........... Vs +0.3 V to $\mathrm{Gnd}-0.3 \mathrm{~V}$
Package Power Dissipation
CerDIP Package $\qquad$ 1 Watt @ +85 ${ }^{\circ} \mathrm{C}$

Plastic Package
0.5 Watt @ +70․ C

Ambient Operating Temperature Range
CerDIP Package $\begin{array}{ll}\text { (MJL) } \ldots \ldots \ldots . .-55^{\circ} \mathrm{C} \text { to }+125^{\circ} \mathrm{C} \\ & \text { (IJL) } \ldots \ldots \ldots \ldots-25^{\circ} \mathrm{C} \text { to }+85^{\circ} \mathrm{C}\end{array}$
Plastic Package (CPL, CBQ, CSQ) ... $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$
Storage Temperature ...................... $-55^{\circ} \mathrm{C}$ to $150^{\circ} \mathrm{C}$
Lead Soldering Temperature ( 60 Seconds) $\ldots . . .+300^{\circ} \mathrm{C}$

Electrical Characteristics: $\mathrm{V}_{\mathrm{S}}= \pm 5 \mathrm{~V}$, Conversion Rate $=2.5$ CONV/SEC, Crystal Frequency $=2.4576 \mathrm{MHz}$,
$\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, Full-Scale Voltage $=3.2768 \mathrm{~V}$, Note 1 .


## 15-Bit Plus Sign Integrating <br> Analog to Digital Converter

- BUS Compatible
- UART Interface

Electrical Characteristics: $\mathrm{V}_{\mathrm{S}}= \pm 5 \mathrm{~V}$, Conversion Rate $=2.5$ CONV/SEC, Crystal Frequency $=2.4576 \mathrm{MHz}$,
$\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, Full-Scale Voltage $=3.2768 \mathrm{~V}$, Note 1 .

| TYPE | NO. | SYMBOL | PARAMETER | TEST |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  | CONDITIONS |  |  |  |

Notes:

1. Parallel Data Transfer ( $\overline{B U S} /$ Hand $=0$. ). See Figure 1
2. Operation at or above the absolute maximum stress ratings is not implied.
3. Static sensitive device. Unused devices must be stored in conductive material. Protect devices from static discharge and static fields.
4. For Pins $18,19,2010=750 \mu \mathrm{~A}$.
5. Crystal source ( 2.4576 mHz )
a. DIGI-KEY Corp

Highway 32 South
P.O. Box 677

Thief River Falls, MN 56701-9988
1-800-344-4539
Part No. X047

## Pin Description and Function



A low data byte enable input or flag output depending on $\overline{B U S} / H A N D ~(P i n ~ 21) ~$ status
18 3

18
$\overline{\text { HBEN } / 4 B F L G}$ (Input/Output)

1. $\overline{B U S} / H A N D=0$ : With Pin 21 low and $\overline{C E} / \overline{L D S T R B}=0($ Pin 20) data bits 8 through 1 are output (pins 9-16) when the input pin $\overline{\text { LBEN }}=0$.
2. $\overline{\mathrm{BUS} / H A N D}=1$ : Valid data on pins $9-16$ is indicated by the flag output LBFLG $=0$.
A high data byte enable input or flag output depending on BUS/HAND (pin 21) status.
3. $\overline{B U S} / H A N D=0$ : With pin 21 low and $\overline{C E} / \overline{\text { LDSTRB }}=0($ pin 20) the high data byte (Sign Bit plus Data Bits 15-9) are output when the input HBEN $=0$
4. $\overline{\mathrm{BUS}} / \overline{\mathrm{HAND}}=1$ : Valid Data on pins $1-8$ is indicated by the flag output $\overline{\mathrm{HBLFG}}=0$.
5. $\overline{\mathrm{BUS}} / \mathrm{HAND}=0: \overline{\mathrm{CE}}$ is master chip enable, With $\overline{\mathrm{CE}}=1$ sign bit plus $\mathrm{DB}_{15}-\mathrm{DB}_{1}$ are disabled (Hi-Impedance State). $\overline{\mathrm{CE}}=0$ enables outputs and data is transferred under control of $\overline{\mathrm{LBEN}}$ and $\overline{\mathrm{HBEN}}$ input signals.

| $\overline{\text { CE }}$ | $\overline{\text { LBEN }}$ | $\overline{\text { HBEN }}$ | FUNCTION |
| :---: | :---: | :---: | :--- |
| 0 | 0 | 1 | Low Data Byte Output |
| 0 | 1 | 0 | High Data Byte Output |
| 0 | 0 | 0 | Low + High Data Byte Output |
| 0 | 1 | 1 | High Impedance State |

2. $\overline{\text { BUS/HAND }}=1: \overline{\text { LDSTRB }}$ is a load strobe output sign. In the handshake mode, $\overline{\text { LDSTRB }}=0$ output signal instructs the receiving device to accept data.
Note:
Pin connections in description section refer to 40-pin package.

## 15-Bit Plus Sign Integrating Analog to Digital Converter

- BUS Compatible
- UART Interface


## Pin Description and Function (Cont.)

| $\begin{gathered} \hline \text { PIN NO. } \\ \text { 40-Pin } \\ \text { DIP) } \end{gathered}$ | PIN NO. (60-Pin FP) | SYMBOL | DESCRIPTION |
| :---: | :---: | :---: | :---: |
| 21 | 39 | BUS/HAND | 1. $\overline{\mathrm{BUS}}=0$ : Parallel output data mode where the $\overline{\mathrm{CE}}, \mathrm{HBEN}$, and $\overline{\text { LBEN }}$ signals are inputs that directly control the 16 data bits. |
|  |  |  | 2. HAND $=1: \overline{\text { LDSTRB }}, \overline{\mathrm{LBFLG}}, \overline{\mathrm{HBFLG}}$ are outputs used in the handshake data transfer mode. |
|  |  |  | 3. Hand $=$ $\qquad$ (Pulsed High): Causes entry into handsake mode for UART interfacing. |
| 22 | 40 | $\mathrm{OSC}_{2}$ | Oscillator input |
| 23 | 41 | $\mathrm{OSC}_{1}$ | Oscillator output |
| 24 | 42 | OSC CON | Selects internal oscillator structure |
|  |  |  | 1. OSC CON = 1: RC oscillator. Internal clock frequency is same frequency and duty cycle as BUF OSC. |
|  |  |  | 2. $\mathrm{OSC} C O N=0$ : Crystal oscillator, Internal clock frequency is frequency at BUF OSC $\div 15$. |
| 25 | 43 | BUFOSC | Buffered oscillator output |
| 26 | 48 | $\begin{aligned} & \text { CONVERT/ } \\ & \text { STOP } \end{aligned}$ | CONVERT = 1: Conversions performed continuously. <br> $\overline{S T O P}=0$ : Conversion process stops 7 counts before entering signal integrate phase. <br> The conversion in progress when STOP $=0$ is completed. |
| 27 | 49 | DRQST | DATA OUTPUT request signal. An input used in the handshake mode that indicates an external device is ready to accept data. If DRQST is not used connect to $\mathrm{V}_{\mathrm{S}}^{+}$. |
| 28 | 50 | $\mathrm{V} \bar{s}$ | Negative power supply |
| 29 | 51 | VREF | Voltage reference input |
| 30 | 52 | COM | Analog common. The TSC800 is auto-zeroed to the analog common potential. |
| 31 | 54 | VINT | Integrator output |
| 32 | 55 | Csz | SYSTEM-ZERO capacitor |
| 33 | 56 | Vbuf | Output of input signal buffer |
| 34 | 57 | $\mathrm{C}^{-}$ | Reference capacitor |
| 35 | 59 | $\mathrm{C}_{\text {+ }}^{+}$ | Reference capacitor |
| 36 | 1 | VIN | Negative differential analog input |
| 37 | 3 | $\mathrm{V}_{\text {IN }}^{+}$ | Positive differential analog input |
| 38 | 5 | $\mathrm{V}_{S}^{+}$ | Positive power supply |
| 39 | 6 | GND | Digital ground. Ground return point for Digital logic. |
| 40 | 7 | $\overline{\text { DVD }}$ | DATA VALID SIGNAL: $\overline{\text { DVD }}=1$ during signal integrate and reference integrate phases until data is latched. <br> $\overline{\mathrm{DVD}}=0$ when in auto zero-phase. Data does not change when $\overline{\mathrm{DVD}}=0$. |

Note:
Pin connections in description section refer to 40-pin package.

## General Theory of Operation Dual Slope Conversion Principles

The TSC800 is a dual slope, integrating analog to digital converter. An understanding of the dual slope conversion technique will aid in following the detailed TSC800 operation theory.
The conventional dual slope converter measurement cycle has two distinct phases:

- Input Signal Integration
- Reference Voltage Integration (Deintegration)

The input signal being converted is integrated for a fixed time period. Time is measured by counting clock pulses. An opposite polarity constant reference voltage is then integrated until the integrator output voltage returns to zero. The reference integration time is directly proportional to the input signal.
In a simple dual slope converter a complete conversion requires the integrator output to "ramp-up" and "ramp-down."

## Basic Dual Slope Converter



The dual slope converter accuracy is unrelated to the integrating resistor and capacitor values as long as they are stable during a measurement cycle. An inherent benefit is noise immunity. Noise spikes are integrated or averaged to zero during the integration periods. Integrating ADCs are immune to the large conversion errors that plague successive approximation converters in high noise environments.

A simple mathematical equation relates the input signal, reference voltage and integration time:

$$
\frac{1}{R C} \int_{0}^{T s I} V_{I N}(t) d t \quad=\frac{V_{R} T_{R I}}{R C}
$$

where:
$\mathrm{V}_{\mathrm{R}}=$ Reference Voltage
TSI $=$ Signal Integration Time (Fixed)
$\mathrm{T}_{\mathrm{RI}}=$ Reference Voltage Integration Time (Variable)
For a constant VIN:
$V_{I N}=V_{R}\left[\frac{T_{R I}}{T_{S I}}\right]$

## TSC800 Analog Input Description

## System Zero Phase (Figure 3A)

During this phase errors due to buffer, integrator and comparator offset voltages are compensated for by charging Csz (system-zero capacitor) with a compensating error voltage. With a zero input voltage the integrator output will remain at zero.
The external input signal is disconnected from the internal circuitry by opening the two SWI switches. The internal input points connect to analog common. The reference capacitor charges to the reference voltage potential through SWR. A feedback loop, closed around the integrator and comparator, charges the Csz capacitor with a voltage to compensate for buffer amplifier, integrator and comparator offset voltages.


Figure 3A: TSC800 System Zero Phase

# 15-Bit Plus Sign Integrating <br> Analog to Digital Converter <br> - BUS Compatible <br> - UART Interface 

TSC800

## Analog Input Signal Integration Phase <br> (Figure 3B)

The TSC800 integrates the differential voltage between the + input and - input. The differential voltage must be within the device common-mode range; 1 V from either supply rail typically. The input signal is integrated for 16, 384 clock cycles.
The input signal polarity is determined at the end of the phase.


Figure 3B: TSC800 Input Signal Integration Phase

## Reference Voltage Integration (Figure 3C)

The previously charged reference capacitor is connected with the proper polarity to ramp the integrator output back to zero. The time for the output to return to zero is proportional to the input signal magnitude. The phase lasts for a maximum of 32,768 clock periods.


Figure 3C: TSC800 Reference Voltage Integration Cycle

## Integrator Output Zero (Figure 3D)

This phase guarantees the integrator output is at zero volts when the system zero phase is entered and that the true system offset voltages are compensated for. This phase normally lasts 4096 clock cycles.


Figure 3D: TSC800 Integrator Output Zero Phase

Differential Inputs (VIN (Pin 37) and VIN (Pin 36))
The TSC800 operates with differential voltages within the input amplifier common-mode range. The input amplifier common-mode range extends from 1.0 V below the positive supply to 1.0 V above the negative supply. Within this com-mon-mode voltage range an 86 dB common-mode rejection ratio is typical.

The integrator output also follows the common-mode voltage. The integrator output must not be allowed to saturate. A worst case condition exists, for example, when a large positive common-mode voltage with a near full scale negative differential input voltage is applied. The negative input signal drives the integrator positive when most of its swing has been used up by the positive common-mode voltage. For these critical applications the integrator swing can be reduced. The integrator output can swing within 0.4 volts of either supply without loss of linearity.

## Analog Common (Pin 30)

Analog common is used as the Vin return during system-zero and reference-integrate. If Vī is different from analog common, a common-mode voltage exists in the system. This signal is rejected by the excellent CMRR of the converter. In most applications Vīn will be set at a fixed known voltage (power supply common, for instance). In this application, analog common should be tied to the same point, thus removing the common-mode voltage from the converter. The reference voltage is referenced to analog common.

## Digital Section Description

## Digital Control Signals

## BUS/Hand (Pin 21)

The BUS/Hand input signal selects the parallel BUS data transfer mode or handshake transfer mode. An internal pulldown resistor guarantees parallel mode operation when the input pin is open. The handshake mode allows serial data transmission with a UART. In the parallel mode the TSC800 outputs data under control of the $\overline{\text { HBEN }}, \overline{\text { LBEN }}$ and $\overline{\mathrm{CE}}$ signals. In the handshake mode TSC800 output signals communicate with peripheral devices to control the data transmission.
For $\overline{\mathrm{BUS}}=0$ the $\overline{\mathrm{HBEN}}$ (Pin 19), $\overline{\mathrm{LBEN}}$ (Pin 18), and $\overline{\mathrm{CE}}$ (Pin 20) input signals control the TSC800 data transmission. Figure 1 shows typical timing relationships and operation. The $\overline{\text { HBEN }}, \overline{\text { LBEN }}$ and $\overline{\mathrm{CE}}$ signals are asynchronous to the internal conversion clock. Output data is immediately accessed. To avoid accessing data as updates are occuring the DATA VALID ( $\overline{\mathrm{DVD}}$, Pin 40) signal can be used as an enable signal. Data will not change if $\overline{\mathrm{DVD}}=0$.
In the handshake mode two data transfer methods are possible. If HAND is pulsed high (HAND $=\Omega$ ) for a minimum of 70 nsec the TSC800 enters the handshake mode. If HAND $=1$ continuously the parallel mode is not re-entered, and a handshake data transfer will occur at the end of each conversion cycle.
The $\overline{B U S} /$ Hand input signal configures dual purpose pins 18, 19 and 20 as inputs or outputs. In conjunction with the DATA REQUEST (DRQST, Pin 27) input signal the handshake data transfer is controlled by the output signals: $\overline{\text { LBFLG, }} \overline{\mathrm{HBFLG}}$, and $\overline{\mathrm{LDSTRB}}$.

## Data Request Input (DRQST, Pin 27)

This input is used only in the handshake data transfer mode. a DRQST $=1$ input signal indicates an external receiving device is ready to accept data from the TSC800. It serves as a send data command. When $\overline{B U S} / H A N D=0$, DRQST should be tied to $\mathrm{V}_{\mathrm{S}}^{+}$.

## Convert/Stop Input (CONV/STOP, Pin 26)

The CONV/ $\overline{\text { TTOP }}$ control input is pulled high through an internal pull-up resistor. If CONV $/ \overline{S T O P}=1$ or left open the TSC800 continuously performs conversions. Each measurement cycle will be 65,536 counts long. The measurement cycle time for one conversion is:

$$
\text { T Conversion }(\mathrm{msec})=65.5361 / \mathrm{f}_{\mathrm{c}}(\mathrm{kHz})
$$

Where: $f_{c}=$ Internal Clock Frequency in kHz .
If CONV $/ \overline{\mathrm{STOP}}=0$ during the reference integrate phase and after a zero-crossing has been detected the integrator zero phase is immediately entered and completed. This eliminates the time spent in the reference integrate phase after the output data latches are updated.

If CONV/ $\overline{\text { STOP }}$ remains low, the TSC800 will wait in the system zero phase. The signal integrate phase will begin 7 clock counts after a CONV $=1$ signal is detected. The CONV/STOP signal is detected synchronously with the internal clock. The system zero phase should last a minimum of 70 msec . See Figures 6 and 7 for CONV/STOP conversion timing diagrams.

If CONV/STOP goes low and remains low during the system zero phase, the TSC800 will stop at the end of the phase and wait for CONV $=1$. The signal integrate phase will start seven clock counts after CONV $=1$ is detected.

| OPERATING MODE | PIN DESCRIPTION |  |  |
| :---: | :---: | :---: | :---: |
| $\overline{\text { BUS }}$ Transfer Mode | $\begin{aligned} & \overline{\overline{\mathrm{LBEN}} / \overline{\mathrm{LBFLG}}} \\ & (\operatorname{Pin} 18) \end{aligned}$ | $\begin{aligned} & \overline{\text { HBEN } / \overline{\text { MBFLG }}} \\ & (\text { Pin 19) } \end{aligned}$ | $\begin{gathered} \overline{\mathrm{CE} / \overline{\text { LDSTRB }}} \\ (\text { Pin } 20) \end{gathered}$ |
| $\overline{\text { BUS }} /$ HAND $=0$ | LBEN: Low Data Byte Enable Input. A logic 0 activates the low order data ( $\mathrm{DB}_{8}-\mathrm{DB}_{1}$ ) if $\overline{C E}=0$. | HBEN: High Data Byte Enable Input. A logic 0 activates the high order data (SGN, DB15 - DB 9 ) if $\overline{\mathrm{CE}}=0$. | $\overline{\mathrm{CE}}:$ Master Output Enable Input. When $\overline{C E}=1$ outputs (SGN, DB ${ }_{15}-\mathrm{DB}_{1}$ ) are disabled and in a high impedance state. |
| Handshake Transfer <br> Mode <br> $\overline{\mathrm{BUS}} / \mathrm{HAND}=1$ or $\Omega$ | LBFLG: Low Data Byte Flag Output. Indicates output data is $\mathrm{DB}_{8}-\mathrm{DB}_{1}$. | HBFLG: High Data Byte Flag Output. Indicates output data is $\mathrm{DB}_{15}$ - $\mathrm{DB}_{9}$. | LDSTRB: Load Strobe Output Signal. <br> A logic 0 or falling edge indicates valid data is present at the output. |

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Figure 6: Convert on Command Operation. (CONV/STOP = 0 After Zero Crossing Detected)


Figure 7: Continuous Conversion (CONV/STOP = 1)

## Test Input (Pin 17)

When Test = 1 the counter data latches are enabled. If Test = 0 the counter outputs are forced to a 1 state and the internal clock is disabled. When Test is returned to a logic 1 and one clock pulse is applied all the counter outputs are clocked low.

Data Valid (DVD, Pin 40)
$\overline{\mathrm{DVD}}=1$ at the start of signal integrate and $\overline{\mathrm{DVD}}=0$ one half clock period after new data is stored in the data latches. Since $\overline{D V D}$ is always low when data is not changing the signal may be used as a "Data Valid Flag". See Figures 6 and 7 for timing relationships.

## 15-Bit Plus Sign Integrating Analog to Digital Converter

## Data Output Description

## Parallel Mode Data Interface

With $\overline{\mathrm{BUS}} /$ Hand $=0$ the sign and data bits are controlled by the $\overline{C E}$ (Pin 20), $\overline{\text { LBEN (Pin 18) and HBEN (Pin 19) inputs. All }}$ three inputs have internal pullup resistors. Inactive data bits are in a high impedance state.
The $\overline{H B E N}$ signal controls the most significant data byte (SGN, $\mathrm{DB}_{15}-\mathrm{DB}_{9}$ ). $\overline{\text { LBEN }}$ controls the least significant data byte ( $\left.D B_{8}-D B_{1}\right)$.

| CE | HBEN | LBEN | High Data Byte (SGN, DB ${ }_{15}$ - DBg) | Low Data Byte (DB8 $-D_{1}$ ) |
| :---: | :---: | :---: | :---: | :---: |
| 1 | X | X | Inactive (High Z State) | Inactive <br> (High Z State) |
| 0 | 0 | 0 | Active | Active |
| 0 | 0 | 1 | Active | Inactive <br> (High Z State) |
| 0 | 1 | 0 | Inactive (High Z State) | Active |
| 0 | 1 | 1 | Inactive (High Z State) | Inactive <br> (High Z State) |

" $X$ " = 1 or 0
The $\overline{H B E N}, \overline{L B E N}$ and $\overline{C E}$ input signals are asynchronous with the internal conversion clock. Output data is immediately available. To avoid accessing data as data updates occur the DATA VALID (Pin 40) signal can control the data access. DATA will not change if $\overline{D V D}=0$.


Figure 1A: Parallel Data Transfer - Two 8-Bit Bytes


Figure 1B: Parallel Data Transfer - 16-Bit Bytes

## Handshake Mode Data Transfer

The TSC800 actively controls the data transfer to peripherals through the handshake data transfer mode. In the handshake mode pins 18, 19 and 20 ( $\overline{\text { LBFLG, HBFLG, and } \overline{\text { LDSTRB }} \text { ) are }}$ TTL compatible outputs. The LDSTRB signal indicates valid data is available for the peripheral. The $\overline{L B F L G}$ and $\overline{\text { HBFLG }}$ signals indicate which data byte is being transferred. The data request signal (DRQST, Pin 27) informs the TSC800 a peripheral is ready to accept data. A complete cycle transfers two 8-bit bytes.
The $\overline{\mathrm{BUS}} /$ Hand signal is ignored after the handshake mode is entered. Conversions continue but data latch updating is inhibited until the TSC800 transfers two data bytes and clears the internal mode latch.
The handshake mode is entered in two ways:

- Set $\overline{B U S} /$ Hand $=1$
- Pulse $\overline{B U S} /$ Hand High ( $\Omega$ )


## $\overline{B U S} /$ Hand $=1$

With Hand $=1$ the TSC800 will enter the handshake mode after data is stored in the output data latches. Once the handshake mode internal latch signal is set the $\overline{B U S} /$ Hand signal is ignored. The Data Request Input Signal (DRQST) signal controls data transfer to the external requesting peripheral. Figure 2 shows the timing diagram for the data transfer with $\overline{B U S} /$ Hand $=1$ (throughout the transfer). Note that DRQST $=$ 1 throughout the transfer. The data transfer rate is set by the TSC800 internal clock. A complete data transfer occurs in 4 clock periods after a DRQST $=1$ is detected on a high to low internal clock edge transition.
For peripherals that cannot accept data at the TSC800 clock rate the DRQST input signal can be used to delay the transmit sequence. This mode is useful in interfacing to UARTS. Figure 3 shows a typical 2502 UART interface.

## 15-Bit Plus Sign Integrating Analog to Digital Converter <br> - BUS Compatible <br> - UART Interface



Figure 2: Data Transfer with BUS/Hand = 1


Figure 3A: Typical UART Interface Timing with DRQST Signal Controliing Data Transier Timing

The UART data transfer sequence begins with a DRQST $=1$ signal. This indicates the UART transmitter buffer register is empty (TBMT = 1). LDSTRB and HBFLG become active when DRQST is sensed synchronously. The high order data byte is stored in the UART transmitter buffer register when LDSTRB $=1$. This occurs one clock period after DRQST is sensed. The


Figure 38: Typical UART to TSC800 Connection

DRQST signal (TBMT) goes low halting the cycle with the SGN and DBN 15 - DB9 data bits active. After the UART transfers the received data to the transmitter registor the DRQST input (TBMT) again goes high. On the first high to low internal clock transition the high byte data is disabled and one-half clock period later $\mathrm{HBFLG}=1$. Concurrently $\overline{L D S T R B}=0$ and $\mathrm{DB}_{8}-\mathrm{DB}_{1}$, become active. One clock period later [DSTRB = 1 and the low data byte is clocked into the UART transmitter buffer register. DRQST goes low. When DRQST returns high it will be sensed on the first TSC800 internal clock high to low edge transition thus causing all outputs to be disabled. One half clock period later the internal handshake mode latch is cleared and $\overline{\mathrm{DDSTRB}}=\overline{\mathrm{HBFLG}}=\overline{\mathrm{LBFLG}}=1$. The outputs remain active as long as Hand $=1$.

## $\overline{\text { BUS }} /$ Hand $=\Omega$ (Pulse)

The TSC800 outputs every conversion (except those completed during a handshake transfer) with Hand held high. Handshake output sequences on demand are possible by triggering the Hand control input with a low to high edge. Figure 4 shows a typical data transfer. The output cycle is controlled by the DRQST input signal. The complete two byte data transfer can take any length of time. Conversions are made and the $\overline{D V D}$ and CONV/STOP inputs function normally but new data will not be latched until the handshake mode is terminated.


Figure 4: Handshake Output on Command (DRQST Signal Controls Transfer)

## 15-Bit Plus Sign Integrating Analog to Digital Converter

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TSC800

## Oscillator Control and Operation

OSC CON (Pin 24) configures the internal oscillator as a crystal or RC oscillator. OSC CON = 1 establishes the RC oscillator. R should be $50 \mathrm{k} \Omega$ or larger. The internal clock matches the frequency and phase of the BUF OSC (Pin 25) signal. In the crystal oscillator mode (OSC CON $=0$ ) $a \div 15$ is between the buffered oscillator output and the internal clock. The internal oscillator may be over-driven by driving OSC 1 (Pin 23). The OSC CON pin controls whether the internal clock is divided by 15.

| Oscillator <br> Type | OSC CON <br> (Pin 24) | Internal <br> Clock <br> Frequency | Signal <br> Integration <br> Time | Conversion <br> Cycle Time |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| RC | VSt or open | $.45 / \mathrm{RC}$ | 16384 | $\left(\frac{\mathrm{RC}}{.45}\right)$ | $\frac{\text { RC }}{.45}[65,536]$ |
| Crystal. | Ground | fXTAL $\div 15$ | $16384\left(\frac{15}{\text { fXTAL }}\right)$ | $\frac{15}{\text { fXTAL }}[65,536]$ |  |

fxtal $=$ Crystal Frequency
Typical Crystal Operation:

- $f_{x}=2.4576 \mathrm{mHz}$
- Internal Clock Frequency $=163.8 \mathrm{kHz}$
- Signal Integration Time $=100 \mathrm{msec}$
- Conversion Cycle Time $=400 \mathrm{msec}$ (2.5Conversions $/ \mathrm{Sec}$ )


## External Oscillator Control



## Internal RC Oscillator Configuration



Internal Crystal Oscillator Configuration


## Component Value Selection Integrating Resistor (Rint)

The desired full-scale input voltage and output current capability of the input buffer and integrator amplifier set the integration resistor value. The internal class A output stage amplifiers will supply a $20 \mu \mathrm{~A}$ drive current with minimal linearity error. RINT is easily calculated for a $20 \mu \mathrm{~A}$ full scale current:

$$
\text { RINT }(\mathrm{M} \Omega)=\frac{\text { Full-Scale Input Voltage }(\mathrm{V})}{20}
$$

| Full-Scale Input Voltage (VFS) | RINT |
| :---: | :---: |
| 3.2768 | $160 \mathrm{k} \Omega$ |
| 4.0000 | $200 \mathrm{k} \Omega$ |

## Integrating Capacitor ( $\mathrm{C}_{\mathrm{INT}}$ )

The integrating capacitor should be selected to maximize integrator output swing. The integrator output will swing to within 0.4 V of $\mathrm{V} \pm$ or V s without saturating. With $\pm 5 \mathrm{~V}$ power supplies and analog common connected to supply ground a 3.5 V to 4.3 V swing is adequate.

Using the suggested $20 \mu \mathrm{~A}$ full-scale buffer output current the integrating capacitor is easily calculated:

$$
\mathrm{C}_{\text {INT }}(\mu \mathrm{F})=\frac{16.384\left(\frac{1}{\text { flat (kHz) }}\right) 20 \mu \mathrm{~A}}{\text { Integrator Output Voltage Swing (V) }}
$$

Where: fclk = Internal Clock Frequency

## Component Value Selection (Cont.) Integrating Capacitor (Cint)

For 2.5 CONV/SEC the internal clock is 163.8 kHz . The TSC800 operates at 2.5 CONV/SEC with an external crystal equal to 2.4576 MHz . A $0.47 \mu \mathrm{~F}$ capacitor is recommended.
The integrating capacitor should be selected for low dielectric absorption to prevent roll-over errors. Polypropylene capacitors are suggested. The outer foil of CINT should be connected to CINT (Pin 31).

## System Zero Capacitor (Csz)

A $1.0 \mu \mathrm{~F}$ polypropylene capacitor is suggested. The inner foil should be conected to Caz (Pin 32).

## Reference Capacitor (CREF)

A $1.0 \mu \mathrm{~F}$ capacitor is suggested. Larger values may be used to limit roll-over errors. Low leakage capacitors such as polypropylene or Teflon ${ }^{\circledR}$ should be used.

## Reference Voltage

The analog input required to generate the 32,768 full-scale count is Vinput $=2$ Vref. The reference voltage source should be selected for temperature stability. The TSC800 provides 30 ppm resolution. With a $5 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ reference a $6^{\circ}$
change will introduce a 1-bit absolute error. A stable reference must be used where ambient temperature is controlled and accurate absolute measurements are needed.
The reference voltage input must be a positive voltage with respect to analog common. Reference voltage circuits are shown below.
Reference Voltage Circuits


## Delay Resistor (Rs)

The Rs, CINT combination compensates for comparator delay time. With a $0.47 \mu \mathrm{~F}$ integrating capacitor a $20 \Omega$ series resistor is suggested.

## Applications Information <br> TSC800 Parallel Interface to 6522 Versatile Interface Adapter



## Applications Information (Cont.)

TSC800 Interface to 6520 VIA



Handshake Timing Diagram: TSC800 to 6520 Peripheral Interface Adapter

## Pin Configuration and Ordering Information



## Package Dimensions



## General Description

The TSC7109 is a 12-bit plus sign CMOS low power A/D Converter. The single CMOS IC contains all the necessary active devices to interface with microprocessors.

In direct mode, Chip Select and High/Low Byte Enables conirol parallel bus interface. In the handshake mode the TSC7109 will operate with industry standard UART's in controlling serial data trensmission, ideal for remote data logging. Control and monitoring of conversion timing is provided by the RUN/ $\overline{H O L D}$ and STATUS outputs. The TSC7109 requires only the addition of eight passive components plus a crystal to operate as a dual slope integrating A/D converter. The TSC7109 has features that make it an attractive per-channel alternative to analog multiplexing for many data acquisition applications. These features include typical input bias current of 1 pA , drift of less than $1 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$, input noise typically $15 \mu \mathrm{~V} p-\mathrm{p}$, and auto-zero. True differential input and reference allows the measurement of bridge-type transducers such as load cells, strain gauges and temperature transducers.
For applications requiring more resolution see the TSC800, 15-bit plus sign data sheet.

## Ordering Information

| Part No. | Package | Temp. <br> Range |
| :--- | :--- | ---: |
| TSC7109CPL | $40-$ Pin Plastic Dip | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ |
| TSC7109BCPL | $40-$ Pin Plastic Dip | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ |
| TSC7109IJL | $40-$ Pin CerDIP | $-25^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
| TSC7109BIJL | $40-$ Pin CerDIP | $-25^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
| TSC7109MJL | $40-$ Pin CerDIP | $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |

## Features

- 12-Bit Plus Sign Integrating A/D Converter with Overrange Indication
- Sign Magnitude Coding Format
- True Differential Signal Input and Differential Reference Input
- Low Noise - Typically $15 \mu \mathrm{Vp}-\mathrm{p}$
- High Normal Mode Noise and Line Frequency Rejection
- 1 pA Typical Input Current
- No Zero Adjustment
- TTL Compatible Byte Organized Tri-State Outputs
- UART Handshake Mode for Simple Serial Data Transmission
- Direct Bus Connection for 8 or $16-$ Bit Bus -3.58 mHz Crystal Provides 7.5 Conversions Per Second for 60 Hz Rejection - External RC Network Provides up to 30 Conversions Per Second
- Power Dissipation Typically Less Than 20 mW
- Internal Voltage Reference

| Part No. | Package | Temp. <br> Range |
| :--- | :--- | ---: |
| TSC7109CBQ | 60-Pin Plastic <br> Flat Package: <br> Formed Leads | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ |
| TSC7109CSQ | 60-Pin Plastic <br> Flat Package: <br> Unformed Leads | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ |
| Devices Avallable with 160 Hour, $+125^{\circ} \mathrm{C}$ Burn-In |  |  |
| TSC7109CPL/BI | $40-$ Pin Plastic Dip | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ |
| TSC7109IJL/BI | $40-$ Pin CerDIP | $-25^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |

Test Circult (See Figure 1 for typical connection to A UART or Microcomputer)


## Absolute Maximum Ratings

Positive Supply Voltage (GND to $\mathrm{V}^{+}$)
$+6.2 \mathrm{~V}$
Negative Supply Voltage (GND to $\mathrm{V}^{-}$) $\ldots \ldots . . . . . .$. Analog Input Voltage (LOW or HIGH) (Note 1) ... $\mathrm{V}^{+}$to $\mathrm{V}^{-}$ Reference Input Voltage (LOW or HIGH) (Note 1)... $\mathrm{V}^{+}$to $\mathrm{V}^{-}$ Digital Input Voltage
(Pins 2-27) (Note 2)

```
            .
```

Power Dissipation (Note 3)
Ceramic Package ....................... $1 \mathrm{~W} @+85^{\circ} \mathrm{C}$
Plastic Package ................... $500 \mathrm{~mW} @+70^{\circ} \mathrm{C}$
Operating Temperature
Ceramic Package (M) $\ldots \ldots . .-55^{\circ} \mathrm{C} \leq T_{A} \leq+125^{\circ} \mathrm{C}$
(1) $\ldots \ldots \ldots . .-25^{\circ} \mathrm{C} \leq T_{A} \leq+85^{\circ} \mathrm{C}$
Plastic Package (C) $\ldots \ldots \ldots . .0^{\circ} \mathrm{C} \leq T_{A} \leq+70^{\circ} \mathrm{C}$
Storage Temperature $. . . . . . . . . . . . .-55^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+125^{\circ} \mathrm{C}$
Lead Temperature (Soldering, 60 sec .) $\ldots . . . . . . .+300^{\circ} \mathrm{C}$
This device contains circuitry to protect the inputs from damage due to high
static voltage or electric fields. It is advised that voltages great than those listed
under absolute maximum ratings, may cause permanent damage to the devices. Normal precautions should be taken to avoid application of any voltage higher than maximum ratings.

## Notes:

1. Input voltages may exceed the supply voltages if the input current is limited to $\pm 100 \mu \mathrm{~A}$.
2. Connecting any digital inputs or outputs to voltages greater than $\mathrm{V}^{+}$or less than GND may cause destructive device latchup. Therefore, it is recommended that inputs from sources other than the same power supply should not be applied to the TSC7 109 before its power supply is established. In multiple supply systems, the supply to the TSC7109 should be activated first.
3. This limit refers to that of the package and will not occur during the normal operation.
4. HANDLING PRECAUTIONS: These devices are CMOS and must be handled correctly to prevent damage. Package and store only in conductive foam, anti-static tubes or other conducting material. Use proper anti-static handling procedures. Do not connect in circuits under "power-on" conditions, as high transients may cause permanent damage.

Electrical Characteristics: All parameters with $\mathrm{V}^{+}=+5 \mathrm{~V}, \mathrm{~V}^{-}=-5 \mathrm{~V}, \mathrm{GND}=0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, unless otherwise indicated.
Test circuit as shown on page 1.


## 12-Bit Plus Sign <br> Integrating A/D Converter

- BUS Compatible
- Serial Data Transmission w/UART

TSC7109

Electrical Characteristics: All parameters with $\mathrm{V}^{+}=+5 \mathrm{~V}, \mathrm{~V}^{-}=-5 \mathrm{~V}, \mathrm{GND}=0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, unless otherwise indicated.
Test circuit as shown on page 1.

| TYPE | NO. | SYMBOL | PARAMETER | TEST CONDITIONS | MIN | $\begin{aligned} & \text { TSC7109 } \\ & \text { TYP } \end{aligned}$ | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 16 | VOH | Output High Voltage | $\begin{aligned} & \text { lout }=100 \mu \mathrm{~A} \\ & \text { Pins } 2-16,18,19,20 \end{aligned}$ | 3.5 | 4.3 | - | V |
|  | 17 | VOL | Output Low Voltage | IOUT $=1.6 \mathrm{~mA}$ | - | 0.2 | 0.4 | V |
|  | 18 |  | Output Leakage Current | Pins 3-16 High Impedance | - | $\pm .01$ | $\pm 1$ | $\mu \mathrm{A}$ |
|  | 19 |  | Control I/O Pullup Current | $\text { Pins } 18,19,20 \text { Vout }=\mathrm{V}^{+}$ $-3 \text { V MODE Input at GND }$ | - | 5 | - | $\mu \mathrm{A}$ |
|  | 20 |  | Control I/O Loading | HBEN Pin 19 LBEN Pin 16 | - | - | 50 | pF |
|  | 21 | VIH | Input High Voltage | Pins 18-21, 26, 27 referred to GND | 2.5 | - | - | V |
|  | 22 | VIL | Input Low Voltage | Pins 18-21, 26, 27 Referred to GND | - | - | 1 | V |
|  | 23 |  | Input Pullup Current | Pins 26, 27 Vout $=\mathrm{V}^{+}-3 \mathrm{~V}$ | - | 5 | - | $\mu \mathrm{A}$ |
|  | 24 |  | Input Pullup Current | Pins 17, 24 Vout $=\mathrm{V}^{+}-3 \mathrm{~V}$ | - | 25 | - | $\mu \mathrm{A}$ |
|  | 25 |  | Input Pulldown Current | Pin 21, Vout $=$ GND +3 V | - | 5 | - | $\mu \mathrm{A}$ |
|  | 26 | OOH | Oscillator Output High | Vout $=2.5 \mathrm{~V}$ | - | 1 | - | mA |
|  |  | OOL | Current Low | Vout $=2.5 \mathrm{~V}$ | - | 1.5 | - | mA |
|  | 27 | BOOH | Buffered Oscillator High | Vout $=2.5 \mathrm{~V}$ | - | 2 | - | mA |
|  |  | BOOL | Output Current Low | VOUT $=2.5 \mathrm{~V}$ | - | 5 | - | mA |
|  | 28 | tw | MODE Input Pulse Width |  | 50 | - | - | ns |

## Pin Description

| 40-Pin DIP <br> Pin Number <br> Normal/(Reverse) | 60-Pin <br> Flat Package Pin Number | Name | Description |
| :---: | :---: | :---: | :---: |
| 1 | 9 | GND | Digital Ground, 0 V, Ground Return for all digital logic. |
| 2 | 10 | STATUS | Output High during integrate and deintegrate until data is latched. Output Low when analog section is in Auto-Zero configuration. |
| 3 | 11 | POL | Polarity - High for Positive Input. |
| 4 | 12 | OR | Overrange - High if Overranged. |
| 5 | 13 | B12 | Bit 12 (Most Significant Bit). |
| 6 | 18 | $\mathrm{B}_{11}$ | Bit 11. |
| 7 | 19 | B10 | Bit 10. |
| 8 | 20 | B9 | Bit 9.3 All |
| 9 | 21 | B8 | Bit 8.3 three |
| 10 | 22 | $\mathrm{B}_{7}$ | Bit 7.3 state |
| 11 | 24 | B6 | Bit $6 \times$ output |
| 12 | 25 | B5 | Bit 5.8 data |
| 13 | 26 | B4 | Bit 4. ${ }^{\text {bits }}$ |
| 14 | 27 | B3 | Bit 3. |
| 15 | 28 | $\mathrm{B}_{2}$ | Bit 2. |
| 16 | 33 | $\mathrm{B}_{1}$ | Bit 1 (Least Significant Bit). |
| 17 | 34 | TEST | Input High - Normal Operation. Input Low - Forces all bit outputs high. Note: This input is used for test purposes only. |

## Pin Description (Cont.)

| 40-PIn DIP Pin Number Normal/(Reverse) | 60-Pin <br> Flat Package Pin Number | Name | Description |
| :---: | :---: | :---: | :---: |
| 18 | 35 | LBEN | Low Byte Enable - With MODE (Pin 21) low, and CE/[OAD (Pin 20) low, taking this pin low activates low order byte outputs B1-B8. With MODE (Pin 21) high, this pin serves as low byte flag output used in handshake mode. See Figures 7, 8, 9. |
| 19 | 36 | HBEN | High Byte Enable - With MODE (Pin 21) low, and CE/LOAD (Pin 20) low, taking this pin low activates high order byte outputs B9-B12, POL, OR. With MODE (Pin 21) high, this pin serves as high byte flag output used in handshake mode. See Figures 7, 8. 9. |
| 20 | 37 | $\overline{C E} / \overline{L O A D}$ | Chip Enable Load - With MODE (Pin 21)low, $\overline{\mathrm{CE}} / \overline{\mathrm{LOAD}}$ serves as a master output enable. When high, B1-B12, POL, OR outputs are disabled. When MODE (Pin 21) low, a load strobe used in handshake mode. <br> See Figures 7, 8, 9. |
| 21 | 39 | MODE | Input Low - Direct output mode where $\overline{\mathrm{CE}} / \overline{\mathrm{LOAD}}$ (Pin 20), FBEN (Pin 19) and LBEN (Pin 18) act as inputs directly controlling byte outputs. Input Pulsed High - Causes immediate entry into handshake mode and output of data as in Figure 9. Input High - Enables CE/ $\overline{\text { LOAD }}$ (Pin 20); HBEN (Pin 19), and LBEN (Pin 18) as outputs, handshake mode will be entered and data output as in Figures 7 and 8 at conversions completion. |
| 22 | 40 | OSC IN | Oscillator Input |
| 23 | 41 | OSC OUT | Oscillator Output |
| 24 | 42 | OSC SEL | Oscillator Select - Input high configures OSC IN, OSC OUT, BUF OSC OUT as RC oscillator - clock will be same phase and duty cycle as BUF OSC OUT. Input Iow configures OSC IN, OSC OUT for crystal oscillator clock frequency will be $1 / 58$ of frequency at BUF OSC OUT. |
| 25 | 43 | BUF OSC OUT | Buffered Oscillator Output. |
| 26 | 48 | RUN/ $/ \overline{\text { HOLD }}$ | Input High - Conversions continuously performed every 8192 clock pulses. Input Low - Conversion in progress completed, converter will stop in AutoZero seven counts before integrate. |
| 27 | 49 | SEND | Input - Used in handshake mode to indicate ability of an external device to accept data. Connect to $\mathrm{V}_{S}^{+}$if not used. |
| 28 | 50 | $\mathrm{V}^{-}$ | Analog Negative Supply - Nominally -5 V with respect to GND (Pin 1). |
| 29 | 51 | REF OUT | Reference Voltage Output - Nominally 2.8 V down from $\mathrm{V}^{+}$(Pin 40). |
| 30 | 52 | BUFFER | Buffer Amplifier Output. |
| 31 | 54 | AUTO-ZERO | Auto-Zero Node - Inside foil of Caz. |
| 32 | 55 | INTEGRATOR | Integrator Output - Outside foil of Cint. |
| 33 | 56 | COMMON | Analog Common - System is Auto-Zeroed to COMMON. |
| 34 | 57 | INPUT LOW | Differential Input Low Side. |
| 35 | 59 | INPUT HIGH | Differential Input High Side. |
| 36 | 1 | REF IN + | Differential Reference Input Positive. |
| 37 | 3 | REF CAP + | Reference Capacitor Positive. |
| 38 | 5 | REF CAP - | Reference Capacitor Negative. |
| 39 | 6 | REF IN - | Differential Reference Input Negative. |
| 40 | 7 | $\mathrm{V}^{+}$ | Positive Supply Voltage - Nominally +5 V with respect to GND (Pin 1). |

NOTE: All digital levels are positive true.

## Pin Configuration




Figure 1A: TSC7109 UART Interface. Send Any Word to UART to Transmit Latest Result.


Figure 1B: TSC7109 Parallel Interface with 8048/8049 Microcomputer

## Detailed Description

## Analog Section

Figure 2 shows a block diagram of the Analog Section of the TSC7109. The circuit will perform conversions at a rate determined by the clock frequency ( 8192 clock periods per cycie), when the RUN/HOLD input is left open or connected to $\mathrm{V}^{+}$. Each measurement cycle is divided into three phases as shown in Figure 3. They are: (1) Auto-Zero (AZ), (2) Signal Integrate (INT), (3) Reference Deintegrate (DE).

## Auto-Zero Phase

The buffer and the integrator inputs are disconnected from input high and input low and connected to analog common. The reference capacitor is charged to the reference voltage. A feedback loop is closed around the system to charge the auto-zero capacitor, CAZ, to compensate for offset voltage in the buffer amplifier, integrator, and comparator. Since the comparator is included in the loop, the A-Z accuracy is limited only by the noise of the system. The offset referred to the input is less than $10 \mu \mathrm{~V}$.


Figure 2: Analog Section

## Signal Integrate Phase

The buffer and integrator inputs are removed from COMMON and connected to input high and input low. The auto-zero loop is opened. The auto-zero capacitor is placed in series in the loop to provide an equal and opposite compensating offset voltage. The differential voltage between input high and input low is integrated for a fixed time of 2048 clock periods. At the end of this phase, the polarity of the integrated signal is determined. If the input signal has no return to the converter power supply, input low can be tied to analog common to establish the correct common-mode voltage.

## De-Integrate Phase

Input high is connected across the previously charged reference capacitor and input low is internally connected to analog common. Circuitry within the chip ensures that the capacitor will be connected with the correct polarity to cause the integrator output to return to the zero crossing (established by AUTO-ZERO) with a fixed slope. The time, represented by the number of clock periods counted for the output to return to zero, is proportional to the input signal.

## Differential Input

The TSC7109 has been optimized for operation with analogcommon near digital ground. With +5 V and -5 V power supplies, a full $\pm 4 \mathrm{~V}$ full-scale integrator swing maximizes the analog section's performance.

A typical CMRR of 86 dB is achieved for input differential voltages anywhere within the common-mode range of 0.5 volts below the positive supply to 1.0 volts above the negative supply. However, since the integrator also swings with the common-mode voltage, care must be exercised to assure the integrator output does not saturate. A worst case condition is near a full-scale negative differential input voltage with a large positive common-mode voltage. The negative input
signal drives the integrator positive when most of its swing has been used up by the positive common-mode voltage. In such cases, the integrator swing can be reduced to less than the recommended $\pm 4 \mathrm{~V}$ full-scale value, with some loss of accuracy. The integrator output can swing to within 0.3 volts of either supply without loss of linearity.

## Differential Reference

The reference voltage can be generated anywhere within the power supply voltage of the converter. Rollover voltage is the main source of common-mode error. It is caused by the reference capacitor losing or gaining charge due to stray capacity on its modes. With a large common-mode voltage, the reference capacitor can gain charge (increase voltage) when called up to de-integrate a positive signal and lose charge (decrease voltage) when called up to de-integrate a negative input signal. This difference in reference for ( + ) or $(-)$ input voltage will cause a roll-over error. This error can be held to less than 0.5 count worst case by using a large reference capacitor in comparision to the stray capacitance. To minimize roll-over error from these above sources keep the reference common-mode voltage near or at analog common.

## Digital Section

The digital section is shown in block diagram Figure 4 and includes the clock oscillator and scaling circuit, a 12-bit binary counter with output latches and TTL-compatible three-state output drivers, UART handshake logic, polarity, overrange and control logic. Logic levels are referred to as "low"or "high". The actual logic levels are defined in Table 1 "Operating Characteristics."
Inputs driven from TTL gates should have 3-5 k pullup resistors added for maximum noise immunity. For minimum power consumption, all inputs should swing from GND (low) to $\mathrm{V}^{+}$(high).


Figure 3: Conversion Timing (RUN/HOLD Pin High)


Figure 4: Digital Section

## STATUS Output

During a conversion cycle, the STATUS output goes high at the beginning of Signal Integrate and goes low one-half clock period after new data from the conversion has been stored in the output latches. See Figure 3. The signal may be used as a "data valid" flag to drive interrupts, or for monitoring the status of the converter. (Data will not change while STATUS is Iow).

## MODE Input

The output mode of the converter is controlled by the MODE input. The converter is in its "Direct" output mode, when the MODE pin is low or left open. The output data is directly accessible under the control of the chip and byte enable inputs (this input is provided with a pulldown resistor to ensure a low level when the pin is left open). When the MODE input is pulsed high, the converter enters the UART
handshake mode and outputs the data in two bytes, then returns to "direct" mode. When the MODE input is kept high, the converter will output data in the handshake mode at the end of every conversion cycle with MODE $=0$ (Direct BUS Transfer) the send input should be tied to $\mathrm{V}^{+}$. (See Handshake Mode Section).

## RUN/ $\overline{\text { HOLD }}$ Input

With RUN/FOLD high or open, the circuit operates normally as a dual slope A/D as shown in Figure 3. Conversion cycles operate continuously with the output latches updated after zero crossing in the de-integrate mode. An internal pullup resistor is provided to insure a high level with an open input. The RUN/ $\overline{\text { HOLD }}$ may be used to shorten conversion time. If the RUN/ $\overline{H O L D}$ goes low at anytime after zero crossing in the de-integrate mode, the circuit will jump to auto-zero and eliminate that portion of time normally spent in de-integrate.


Figure 5: TSC7109 RUN/HOLD Operation

If RUN/HOLD stays or goes low the conversion will complete with minimum time in de-integrate. It will stay in auto-zero for the minimum time and wait in auto-zero for a high in the RUN/ $\overline{\mathrm{HOLD}}$ input. As shown in Figure 5, the STATUS output will go high seven clock periods after RUN/HOLD is changed to high, and the converter will begin the integrate phase of the next conversion.
The RUN/ $\overline{H O L D}$ input allows controlled conversion interface. The converter may be held at idle in auto-zero with RUN/HOLD low. The conversion is started when RUN/HOLD goes high and the new data is valid when the STATUS output goes low (or is transferred to the UART - see Handshake Mode.) RUN/HOLD may now go low, terminating deintegrate and ensuring a minimum auto-zero time before stopping to wait for the next conversion. Conversion time can be minimized by ensuring RUN/HOLD goes low during deintegrate, after zero crossing, and goes high after the hold point is reached. The required activity on the RUN/ $\overline{H O L D}$ input can be provided by connecting it to the Buffered Oscillator output. In this mode, the input value measured determines the conversion time.

## Direct Mode

The data outputs (bits 1 through 8 low order byte, bits 9 through 12, polarity and overrange high order byte) are accessible under control of the byte and chip enable terminals as inputs with the MODE pin at a low level. These three inputs are all active low. Internal pullup resistors are provided for an inactive high level when left open. When the chip erable input is low, a byte enable input low will allow the outputs of that byte to become active. A variety of parallel data accessing techniques may be used, as shown in the section entitled "Interfacing." (See Figure 6 and Table 3)
The access of data should be synchronized with the conversion cycle by monitoring the STATUS output. This will prevent accessing the data while it is being updated and eliminate the acquisition of erroneous data.


Figure 6: TSC7109 Direct Mode Output TIming

| Symbol | Description | Min. | Typ. Max. | Units |  |
| :--- | :--- | :--- | :--- | :--- | :--- |
| tBEA | Byte Enable Width | 350 | 220 |  | ns |
| tDAB | Data Access Time <br> from Byte Enable | 150 | 350 | ns |  |
| tDHB | Data Hold Time <br> from Byte Enable | 150 | 300 | ns |  |
| tCEA | Chip Enable Width | 400 | 260 |  | ns |
| tDAC | Data Access Time <br> from Chip Enable | 260 | 400 | ns |  |
| tDHC | Data Hold Time <br> from Chip Enable | 240 | 400 | ns |  |

Table 3. TSC7109 Direct Mode TIming Requirements Handshake Mode
An alternative means of interfacing the TSC7109 to digital systems is provided when the handshake output mode of the TSC7109 becomes active in controlling the flow of data instead of passively responding to chip and byte enable inputs. This mode allows a direct interface between the TSC7109 and industry-standard UART's with no external logic required. The TSC7109 provides all the control and flag signals necessary to sequence the two bytes of data into the UART and initiate their transmission in serial form when triggered into the handshake mode. The cost of designing remote data acquisition stations is reduced using serial data transmission to minimize the number of lines to the central controlling processor.

The MODE pin controls the handshake mode. When the MODE terminal is held high, the TSC7109 will enter the handshake mode after new data has been stored in the output latches at the end of every conversion performed (see Figures 7 and 8). Entry into the handshake mode may be triggered on demand by the MODE terminal. At any time during the conversion cycle, the low to high transition of a short pulse at the MODE input will cause immediate entry into the handshake mode. If this pulse occurs while new data is being stored, the entry into handshake mode is delayed until the data is stable. The MODE input is ignored in the handshake mode, and until the converter completes the output cycle and clears the handshake mode data updating will be inhibited (see Figure 9).
When the MODE input is high or when the converter enters the handshake mode, the chip and byte enable terminals become TTL-compatible outputs which provide the output cycle control signals (see Figures 7,8 and 9).
The SEND input is used by the converter as an indication of the ability of the receiving device (such as a UART) to accept data in the handshake mode. The sequence of the output cycle with SEND held high is shown in Figure 7. The handshake mode (Internal MODE high) is entered after the data latch pulse (the $\overline{C E} / \overline{L O A D}, \overline{L B E N}$ and $\overline{\mathrm{HBEN}}$ terminals are active as outputs since MODE remains high).
The high level at the SEND input is sensed on the same high to low internal clock edge. On the next low to high internal clock edge the high-order byte (bits 9 through 12, POL, and OR) outputs are enabled and the $\overline{C E / \overline{L O A D} \text { and the } \overline{\mathrm{HBEN}}}$
outputs assume a low level. The $\overline{C E} / \overline{L O A D}$ output remains low for one full internal clock period only; the data outputs remain active for $1-1 / 2$ internal clock periods; and the high byte enable remains low for two clock periods. The $\overline{C E} / \overline{L O A D}$ output low level or low to high edge may be used as a synchronizing signal to ensure valid data, and the byte enable as an output may be used as a byte identification flag. With SEND remaining high the converter completes the output cycle using $\overline{C E} /$ LOAD and LBEN while the low order byte outputs (bits 1 through 8) are activated. When both bytes are sent the handshake mode is terminated. The typical UART interfacing timing is shown in Figure 8. The SEND input is used to delay portions of the sequence, or handshake to ensure correct data transfer. This timing diagram shows an industry-standard HD6402 or CDP1854 CMOS UART to interfacing serial data channels. The SEND input to the TSC7109 is driven by the TBRE (Transmitter Buffer Register Empty) output of the UART, and the CE/LOAD terminal of the TSC7109 drives the TBRL (Transmitter Buffer Register Load) input to the UART. The eight transmitter Buffer Register inputs accept the parallel data outputs. With the UART Transmitter Buffer Register empty, the SEND input will be high when the handshake mode is entered after new data is stored. The high order byte outputs become active and the CE/LOAD and HBEN terminals will go low after SEND is sensed. When $\overline{C E} / L O A D$ goes high at the end of one clock period, the high order byte data is clocked into the UART Transmitter Buffer Register. The UART TBRE output will go low, which halts the output cycle with the HBEN
output low, and the high order byte outputs active. When the UART has transferred the data to the Transmitter Register and cleared the Transmitter Buffer Register, the TBRE returns high. The high order byte outputs are disabled on the next TSC7109 internal clock high to low edge, and one-half internal clock later, the HBEN output returns high. The $\overline{C E / L O A D}$ and LBEN outputs go low at the same time as the low order byte outputs become active. When the $\overline{C E / L O A D}$ returns high at the end of one clock period, the low order data is clocked into the UART Transmitter Buffer Register, and TBRE again goes low. The next TSC7109 internal clock high to low edge will sense when TBRE returns to a high, disabling the data outputs. One-half internal clock later, the handshake mode is cleared, and the CE/LOAD, $\overline{\text { HBEN }}$ and LBEN terminals return high and stay active, if MODE still remains high.
Handshake output sequences may be performed on demand by triggering the converter into handshake mode with a low to high edge on the MODE input. A handshake output sequence triggered is shown in Figure 9. The SEND input is low when the converter enters handshake mode. The whole output sequence is controlled by the SEND input, and the sequence for the first (high order) byte is similar to the sequence for the second byte.

This diagram also shows that the output sequence takes Ionger than a conversion cycle. New data will not be latched when the handshake mode is still in progress and is therefore lost.


Figure 7: TSC7109 Handshake with Send Input Held Positive


Figure 8: TSC7109 Handshake - Typical UART Interface Timing


Figure 9: TSC7109 Hardshake Triggered by Mode Input

# 12-Bit Plus Sign Integrating A/D Converter - BUS Compatible - Serial Data Transmission w/UART 

## Oscillator

The oscillator may be overdriven, or may be operated as an RC or crystal oscillator. The OSCILLATOR SELECT input optimizes the internal configuration of the oscillator for RC or crystal operation. The OSCILLATOR SELECT input is provided with a pullup resistor. When the OSCILLATOR SELECT input is high or left open, the oscillator is configured for RC operation. The internal clock will be the same frequency and phase as the signal at the BUFFERED OSCILLATOR OUTPUT. Connect the resistor and capacitor as in Figure 10. The circuit will oscillate at a frequency given by $f=$ $0.45 / R C$. a 100 k resistor is recommended for useful ranges of frequency. The capacitor value should be chosen such that 2048 clock periods are close to an integral multiple of the 60 Hz period for optimum 60 Hz line rejection.
With OSCILLATOR SELECT input low, two on-chip capacitors and a feedback device are added to the oscillator. In this configuration, the oscillator will operate with most crystals in the 1 to 5 MHz range with no external components (Figure 11). The OSCILLATOR SELECT input low inserts a fixed $\div 58$ divider circuit between the BUFFERED OSCILLATOR OUTPUT and the internal clock. A 3.58 MHz TV crystal gives a division ratio providing an integration time given by:

$$
\mathrm{T}=\left(2048 \text { clock periods) } \frac{58}{3.58 \mathrm{MHz}}=33.18 \mathrm{~ms}\right.
$$

The error is less than one percent from two 60 Hz periods or 33.33 ms which will give better than $40 \mathrm{~dB}, 60 \mathrm{~Hz}$ rejection. The converter will operate reliably at conversion rates of up to 30 per second, corresponding to a clock frequency of 245.8 kHz .


Flgure 10: TSC7109 RC Oscillator


Figure 11: TSC7109 Crystal Oscillator

When the oscillator is to be overdriven, the OSCILLATOR OUTPUT should be left open, and the overdriving signal should be applied at the OSCILLATOR INPUT. The internal clock will be of the same duty cycle, frequency and phase as the input signal. When the OSCILLATOR SELECT is at GND, the clock will be $1 / 58$ of the input frequency.

## Test Input

The counter and its outputs may be tested easily. When the TEST input is connected to GND, the internal clock is disabled, and the counter outputs are all forced into the high state. When the input returns to the $1 / 2\left(\mathrm{~V}^{+}-\mathrm{GND}\right)$ voltage or to $\mathrm{V}^{+}$and one clock is input, the counter outputs will all be clocked to the low state.

The counter output latched are enabled when the TEST input is taken to a level halfway between $\mathrm{V}^{+}$and GND allowing the counter contents to be examined anytime.

## Component Value Selection

The integrator output swing for full-scale should be as large as possible. For example, with +5 V supplies and COMMON connected to GND, the nominal integrator output swing at full-scale is $\pm 4 \mathrm{~V}$. Since the integrator output can go to 0.3 V from either supply without significantly affecting linearity, a 4 V integrator output swing allows 0.7 V for variations in output swing due to component value and oscillator tolerances. With $\pm 5 \mathrm{~V}$ supplies and a common-mode voltage range of $\pm 1 \mathrm{~V}$ required, the component values should be selected to provide $\pm 3 \mathrm{~V}$ integrator output swing. Noise and rollover errors will be slightly worse than in the $\pm 4 \mathrm{~V}$ case. For large common-mode voltage ranges, the integrator output swing must be reduced further. This will increase both noise and rollover errors. To improve the performance, $\pm 6 \mathrm{~V}$ supplies may be used.

## Integrating Capacitor

The integrating capacitor CINT should be selected to give the maximum integrator output voltage swing that will not saturate the integrator to within 0.3 volt from elther supply. $A \pm 3.5$ to $\pm 4$ volt integrator output swing is nominal for the TSC7109 with $\pm 5$ volt supplies and analog common connected to GND. For 7-1/2 conversions per second ( 61.72 kHz internal clock frequency) nominal values $\mathrm{C}_{\text {INT }}$ and $\mathrm{C}_{A z}$ are $0.15 \mu \mathrm{~F}$ and $0.33 \mu \mathrm{~F}$, respectively. These values should be changed if different clock frequencies are used to maintain the integrator output voltage swing. The value of CINT is given by:

$$
\mathrm{C}_{\text {INT }}=\frac{(2048 \times \text { Clock Period })(20 \mu)}{\text { Integrator Output Voltage Swing }}
$$

The Integrating capacitor must have low dielectric absorption to prevent rollover errors. Polypropylene capacitors give undetectable errors at reasonable cost up to $85^{\circ} \mathrm{C}$. Tefion ${ }^{*}$ capacitors are recommended for the military temperature range. While their dielectric absorption characteristics vary somewhat between units, devices may be selected to less than 0.5 count of error due to dielectric absorption.

## Integrating Resistor

The integrator and the buffer amplifier both have a class A output stage with $100 \mu \mathrm{~A}$ of quiescent current. They supply $20 \mu \mathrm{~A}$ of drive current with negligible non-linearity. The integrating resistor should be large enough to remain in this very linear region over the input voltage range, but small enough that undue leakage requirements are not placed on the PC board. For 4.095 volt full-scale a $200 \mathrm{k} \Omega$ and for 409.6 mV fullscale a $20 \mathrm{k} \Omega$ are recommended. Rint may be selected for other values of full-scale by:

$$
\text { RINT }=\frac{\text { Full-Scale Voltage }}{20 \mu \mathrm{~A}}
$$

## Auto-Zero Capacitor

As the auto-zero capacitor is made large the system noise is reduced. Since it is in parallel with the integrating capacitor, it forms an RC time constant that determines the error that exists at the end of an auto-zero cycle and speed of recovery from overloads. For 4.096 V full-scale where recovery is most important, a value of $\mathrm{C}_{A Z}$ equal to half of $\mathrm{C}_{\text {INT }}$ should be used.
For 409.6 mV full-scale where noise is very important and the integrating resistor is small, use a value of CAZ twice CInt. The inner foil of $\mathrm{C}_{A Z}$ should be connected to pin 31 and the outer foil to the RC summing junction. The inner foil of $\mathrm{C}_{\text {INT }}$ should be connected to the RC summing junction and the outer foil to pin 32 for best rejection of the stray pickup. For low leakage at temperatures above $85^{\circ} \mathrm{C}$ use Teflon ${ }^{( }$ capacitors.

## Reference Capacitor

A $1 \mu \mathrm{~F}$ capacitor is recommended for most circuits. However, where a large common-mode voltage exists a larger value is required to prevent rollover error (for example: the reference low is not analog common) and a 409.6 mV scale is used. The rollover error will be held to 0.5 count with a $10 \mu \mathrm{~F}$ capacitor. For temperatures above $80^{\circ} \mathrm{C}$ use Teflon® or equivalent capacitors for their low leakage characteristics.

## Reference Voltage

To generate full-scale output of 4096 counts the analog input required is $\mathrm{V}_{\text {IN }}=2 \mathrm{~V}_{\text {REF }}$. For a 4.096 V full-scale use a reference of 2.048 V . In many applications where the $A / D$ is connected to a transducer, there will exist a scale factor between the input voltage and the digital reading. For instance, in a measuring system, the designer might like to have a fullscale reading when the voltage from the transducer is 700 mV . Instead of dividing the input down to 409.6 mV , the designer should use the input voltage directly and select $V_{R E F}=350 \mathrm{mV}$. Suitable values for integrating resistor and capacitor would be 34 k and $0.15 \mu \mathrm{~F}$. This makes the system slightly quieter and also avoids a divider network on the input. Another advantage of this system occurs when temperature and weight measurements with an offset or tare are desired for non-zero input. The offset may be introduced by connecting the voltage output of the transducer between
common and analog high, and the offset voltage between common and analog low, observing polarities carefully. In processor-based systems using the TSC7109, it may be more desirable to use software and perform this type of scaling or tare subtraction digitally.

## Reference Sources

A major factor in the absolute accuracy of the converter is the stability of the reference voltage. The 12-bit resolution of the TSC7109 is one part in 4096, or 244 ppm . Thus, for the onboard reference temperature coefficient of $80 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ a temperature difference of $3^{\circ} \mathrm{C}$ will introduce a one-bit absolute error. Where the ambient temperature is not controlled or where high-accuracy absolute measurements are being made it is recommended that an external high-quality reference be used.
A Reference Output (pin 29) is provided which may be used with a resistive divider to generate a suitable reference voltage. 20 mA may be sunk without significant variation in output voltage. A pullup bias device is provided which sources about $10 \mu \mathrm{~A}$. The output voltage is nominally 2.8 V below $\mathrm{V}^{+}$. When using the on-board reference, Ref Out (pin 29) should be connected to Ref - (Pin 39), and Ref + should be connected to the wiper of a precision potentiometer between Ref Out and $\mathrm{V}^{+}$. The test circuit shows the circuit for a 204.8 mV reference, generated by a $2 \mathrm{k} \Omega$ precision potentiometer in series with a $24 \mathrm{k} \Omega$ fixed resistor.

## Interfacing <br> Direct Mode

Combinations of chip enable and byte enable control signals which may be used when interfacing the TSC7109 to parallel data lines as shown in Figure 12. The $\overline{C E / L O A D}$ input may be tied low, allowing either byte to be controlled by its own enable (Figure 12A). Figure 12 B shows the HBEN and LBEN as flag inputs, and $\overline{C E} / \overline{L O A D}$ as a master enable, which could be the READ strobe available from most microprocessors. Figure 12 C shows a configuration where the two byte enables are connected together. The $\overline{\mathrm{CE}} / \overline{\mathrm{LOAD}}$ is a chip enable, and the $\overline{H B E N}$ and $\overline{\text { LBEN }}$ may be used as a second chip enable or connected to ground. The 14 data outputs will be enabled at the same time. In the direct MODE, SEND should be tied to $\mathrm{V}^{+}$.
Figure 13 interfaces several TSC7109's to a bus, ganging the HBEN and LBEN signals to several converters together, and using the $\overline{C E} / \overline{L O A D}$ inputs to select the desired converter.
Figures 14-19 give practical circuits utilizing the parallel tristate output capabilities of the TSC7109. Figure 14 shows parallel interface to the intel MCS-48, -80 and -85 systems via an 8255 PPI, where the TSC 7109 data outputs are active atall times. The 8155 I/O ports may be used in an identical manner. This interface can be used in an identical manner. This interface can be used in a read-after-update sequence, as shown in Figure 15. The data is accessed by the high to low transition of the STATUS driving an interrupt to the microprocessor.


Figure 12: Direct Mode Chip and Byte Enable Combinations

The RUN/ $\overline{\text { HOLD }}$ input is also used to initiate conversions under software control. Figure 16 gives an interface to Motorola MC6800 or MOS technology MCS650X systems.
An interrupt is generated through the control Resistor B, CB1 line from the high to low transition of the STATUS output. The RUN/HOLD pin is controlled by CB2 through Control Register B, allowing software control of conversions.
Direct interfacing to most microprocessor busses is easily
accomplished through the tri-state output of the TSC7109.
Figures 1B, 17 and 18 are typical connection diagrams. To be sure that requirements for setup and hold times, minimum pulse widths, and the drive limitations on long busses are met, it is necessary to carefully consider the system timing in this type of interface. This type of interface is used when the memory peripheral address density is low providing simply address decoding. Interrupt handling can be simplified by using an interface to reduce the component count.


Figure 13: Three-Stating Several TSC7109's to a Small Bus

## 12-Bit Plus Sign

Integrating A/D Converter

- BUS Compatible
- Serial Data Transmission w/UART


Figure 14: Full-Time Parallel Interface to MCS-48, -80, -85 Microcomputer Systems


Figure 15: Full-Time Parallel Interface to MCS-48, -80, -85 Microcomputers with Interrupt


Figure 16: Full-Time Parallel Interface to MC6800 or MCS650X Microprocessors


Figure 17: Direct Interface - TSC7109 to 8080/8085

## Handshake Mode

The handshake mode provides an interface to a wide variety of external devices. The byte enables may be used as byte identification flags or as load enables and external latches may be clocked by the rising edge of $\overline{C E} / \overline{\mathrm{OAD}}$. A handshake interface to Intel microprocessors using an 8255 PPI as shown in Figure 19. The handshake operation with the 8255 is controlled by inverting its Input Buffer Full (IBF) flag to drive the SEND input to the TSC7109, and using the $\overline{\mathrm{CE}} / \overline{\mathrm{LOAD}}$ to drive the 8255 strobe. The internal control register of the PPI should be set in MODE 1 for the port used. If the 8255 IBF flag is low and the TSC7.109 is in handshake mode the next word will be strobed into the port. The strobe will cause IBF to go high (SEND goes low), which will keep the enabled byte outputs active. The PPI will generate an interrupt which when executed will result in the data being read. The IBF will be reset low when the byte is read causing the TSC7109 to sequence into the next byte. The MODE input to the TSC7109 is connected to the control line on the PPI.
The data from every conversion will be sequenced in two bytes in the system, if this output is left high, or tied high separately. (The data access must take less time than a conversion). The output sequence can be obtained on demand if this output is made to go from low to high and the interrupt may be used to reset the MODE bit.
Conversions may be obtained on command under software control by driving the RUN/ $\overline{H O L D}$ input to the TSC7109 by a
bit of the 8255. Another peripheral device may be serviced by the unused port of the 8255. The 8155 may be used in a similar manner. The MCS650X microprocessors are shown in Figure 20 with MODE and RUN/HOLD tied high to save port outputs.
The handshake mode is particularly useful for directly interfacing to industry standard UARTs (such as Western Digital TR1602) providing a means of serially transmitting converted data with minimum component count.
A typical UART connection is shown in Figure 1A. In this circuit, any word received by the UART causes the UART DR (Data Ready) output to go high. The MODE input to the TSC7109 goes high, triggering the TSC7109 into handshake mode. The high order byte is output to the UART and when the UART has tranferred the data to the Transmitter Register, TBRE (SEND) goes high again, $\overline{\text { LBEN }}$ will go high, driving the UART DRR (Data Ready Reset) which will signal the end of the transfer of data from the TSC7109 to the UART.
An extension of the Typical Connection to several TSC7109's with one UART is shown in Figure 21. In this circuit, the word received by the UART (available at the RBR outputs when DR is high) is used to select which converter will handshake with the UART. Up to eight TSC7109's may interface with one UART, with no external components. Up to 256 converters may be accessed on one serial line with additional components.


Figure 18: Direct TSC7109 - MC6800 Bus Interface


Figure 19: Handshake Interface - TSC7109 to MCS-48, -80, -85


FIgure 20: Handshake Interface - TSC7109 to MC6800, MCS650X

## 12-Bit Plus Sign

Integrating A/D Converter

## - BUS Compatible

- Serial Data Transmission w/UART


FIgure 21: Handshake Interface for Multiplexed Converters

## Integrating Converter Features

The output of Integrating A/D converters represents the integral or average of an input voltage over a fixed period of time. Compared with techniques in which the input is sampled and held, the integrating converter will average the effects of noise. A second important characteristic is that time is used to quantise the answer, resulting in extremely small nonlinearity errors and no missing output codes. The integrating converter also has very good rejection of frequencies whose periods are an integral multiple of the measurement period. This feature can be used to advantage in reducing line frequency noise. (Figure 22)

## Crystals

The 3.58 mHz oscillator crystal is available from:

1. Jameco Electronics

1355 Shoreway Road
Belmont, CA 94002
(415) 592-8097

Part No. CY 3.57


Figure 22: Normal Mode Rejectlon of Dual-Slope Converter as a Function of Frequency.
2. DIGI-KEY Corp.

Highway 32 South
P.O. Box 677

Thief River Falls, MN 56701-9988
1-800-344-4539
Part No. X0005

## Package Information



## General Description

The TSC8700/8701/8702s are 8/10/ 12 bit monolithic CMOS analog-to-digital converters. Fully self-contained in a single 24-pin dual in-line package, each converter requires only passive support components, reference and power supplies.
Conversion is performed by an incremental charge balancing technique which has inherently high accuracy, linearity and noise immunity. An amplifier integrates the sum of the unknown analog current and pulses of a reference current, and the number of pulses (charge increments) needed to maintain the amplifier summing junction near zero is counted. At the end of conversion the total count is latched into the digital outputs as an 8/10/12-bit binary word.

## Ordering Information

| Part No. | Resolution | Conv. Time | Package | Temp. Range |
| :---: | :---: | :---: | :---: | :---: |
| TSC8700CJ | 8-Bit | $\begin{array}{r} 1.25 \\ \mathrm{mSec} \end{array}$ | $24-\mathrm{Pin}$ <br> Plastic Dip | $\begin{aligned} & 0^{\circ} \mathrm{C} \text { to } \\ & +70^{\circ} \mathrm{C} \end{aligned}$ |
| TSC8700CL | 8-Bit | $\begin{array}{r} 1.25 \\ \mathrm{mSec} \end{array}$ | $\begin{array}{r} 24-\mathrm{Pin} \\ \text { CerDIP } \end{array}$ | $\begin{array}{r} -40^{\circ} \mathrm{C} \text { to } \\ +85^{\circ} \mathrm{C} \end{array}$ |
| TSC8701CL | 10-Bit | $\begin{array}{r} 5.0 \\ \mathrm{mSec} \end{array}$ | $\begin{array}{r} 24-\mathrm{Pin} \\ \text { CerDIP } \end{array}$ | $\begin{array}{r} -40^{\circ} \mathrm{C} \text { to } \\ +85^{\circ} \mathrm{C} \end{array}$ |
| TSC8702CN | 12-Bit | $\begin{array}{r} 20 \\ \mathrm{mSec} \end{array}$ | 24-Pin Ceramic | $\begin{array}{r} -40^{\circ} \mathrm{C} \text { to } \\ +85^{\circ} \mathrm{C} \end{array}$ |

## Pin Configuration



## Note:

Do not make connections to pin 1, 2, 3 or 4 on 8700; pin 1 or 2 on 8701 These pins are internally connected.

## Features

- High Accuracy - Up to 12-Bit Resolution With < $\pm 1 / 2$ LSB Error
- Tight DNL of $< \pm 1 / 2$ LSB
- Monotonic Performance - No Missing Codes
- Monolithic CMOS Construction Gives Low Power Dissipation - 20 mW Typical
- Contains All Required Active Elements - Needs only Passive Support Components, Reference Voltage and Dual Power Supply
- High Stability Over Full Temperature Range
- Gain Temperature Coefficient Typically $<25 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$
- Zero Drift Typically $<30 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$
- Differential Non-Linearity Drift Typically $<25 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$
- Latched Parallel Binary Outputs
- LPTTL, 74LS, CMOS Compatible Outputs and Control Inputs
- Strobed or Free Running Conversion
- Infinite Input Range - Any Positive Voltage Can Be Applied Via a Scaling Resistor


## Absolute Maximum Ratings

Storage Temperature
$-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$
Operating Temperature
(L, N) Package ....................... $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$
J Package ................................ $0^{\circ}$ to $+70^{\circ} \mathrm{C}$
VDD -VSS ........................................................ 18 V
IIN $\pm 10 \mathrm{~mA}$
Iref $\pm 10 \mathrm{~mA}$
Digital Input Voltage .................. - 0.3 to VDD +0.3 V
Operating VDD and VSS Range ................ 3.5 V to 7 V
Package Dissipation ................................. 500 mW
Lead Temperature ........................................ . $300^{\circ} \mathrm{C}$
(Soldering, 10 seconds)

## Handling Precautions

The 8700 series are CMOS devices must be handled correctly to prevent damage. Package and store only in conductive foam, anti-static tubes or other conductive material. Use proper anti-static handling procedures. Do not connect in circuits under "power on" conditions, as high transients may cause permanent damage.

Electrical Characteristics: Unless otherwise specified, $V_{D D}=+5 \mathrm{~V}, \mathrm{~V}_{S S}=-5 \mathrm{~V}, \mathrm{~V}_{G N D}=0, \mathrm{~V}_{\mathrm{REF}}=-6.4 \mathrm{~V}, \mathrm{R}_{\mathrm{B}} \mathrm{AS}=$ $100 \mathrm{k} \Omega$, test circuit shown. $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ unless Full Temperature Range is specified $\left(-40^{\circ} \mathrm{C}\right.$ to $+85^{\circ} \mathrm{C}$ for N and L package, $0^{\circ}$ to $70^{\circ} \mathrm{C}$ for J package).

| PARAMETER | CONDITIONS | DEFINITION | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Accuracy Resolution Accuracy |  | Binary Word Length Of Digital Output TSC8700 TSC8701 TSC8702 | $\begin{array}{r} 8 \\ 10 \\ 12 \end{array}$ | - | 二 | $\begin{aligned} & \text { Bits } \\ & \text { Bits } \\ & \text { iits } \end{aligned}$ |
| Relative Accuracy |  | Output Deviation From Straight <br> Line Between Normalized <br> Zero and Full-Scale Input | - | - | $\pm 1 / 2$ | LSB |
| Differential Non-Linearity |  | Deviation From 1 LSB <br> Between Transition Points | - | $\pm 1 / 4$ | $\pm 1 / 2$ | LSB |
| Differential <br> Non-Linearity <br> Temperature Drift | Full <br> Temperature Range | Variation in Differential Non-Linearity Due To Temperature Change | - | $\pm 2.5$ | $\pm 5$ | $\mathrm{ppm} /{ }^{\circ} \mathrm{C}$ |
| Gain Variance |  | Variation From Exact A (Compensate By Trimming Rin or RREF) | - | $\pm 2$ | $\begin{aligned} & +5 \\ & -3 \end{aligned}$ | $\%$ of Nominal |
| Gain <br> Temperature <br> Drift | Full <br> Temperature <br> Range | Variation In A <br> Due To <br> Temperature Change | - | $\pm 25$ | $\pm 75$ | $\mathrm{ppm} /{ }^{\circ} \mathrm{C}$ |
| Zero Offset (TSC8700) | $\begin{aligned} & \mathrm{IIN}_{\mathrm{N}}=0 \\ & \mathrm{C}_{\mathrm{NT}}=68 \mathrm{pF} \\ & \mathrm{RADJ}^{2}=1.6 \mathrm{k} \Omega \\ & \text { See Test Circuit. } \end{aligned}$ | Correction at Zero Adjust to Give Zero Output When Input Is Zero Integration Cap. $=68 \mathrm{pF}$ $R_{A D J}=1.6 \mathrm{k} \Omega$ | - | - | $\pm 80$ | mV |
| Zero Offset (TSC8700) | $\begin{aligned} & \mathrm{IIN}=0 \\ & C_{I N T}=33 \mathrm{pF} \\ & R_{A D J}=1.0 \mathrm{k} \Omega \\ & \text { See Test Circuit. } \end{aligned}$ | Correction at Zero Adjust to Give Zero Output When Input Is Zero Integration Cap. $=33 \mathrm{pF}$ $R_{A D J}=1.0 \mathrm{k} \Omega$ | - | $\pm 10$ | $\pm 50$ | mV |
| Zero Offset (TSC8701) (TSC8702) | $\begin{aligned} & \mathrm{IIN}=0 \\ & \mathrm{C}_{\mathrm{INT}}=68 \mathrm{pF} \\ & \mathrm{RADJ}^{2}=1.0 \mathrm{k} \Omega \\ & \text { See Test Circuit. } \end{aligned}$ | Correction at Zero Adjust to Give Zero Output When Input Is Zero Integration Cap. $=68 \mathrm{pF}$ $R_{A D J}=1.0 \mathrm{k} \Omega$ | - | $\pm 10$ | $\pm 50$ | mV |
| Zero Temperature Drift | Full Temperature Range | Variation in Zero Offest Due to Temperature Change | - | $\pm 30$ | $\pm 50$ | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
| Analog Inputs lin Full-Scale |  | Full-Scale Analog Input Current To Achieve Specified Accuracy | - | 10 | - | $\mu \mathrm{A}$ |
| IREF (Note 1) |  | Reference Current Input To Achieve Specified Accuracy | - | -20 | - | $\mu \mathrm{A}$ |
| Digital Inputs | Full Temperature Range | Logical "1" Input Threshold For Initiate Conversion Input | 3.5 | - | - | V |
| $V_{1 N}{ }^{(0)}$ | Full Temperature Range | Logical "0" Input Threshold For Initiate Conversion Input | - | - | 1.5 | V |
| Digital Outputs Vout ${ }^{(1)}$ | Full Temp. Range lout $=-10 \mu \mathrm{~A}$ <br> IOUT $=-360 \mu \mathrm{~A}$ | Logical "1" Output Voltage For Digits Out, Busy, and Data Valid Outputs | $\begin{aligned} & 4.5 \\ & 2.4 \end{aligned}$ | - | 二 | V |
| Vout ${ }^{(0)}$ | $\begin{aligned} & \text { Full Temp. Range } \\ & \text { VDD }=4.75 \mathrm{~V} \\ & \text { IOUT }=360 \mu \mathrm{~A} \end{aligned}$ | Logical "0" Output Voltage For Digits Out, Busy, and Data Valid Outputs | - | - | 0.4 | V |
| Dynamic Conversion Time | Full Temp. Range | Time Required to Perform One Complete A/D Conversion TSC8700 TSC8701 TSC8702 | - | 1.25 5 20 | $\begin{array}{r}1.8 \\ 6 \\ 24 \\ \hline\end{array}$ | ms ms ms |
| Conversion Rate in Free-Run Mode | VINT CONV $=+5 \mathrm{~V}$ | $\begin{aligned} & \text { TSC8700 } \\ & \text { TSC8701 } \\ & \text { TSC8702 } \end{aligned}$ | $\begin{array}{r} 555 \\ 167 \\ 42 \end{array}$ | $\begin{array}{r} 800 \\ 200 \\ 50 \end{array}$ | - | Conv'ns per Second |

Electrical Characteristics (Cont.)

| PARAMETER | CONDITIONS | DEFINITION | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Minimum Pulse Width for Initiate Conversion | Full Temp. Range |  | 500 | - | - | ns |
| Supply Current IDD Quiescent (L/N Package) (J Package) | Full Temp. Range <br> VINT CONV $=0 \mathrm{~V}$ | Current Required From Positive Supply During Operation | - | $\begin{aligned} & 1.4 \\ & 1.4 \end{aligned}$ | $\begin{aligned} & 2.5 \\ & 5.0 \end{aligned}$ | mA ma |
| Iss Quiescent (L/N Package) (J Package) | Full Temp. Range <br> VINIT CONV $=0 \mathrm{~V}$ | Current Required From Negative Supply During Operation | - | $\begin{aligned} & -1.4 \\ & -1.4 \end{aligned}$ | $\begin{aligned} & -2.5 \\ & -5.0 \end{aligned}$ | mA $m A$ |
| Supply Sensitivity | $V_{\text {D }} \pm 1 \mathrm{~V}, \mathrm{~V}_{\text {Ss }} \pm 1 . \mathrm{V}$ | Change in Full-Scale Gain vs Supply Voltage Change | - | $\pm 0.5$ | $\pm 1.0$ | \%/V |
|  | $\left\|\mathrm{V}_{\mathrm{DD}}\right\|=\left\|\mathrm{VSS}_{\text {S }}\right\|=5 \mathrm{~V} \pm 1$ | Change in Full-Scale Gain vs Supply Voltage Change for Tracking Supplies | - | $\pm 0.05$ | $\pm 0.1$ | \%/V |

## NOTE:

IIN and IREF pins connect to the summing junction of an operational amplifier. Voltage sources cannot be attached directly but must be buffered by external resistors. See Test Circuit.

## Test Circuit


2.

Note:

1. Any $V_{\text {REF }}$ greater than -1 V can be used.
$R_{\text {REF }}=\frac{V_{\text {REF }}}{-20 \mu \mathrm{~A}}$
For example with $V_{\text {REF }}=-5 \mathrm{~V}$, RREF $=250 \mathrm{~K}$.

| Part No. | R $_{\text {ADJ }}$ | CINT | Zero Offset Spec |
| :--- | ---: | ---: | ---: |
| TSC8700 | $1.6 \mathrm{k} \Omega$ | 68 pF | $\pm 80 \mathrm{mV}$ |
| TSC8700 | $1.0 \mathrm{k} \Omega$ | 33 pF | $\pm 50 \mathrm{mV}$ |
| TSC8701/8702 | $1.0 \mathrm{k} \Omega$ | 68 pF | $\pm 50 \mathrm{mV}$ |

## Circuit Description

During conversion the sum of a continuous current $I_{\mathrm{N}}$ and pulses of a reference current IREF is integrated for a fixed number of clock periods. lin is proportional to the analog input voltage; IREF is switched in for exactly one clock period just frequently enough to maintain the output of the integrator near zero. Thus, the charge from the continuous lin current is balanced against the pulses of Iref current. The total number of Iref pulses needed during the conversion
period to maintain the charge balance is counted, and the result (in Binary) is latched into the outputs at the end of conversion.

The converter contains two counters and a clock in addition to an operational amplifier, comparator, latching output buffers and housekeeping logic. One counter is a clock counter which (after a reset pulse) starts counting clock pulses; when the required count is reached, the clock counter generates a pulse to start the end-of-conversion routine.

Timing Diagrams (Rise, fall times $=200 \mathrm{~ns}$ typ., $C_{L}=50 \mathrm{pF}$ )


The other counter is a data counter, which is reset synchronously with the clock counter and counts the number of times the Iref current is switched into the summing input of the amplifier during the period defined by the clock counter.
When the Initiate Conversion input is strobed with a positive signal, the busy line latches high and a $10 \mu \mathrm{~s}$ (times given are approximate) start up cycle begins. The integrating capacitor is discharged and both counters are reset during this start up period. Conversion begins at the end of the reset pulse and ends with a pulse generated either by the clock counter or by an overflow condition in the data counter. This pulse disables further inputs into both counters and triggers a $10 \mu$ s shutdown cycle. During the shutdown cycle Data Valid goes low for $5 \mu \mathrm{~s}$. This binary sequence is shown in the timing diagrams. Busy is true high, and when the circuit is busy, Initiate Conversion has no effect and may be high or low. Data Valid is also true high. The data from a conversion remain valid for as long as power is applied to the circuit or until Data Valid falls at the end of a subsequent conversion, at which time the output data are updated to reflect the latest conversion.

## Pin Functions

## Initiate Conversion Input

Accepts CMOS and most 5 V logic inputs. Applying a logic " 1 " to the Initiate Conversion pin initiates the A/D conversion cycle. Once conversion has been initiated, the cycle cannot be interrupted, and the Initiate Conversion pin is disabled until conversion is complete. Two modes of operation are permitted, clocked or free-running. For clocked operation the Initiate Conversion input is held at logic " 0 " for standby and taken to logic " 1 " when a conversion is desired. For freerunning operation the Initiate Conversion pin is connected to VDD or similar permanent logic "1" voltage.

## Busy Output

A digital status output which is compatible with CMOS logic and low power TTL (can sink and source $500 \mu \mathrm{~A}$ ). A logic " 1 " output on the Busy pin indicates a conversion cycle is in
process. A logic " 1 " to logic " 0 " transition indicates that conversion is complete and the result has been latched at the Digits Out pins. A logic " 0 " to logic " 1 " transition indicates a new conversion cycle has been initiated. If the device is operating in the free-running mode, the Busy output will remain low for approximately $2.5 \mu \mathrm{~s}$, marking the completion and initiation of consecutive conversion cycles.

## Data Valid Output

A digital status which is compatible with CMOS logic and low power TTL (can sink and source $50 \mu \mathrm{~A}$ ). A logic " 1 " output at the Data Valid pin indicates that the Digits Out pins are latched with the result of the last conversion cycle. The Data Valid output goes to logic " 0 " approximately $5 \mu$ s before the completion of a conversion cycle. During this $5 \mu \mathrm{~s}$ interval new data is being transferred to the Digits Out pins, and the Digits Out are not valid.

## Digits Out

(Bit 0, Bit 1, etc.)
The binary digit outputs which are the result of the A/D conversion. These outputs are CMOS logic and low power TTL compatible.

## Applications Information Input/Output Relationships

The analog input voltage $\left(\mathrm{V}_{\mathrm{IN}}\right)$ is related to the output by the transfer equation:

$$
\begin{aligned}
\text { Digital Counts } & =\frac{V_{I N} \cdot A \cdot R_{\text {REF }}}{R_{\text {IN }} \cdot V_{\text {REF }}} \\
A & =528 \text { for } 8700 \\
A & =2064 \text { for } 8701 \\
A & =8208 \text { for } 8702
\end{aligned}
$$

where Digital Counts is the value of the binary output word presented at Digits Out pins in response to VIN.

The digital output code format is as follows:

| Analog <br> Input | Digital <br> Output |
| :---: | :---: |
| VIN $\geq$ Full-Scale | $1 \ldots 111 \ldots 1$ |
| $=$ Full-Scale -1 LSB | $1 \ldots 111 \ldots 1$ |
| $=1$ LSB | $0 \ldots 000 \ldots 1$ |
| $\leq 0$ | $0 \ldots 000 \ldots 0$ |

Two's complement coding can be generated by inverting the Most Significant Bit (MSB) signal.

## External Component Selection

Obtaining a high accuracy conversion system depends on the voltage regulation of VREF and the thermal stability of RIN and Rref. The exact dependence is given by the transfer function. System accuracy also depends, to a lesser degree, on the voltage regulation of VDD and Vss. The supply connections VDD and VSS should have bypass capacitors of value $0.1 \mu \mathrm{~F}$ or larger right at the device pins.

## $\mathbf{R i n}_{\mathrm{I}}, \mathbf{R e F}_{\mathrm{EF}}$

Values of these components are chosen to give a full-scale input current of approximately $10 \mu \mathrm{~A}$ and a reference current of approximately $-20 \mu \mathrm{~A}$.

$$
R_{I N} \cong \frac{V_{\text {IN Full-Scale }}}{10 \mu \mathrm{~A}} \quad R_{\text {REF }} \cong \frac{V_{\text {REF }}}{-20 \mu \mathrm{~A}}
$$

Examples:

$$
R_{\mathbb{N}} \cong \frac{10 \mathrm{~V}}{10 \mu \mathrm{~A}}=1 \mathrm{M} \Omega \quad R_{R E F} \cong \frac{-6.4 \mathrm{~V}}{-20 \mu \mathrm{~A}}=320 \mathrm{k} \Omega
$$

Note that these values are approximations, and the exact relationships are defined by the transfer equation. In practice, the value of Rin typically would be trimmed using the optional gain adjust circuit to obtain full-scale output at $V_{I N}$ Full-Scale (see adjustment procedure). Metal film resistors with $1 \%$ tolerance or better are recommended for high accuracy applications because of their thermal stability and low noise generation.

## RBIAS

Specifications for the TSC87XX are based on RBIAS $=100 \mathrm{k} \Omega$ $\pm 10 \%$ unless otherwise noted. However, there are instances when the designer may want to change this resistor in order to affect the conversion time and the supply current. By decreasing RBIAs the A/D will convert much faster and the supply current will be higher. (For example: When RbiAs is 20 k the conversion time is reduced by $1 / 3$, and the supply current will increase from 2 mA to 7 mA .) Likewise, if the

RBIAS is increased the conversion time will be longer and the supply current will be much lower. (For example: When RBIAS $=1 \mathrm{M} \Omega$ the conversion time will be six times longer, and the supply current is now reduced to .5 mA ). For details of this relationship refer to AN 9 typical performance curves.

## Rdamp

Exact value not critical but should have a nominal value of $100 \Omega \pm 10 \%$. Locate close to pin 14.

## Cdamp

Exact value not critical but should have a nominal value of $270 \mathrm{pF} \pm 20 \%$. Locate close to pin 14.

## Cint

Exact value not critical but should have a nominal value of $68 \mathrm{pF} \pm 10 \%$. Low leakage types are recommended, although mica or ceramic devices can be used in applications where their temperature limits are not exceeded. Locate as close as possible to pins 14,15 . For the TSC8700 CINT $=33 \mathrm{pF}$ is adequate with $R_{A D J}=1.0 \mathrm{k} \Omega$.

## Vref

A negative reference voltage must be supplied. This may be obtained from a constant current source circuit or from the negative supply.

## VDD, Vss

Power supplies of $\pm 5 \mathrm{~V}$ are recommended, with $0.05 \%$ line and load regulation and $0.1 \mu \mathrm{~F}$ decoupling capacitors.

## Adjustment Procedure

The test circuit diagram shows optional circuits for trimming the zero location and full-scale gain. Because the digital outputs remain constant outside of the normal operating range (i.e. below zero and above full-scale), it is recommended that transition points be used in setting the zero and full-scale values. Recommended procedure is as follows:

- Set the initiate conversion control high to provide free-run operation and verify that converter is operating.
- Set VIN to $+1 / 2$ LSB and trim the zero adjust circuit to obtain a $000 \ldots 000 \ldots$ to $000 \ldots 001$ transition. This will correctly locate the zero end.
- For full-scale adjustment, set VIN to the full-scale value less $11 / 2$ LSB and trim the gain adjust circuit for a 111 . . . 110 to 111 . . 111 transition.
If adjustments are performed in this order, there should be no interaction and they should not have to be repeated.


## Typical Circuits

## Reference Voltage Supply



## Power Reduction (Reduces Power Consumption to Approximately $500 \mu \mathrm{~A}$ ).



Switch Controlled - Relay Could be Substituted for Switch


TTL System-Controlled - Trades Off Additional Power Consumption at System for Reduced Usage at Remote A/D

## Free-Running Conversion Rate Control



[^5]
## Bipolar Operation




Magnitude-and-Sign Binary

## 12-Bit Serial or $3 \times 4$-Bit Parallel Output Format



## Digital Temperature Monitor



## 8-Bit Microprocessor Interface



- High Speed Conversion: 1-20 mSec
- Latched Parallel Outputs


## TYPICAL PERFORMANCE CURVES



CONVERSION TIME vs SUPPLY VOLTAGE


SUPPLY CURRENT



SUPPLY CURRENT vs SUPPLY VOLTAGE


SUPPLY CURRENT vs TEMPERATURE


## TYPICAL PERFORMANCE CURVES






OUTPUT SINK CURRENT vs SUPPLY VOLTAGE


TRI-STATE PROPAGATION DELAY


## Package Information



## General Description

The TSC8703/8704/8705 are 8/10/ 12 bit monolithic CMOS analog-to-digital converters. Fully self-contained in a single 24-pin dual in-line package, each converter requires only passive support components, reference and power supplies.
Conversion is performed by an incremental charge balancing technique which has inherently high accuracy, linearity and noise immunity. An amplifier integrates the sum of the unknown analog current and pulses of a reference current, and the number of pulses (charge increments) needed to maintain the amplifier summing junction near zero is counted. At the end of conversion the total count is latched into the digital outputs as an $8 / 10 / 12$ bit binary word. The Output Enable control switches the outputs to a high impedance or off state when held high. The off state allows bus organized output connections.

## Ordering information

| Part No. | Resolution | Conv. Time | Package | Temp. Range |
| :---: | :---: | :---: | :---: | :---: |
| TSC8703CJ | 8-Bit | $\begin{array}{r} 1.25 \\ \mathrm{mSec} \end{array}$ | $\begin{array}{r} 24-\text { Pin } \\ \text { Plastic Dip } \end{array}$ | $\begin{aligned} & 0^{\circ} \mathrm{C} \text { to } \\ & +70^{\circ} \mathrm{C} \end{aligned}$ |
| TSC8703CL | 8-Bit | $\begin{array}{r} 1.25 \\ \mathrm{mSec} \end{array}$ | 24-Pin CerDIP | $\begin{array}{r} -40^{\circ} \mathrm{C} \text { to } \\ +85^{\circ} \mathrm{C} \end{array}$ |
| TSC8703BL | 8-Bit | $\begin{array}{r} 1.25 \\ \mathrm{mSec} \end{array}$ | $24-\mathrm{Pin}$ CerDIP | $\begin{array}{r} -55^{\circ} \mathrm{C} \text { to } \\ +125^{\circ} \mathrm{C} \end{array}$ |
| TSC8704CJ | 10-Bit | $\begin{array}{r} 5.0 \\ \mathrm{mSec} \\ \hline \end{array}$ | $\begin{array}{r} 24-\mathrm{Pin} \\ \text { Plastic Dip } \\ \hline \end{array}$ | $\begin{aligned} & 0^{\circ} \mathrm{C} \text { to } \\ & +70^{\circ} \mathrm{C} \end{aligned}$ |
| TSC8704CL | 10-Bit | $\begin{array}{r} 5.0 \\ \mathrm{mSec} \end{array}$ | $\begin{aligned} & 24 \text {-Pin } \\ & \text { CerDIP } \end{aligned}$ | $\begin{array}{r} -40^{\circ} \mathrm{C} \text { to } \\ +85^{\circ} \mathrm{C} \end{array}$ |
| TSC8704BL | 10-Bit | $\begin{array}{r} 5.0 \\ \mathrm{msec} \end{array}$ | $\begin{aligned} & 24 \text {-Pin } \\ & \text { CerDIP } \end{aligned}$ | $\begin{array}{r} -55^{\circ} \mathrm{C} \text { to } \\ +125^{\circ} \mathrm{C} \\ \hline \end{array}$ |
| TSC8705CJ | 12-Blt | $\begin{array}{r} 20 \\ \mathrm{mSec} \end{array}$ | $\begin{array}{r} 24-\mathrm{Pin} \\ \text { Plastic Dip } \\ \hline \end{array}$ | $\begin{aligned} & 0^{\circ} \mathrm{C} 10 \\ & +70^{\circ} \mathrm{C} \\ & \hline \end{aligned}$ |
| TSC8705CN | 12-Bit | $\begin{array}{r} 20 \\ \mathrm{mSec} \\ \hline \end{array}$ | 24-Pin <br> Ceramic | $\begin{array}{r} -40^{\circ} \mathrm{C} \text { to } \\ +85^{\circ} \mathrm{C} \\ \hline \end{array}$ |
| TSC8705BN | 12-B\|t | $\begin{array}{r} 20 \\ \mathrm{msec} \end{array}$ | $\begin{gathered} 24-\mathrm{Pin} \\ \text { Ceramic } \end{gathered}$ | $\begin{array}{r} -55^{\circ} \mathrm{C} \text { to } \\ +125^{\circ} \mathrm{C} \end{array}$ |
| Devicus with MIL-STD-883 Processing* |  |  |  |  |
| TSC8703BL/883 | 8-Bit | $\begin{array}{r} 1.25 \\ \mathrm{mSec} \end{array}$ | $24-\mathrm{Pin}$ CerDIP | $\begin{array}{r} -55^{\circ} \mathrm{C} \text { to } \\ +125^{\circ} \mathrm{C} \end{array}$ |
| TSC8704BL/883 | 10-Blt | $\begin{array}{r} 5.0 \\ \mathrm{msec} \\ \hline \end{array}$ | $\begin{array}{r} 24-\mathrm{Pin} \\ \text { CerDIP } \\ \hline \end{array}$ | $\begin{array}{r} -55^{\circ} \mathrm{C} \text { to } \\ +125^{\circ} \mathrm{C} \\ \hline \end{array}$ |
| TSC8705BN/883 | 12-BIt | $\begin{array}{r} 20 \\ \mathrm{mSec} \end{array}$ | $\begin{array}{r} 24-\text { Pin } \\ \text { Ceramic } \end{array}$ | $\begin{aligned} & -55^{\circ} \mathrm{C} \text { to } \\ & +125^{\circ} \mathrm{C} \end{aligned}$ |

*Level B, MIL-STD-883 Revision B

## Features

- High Accuracy - Up to 12 Bit Resolution With < $\pm 1 / 2$ LSB Error
- Monotonic Performance - No Missing Codes
- Monolithic CMOS Construction Gives Low Power Dissipation - 20 mW Typical
- Contains All Required Active Elements - Needs only Passive Support Components, Reference Voltage and Dual Power Supply
- High Stability Over Full Temperature Range
- Gain Temperature Coefficient Typically $<25 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$
- Zero Drift Typically $<30 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$
- Differential Non-Linearity Drift Typically $<25 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$
- Latched Parallel Binary Outputs
- LPTTL, 74LS, CMOS Compatible Outputs and Control Inputs
- Strobed or Free Running Conversion
- Infinite Input Range - Any Positive Voltage Can Be Applied Via a Scaling Resistor


## Pin Configuration



Note:
Do not make connections to pin 1,2,3 or 4 on 8703; pin 1 or 2 on 8704. These pins are internally connected.

## Handling Precautions

The 8700 series are CMOS devices must be handied correctly to prevent damage. Package and store only in conductive foam, anti-static tubes or other conductive material. Use proper anti-static handling procedures. Do not connect in circuits under "power on" conditions, as high transients may cause permanent damage.

| Absolute Maximum Ratings |  |
| :---: | :---: |
| Storage Temperature | $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
| Operating Temperature |  |
| (BL, BN) | $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |
| (CL) Package | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
| (CJ) Package | $\ldots 0^{\circ}$ to $+70^{\circ} \mathrm{C}$ |
| VDD -VSS | 18 V |


| In | $\pm 10 \mathrm{~mA}$ |
| :---: | :---: |
| Iref | $\pm 10 \mathrm{~mA}$ |
| Digital Input Voltage | -0.3 to $V_{D D}+0.3 \mathrm{~V}$ |
| Operating VDD and VSS Range | .. 3.5 V to 7 V |
| Package Dissipation | 500 mW |
| Lead Temperature .......... (Soldering, 10 seconds) | $\ldots 300^{\circ} \mathrm{C}$ |

Electrical Characteristics: Unless otherwise specified, $\mathrm{V}_{D D}=+5 \mathrm{~V}, \mathrm{~V}_{S S}=-5 \mathrm{~V}, \mathrm{~V}_{\mathrm{GND}}=0, \mathrm{~V}_{\mathrm{REF}}=-6.4 \mathrm{~V}$, RBIAS $=$ $100 \mathrm{k} \Omega$, test circuit shown. $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ unless Full Temperature Range is specified $\left(-55^{\circ} \mathrm{C}\right.$ to $+125^{\circ} \mathrm{C}$ for BN and BL package, $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ for CL package, $0^{\circ}$ to $70^{\circ} \mathrm{C}$ for CJ package).

| PARAMETER | CONDITIONS | DEFINITION | MIN | TYP | $\begin{gathered} \text { CJ/CN } \\ \text { MAX } \end{gathered}$ | BN/BL MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Accuracy |  |  |  |  |  |  |  |
| Resolution |  | Binary Word Length |  |  |  |  |  |
| Accuracy |  | Of Digital Output |  |  |  |  |  |
|  |  | TSC8703 | 8 | - | - | - | Bits |
|  |  | TSC8704 | 10 | - | - | - | Bits |
|  |  | TSC8705 | 12 | - | - | - | Bits |
| Relative Accuracy |  |  |  |  |  |  |  |
|  |  | Line Between Normalized | - | $\pm 1 / 4$ | $\pm 1 / 2$ | $\pm 1 / 2$ | LSB |
|  |  | Zero and Full-Scale Input |  |  |  |  |  |
|  |  | TSC8705CJ (Only) | - | 1.0 | $\pm 1.5$ |  | LSB |
| Differential Non-Linearity |  | Deviation From 1 LSB Between Transition Po | - | $\pm 1 / 4$ | $\pm 1 / 2$ | $\pm 1 / 2$ | LSB |
| Differential | Full | Variation in Differential |  |  |  |  |  |
| Non-Linearity | Temperature | Non-Linearity Due To | - | $\pm 2.5$ | $\pm 5$ | $\pm 5$ | $\mathrm{ppm} /{ }^{\circ} \mathrm{C}$ |
| Temperature Drift | Range | Temperature Change |  |  |  |  |  |
| Gain <br> Variance <br> Gain |  | Variation From Exact A (Compen- |  | +2 | $\pm 5$ | +5 | \% of |
|  |  | sate By Trimming Rin or Rref) |  | $\pm 2$ | $\pm 5$ | $\pm 5$ | Nominal |
|  | Full | Variation In A |  |  |  |  |  |
| Temperature | Temperature | Due To | - | $\pm 25$ | $\pm 75$ | $\pm 80$ | $\mathrm{ppm} /{ }^{\circ} \mathrm{C}$ |
| Drift | Range | Temperature Change |  |  |  |  |  |
| $\begin{aligned} & \text { Zero Offset } \\ & \text { (TSC8703) } \end{aligned}$ | $\mathrm{lin}=0$ | Correction at Zero Adjust to Give |  |  |  |  |  |
|  | $\mathrm{C}_{\mathrm{INT}}=68 \mathrm{pF}$ |  | - | - | $\pm 80$ | $\pm 80$ | mV |
|  | $R_{\text {ADJ }}=1.6 \mathrm{k} \Omega$ See Test Circuit. | $\begin{aligned} & \text { Integration Cap. }=68 \mathrm{pF} \\ & \mathrm{R}_{\mathrm{ADJ}}=1.6 \mathrm{k} \Omega \end{aligned}$ |  |  |  |  |  |
| Zero Offset (TSC8703) | $\mathrm{lin}=0$ | Correction at Zero Adjust to Give |  |  |  |  |  |
|  | $\begin{aligned} & \mathrm{CINT}=33 \mathrm{pF} \\ & \mathrm{R}_{A D J}=1.0 \mathrm{k} \Omega \end{aligned}$ | Zero Output When Input Is Zero Integration Cap. $=33 \mathrm{pF}$ | - | $\pm 10$ | $\pm 50$ | $\pm 50$ | mV |
|  | See Test Circuit. | RADJ $=1.0 \mathrm{k} \Omega$ |  |  |  |  |  |
| Zero Offset (TSC8704) (TSC8705) |  | Correction at Zero Adjust to Give |  |  |  |  |  |
|  | $\mathrm{C}_{\mathrm{INT}}=68 \mathrm{pF}$ $\mathrm{R}_{\mathrm{AD}, \mathrm{~J}}=1.0 \mathrm{k} \Omega$ | Zero Output When Input Is Zero Integration Cap $=68 \mathrm{pF}$ | - | $\pm 10$ | $\pm 50$ | $\pm 50$ | mV |
|  | See Test Circuit. | $\begin{aligned} & \text { Integration Cap. }=68 \mathrm{pF} \\ & \text { RADJ }^{2} 1.0 \mathrm{k} \Omega \end{aligned}$ |  |  |  |  |  |
| Zero Temperature Drift | Full Temperature Range | Variation in Zero Offest Due to Temperature Change | - | $\pm 3$ | $\pm 5$ | $\pm 8$ | ppm $/{ }^{\circ} \mathrm{C}$ |
| Analog Inputs lin Full-Scale |  |  |  |  |  |  |  |
|  |  | Full-Scale Analog Input Current To Achieve Specified Accuracy | - | 10 | - | - | $\mu \mathrm{A}$ |
| I ReF (Note 1) |  | Reference Current Input To Achieve Specified Accuracy | - | -20 | - | - | $\mu \mathrm{A}$ |
| $\underset{\mathrm{V}_{\text {IN }}(1)}{\text { Digital }}$ |  |  |  |  |  |  |  |
|  | Full Temperature Range | For Initiate Conversion Input | 3.5 | - | - | - | V |
| VIN ${ }^{(0)}$ | Full Temperature Range | Logical "0" Input Threshold For Initiate Conversion Input | - | - | 1.5 | 1.5 | V |
| Propagation Delay Output Enable | $C_{L}=100 \mathrm{pF}, \mathrm{R}_{\mathrm{L}}=$ | Tplh, TPHL | - | 500 | - | 1,000 | ns |

Electrical Characteristics (Cont.)

| PARAMETER | CONDITIONS | DEFINITION | MIN | TYP | $\begin{aligned} & \text { CJ/CN } \\ & \text { MAX } \end{aligned}$ | BN/BL MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Digital Outputs |  |  |  |  |  |  |  |
| 10(OFF) | $0.4 \mathrm{~V}<\mathrm{Vc}^{\text {c }}<2.4$ | Off-state Output Current | - | 0.1 | $\pm 10$ | $\pm 10$ | $\mu \mathrm{A}$ |
|  | Full Temp. Range | Logical "1" Output Voltage |  |  |  |  |  |
| Vout ${ }^{(1)}$ | lout $=-10 \mu \mathrm{~A}$ | For Digits Out, Busy, and | 4.5 2.4 | - | - | - | v |
|  | lout $=-500 \mu \mathrm{~A}$ | Data Valid Outputs |  | - | - |  |  |
|  | Full Temp. Range | Logical "0" Output Voltage |  |  |  |  |  |
| Vout ${ }^{(0)}$ | $V_{D D}=4.75 \mathrm{~V}$ | For Digits Out, Busy, and | - | - | 0.4 | 0.4 | V |
|  | lout $=500 \mu \mathrm{~A}$ | Data Valid Outputs |  |  |  |  |  |
| Dynamic |  |  |  |  |  |  |  |
| Conversion Time | Full Temp. Range | Time Required to Perform Complete A/D Conversion |  |  |  |  |  |
|  |  | TSC8703 | - | 1.25 | 1.8 | 1.8 | ms |
|  |  | TSC8704 | - | 5 | 6 | 6 | ms |
|  |  | TSC8705 | - | 20 | 24 | 24 | ms |
| Conversion |  | TSC8703 | 595 | 800 | - | - | Conv'ns |
| Rate in | V INT CONV $=+5 \mathrm{~V}$ | TSC8704 | 167 | 200 | - | - | per |
| Free-Run Mode |  | TSC8705 | 42 | 50 | - | - | Second |
| Minimum Pulse Width for Initiate Conversion | Full Temp. Range |  | 500 | - | - | - | ns |


| Supply Current IDD Quiescent (L/N Package) (J Package) | Full Temp. Range <br> VINT CONV $=0 \mathrm{~V}$ | Current Required From Positive Supply During Operation | - | $\begin{aligned} & 1.4 \\ & 1.4 \end{aligned}$ | $\begin{aligned} & 2.5 \\ & 5.0 \end{aligned}$ | 3.5 | mA mA |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Iss Quiescent (L/N Package) (J Package) | Full Temp. Range <br> VINIT CONV = OV | Current Required From Negative Supply During Operation | - | $\begin{aligned} & -1.6 \\ & -1.6 \end{aligned}$ | $\begin{aligned} & -2.5 \\ & -5.0 \end{aligned}$ | -3.5 | mA mA |
| Supply Sensitivity | $V_{D D} \pm 1 \mathrm{~V}, \mathrm{~V}_{\text {Ss }} \pm 1 \mathrm{~V}$ | Change in Full-Scale Gain vs Supply Voltage Change | - | $\pm 0.5$ | $\pm 1.0$ | $\pm 1.0$ | \%/V |
|  | $\left\|V_{D D}\right\|=\left\|V_{S S}\right\|=5 \mathrm{~V} \pm 1 \mathrm{~V}$ | Change in Full-Scale Gain vs Supply Voltage Change for Tracking Supplies | - | $\pm 0.05$ | $\pm 0.1$ | $\pm 0.1$ | \%/ |

## NOTE:

In and Iref pins connect to the summing junction of an operational amplifier Voltage sources cannot be attached directly but must be buffered by external resistors. See Test Circuit.

## Circuit Description

During conversion the sum of a continuous current lin and pulses of a reference current lref is integrated for a fixed number of clock periods. lin is proportional to the analog input voltage; IREF is switched in for exactly one clock period just frequently enough to maintain the output of the integrator near zero. Thus, the charge from the continuous lin current is balanced against the pulses of Iref current. The total number of Iref pulses needed during the conversion period to maintain the charge balance is counted, and the result (in Binary) is latched into the outputs at the end of the conversion.

The converter contains two counters and a clock in addition to an operational amplifier, comparator, latching output buffers and housekeeping logic. One counter is a clock counter which (after a reset pulse) starts counting clock pulses; when the required count is reached, the clock counter generates a pulse to start the end-of-conversion routine. The other counter is a data counter, which is reset synchronously with the clock counter and counts the number of times
the Iref current is switched into the summing input of the amplifier during the period defined by the clock counter.
When the Initiate Conversion input is strobed with a positive signal, the busy line latches high and a $10 \mu \mathrm{~s}$ (times given are approximate) start up cycle begins. The integrating capacitor is discharged and both counters are reset during this start up period. Conversion begins at the end of the reset pulse and ends with a pulse generated either by the clock counter or by an overflow condition in the data counter. This pulse disables further inputs into both counters and triggers a $10 \mu \mathrm{~s}$ shutdown cycle. During the shutdown cycle Data Valid goes low for $5 \mu \mathrm{~s}$. This binary sequence is shown in the timing diagrams. Busy is true high, and when the circuit is busy, Initiate Conversion has no effect and may be high or low. Data Valid is also true high. The data from a conversion remain valid for as long as power is applied to the circuit or until Data Valid falls at the end of a subsequent conversion, at which time the output data are updated to reflect the latest conversion.

## Test Circuit


2.

## Note:

1. Any Vref greater than -1 V can be used.
$R_{\text {REF }}=\frac{V_{\text {REF }}}{-20 \mu A}$
For example with $V_{\text {ref }}=\mathbf{- 5} \mathrm{V}$, Rref $=250 \mathrm{k}$.

| Part No. | RADJ | CINT | Zero Offset Spec |
| :--- | ---: | ---: | ---: |
| TSC8703 | $1.6 \mathrm{k} \Omega$ | 68 pF | $\pm 80 \mathrm{mV}$ |
| TSC8703 | $1.0 \mathrm{k} \Omega$ | 33 pF | $\pm 50 \mathrm{mV}$ |
| TSC8704/8705 | $1.0 \mathrm{k} \Omega$ | 68 pF | $\pm 50 \mathrm{mV}$ |

Timing Dlagrams (Rise, fall times = 200 ns typ., $C_{L}=50 \mathrm{pF}$ )


FREERUN MODE
$\qquad$


## Pin Functions <br> Initiate Conversion Input

Accepts CMOS and most 5 V logic inputs. Applying a logic " 1 " to the Initiate Conversion pin initiates the A/D conversion cycle. Once conversion has been initiated, the cycle cannot be interrupted, and the Initiate Conversion pin is disabled until conversion is complete. Two modes of operation are permitted, clocked or free-running. For clocked operation the Initiate Conversion input is held at logic " 0 " for standby and taken to logic " 1 " when a conversion is desired. For freerunning operation the Initiate Conversion pin is connected to VDD or similar permanent logic " 1 " voltage.

## Busy Output

A digital status output which is compatible with CMOS logic and low power TTL (can sink and source $500 \mu \mathrm{~A}$ ). A logic " 1 " output on the Busy pin indicates a conversion cycle is in process. A logic " 1 " to logic " 0 " transition indicates that conversion is complete and the result has been latched at the Digits Out pins. A logic " 0 " to logic " 1 " transition indicates a new conversion cycle has been initiated. If the device is operating in the free-running mode, the Busy output will remain low for approximately $2.5 \mu \mathrm{~s}$, marking the completion and initiation of consecutive conversion cycles.

## Data Valid Output

A digital status which is compatible with CMOS logic and low power TTL (can sink and source $50 \mu \mathrm{~A}$ ). A logic " 1 " output at the Data Valid pin indicates that the Digits Out pins are latched with the result of the last conversion cycle. The Data Valid output goes to logic " 0 " approximately $5 \mu \mathrm{~s}$ before the completion of a conversion cycle. During this $5 \mu \mathrm{~s}$ interval new data is being transferred to the Digits Out pins, and the Digits Out are not valid.

## Digits Out

(Bit 0, Bit 1, etc.)
The binary digit outputs which are the result of the A/D conversion. These outputs are CMOS logic and low power TTL compatible.

## Applications Information <br> Input/Output Relationships

The analog input voltage (VIN) is related to the output by the transfer equation:

$$
\begin{aligned}
\text { Digital Counts } & =\frac{V_{\text {IN }} \cdot A \cdot R_{\text {REF }}}{\text { RII } \cdot V_{\text {REF }}} \\
A & =528 \text { for } 8703 \\
A & =2064 \text { for } 8704 \\
A & =8208 \text { for } 8705
\end{aligned}
$$

where Digital Counts is the value of the binary output word presented at Digits Out pins in response to Vin.
The digital output code format is as follows:

| Analog <br> Input | Digital <br> Output |  |
| :---: | :---: | :---: |
| MSB | LSB |  |
| VIN Full-Scale | $1 \ldots 111 \ldots 1$ |  |
| $=$ Full-Scale -1 LSB | $1 \ldots 111 \ldots 1$ |  |
| $=1$ LSB | $0 \ldots 000 \ldots 1$ |  |
| $\leq 0$ | $0 \ldots 000 \ldots 0$ |  |

Two's complement coding can be generated by inverting the Most Significant Bit (MSB) signal.

## External Component Selection

Obtaining a high accuracy conversion system depends on the voltage regulation of VREF and the thermal stability of RIN and Rref. The exact dependence is given by the transfer function. System accuracy also depends, to a lesser degree, on the voltage regulation of $V_{D D}$ and $V_{s s}$. The supply connections VDD and VSs should have bypass capacitors of value $0.1 \mu \mathrm{~F}$ or larger right at the device pins.

## Rin, Ref

Values of these components are chosen to give a full-scale input current of approximately $10 \mu \mathrm{~A}$ and a reference current of approximately $-20 \mu \mathrm{~A}$.

$$
R_{\text {IN }} \cong \frac{V_{\text {IN Full-Scale }}}{10 \mu \mathrm{~A}} \quad R_{\text {REF }} \cong \frac{V_{\text {REF }}}{-20 \mu \mathrm{~A}}
$$

Examples:

$$
R_{\operatorname{IN}} \cong \frac{10 \mathrm{~V}}{10 \mu \mathrm{~A}}=1 \mathrm{M} \Omega \quad R_{R E F} \cong \frac{-6.4 \mathrm{~V}}{-20 \mu \mathrm{~A}}=320 \mathrm{k} \Omega
$$

Note that these values are approximations, and the exact relationships are defined by the transfer equation. In practice, the value of Rin typically would be trimmed using the optional gain adjust circuit to obtain full-scale output at ViN full-scale (see adjustment procedure). Metal film resistors with $1 \%$ tolerance or better are recommended for high accuracy applications because of their thermal stability and low noise generation.

## RBIAS

Specifications for the 87XX are based on RBIAS $=100 \mathrm{k} \Omega$ $\pm 10 \%$ unless otherwise noted. However, there are instances when the designer may want to change this resistor in crder to affect the conversion time and the supply current. By decreasing RBIAS the A/D will convert much faster and the supply current will be higher. (For example: When RBIAS is 20 k the conversion time is reduced by $1 / 3$, and the supply current will increase from 2 mA to 7 mA .) Likewise, if the RBIAS is increased the conversion time will be longer and the supply current will be much lower. (For example: When RBIAS $=1 \mathrm{~m} \Omega$ the conversion time will be six times longer, and supply current is now reduced to .5 mA ). For details of this relationship refer to AN9 typical performance curves.

## Applications Information (Cont.)

Rdamp
Exact value not critical but should have a nominal value of $100 \Omega \pm 10 \%$. Locate close to pin 14.

## Cdamp

Exact value not critical but should have a nominal value of $270 \mathrm{pF} \pm 20 \%$. Locate close to pin 14.

## Cint

Exact value not critical but should have a nominal value of $68 \mathrm{pF} \pm 10 \%$. Low leakage types are recommended, although mica or ceramic devices can be used in applications where their temperature limits are not exceeded. Locate as close as possible to pins 14, 15. For the TSC8703 CINT $=33 \mathrm{pF}$ is adequate with $R_{A D J}=1 \mathrm{k} \Omega$.

## $V_{\text {REF }}$

A negative reference voltage must be supplied. This may be obtained from a constant current source circuit or from the negative supply.

## $V_{\text {DD }}$, Vss

Power supplies of $\pm 5 \mathrm{~V}$ are recommended, with $0.05 \%$ line and load regulation and $0.1 \mu \mathrm{~F}$ decoupling capacitors.

## Adjustment Procedure

The test circuit diagram shows optional circuits for trimming the zero location and full-scale gain. Because the digital outputs remain constant outside of the normal operating range (i.e. below zero and above full-scale), it is recommended that transition points be used in setting the zero and full-scale values. Recommended procedure is as follows:

- Set the initiate conversion control high to provide free-run operation and verify that converter is operating.
- Set $V_{I N}$ to $+1 / 2$ LSB and trim the zero adjust circuit to obtain a $000 \ldots 000 \ldots$ to $000 \ldots 001$ transition. This will correctly locate the zero end.
- For full-scale adjustment, set ViN to the full-scale value less $11 / 2$ LSB and trim the gain adjust circuit for a 111 . . 110 to $111 \ldots 111$ transition.

If adjustments are performed in this order, there should be no interaction and they should not have to be repeated.

## TSC8705 Interface to MC6821 PIA



- Three State, Latched Outputs
- High Speed Conversion: 1-20 mSec


## Application/Design Circuits

## Bipolar Operation (+ and -Inputs)


*Optional visual indication of negative input
NOTE: Values for R should be between $10 \mathrm{~K} \Omega$ and $100 \mathrm{~K} \Omega$

Absolute Value Circuit With Sign

## 8-Bit Microprocessor Interface



TYPICAL PERFORMANCE CURVES

CONVERSION TIME
vs SUPPLY VOLTAGE



$$
V_{D D}=V_{S S}(\text { VOLTS })
$$



OUTPUT SOURCE CURRENT
vs TEMPERATURE

$\mathrm{IOH}^{(m A)}$

OUTPUT SINK CURRENT vs TEMPERATURE



OUTPUT SINK CURRENT


TRI-STATE PROPAGATION


## Application/Design Circuits (Cont.)

Reference Voltage Supply


2 V Reference Voltage Using Voltages Derived from $8080 \mathrm{~A} \mu \mathrm{P}$.

Package Information



V/F, F/V Converters

## Section 9

Voltage to Frequency/Frequency to Voltage Converters ..... 9-3
TSC9400 Voltage to Frequency (0.05\% Linearity) ..... 9-5TSC9401 Voltage to Frequency ( $0.01 \%$ Linearity)9-5
TSC9402Voltage to Frequency ( $0.25 \%$ Linearity)9-5

## General Description

The TSC9400/9401/9402 are low cost Voltage-io-Frequency converters combining Bipolar and CMOS technology on the same substrate. The converters accept a variable analog input signal and generate an output pulse train whose frequency is linearly proportional to the input voltage.

The devices can also be used as highly accurate Frequency-to-Voltage converters, accepting virtually any input frequency waveform and providing a linearly proportional voltage output.
A complete V/F or F/V system requires the addition of two capacitors, three resistors and reference voltage.

## Applications

## Voltage-to-Frequency

- Temperature Sensing and Control
- $\mu \mathrm{P}$ Data Acquisition
- Instrumentation
- 13-Bit A/D Converters
- Digital Panel Meters
- Analog Data Transmission and Recording
- Phase Locked Loops
- Medical Isolation
- Transducer Encoding
- Alternate to 555 Astable Timer


## Frequency-to-Voltage

- Frequency Meters/Tachometer
- Speedometers
- Analog Data Transmission and Recording
- Medical Isolation
- Motor Control
- RPM Indicator
- FM Demodulation
- Frequency Multiplier/Divider
- Flow Measurement and Control


## Ordering Information

| Part No. | Linearity <br> $(V / F)$ | Package | Temperature <br> Range |
| :--- | :--- | ---: | ---: |
| TSC9400CJ | $0.05 \%$ | 14 -Pin Plastic Dip | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ |
| TSC9400CL | $0.05 \%$ | 14 -Pin CerDIP | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
| TSC9401CJ | $0.01 \%$ | 14 -Pin Plastic Dip | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ |
| TSC9401CL | $0.01 \%$ | 14 -Pin CerDIP | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
| TSC9402CJ | $0.25 \%$ | 14 -Pin Plastic Dip | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ |
| TSC9402CL | $0.25 \%$ | 14 -Pin CerDIP | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |

## Features

Voltage-to-Frequency

- 1 Hz to 100 kHz Operation
- Choice Guaranteed Linearity:
- TSC9401 0.01\%
- TSC9400 0.05\%
- TSC9402 0.25\%
- $\pm 25 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ Typical Gain Temperature Stability
- Open Collector Output
- Output Can Interface with Any Form of Logic
- Pulse and Square Wave Outputs
- Programmable Scale Factor
- Low Power Dissipation (27 mW Typ.)
- Single Supply Operation (8 V to 15 V )
- Dual Supply Operation ( $\pm 4 \mathrm{~V}$ to $\pm 7.5 \mathrm{~V}$ )
- Current or Voltage Input


## Frequency-to-Voltage

- DC to 100 kHz Operation
- Choice of Guaranteed Linearity:
- TSC9401 0.02\%
- TSC9400 0.05\%
- TSC9402 0.25\%
- Op Amp Output
- Programmable Scale Factor
- High Input Impedance (>10 M $\Omega$ )
- Accepts any Voltage Wave Shape

HANDLING PRECAUTIONS: The TSC9400 Series are CMOS Bipolar devices and must be handled correctly to prevent damage. Package and store only in conductive foam, antistatic tubes or other ocnductive material. Use proper antistatic handling procedures. Do not connect in circuits under "power on" conditions, as high transients may cause permanent damage.

## Pin Configuration



# Voltage to Frequency/ <br> <br> Frequency to Voltage Converters 

 <br> <br> Frequency to Voltage Converters} TSC9402 (0.25\%)

## Absolute Maximum Ratings

| Storage Temperature | $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ | IIN ................................................... 10 mA |
| :---: | :---: | :---: |
| Operating Temperature |  | Vout Max -Vout Common ........................... 25 V |
| $J$ Package | $0^{\circ} \mathrm{C}$ to $70^{\circ} \mathrm{C}$ | VREF -VSS ......................................... 1.5 .5 T - |
| L Package | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | Package Dissipation ............................. 500 mW |
| VDD-Vss | . 18 V | Lead Temperature (Soldering, 10 sec ) ............ $300^{\circ} \mathrm{C}$ |

Electrical Characteristics, V/F Mode: Unless otherwise specified, $\mathrm{V}_{\mathrm{DD}}=+5 \mathrm{~V}, \mathrm{~V}_{\mathrm{SS}}=-5 \mathrm{~V}, \mathrm{~V}_{\mathrm{GND}}=0, \mathrm{~V}_{\mathrm{REF}}=-5 \mathrm{~V}$, RBIAS $=100 \mathrm{k} \Omega$, Full-Scale $=10 \mathrm{kHz} . \mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ unless Full Temperature Range is specified $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ for L package, $0^{\circ} \mathrm{C}$ to $70^{\circ} \mathrm{C}$ for J package.

| VOLTAGE-TO-FREQUENCY |  | TSC9401 |  |  | TSC9400 |  |  | TSC9402 |  |  | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PARAMETER | DEFINITION | MIN | TYP | MAX | MIN | TYP | MAX | MIN | TYP | MAX |  |
| Accuracy Linearity 10 kHz | Output Deviation From Straight Line Between Normalized Zero and Full-Scale Input |  | 0.004 | 0.01 | - | 0.01 | 0.05 | - | 0.05 | 0.25 | \% FullScale |
| Linearity 100 kHz |  | - | 0.04 | 0.08 | - | 0.1 | 0.25 | - | 0.25 | 0.50 | \% FullScale |
| Gain Temperature Drift (Note 1) | Variation in Gain A due to Temperature Change | - | $\pm 25$ | $\pm 40$ | - | $\pm 25$ | $\pm 40$ | - |  | $\pm 100$ | ppm $/{ }^{\circ} \mathrm{C}$ FullScale |
| Gain Variance | Variation from Exact A Compensate by Trimming Rin, Vref, or Cref | - | $\pm 10$ | - | - | $\pm 10$ | - | - | $\pm 10$ | - | $\%$ of Nominal |
| Zero Offset (Note 2) | Correction at Zero Adjust for Zero Output When Input is Zero | - | $\pm 10$ | $\pm 50$ | - | $\pm 10$ | $\pm 50$ | - |  | $\pm 100$ | mV |
| Zero Temperature Drift (Note 1) | Variation in Zero Offset Due to Temperature Change | - | $\pm 25$ | $\pm 50$ | - | $\pm 25$ | $\pm 50$ | - | $\pm 50$ | $\pm 100$ | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
| Analog Inputs lin Full-Scale | Full-Scale Analog Input Current to Achieve Specified Accuracy | - | 10 | - | - | 10 | - | - | 10 | - | $\mu \mathrm{A}$ |
| InN Overrange | Overrange Current | - | - | 50 | - | - | 50 | - | - | 50 | $\mu \mathrm{A}$ |
| Response Time | Settling Time to 0.01\% Full-Scale | - | 2 | - | - | 2 | - | - | 2 | - | Cycles |
| Digital Outputs <br> VSAT @ IOL $=10 \mu \mathrm{~A}$ (Note 3) | Logical "0" Output Voltage | - | - | 0.4 | - | - | 0.4 | - | - | 0.4 | V |
| $\begin{aligned} & \hline \text { Vout Max- } \\ & \text { Vout Common (Note 4) } \\ & \hline \end{aligned}$ | Voltage Range Between Output and Common | - | - | 18.0 | - | - | 18.0 | - | - | 18.0 | V |
| Pulse Frequency Output Width |  | - | 3.0 | - | - | 3.0 | - | - | 3.0 | - | $\mu \mathrm{sec}$ |
| Supply Current IdD Quiescent <br> (L Package) (Note 9) <br> (J Package) | Current Required From Positive Supply During Operation | - | 2.0 2.0 | $\begin{aligned} & 4.0 \\ & 6.0 \\ & \hline \end{aligned}$ |  | 2.0 <br> 2.0 | 4.0 6.0 | - | 3.0 | 10.0 | $\begin{aligned} & \mathrm{mA} \\ & \mathrm{~mA} \\ & \hline \end{aligned}$ |
| $\begin{aligned} & \text { Iss Quiescent } \\ & \text { (L Package) (Note 10) } \\ & \text { (J Package) } \end{aligned}$ | Current Required From Negative Supply During Operation | - | $\begin{aligned} & -1.5 \\ & -1.5 \end{aligned}$ | $\begin{aligned} & -4.0 \\ & -6.0 \end{aligned}$ | - | $\begin{aligned} & -1.5 \\ & -1.5 \end{aligned}$ | $\begin{aligned} & -4.0 \\ & -6.0 \end{aligned}$ | - | -3.0 | $-10.0$ | $\begin{aligned} & \mathrm{mA} \\ & \mathrm{~mA} \\ & \hline \end{aligned}$ |
| VDD Supply | Operating Range of Positive Supply | 4.0 | - | 7.5 | 4.0 | - | 7.5 | 4.0 | - | 7.5 | V |
| Vss Supply | Operating Range of Negative Supply | -4.0 | - | -7.5 | -4.0 | - | -7.5 | -4.0 | - | -7.5 | V |
| Reference Voltage VREF-VSS | Range of Voltage Reference Input | -1.0 | - | - | -1.0 | - | - | -1.0 | - | - | V |

[^6]8. $R \mathrm{~L} \geq 2 \mathrm{k} \Omega$.
9. Full temperature range. $\mathrm{V}_{\mathrm{I}}=-0.1 \mathrm{~V}$.
1.0. $\mathrm{V} \mathrm{IN}=-0.1 \mathrm{~V}$.
11. Ins connects the summing junction of an operational amplifier. Voltage sources cannot be attached directly but must be buffered by external

## V/F Circuit Description



Figure 1: 10 Hz to 10 kHz V/F Converter


Figure 2: Output Waveforms

## Voltage to Frequency/ Frequency to Voltage Converters

## V/F Circuit Description (Cont.)

The TSC9400 V/F Converter operates on the principal of charge balancing. The input voltage ( $\mathrm{V}_{\mathrm{IN}}$ ) is converted to a current ( $\mathrm{I}_{\mathrm{N}}$ ) by the input resistor. This current is then converted to a charge by the integrating capacitor and shows up as linearly decreasing voltage at the output of the op amp. The zero crossing of the output is sensed by the comparator causing the reference voltage to be applied to the reference capacitor for a time period long enough to virtually charge the capacitor to the reference voltage. This action reduces the charge on the integrating capacitor by a fixed amount ( $q=C_{\text {REF }} \times V_{\text {REF }}$ ) causing the op amp output to step up a finite amount.
At the end of the charging period, CREF is shorted out dissipating the stored reference charge so that when the output again crosses zero, the system is ready to recycle. In this manner, the continued discharging of the integrating capacitor by the input is balanced out by fixed charges from the reference voltage. As the input voltage is increased, the number of reference pulses required to maintain balance increases causing the output frequency to also increase. Since each charge increment is fixed the increase in frequency with voltage is near. In addition, the accuracy of the output pulses does not directly effect the linearity of the V/F. It must simply be long enough for full charge transfer to take place.
The TSC9400 contains a "self-start" circuit to assure that the V/F will always operate properly when power is first applied. In the event that during "Power-on" the op amp output is below the comparator threshold and Cref is already charged, a positive voltage step will not occur. The op amp output will continue to decrease until it crosses the -2.5 volt threshold of the "self-start" comparator. When this happens a resistor is connected to the op amp input causing the output to quickly go positive until the TSC9400 is once again in its normal operating mode.

The TSC9400 utilizes both bipolar and MOS transistors on the same substrate, taking advantage of the best features of each. MOS transistors are used at the inputs to reduce offset and bias currents. Bipolar transistors are used in the op amp, for high gain, and on all outputs for excellent current driving capabilities, CMOS logic is used throughout to minimize power consumption.

## Pin Functions

## Comparator Input

In the V/F mode, this input is connected to the amplifier output (Pin 12) and triggers the $3 \mu \mathrm{sec}$ pulse delay when the input voltage passes its threshold. In the F/V mode, the input frequency is applied to the comparator input.

## Pulse Freq Out

This output is an open-collector bipolar transistor providing a pulse wafeform whose frequency is proportional to the input voltage. This output requires a pull up resistor and interfaces directly with MOS, CMOS and TTL logic.

## Freq/2 Out

This output is an open-collector bipolar transistor providing a square wave that is one-half the frequency of the pulse frequency output. This output requires a pull up resistor and interfaces directly with MOS, CMOS, and TTL logic.

## Output Common

The emitters of both the freq/2 out and the puls freq out are connected to this pin. An output level swing from the collector voltage to ground or to the Vss supply may be obtained by connecting to the appropriate point.

## Rbias

Specifications for the TSC9400 are based on RBIAS $=100 \mathrm{k}$ $\pm 10 \%$ unless otherwise noted. RBIAS may be varied between the range of $82 \mathrm{k} \leq \mathrm{R}_{\mathrm{BI}} \mathrm{AS} \leq 120 \mathrm{k}$.

## Amplifier Out

The output stage of the operational amplifier. A negative going ramp signal is available at this pin in the V/F mode. In the F/V mode a voltage proportional to the frequency input is generated.

## Zero Adjust

The non-inverting input of the operational amplifier. The low frequency set point is determined by adjusting the voltage at this pin.

## IIN

The inverting input of the operational amplifier and the summing junction when connected in the V/F mode. An input current of $10 \mu \mathrm{~A}$ is specified for nominal full-scale but an overrange current up to $50 \mu \mathrm{~A}$ can be used without detrimental effect to the circuit operation.

## $V_{\text {REF }}$

A reference voltage from either a precision source or the Vss supply may be applied to this pin. Accuracy will be dependent on the voltage regulation and temperature characteristics of the circuitry.

## VRef OUT

The charging current for CREF is derived from the internal circuitry and switched by the break-before-make switch to this pin.

## V/F Design Information Input/Output Relationships

The output frequency is related to the analog input voltage (VIN) by the transfer equation:

$$
\text { Frequency Out }=\frac{V_{I N}}{R_{I N}} \times \frac{1}{\left(V_{R E F}\right)\left(C_{R E F}\right)}=f_{0}
$$

## V/F Design Information (Cont.) External Component Selection RIN

The value of this component is chosen to give a full-scale input current of approximately $10 \mu \mathrm{~A}$.

## Example:

$$
R_{I N} \cong \frac{V_{I N} \text { Full-Scale }}{10 \mu \mathrm{~A}} \quad R_{I N} \cong \frac{10 \mathrm{~V}}{10 \mu \mathrm{~A}}=1 \mathrm{M} \Omega
$$

Note that the value is an approximation, and the exact relationship is defined by the transfer equation. In practice, the value of RIN typically would be trimmed to obtain full-scale frequency at $V_{I N}$ Full-Scale (see adjustment procedure). Metal film resistors with $1 \%$ tolerance or better are recommended for high accuracy applications because of their thermal stability and low noise generation.

## Cint

Exact value not critical but is related to CREF by the relationship:

$$
3 C_{\text {REF }} \leq \mathrm{C}_{\mathrm{INT}} \leq 10 \mathrm{C}_{\text {REF }}
$$

Improved stability and linearity is obtained when CINT $\leq$ 4CREF. Low leakage types are recommended although mica and ceramic devices can be used in applications where their temperature limits are not exceeded. Locate as close as possible to pins 12 and 13.

## Cref

Exact value not critical and may be used to trim the full-scale frequency (See input/output relation). Glass film or air trimmer capacitors are recommended because of their stability and low leakage. Locate as close as possible to pins 5 and 3.

## Vod, Vss

Power supplies of $\pm 5 \mathrm{~V}$ are recommended. For high accuracy requirement $0.05 \%$ line and load regulation and $0.1 \mu \mathrm{~F}$ disc decoupling capacitors located near the pins are recommended.

## Adjustment Procedure

Figure 1 shows a circuit for trimming the zero location. Fullscale may be trimmed by adjusting Rin, Vref, or Cref. Recommended procedure is as follows for a 10 kHz full-scale frequency.

1. Set $\mathrm{V}_{\mathrm{I}}$ to 10 mV and trim the zero adjust circuit to obtain a 10 Hz output frequency.
2. Set VIN to 10.000 V and trim either Rin, VREF, or Cref to obtain a 10 kHz output frequency.
If adjustjments are performed in this order, there should be no interaction and they should not have to be repeated.


Figure 3: Recommended Cref vs $V_{\text {ref }}$

## V/F Single Supply Operation




Figure 5: Variable Voltage - Single Supply Operation

## Voltage to Frequency/ <br> Frequency to Voltage Converters

TSC9402 (0.25\%)


## See TSC7660 Data Sheet for $\pm 5$ V Operating Clircult from Single +5 V Supply.

Figure 6: Sincle Variable Supply Voltage with Offset and Gain Adjust

Electrical Characteristics, F/V Mode: Unless otherwise specified, $\mathrm{V}_{\mathrm{DD}}=+5 \mathrm{~V}, \mathrm{~V}_{S S}=-5 \mathrm{~V}, \mathrm{~V}_{G N D}=0, \mathrm{~V}_{\mathrm{REF}}=-5 \mathrm{~V}$, RBIAS $=100 \mathrm{k} \Omega$, Full-Scale $=10 \mathrm{kHz}$. $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ unless Full Temperature Range is specified $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ for L package, $0^{\circ} \mathrm{C}$ to $70^{\circ} \mathrm{C}$ for J package.

| FREQUENCY-TO-VOLTAGE |  | TSC9401 |  |  | TSC9400 |  |  | TSC9402 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PARAMETER | DEFINITION | MIN | TYP | MAX | MIN | TYP | MAX | MIN |  | MAX | UNITS |
| Accuracy Non-Linearity (Note 5) | Deviation From Ideal Transier Function as a Percentage Full-Scale Voltage | - | 0.01 | 0.02 | - | 0.02 | 0.05 | - | 0.05 | 0.25 | \% Full- Scale |
| Input Frequency <br> Range (Note 6) | Frequency Range for Specified Non-Linearity | 10 |  | 100 k | 10 |  | 100 k | 10 |  | 100 k | Hz |
| Frequency Inputs Positive Excursion (Note 7) | Voltage Required to Turn Comparator On | 0.4 | - | VDD | 0.4 | - | VDD | 0.4 | - | VDD | V |
| Negative Excursion (Note 7) | Voltage Required to Turn Comparator Off | -0.4 | - | -2 | -0.4 | - | -2 | -0.4 | - | -2 | V |
| Min. Positive Pulse Width (Note 7) | Time Between Threshold Crossings | - | 5.0 | - | - | 5.0 | - | - | 5.0 | - | $\mu \mathrm{S}$ |
| Min. Negative Pulse Width (Note 7) | Time Between Threshold Crossings | - | 0.5 | - | - | 0.5 | - | - | 0.5 | - | $\mu \mathrm{S}$ |
| Input Impedance |  | 10 | - | - | 10 | - | - | 10 | - |  | M $\Omega$ |
| Analog Outputs Output voltage (Note 8) | Voltage Range of Op Amp Output for Specified Non-Linearity | -VDD-1 |  | - |  |  | - | -VDD-1 |  | - V |  |
| Output Loading | Resistive Loading at Output of Op Amp | 2 k | - | - | 2 k | - | - | 2 k | - | - | $\Omega$ |
| Supply Current Iod Qulescent (L Package) (Note 9) (J Package) | Current Required From Positive Supply During Operation |  | 2.0 2.0 | 4.0 6.0 | - | 2.0 2.0 | 4.0 6.0 | - | 3.0 | 10.0 | mA mA |
| Iss Qulescent <br> (L Package) (Note 10) <br> (J Package) | Current Required From Negative Supply During Operation | - | $\begin{aligned} & -1.5 \\ & -1.5 \end{aligned}$ | -4.0 -6.0 | - | -1.5 -1.5 | -4.0 -6.0 | - |  | -10.0 | mA mA |
| Vod Supply | Operating Range of Positive Supply | 4.0 | - | 7.5 | 4.0 | - | 7.5 | 4.0 | - | 7.5 | V |
| Vss Supply | Operating Range of Negative Supply | -4.0 | - | -7.5 | -4.0 | - | -7.5 | -4.0 | - | -7.5 | V |
| $\begin{aligned} & \hline \text { Reference Voltage } \\ & \text { VREF -VSS } \end{aligned}$ | Range of Voltage Reference Input | -1.0 | - | - | -1.0 | - | - | -1.0 | - | - | V |
| Notes: <br> 1. Full temperature range <br> 2. $\operatorname{IIN}=0$. <br> 3. Full temperature range. lout $=10 \mathrm{~mA}$. <br> 4. IOUT $=10 \mu \mathrm{~A}$ <br> 5. 10 Hz to 100 kHz . <br> 6. $5 \mu \mathrm{~s} \mathrm{~min}$. positive pulse width and $0.5 \mu \mathrm{~s} \mathrm{~min}$. negative pulse width. |  | 7. $T_{r}=t_{t}=20 \mathrm{~ns}$. <br> 8. $R_{L} \geq 2 \mathrm{k} \Omega$. <br> 9. Full temperature range. $\mathrm{V}_{\mathrm{IN}}=-0.1 \mathrm{~V}$. <br> 10. $V_{I N}=-0.1 \mathrm{~V}$. <br> 11. IIN connects the summing junction of an operational amplifier. Voltage sources cannot be attached directly but must be buffered by external resistors. |  |  |  |  |  |  |  |  |  |

RTELEDYNE SEMICONDUCTOR


Figure 7: DC - 10 kHz F/V Converter

## F/V Circuit Description

The TSC9400, when used as a frequency to voltage converter, generates an output voltage which is linearly proportional to the input frequency wave form.
Each zero crossing at the comparator's input causes a precise amount of charge ( $q=C_{\text {REF }} \times V_{\text {REF }}$ ) to be dispensed into the op amp's summing junction. This charge in turn flows through the feedback resistor generating voltage pulses at the output of the op amp. A capacitor (CINT) across RINT averages these pulses into a DC voltage which is linearly proportional to the input frequency.

## F/V Design Information

## Input/Output Relationships

The output voltage is related to the input frequency (FIN) by the transfer equation:

$$
\text { Vout }=[\text { V REF CREF RINT }] \text { FIN }
$$

The response time to a change in $F_{\text {IN }}$ is equal to (RINT CINT). The amount of ripple on Vout is inversely proportional to CINT and the Input Frequency.
CInt can be increased to lower the ripple. $1 \mu \mathrm{~F}$ to $100 \mu \mathrm{~F}$ are perfectly acceptable values for low frequencies.

When TSC9400 is used in the single supply mode, VREF is defined as the voltage difference between Pin 7 and Pin 2.

## Input Voltage Levels

The input signal must cross through zero in order to trip the comparator. In order to overcome the hysteresis the amplitude must be greater than $\pm 200 \mathrm{mV}$.
If only a unipolar input signal (FIN) is available, it is recommended that either an offset circuit using resistor be used or that the signal be coupled in a via a capacitor.
For 100 kHz maximum input RINT should be decreased to $100 \mathrm{k} \Omega$.


NOTE: Cref should be increased for low Fin max. Adjust CREF so that $V_{O}$ is approximately 2.5 to 3.0 volts for the maximum input frequency. When Fin max is less than 1 kHz , the duty cycle should be greater than 20\% to insure that CREF is fully charged and discharged.

## Voltage to Frequency/ Frequency to Voltage Converters

## F/V Design Information (Cont.)

## Input Buffer

$f_{0}$ and $f_{0} / 2$ are not used in the F/V mode. However, these outputs may be useful for some applications, such a buffer to feed additional circuitry. Fo will then follow the input frequency wave form; except that fo will go high $3 \mu$ s after Fin goes high. $\mathrm{fo}_{0} / 2$ will be square wave with a frequency of one half $\mathrm{f}_{\mathrm{o}}$.

If these outputs are not use, then Pins 8, 9 and 10 may be left floating or connected to ground.


Figure 8: F/V Digital Outputs


Figure 9: F/V Single Supply

## Notes:

1. The input is now referenced to 6.2 V (Pin 6). The input signal must therefore be restricted to be greater than 4 volts (Pin 6-2 V) and less than 10 to 15 V (VDD).
If the signal is $A C$ coupled then a resistor ( 100 k to $10 \mathrm{~m} \Omega$ ) must be placed between the input (Pin 11) and Pin 6.
2. The output will now be referenced to Pin 6 which is at $6.2 \mathrm{~V}(\mathrm{Vz})$. For frequency meter applications a 1 mA meter with a series scaling resistor can be placed across Pins 6 and 12.

The sawtooth ripple which is on the output of an F/V can be eliminated without affecting the $F / V$ 's response time by using the circuit in Figure 10. The circuit has a DC gain of +1. Any AC components such as a ripple are amplified both positively, via the lower path, and negatively, via the upper path.

When both paths have the same gain, the AC ripple is cancelled. The amount of cancellation is directly proportional to gain matching. If the two paths are matched within $10 \%$, then the ripple will be lowered by $1 / 10$. For $1 \%$ matching, the ripple is lowered by $1 / 100$. The 10 k potentiometer is used to make the gain equal in both paths. This circuit is insensitive to both frequency changes and to signal wave shape.


Figure 10: F/V Ripple Eliminator

## F/V Power-On Reset

In the F/V mode, the TSC9400 output voltage will occasionally be at its maximum value when power is first applied. This condition will remain until the first pulse is applied to the Fin input. In most frequency-measurement applications this is not a problem, because proper operation begins as soon as the frequency input is applied.
In some cases, however, the TSC9400 output must be zero at power-on without a frequency input. In such cases, a capacitor connected from Pin 11 to VDD will usually be sufficient to pulse the TSC9400 and provide a power on reset (Figure 11a). Where predictable power-on operation is critical, a more complicated circuit, such as Figure 11b, may be required.


Figure 11

Section 10
Display Drivers ..... 10-3
TSC700A High Current Four Digit LED Driver ..... 10-5
TSC701AM High Current Bus Compatible Four Digit LED Driver ..... 10-13
TSC7211A
TSC7211A Four Digit LCD Driver ..... 10-21
TSC7212A Four Digit LED Driver ..... 10-21
TSC7211AM Bus Compatible Four Digit LCD Driver ..... 10-33
TSC7212AM Bus Compatible Four Digit LED Driver ..... 10-33

## General Description

The TSC700A drives common anode LED displays with 28 high current, open-drain $N$ channel output transistors. Four seven segment LED displays may be driven. Drive current is guaranteed to be 11 mA minimum. This is twice the minimum drive current available from comparable devices and will provide high LED luminance. High luminous intensity is an important factor when a dark contrasting background is unavailable or the LED is viewed at a distance. The TSC700A current capability makes it an ideal large character LED driver.

Four data bit inputs and four digit select signals permit interfacing to multiplexed BCD or binary output devices. The four bit data input is decoded into the seven segment alphanumeric code known as "Code B". A 0 to 9, -, E, H, L, P or "blank" reading may be displayed.
An added feature includes a brightness control input that adjusts segment drive current. The control pin may also be used as a digital display enable. The TSC700A is an improved pin compatible and functional equivalent to the ICM7212A and TSC7212A.

## Ordering Information

| Part No. | Package | Temp. <br> Range | LED <br> Segment <br> Current | Output <br> Code |
| :--- | :--- | :--- | :--- | :--- | :--- |
| TES700AMJL**$40-$ Pin <br> CerDIP | $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 14 mA | Code B |  |
| TSC700AIJL* | $40-\mathrm{Pin}$ <br> CerDIP | $-25^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 14 mA | Code B |
| TSC700A/Y | CHIP | $25^{\circ} \mathrm{C}$ | 14 mA | Code B |

* Add $/ \mathrm{BI}$ to part number suffix for 160 hour, $+125^{\circ} \mathrm{C}$ burn-in.


## Features

- High Drive Current for High Luminance LED Display
- Guaranteed High LED Segment Current 11 mA Minimum
- 28 Common Anode LED Drivers (4 Digits)
- Code B Output Format ... 0 to 9, -, E, H, L, P, "blank"
- BCD/Binary Input to Seven Segment LED Code
- Four Separate Digit Selects for Multiplexed Input
- Digital or Analog Brightness Control
- Digital Display Enable
- Low Thermal Resistance Package
- Military Temperature Range Devices Available
- Pin Compatible With TSC7212A, ICM7212A

Pin Configuration


If Brightness Control is not needed, connect BRT (pin 5) to Vs.

## Functional Diagram



# Four Digit LED Display Decoder and Driver 

TSC700A

## Absolute Maximum Ratings (Notes 1, 2)

Power Dissipation ................................. *1.0 W
Supply Voltage .......................................... 6.5 V
Input Voltage (Any Terminal) V s +0.3 V to Ground -0.3 V Operating Temperature

| $\text { I Version .................................. }-25^{\circ} \mathrm{C} \text { to }+85^{\circ} \mathrm{C}$ |  |
| :---: | :---: |
|  |  |

Maximum Chip Temperature .................... $+150^{\circ} \mathrm{C}$
Storage Temperature ................... $-55^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$
Lead Temperature (10 Sec) ........................ $300^{\circ} \mathrm{C}$

* To $85^{\circ} \mathrm{C}$, See Derating Curve on Page 4 for operation above $85^{\circ} \mathrm{C}$.

Electrical Characteristics: Specifications measured with $V_{S}=5.0 \mathrm{~V}$ at $T_{A}=25^{\circ} \mathrm{C}$.

| TYPE | NO. | SYMBOL | PARAMETER | TEST CONDITIONS | MIN | $\begin{gathered} \text { TSC700A } \\ \text { TYP } \\ \hline \end{gathered}$ | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1 | Iseg | Segment ON Current | Test Circuit | 11 | 14 | 18 | mA |
|  | 2 | IsLK | Segment Leakage |  | - | $\pm 0.01$ | $\pm 1.0$ | $\mu \mathrm{A}$ |
| $\begin{aligned} & \mathbf{I} \\ & \mathbf{N} \\ & \mathbf{P} \\ & \mathbf{U} \\ & \mathbf{T} \end{aligned}$ | 3 | VIH | Logic "1" Input Voltage |  | 3.0 | - | - | V |
|  | 4 | VIL | Logic "0" Input Voltage |  | - | - | 1.0 | V |
|  | 5 | lin | Input Current | Pins 27-34 | - | $\pm 0.01$ | $\pm 1.0$ | $\mu \mathrm{A}$ |
|  | 6 | CIN | Digital Input Capacitance | Pins 27-34 | - | 5 | - | pF |
|  | 7 | CbR | Brightness Input Capacitance |  | - | 200 | - | pF |
| $\begin{gathered} \mathbf{T} \\ \mathbf{I} \\ \mathbf{M} \\ \mathbf{I} \\ \mathbf{N} \\ \mathbf{G} \end{gathered}$ | 8 | tpw | Digit Select Pulse Width | See Timing Diagram | 1.0 | - | - | $\mu \mathrm{S}$ |
|  | 9 | tos | Data Setup Time | See Timing <br> Diagram | - | - | 100 | ns |
|  | 10 | toh | Data Hold Time | See Timing Diagram | - | 0 | - | ns |
|  | 11 | tids | Inter-Digit Select Time | See Timing Diagram | 2.0 | - | - | $\mu \mathrm{S}$ |
| $\begin{gathered} \mathbf{P} \\ 0 \\ \mathbf{W} \\ \mathbf{E} \\ \mathbf{R} \end{gathered}$ | 12 | Vs | Operating <br> Supply Voltage Range |  | 4 | 5 | 6 | V |
|  | 13 | Is | Supply Current | Display OFF | - | - | 50 | $\mu \mathrm{A}$ |
|  | 14 | lop | Operating Current | Pin 5, 27-34 at GND, Display all "8's" | - | 440 | - | mA |

## Notes:

1. Functional operation above the absolute maximum stress ratings is not
2. Static Sensitive device. Unused devices must be stored in conductive material to protect devices from static discharge and static fields.

## Output Pin Description and Function

| OUTPUT | TERMINAL |  | FUNCTION |  | OUTPUT | TERMINAL |  | FUNCTION |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A1 | 37 | A | Segment Dr. Digit 1 | (LSD) | A3 | 13 | A | Segment Dr. Digit 3 |  |
| B1 | 38 | B |  |  | B3 | 14 | B |  |  |
| C1 | 39 | C |  |  | C3 | 15 | C |  |  |
| D1 | 40 | D |  |  | D3 | 16 | D |  |  |
| E1 | 2 | E |  |  | E3 | 17 | E |  |  |
| F1 | 4 | F | $\downarrow$ | $\pm$ | F3 | 19 | F |  |  |
| G1 | 3 | G |  | , | G3 | 18 | G |  |  |
| A2 | 6 | A | Segment Dr. Digit 2 |  | A4 | 20 | A | Segment Dr. Digit 4 | (MSD) |
| B2 | 7 | B | 1 |  | B4 | 21 | B | 1 | I |
| C2 | 8 | C |  |  | C4 | 22 | C |  |  |
| D2 | 9 | D |  |  | D4 | 23 | D |  |  |
| E2 | 10 | E |  |  | E4 | 24 | E |  | , |
| F2 | 12 | F | 1 |  | F4 | 26 | F | $\checkmark$ | $\downarrow$ |
| G2 | 11 | G | , |  | G4 | 25 | G | $\checkmark$ |  |

Input Pin Description and Function

| INPUT | TERMINAL | FUNCTION |
| :--- | :---: | :--- |
| B0 | 27 | Ones (Least Significant) |
| B1 | 28 | Twos |
| B2 | 29 | Fours |
| B3 | 30 | Eights (Most Significant) |
| D1 | 31 | D1 (Least Significant) Digit Select |
| D2 | 32 | D2 Digit Select |
| D3 | 33 | D3 Digit Select |
| D4 | 34 | D4 (Most Significant) Digit Select INPUTS BITS |
| BRT | 5 | Brightness Control: Logic 1 = ON |
| Logic 0 OF OF <br> See Typical Characteristic Curve for ISEG Vs <br> Brightness Control Voltage |  |  |

Segment Assignment
$\square$

Timing Diagram


## Electrical Operating Characteristics



## LED Segment Current vs Output Voltage

LED Segment Current vs Brightness Control Voltage


Four Digit LED Display Decoder and Driver

## Operation Description

## Output Format

The TSC700A accepts four bit binary information at pins 27 (LSB) through 30 (MSB). The binary input is decoded to the seven segment output in a format known as "Code B". The display format is 0 to $9,-, E, H, L, P$ and "blank".

## Output Code

| Binary input |  |  |  | TSC700A |
| :---: | :---: | :---: | :---: | :---: |
|  | B2 | B1 |  | "Code B" |
| 0 | 0 | 0 | 0 | 0 |
| 0 | 0 | 0 | 1 | 1 |
|  | 0 | 1 | 0 | 2 |
|  | 0 | 1 | 1 | 3 |
|  | 1 | 0 | 0 | 4 |
|  | 1 | 0 | 1 | 5 |
|  | 1 | 1 | 0 | 6 |
|  | 1 | 1 | 1 | 7 |
|  | 0 | 0 | 0 | 8 |
| 1 | 0 | 0 | 1 | 9 |
| 1 | 0 | 1 | 0 | - |
| 1 | 0 | 1 | 1 | E |
| 1 | 1 | 0 | 0 | H |
| 1 | 1 | 0 | 1 | L |
| 1 | 1 | 1 | 0 | P |
| 1 | 1 | 1 |  | (Blank) |

Segment Assignment


## Special Order Output Format

The TSC700A is mask programmed to give 16 combinations of seven segment output codes. For large volume orders ( 50 K minimum pieces) custom decoder options are available. Contact factory for details.

## Brightness Control Operation

The voltage at the brightness control input is transferred to the output transistor gate for "ON" segments. The brightness voltage directly modulates the segment driver "ON" resistance. A brightness input (pin 5) can be used in two ways to control output transistor drain current. A variable brightness control may be implemented with a single potentiometer. A high value potentiometer ( $100 \mathrm{~K} \Omega$ to $1 \mathrm{M} \Omega$ ) will minimize power consumption.

## Brightness Control



A logic signal of varying duty cycle will also control display brightness.


The display may be blanked (all segments OFF) by applying the input code 1111 or by driving the brightness pin with a logic 0 . If brightness control is not needed, pin 5 should be tied to 5.0 V .

## Package Power Dissipation Minimization

The TSC700A high LED current drive capability requires package power dissipation be limited and that a low thermal resistance packaae be used. The cerDIP package thermal resistance ( $\theta \mathrm{jc}=30^{\circ} \mathrm{C} / \mathrm{W}, \theta \mathrm{ja}=60^{\circ} \mathrm{C} / \mathrm{W}$ ) permits operation over the full $-25^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ industrial operating temperature range. Power dissipation is easily controlled by reducing the applied voltage at the segment driver outputs. A $2.5 \Omega$ voltage dropping resistor placed in series with the common anode LED display voltage will maintain dissipation under 1 watt with a worst case continuous 8888 display. Figure 1 gives the package power dissipation vs the number of "ON" LED segments for the operating circuit in Figure 2. Driver outputs should be maintained above 1.85 V for constant current operation.


| Character Displayed | No of "ON" Segments |
| :---: | :---: |
| 0 | 6 |
| 1 | 2 |
| 2 | 5 |
| 3 | 5 |
| 4 | 4 |
| 5 | 5 |
| 6 | 6 |
| 7 | 3 |
| 8 | 7 |
| 9 | 6 |
| - | 1 |
| $E$ | 5 |
| $H$ | 5 |
| L | 3 |
| P | 5 |

Figure 1: Package Power Dissipation


$$
P_{D}=v_{S} I_{s}+I_{\text {SEG }}(N)\left[V^{+}-V_{\text {LED }}-N\left(I_{S E G}\right) R_{D}\right]
$$

$$
\approx I \operatorname{sEG}(N)\left[V^{+}-V_{\text {LED }}-N\left(I_{\text {SEG }}\right) R_{D}\right]
$$

Where:
IsEG = LED Segment Current $N$ = Number of ON Segments
VLED $=$ Voltage Across on LED
$P_{D}=$ Max. Package Power Dissipation
$\mathrm{V}_{\mathrm{S}}=$ TSC700A Power Supply Voltage (5 V)
Is $=$ TSC700A Quiescent Current $(\approx 50 \mu \mathrm{~A})$

Figure 2: Operating Circuit

## Applications Information:

## 3 1/2 Digit ADC with LED Display



## $\mu$ - Processor Controlled Display



## Applications Information (continued)

## 4 1/2 Digit Counter



## Package Information



## General Description

The TSC701AM is a CMOS direct drive，four digit，seven segment LED display decoder and driver．The device is bus compatible making microprocessor controlled displays possible．Two chip select signals control data and digit select code latching prior to decoding and display．External data latches are unnecessary．
The TSC701AM drives common anode LED displays with 28 high current，open－drain N channel output transistors．Four seven segment LED displays may be driven．Drive current is guaranteed to be 11 mA minimum（ 18 mA TYP）．This is twice the minimum drive current available from comparable de－ vices and will provide high LED luminance．High luminous intensity is an important factor when a dark contrasting background is unavailable or the LED is viewed at a distance． The TSC701AM current capability makes it an ideal large character LED driver．
Four data bit inputs and four digit select signals permit inter－ facing to multiplexed BCD or binary output devices．The four bit data input is decoded into the seven segment alpha－ numeric code known as＂Code B＂．A 0 to 9，－，E，H，L，P or ＂blank＂reading may be displayed．
An added feature is the brightness control input that adjusts segment drive current．The control pin may also be used as a digital display enable．The TSC701AM is an improved pin compatible and functional equivalent to the ICM7212AM．

## Features

－ 28 Current Limited Outputs Drive Common－Anode LEDs at 18 mA Per Segment．
－Input and Digit Select Data Latches．
－Brightness Input Allows Potentiometer Control of LED Segment Current．Pin Also Serves as Digital Display Enable．
－Input and Digit Select Data Latches．
－Pin Compatible and Functionally Equivalent to ICM7212AM．
－Input Decoded to Seven Segment Code B Output（0 to 9，一，E，H，L，P，＂Blank＂）

0
Ordering Information

| Part No． | Package | Temp． <br> Range | LED <br> Segment <br> Current | Output <br> Code |
| :--- | :--- | :--- | :--- | ---: |
| TSC701AMIJL | $40-$ Pin <br> CerDIP | $-25^{\circ} \mathrm{C}$ <br> to $+85^{\circ} \mathrm{C}$ | 18 mA | Code B |

## Functional Diagram



# Bus Compatible Four Digit LED Display Driver 

## Absolute Maximum Ratings

Power Dissipation ................................... 1.0 W
Supply Voltage .......................................... 6.5 V
Input Voltage (Any Terminal) $V \mathrm{~S}+0.3 \mathrm{~V}$ to Ground -0.3 V
Operating Temperature
I Version $\qquad$ $-25^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$
Maximum Chip Temperature ..... $+150^{\circ} \mathrm{C}$
Storage Temperature ................... $-55^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$

Electrical Characteristics: Specifications measured with $\mathrm{V}_{\mathrm{S}}=5.0 \mathrm{~V}$ at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$.

| TYPE | NO. | SYMBOL | PARAMETER | $\begin{aligned} & \text { TEST } \\ & \text { CONDITIONS } \end{aligned}$ | MIN | $\begin{aligned} & \text { TSC701AM } \\ & \text { TYP } \end{aligned}$ | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} D \\ L^{R} \\ E I \\ D \\ E \\ R \end{gathered}$ | 1 | Iseg | Segment ON Current | Test Circuit | 11 | 18 | 20 | mA |
|  | 2 | Istk | Segment <br> Leakage |  | - | $\pm 0.01$ | $\pm 1.0$ | $\mu \mathrm{A}$ |
| $\begin{aligned} & \mathbf{I} \\ & \mathbf{N} \\ & \mathbf{P} \\ & \mathbf{U} \\ & \mathbf{T} \end{aligned}$ | 3 | $\mathrm{V}_{1} \mathrm{H}$ | Logic "1" Input Voltage |  | 3.0 | - | - | V |
|  | 4 | VIL | Logic "0" Input Voltage |  | - | - | 1.0 | V |
|  | 5 | IN | Input Current | Pins 27-34, 5 | - | $\pm 0.01$ | $\pm 1.0$ | $\mu \mathrm{A}$ |
|  | 6 | CIN | Digital Input Capacitance | Pins 27-34 | - | 5 | - | pF |
|  | 7 | Cbr | Brightness Input Capacitance |  | - | 200 | - | pF |
| $\begin{gathered} \mathbf{T} \\ \mathbf{I} \\ \mathbf{M} \\ \mathbf{I} \\ \mathbf{N} \\ \mathbf{G} \end{gathered}$ | 8 | t CSA | Chip Select Active Pulse Width | Note 3 | 200 | - | - | ns |
|  | 9 | tDs | Data <br> Setup <br> Time |  | 100 | - | - | ns |
|  | 10 | tDH | Data Hold Time |  | 10 | 0 | - | ns |
|  | 11 | tics | Inter-Chip Select Time |  | 2 | - | - | $\mu \mathrm{S}$ |
| $\begin{aligned} & \mathbf{P} \\ & \mathbf{O} \end{aligned}$ | 12 | Vs | Operating <br> Supply Voltage <br> Range |  | 4 | 5 | 6 | V |
| $\begin{gathered} \mathbf{W} \\ \mathbf{E} \end{gathered}$ | 13 | Is | Supply Current | Display OFF | - | - | 50 | $\mu \mathrm{A}$ |
| R | 14 | lop | Operating Current | Pin 5, at $\mathrm{V}_{\mathrm{S}}^{+}$ Display all " 8 's" | - | 504 | - | mA |

## Notes:

1. Functional operation above the absolute maximum stress ratings is not implied.
2. Static Sensitive device. Unused devices must be stored in conductive material to protect devices from static discharge and static fields.

## Bus Compatible Four Digit <br> LED Display Driver <br> - High Segment Drive Current <br> - Input Data Latches

## Input Definitions

In this table, $\mathrm{V}+$ and GROUND are considered to be normal operating input logic levels. For lowest power consumption, input signals should swing over the full supply.


## Pin Configuration



Timing Diagram

Figure 1: BUS Interface Timing Diagram


# Bus Compatible Four Digit <br> LED Display Driver <br> - High Segment Drive Current 

TSC701AM

## Output Definitions

Output pins are defined by the alphabetical segment assignment and numerical digital assignment.

| OUTPUT | TERMINAL |  | FUNCTION |  | OUTPUT | TERMINAL |  | FUNCTION |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A1 | 37 |  | Segment Dr. Digit 1 | (LSD) | A3 | 13 |  | Segment Dr. Digit 3 |  |
| B1 | 38 | B | A Segment Dr. Digit |  | B3 | 14 | B | 1 |  |
| C1 | 39 | C |  |  | C3 | 15 | C |  |  |
| D1 | 40 | D |  |  | D3 | 16 | D |  |  |
| E1 | 2 | E |  |  | E3 | 17 | E |  |  |
| F1 | 4 | F | $\downarrow$ | $\checkmark$ | F3 | 19 | F | 1 |  |
| G1 | 3 | G |  |  | G3 | 18 | G |  |  |
| A2 | 6 |  | Segment Dr. Digit 2 |  | A4 | 20 | A | Segment Dr. Digit 4 | (MSD) |
| B2 | 7 | B | 1 |  | B4 | 21 | B | + | I |
| C2 | 8 | C |  |  | C4 | 22 | C |  |  |
| D2 | 9 | D |  |  | D4 | 23 | D |  |  |
| E2 | 10 | E |  |  | E4 | 24 | E |  |  |
| F2 | 12 | F | $\downarrow$ |  | F4 | 26 | F | $\downarrow$ | 1 |
| G2 | 11 | G | 1 |  | G4 | 25 | G | 1 |  |

## Digit Assignment



## Bus Compatible Four Digit

 LED Display Driver
## - High Segment Drive Current

- Input Data Latches


## Electrical Operating Characteristics



LED Segment Current vs Output Voltage


LED Segment Current vs Brightness Control Voltage


## Input Configuration and Output Codes

The TSC701AM accepts a four bit, true binary (positive level = logic 1) input at pins 27 (LSB) through 30 (MSB). The output display format is 0 to $9,-, E, H, L, P$ and blank (see Table 1). The TSC701AM correctly decodes binary and BCD true codes to a seven segment output.
The TSC701AM is designed to interface with a data bus and display data under microprocessor control. Four data input bits (Pins 27-30) and two digit select input bits (Pins 31, 32) are written into input buffer latches. The rising edge of either chip select causes data to be latched, decoded and stored in the selected digit output data latch. The two bit digit code selects the appropriate output digit latch. The four bit display data word is decoded to the "Code B" seven segment output format.

For applications where bus compatibility is not required refer to the TSC7211A (LCD), TSC7212A (LED) and the TSC700A (LED) four digit decoder driver data sheets. These devices are designed to accept multiplexed BCD/Binary input data for display under the control of four separate digit select control signals.


Figure 5: Segment Assignment

| BINARY INPUT |  |  |  | CODE B |
| :---: | :---: | :---: | :---: | :---: |
| B3 | B2 | B1 | B0 |  |
| 0 | 0 |  | 0 | 0 |
| 0 | 0 | 0 | 1 | 1 |
| 0 | 0 | 1 | 0 | 2 |
| 0 | 0 | 1 | 1 | 3 |
| 0 | 1 | 0 | 0 | 4 |
| 0 | 1 | 0 | 1 | 5 |
| 0 | 1 | 1 | 0 | 6 |
| 0 | 1 | 1 | 1 | 7 |
| 1 | 0 | 0 | 0 | 8 |
| 1 | 0 | 0 | 1 | 9 |
| 1 | 0 | 1 | 0 | - |
| 1 | 0 | 1 | 1 | E |
| 1 | 1 | 0 | 0 | H |
| 1 | 1 | 0 | 1 | L |
| 1 | 1 | 1 | 0 | $P$ |
| 1 | 1 | 1 | 1 | (Blank) |

Table 1: Output Code

## Applications Information

The TSC701AM has two ground pins. These pins should be connected together.

TSC701AM Interfaced to Z-80 Microprocessor


## Bus Compatible Four Digit

LED Display Driver

- High Segment Drive Current
- Input Data Latches


## Package Information

(Package \#20)

10

## General Description

The TSC7211A (LCD Decoder/Driver) and TSC7212A (LED Decoder/Driver) are direct drive, four digit, seven segment display decoder and drivers.

The TSC7211A drives conventional LCD displays. An RC oscillator, divider chain, backplane driver, and 28 segment outputs are provided on a single CMOS chip. The segment drivers supply square waves of the same frequency as the backplane but in phase for an OFF segment and out of phase for an ON segment. The net d.c. voltage applied between driver segment and backplane is zero.

The TSC7212A drives common anode LED displays with 28 current controlled, low leakage, open drain, N -Channel output transistors. The brightness control input can be used as a digital display enable. A varying voltage at the control input will allow continuous display brightness control.

The TSC7211A (LCD) and TSC7212A (LED) require only four data bit inputs and four digit select signals to interface with multiplexed BCD or binary output devices such as the ICM7217, ICM7226, ICL7103 and TSC7135. The four bit binary input code is decoded into the seven segment alphanumeric code known as "Code B."

The "Code B" output format results in a 0 to $9,-, \mathrm{E}, \mathrm{H}, \mathrm{L}, \mathrm{P}$ or blank display. True BCD or binary inputs will be correctly decoded to the seven segment display format.

The CMOS TSC7211A and TSC7212A are available in a 40pin epoxy dual-in-line package and a compact 60-pin flat package. All inputs are protected against static discharge.

Ordering Information

| Part <br> No. | Driver <br> Type | Package | Output <br> Code | Input <br> Conflg. |
| :--- | :--- | :--- | :--- | ---: |
| TSC7211AIPL | LCD | 40-Pin <br> Epoxy Dip | Code B | Multiplexed <br> 4-Bit Binary <br> or BCD |
| TSC7212AIPL | LED | 40-Pin <br> Epoxy Dip | Code B | Multiplexed <br> 4-Bit Binary <br> or BCD |
| TSC7211A/Y | LCD | DICE | Code B | Multiplexed <br> 4-Bit Binary <br> or BCD |
| TSC7212A/Y | LED | DICE | Code B | Multiplexed <br> 4-Bit Binary <br> or BCD |
| TSC7211AIJL | LCD | 40-Pin | Code B | Multiplexed <br> 4-Bit Binary <br> or BCD |

## TSC7211A Features (LCD Driver)

- Four Digit Non-Multiplexed Seven Segment LCD Display Outputs With Backplane Driver.
- RC Oscillator On Chip Generated Backplane Drive Signal.
- Eliminates DC Bias Which Degrade LCD Display Life.
- Backplane Input/Output Pin Permits Synchronization of Cascaded Slave Device to a Master Backplane Signal.
- Separate Digit Select Inputs to Accept Multiplexed BCD/Binary Inputs.
- Binary and BCD Inputs Decoded to Code B (Oto 9, -, E, H, L, P, Blank).
- Pin Compatible and Functionally Equivalent to ICM7211A and DF411.
- Connect to TSC7135 in Flat Package For Compact 4 1/2 Digit Meter Systems


## TSC7212A Features (LED Driver)

- 28 Current Limited Outputs Drive Common Anode LEDs at Greater Than 5 mA Per Segment.
- Brightness Input Allows Potentiometer Control of LED Segment Current. Pin Also Serves as Digital Display Enable.
- Same Input Configuration and Output Decoding as the TSC7211A.
- Pin Compatible and Functionally Equivalent to ICM7212A.

| Part <br> No. | Driver <br> Type | Package | Output <br> Code | Input <br> Config. |
| :--- | :---: | :---: | ---: | ---: |
| TSC7212AIJL | LED | 40-Pin <br> CerDIP | Code B | Multiplexed <br> 4-Bit Binary <br> or BCD |
| TSC7211AIBQ | LCD | Flat Package <br> Formed Leads | Code B | Multiplexed <br> 4-Bit Binary <br> or BCD |
| TSC7211AISQ | LCD | Flat Package <br> Unformed Leads | Code B | Multiplexed <br> 4-Bit Binary <br> or BCD |
| TSC7212AIBQ | LED | Flat Package <br> Formed Leads | Code B | Multiplexed <br> 4-Bit Binary <br> or BCD |
| TSC7212AISQ | LED | 60-Pin <br> Flat Package <br> Unformed Leads | Code B | Multiplexed <br> 4-Bit Binary <br> or BCD |

Absolute Maximum Ratings
Power Dissipation (Note 1) .................. 0.8 W at $70^{\circ} \mathrm{C}$
Supply Voltage 6.5 V

Input Voltage (Any
Terminal) (Note 2) .......... $\mathrm{V}^{+}+0.3 \mathrm{~V}$, GROUND -0.3 V
Operating Temperature Range .......... $-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$
Storage Temperature Range ........... $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$
Lead Temperature (Soldering 10 sec .)
............. $300^{\circ} \mathrm{C}$
Stresses above those listed under Absolute Maximum Ratings may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions above those indicated
in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.
Note 1: This limit refers to that of the package and will not be realized during normal operation.
Note 2: Due to the SCR structure inherent in the CMOS process, connecting any terminal to voltages greater than $\mathrm{V}^{+}$or less than GROUND may cause destructive device latchup. For this reason it is recommended that no inputs from external sources not operating on the same power supply be applied to the device before its supply is established, and that in multiple supply systems, the supply to the TSC7211A/ TSC7212A be turned on first.

## Table I: Operating Characteristics

Test Conditions: All parameters measured with V+=5V
TSC7211A CHARACTERISTICS (LCD DECODER/DRIVER)

| PARAMETER | SYMBOL | CONDITIONS | MIN | TYP | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Operating Voltage Range, | V Supp |  | 3 | 5 | 6 | V |
| Operating Current | Iop | Test Circuit, Display Blank | - | 10 | 50 | $\mu \mathrm{A}$ |
| Oscillator Input Current | losci | Pin 36 | - | $\pm 2$ | $\pm 10$ | $\mu \mathrm{A}$ |
| Segment Rise/Fall Time | $\mathrm{tris}^{\text {d }}$ | $\mathrm{C}=200 \mathrm{pF}$ | - | 0.5 | - | $\mu \mathrm{A}$ |
| Backplane Rise/Fall Time | $t_{\text {rib }}$ | $C_{L}=5000 \mathrm{pF}$ | - | 1.5 | - | $\mu \mathrm{s}$ |
| Oscillator Frequency | fosc | Pin 36 Floating | - | 16 | - | kHz |
| Backplane Frequency | $f$ bp | Pin 36 Floating | - | 125 | - | Hz |

TSC7212A CHARACTERISTICS (COMMON ANODE LED DECODER/DRIVER)

| PARAMETER | SYMEOL | CONDITIONS | MIN | TYP | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Operating Supply Voltage Range | VSUPP |  | 4 | 5 | 6 | V |
| Operating Current Display Off | Iop | Pin 5 (Brightness), <br> Pins 27-34 - GROUND | - | 10 | 50 | $\mu \mathrm{A}$ |
| Operating Current | Iop | Pin 5 at V+, Display all 8's | - | 200 | - | mA |
| Segment Leakage Current | IsLK | Segment Off | - | $\pm 0.01$ | $\pm 1$ | $\mu \mathrm{A}$ |
| Segment On Current | Iseg | Segment On, $\mathrm{V}_{0}=+3 \mathrm{~V}$ | 5 | 8 | - | mA |

INPUT CHARACTERISTICS (LCD AND LED DECODER/DRIVER)

| PARAMETER | SYMBOL | CONDITIONS | MIN | TYP | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Logical "1" Input Voltage | $V_{1 H}$ |  | 3 | - | - | V |
| Logical "0" Input Voltage | $\mathrm{V}_{\text {IL }}$ |  | - | - | 1 | V |
| Input Leakage Current | IILK | Pins 27-34 | - | $\pm 0.01$ | $\pm 1$ | $\mu \mathrm{A}$ |
| Input Capacitance | $\mathrm{C}_{\text {IN }}$ | Pins 27-34 | - | 5 | - | pF |
| BP/Brightness Input Leakage | I bpLK | Measured at Pin 5 with Pin 36 at GND | - | $\pm 0.01$ | $\pm 1$ | $\mu \mathrm{A}$ |
| BP/Brightness Input Capacitance | $\mathrm{C}_{\text {SPI }}$ | All Devices | - | 200 | - | pF |

## AC CHARACTERISTICS (LCD AND LED DECODER/DRIVER)

| PARAMETER | SYMBOL | CONDITIONS | MIN | TYP | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Digit Select Active Pulse Width | $\mathrm{t}_{\text {sa }}$ | Refer to Timing Diagrams | 1 | - | - | $\mu \mathrm{s}$ |
| Data Valid Time | $t_{\text {ds }}$ | Refer to Timing Diagrams | - | - | 100 | ns |
| Data Hold Time | $t_{\text {dh }}$ | Refer to Timing Diagrams | 200 | - | - | ns |
| Inter-Digit Select Time | $t_{\text {ids }}$ | Refer to Timing Diagrams | 2 | - | - | $\mu \mathrm{s}$ |

## Timing Diagrams



Figure 1: Input Timing Diagram (LED or LCD)

## Test Circuit



Figure 3: Test Circuit



Figure 2: LCD Display Waveforms

## Pin Configuration



Flat Package
NOTES:

1. NC = NO INTERNAL CONNECTION
2. PINS 8, 23, 38 AND 53 ARE CONNECTED TO THE DIE SUBSTRATE. THE POTENTIAL AT THESE PINS IS APPROXIMATELY $\mathrm{V}^{+}$. NO EXTERNAL CONNECTIONS




## Input Definitions

In this table, V+ and GROUND are considered to be normal operating input logic levels. For lowest power consumption, input signals should swing over the full supply.

| INPUT | TERMINAL* | CONDITION | FUNCTION |
| :---: | :---: | :---: | :---: |
| B0 | 27 (49) | $\begin{aligned} & \text { V+= Logical One } \\ & \text { GND }=\text { Logical Zero } \end{aligned}$ | Ones (Least Significant) |
| B1 | 28 (50) | $\begin{aligned} & \text { V+ = Logical One } \\ & \text { GND }=\text { Logical Zero } \end{aligned}$ | Twos $\}$ Data Input Bits |
| B2 | 29 (51) | $\begin{aligned} & \text { V+ = Logical One } \\ & \text { GND }=\text { Logical Zero } \\ & \hline \end{aligned}$ | Fours |
| B3 | 30 (52) | $\begin{aligned} & \text { V+ = Logical One } \\ & \text { GND = Logical Zero } \end{aligned}$ | Eights (Most Significant) |
| OSC $\quad 36$ (1) <br> (LCD Devices <br> only) |  | Floating or with external capacitor GROUND | Oscillator Input |
|  |  | Disables BP output devices, allowing segments to be synchronized to an external signal input at the BP terminal (Pin 5) |
| D1 | 31 (54) |  |  | D1 (Least significant) Digit Select |
| D2 | 32 (55) | V+ = Active | D2 Digit Select |
| D3 | 33 (56) | GND = Inactive | D3 Digit Select |
| D4 | 34 (57) |  | D4 (Most significant) Digit Select |

* 60-Pin Flat Package Pin \# in ( ) .

Output Definitions
Output pins are defined by the alphabetical segment assignment and numerical digital assignment.

| OUTPUT | TERMINA |  | FUNCTION |  |  | OUTPUT | TERMINAL* | FUNCTION |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A1 | 37 (3) | A | Segment Dr. | Digit 1 | (LSD) | A3 | 13 (26) | A | Segment Dr. | Digit 3 |  |
| B1 | 38 (5) | B |  |  |  | B3 | 14 (27) | B |  |  |  |
| C1 | 39 (6) | C |  |  |  | C3 | 15 (28) | C |  |  |  |
| D1 | 40 (7) | D |  |  |  | D3 | 16 (33) | D |  |  |  |
| E1 | 2 (10) | E |  |  |  | E3 | 17 (34) | E |  |  |  |
| F1 | 4 (12) | $F$ |  |  |  | F3 | 19 (36) | F |  |  |  |
| G1 | 3 (11) | G | $V$ | $\nabla$ | 1 | G3 | 18 (35) | G | , | 1 |  |
| A2 | 6 (18) | A | Segment Dr. | Digit 2 |  | A4 | 20 (37) | A | Segment Dr. | Digit 4 | (MSD) |
| B2 | 7 (19) | B | \| | + |  | B4 | 21 (39) | B |  |  |  |
| C 2 | 8 (20) | C |  |  |  | C4 | 22 (40) | C |  |  |  |
| D2 | 9 (21) | D |  |  |  | D4 | 23 (41) | D |  |  |  |
| E2 | 10 (22) | E |  |  |  | E4 | 24 (42) | E |  |  |  |
| F2 | 12 (25) | F |  |  |  | F4 | 26 (48) | F |  |  |  |
| G2 | 11 (24) | G | 1 | 1 |  | G4 | 25 (43) | G | $V$ | 1 | $V$ |

* 60-Pin Flat Package Pin \# in ( ) .


## Digit Assignment



* i.e. E4


## Functional Block Diagram



## Functional Block Diagram



## Typical Operating Characteristics



TSC7212A LED Segment Current as a Function of Brightness Control Voltage


TSC7212A Operating Power (LED Display) as a Function of Supply Voltage


## Basic Operation

## Basic Operation TSC7211A (LCD) Decoder/Driver

The TSC7211A drives four digit by seven segment LCD dispiays. The device contains 28 individual segment drivers, a backplane driver, an on chip oscillator and a divider chain to generate the backplane signal.

The 28 CMOS segment drivers and backplane driver contain ratioed N and P channel transistors for identical "ON" resistance. The equal resistances eliminate the d.c. output driver component resulting from unequal rise and fall times. This ensures maximum LCD display life.

The backplane output driver can be disabled by grounding the oscillator input (pin 36). The 28 output segment drivers can therefore be synchronized directly to an input signal at the backplane terminal (pin 5). Several slave devices may be cascaded to the backplane output of a master device. The backplane signal may also be derived from an external source. These features permit interfacing to single backplane LCD displays with characters in multiples of four.
Each slave's backplane input represents only a 200 pF capacitive load to the master backplane driver (comparable to one additional segment). The number of slave devices driveable by a master device is therefore set by the larger display backplane capacitive load. The master backplane output will drive the display backplane of 16 one-half inch characters with rise and fall times under $5 \mu \mathrm{sec}$. This represents a system
with 3 slave devices and a fourth master TSC7211A driving the backplane.

If more than four devices are slaved together, the backplane signal should be derived externally and all TSC7211A devices slaved to it. The external drive signal must drive a high capacitive load with $1-2 \mu \mathrm{sec}$ rise and fall times. The backplane frequency is normally 125 Hz . At lower display ambient temperatures the frequency may be reduced to compensate for display response time.

The on chip RC oscillator free runs at approximately 16 kHz . A divide by 128 circuit provides the 125 Hz backplane frequency. The oscillator frequency may be reduced by connecting an external capacitor between the oscillator terminal (pin 36) and V+ (see typical operating characteristic curve).

The free running oscillator may be overriden, if desired, by an external clock. The backplane driver, however, must not be disabled during the external clock's negative or low portion as this will result in a d.c. drive component being applied to the LCD display. This would limit the LCD's display's life. To prevent backplane driver disabling, the oscillator input should be driven from the positive supply to no iess than onefifth the supply voltage above ground. A backplane disable signal will not be sensed if the driving signal remains above ground by one-fifth the supply voltage. An alternate method for externally driving the oscillator permits the oscillator input to swing the full supply voltage range. The oscillator input signal duty cycle is skewed so the low portion duration is less than $1 \mu \mathrm{sec}$. The backplane disable sensing circuit will not respond to such a short signal.


Figure 4: TSC7211A Driving 8 Digit LCD Display in Master Slave Configuration.

## TSC7212A LED Decoder/Driver

The TSC7212A directly drives four digit, seven segment, common anode LED displays. The 28 segment drivers are low leakage, current controlled, open drain N -channel MOS transistors.

A brightness input (pin 5) can be used in two ways to control output transistor drain current. The voltage at the brightness control input is transferred to the output transistor gate for "ON" segments. The brightness voltage directly modulates the segment drivers "ON" resistance. A variable brightness control may be implemented with a single potentiometer (Figure 4). A high value potentiometer ( $100 \mathrm{k} \Omega$ to $1 \mathrm{~m} \Omega$ ) will minimize power consumption.

The brightness input may also be operated digitally as a display enable. At a logic 1 the display is fully "ON" and at a logic 0 fully "OFF." The display brightness may be controlled by a logic signal of varying duty cycle also. When operating with LEDs at higher temperatures and/or higher supply voltages, the device power dissipation may need to be reduced to prevent excessive chip temperature rise. The maximum power dissipation is 1 watt at $25^{\circ} \mathrm{C}$. Derated linearly above $35^{\circ} \mathrm{C}$ to 500 mW at $70^{\circ} \mathrm{C}\left(-15 \mathrm{~mW} /{ }^{\circ} \mathrm{C}\right.$ above $35^{\circ} \mathrm{C}$ ). Power dissipation for the device is given by:

$$
P=\left(V^{+}-V_{\text {FLED }}\right)\left(I_{\text {SEG }}\right) \quad\left(n_{\text {SEG }}\right)
$$

where $\mathrm{V}_{\text {FLED }}$ is the LED forward voltage drop, $\mathrm{I}_{\text {SEO }}$ is segment current, and $\mathrm{n}_{\text {sEG }}$ is the number of "ON" segments. If the device is operated at elevated temperatures, the segment current can be limited through the brightness input to keep power dissipation within the limits described above.
For applications requiring brighter LED displays see the TSC700A data sheet.


Figure 5: Brightness Control

## Input Configuration and Output Codes

The TSC7211A/TSC7212A accept a four-bit, true binary (positive level = logic 1) input at pins 27 (LSB) through 30 (MSB). The binary input is decoded to the seven segment output known as "Code B." The output display format is 0-9, dash, E, H, L.,P and blank (see Table 1). The TSC7211A and TSC7212A will correctly decode binary and BCD true codes to a seven-segment output.

The TSC7211A/TSC7212A accept multiplexed binary or BCD input data at pins 27 (LSB) through pin 30 (MSB). Pins 31 (LSD) through 34 (MSD) are the digit select lines. When the digit select line is taken to a logic 1 level the input data is decoded and stored in the enabled output latch of the selected digit. More than one digit select line may be activated simultaneously. The same character will be written into all selected digits. See Figure 5 for decoder segment assignments.

| BINARY INPUT |  |  |  | CODE B |
| :---: | :---: | :---: | :---: | :---: |
| B3 | B2 | B1 | B0 | TSC7212A |
| 0 | 0 | 0 | 0 | 0 |
| 0 | 0 | 0 | 1 | 1 |
| 0 | 0 | 1 | 0 | 2 |
| 0 | 0 | 1 | 1 | 3 |
| 0 | 1 | 0 | 0 | 4 |
| 0 | 1 | 0 | 1 | 5 |
| 0 | 1 | 1 | 0 | 6 |
| 0 | 1 | 1 | 1 | 7 |
| 1 | 0 | 0 | 0 | 8 |
| 1 | 0 | 0 | 1 | 9 |
| 1 | 0 | 1 | 0 | - |
| 1 | 0 | 1 | 1 | E |
| 1 | 1 | 0 | 0 | H |
| 1 | 1 | 0 | 1 | L |
| 1 | 1 | 1 | 0 | P |
| 1 | 1 | 1 | 1 | (Blank) |

Table I: Output Code


Figure 6: Segment Assignment

## Special Order Decoder Option

The TSC7211A and TSC7212A are mask programmed to give the 16 combinations of seven segment output codes. For large volume orders ( 50 k pieces minimum) custom decoder options are available. Contact factory for details.

## Applications Information

The TSC7212A has two ground pins. These pins should be connected together.

## Applications Information (Continued)



Figure 7: LCD Display Interface to 4 Digit Counter


Figure 8: 4 1/2 Digit DPM Interfaced to LCD Display

## Typical Applications



Figure 9: 4 1/2 Digit ADC Interfaced to LCD Display


Figure 10: 4 1/2 Digit ADC Interfaced to LCD Display with Digit Blanking on Overrange

## Typical Applications (continued)



Figure 11: LCD Display Interface to SY6522 VIA


Figure 12: Digital Scale with LCD Readout

## Typical Applications (continued)



Figure 13: TSC7212A Interface to TSC14433 A 3 1/2 Digit ADC.

## Package Dimensions



## General Description

The TSC7211AM (LCD Decoder/Driver) and TSC7212AM (LED Decoder/Driver) are CMOS direct drive, four digit, seven segment display decoder and drivers. The devices are bus compatible making microprocessor controlled displays possible. Two chip select signals control data and digit select code latching prior to decoding and display. External data latches are unnecessary.
The TSC7211AM drives conventional LCD displays. An RC oscillator, divider chain, backplane driver, and 28 segment outputs are provided on a single CMOS chip. The segment drivers supply square waves of the same frequency as the backplane but in phase for an OFF segment and out of phase for an ON segment. The net d.c. voltage applied between driver segment and backplane is near zero maximizing display lifetime.
The TSC7212AM drives common-anode LED displays with 28 current controlled, low leakage, open drain, N -Channel output transistors. The brightness control input can be used as a digital display enable. A varying voltage at the control input will allow continuous display brightness control.

The four bit binary input code is decoded into the seven segment alphanumeric code known as "Code B." The "Code B" output format results in a 0 to $9,-, E, H, L, P$ or blank display. True BCD or binary inputs will be correctly decoded to the seven segment display format.

## Ordering Information

| Part <br> No. | Driver <br> Type | Package | Output <br> Code | Input <br> Config. |
| :--- | :--- | :--- | ---: | ---: |
| TSC7211AMIPL LCD | 40-Pin <br> Plastic | Code B | Digit Select <br> Latches |  |
| TSC7212AMIPL | LED | 40-Pin |  |  |
| Plastic |  |  |  |  | Code B | Digit Select and |
| ---: |
| Latches |

## TSC7211AM Features (LCD Driver)

- Four digit non-multiplexed seven segment LCD display outputs with backplane driver.
- Input and digit select data latches.
- RC oscillator on-chip generates backplane drive signal.
- Eliminates d.c. bias which degrade LCD display life.
- Backplane input/output pin permits synchronization of cascaded slave device to master backplane signal.
- Binary and BCD inputs decoded to code B (0 to 9, 一, E, H, L, P, blank).
- Pin compatible and functionally equivalent to ICM7211AM.


## TSC7212AM Features (LED Driver)

- 28 current limited outputs drive common-anode LEDs at 8 mA per segment.
- Input and digit select data latches.
- Brightness input allows potentiometer control of LED segment current. Pin also serves as digital display enable.
- Same input configuration and output decoding as the TSC7211AM.


## Pin Configuration



## Absolute Maximum Ratings

Power Dissipation (Note 1) ................. 1.0 W at $70^{\circ} \mathrm{C}$ Supply Voltage .............................................. 6.5 V Input Voltage (Any
Terminal) (Note 2) . .......... $\mathrm{V}^{+}+0.3 \mathrm{~V}$, GROUND -0.3 V
Operating Temperature Range ........... $-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$
Storage Temperature Range ........... $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$
Lead Temperature (Soldering 10 sec. ) .............. $300^{\circ} \mathrm{C}$
Stresses above those listed under absolute maximum ratings may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions above those indicated
in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.
Note 1: This limit refers to that of the package and will not be realized during normal operation.
Note 2: Due to the SCR structure inherent in the CMOS process, connecting any terminal to voltages greater than $\mathrm{V}^{+}$or less than GROUND may cause destructive device latchup. For this reason it is recommended that no inputs from external sources not operating on the same power supply be applied to the device before its supply is established, and that in multiple supply systems, the supply to the TSC7211AM/ TSC7212AM be turned on first.

## Table I: Operating Characteristics

Test Conditions: All parameters measured with $\mathrm{V}+=5 \mathrm{~V}$.
TSC7211AM Characteristics (LCD Decoder/Driver)

| PARAMETER | SYMBOL | CONDITIONS | MIN | TYP | MAX | UNIT |
| :--- | :--- | :--- | ---: | ---: | ---: | ---: |
| Operating Voltage Range | VSUPP |  | 3 | 5 | 6 | V |
| Operating Current | lop | Display Blank | - | 10 | 50 | $\mu \mathrm{~A}$ |
| Oscillator Input Current | losCl | Pin 36 | - | $\pm 2$ | $\pm 10$ | $\mu \mathrm{~A}$ |
| Segment Rise/Fall Time | tRFs | $\mathrm{C}_{\mathrm{L}}=200 \mathrm{pF}$ | - | 0.5 | - | $\mu \mathrm{A}$ |
| Backplane Rise/Fall Time | tRFB | $\mathrm{CL}_{\mathrm{L}}=5000 \mathrm{pF}$ | - | 1.5 | - | $\mu \mathrm{s}$ |
| Oscillator Frequency | fosc | Pin 36 Floating | - | 16 | - | kHz |
| Backplane Frequency | fBP | Pin 36 Floating | - | 125 | - | Hz |

TSC7212AM Characteristics (Common-Anode LED Decoder/Driver)

| PARAMETER | SYMBOL | CONDITIONS | MIN | TYP | MAX | UNIT |
| :--- | :--- | :--- | ---: | ---: | ---: | ---: |
| Operating Supply Voltage Range | VSUPP |  | 4 | 5 | 6 | V |
| Operating Current <br> Display Off | lop | Pin 5 (Brightness), <br> Pins 27-34 = GROUND | - | 10 | 50 | $\mu \mathrm{~A}$ |
| Operating Current | IOP | Pin 5 at V + , Display all 8's | - | 200 | - | mA |
| Segment Leakage Current | ISLK | Segment Off | - | $\pm 0.01$ | $\pm 1$ | $\mu \mathrm{~A}$ |
| Segment On Current | ISEG | Segment On, VO $=+3$ V | 5 | 8 | - | mA |

Input Characteristics (LCD and LED Decoder/Driver)

| PARAMETER | SYMBOL | CONDITIONS | MIN | TYP | MAX |
| :--- | :--- | :--- | ---: | ---: | ---: |
| Logical "1" Input Voltage | $\mathrm{V}_{\mathrm{IH}}$ |  | 3 | - | - |
| Logical "0" Input Voltage | $\mathrm{V}_{\mathrm{IL}}$ |  | - | - | 1 |
| Input Leakage Current | IILK | Pins $27-34$ | - | $\pm 0.01$ | $\pm 1$ |
| Input Capacitance | CIN | Pins $27-34$ | - | 5 | - |
| BP/Brightness Input Leakage | IBPLK | Measured at Pin 5 with Pin 36 <br> at GND | - | $\pm 0.01$ | V |
| BP/Brightness Input Capacitance | CBPI | All Devices | - | 200 | - |

AC Characteristics (LCD and LED Decoder/Driver)

| PARAMETER | SYMBOL | CONDITIONS | MIN | TYP | MAX |
| :--- | :--- | :--- | :--- | :---: | :---: |
| Chip Select Active Pulse Width | tcsA | Note 1 | 200 | - | - |
| Data Setup Time | tDS |  | 100 | - | - |
| Data Hold Time | toH |  | 10 | 0 | - |
| Inter-Chip Select Time | tics |  | 2 | - | - |

Note:

1. Other Chip Select $\overline{(C S)}$ is either held at logic zero or both $\overline{\mathrm{CS} 1}$ and $\overline{\mathrm{CS} 2}$ driven together.

TSC7211AM (LCD)

## Timing Diagrams



Figure 1: BUS Interface Timing Diagram (LED or LCD)


Figure 2: LCD Display Waveforms

## Input Definitions

In this table, $\mathrm{V}+$ and GROUND are considered to be normal operating input logic levels. For lowest power consumption, input signals should swing over the full supply.


## Output Definitions

Output pins are defined by the alphabetical segment assignment and numerical digital assignment.

| OUTPUT | TERMINAL | FUNCTION |  | OUTPUT | TERMINAL |  | FUNCTION |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A1 | 37 | A Segment Dr. Digit 1 | (LSD) | A3 | 13 | A | Segment Dr. Digit 3 |  |
| B1 | 38 | B \| |  | B3 | 14 | B | - |  |
| C1 | 39 | C |  | C3 | 15 | C |  |  |
| D1 | 40 | D |  | D3 | 16 | D |  |  |
| E1 | 2 | E |  | E3 | 17 | E |  |  |
| F1 | 4 | F | $\checkmark$ | F3 | 19 | F | 1 |  |
| G1 | 3 | G | $V$ | G3 | 18 | G | $V$ |  |
| A2 | 6 | A Segment Dr. Digit 2 |  | A4 | 20 | A | Segment Dr. Digit 4 | (MSD) |
| B2 | 7 | B \| |  | B4 | 21 | B | A SegmentDr. Digit |  |
| C2 | 8 | C |  | C4 | 22 | C |  |  |
| D2 | 9 | D |  | D4 | 23 | D |  |  |
| E2 | 10 |  |  | E4 | 24 | E |  |  |
| F2 | 12 | $F \quad \downarrow$ |  | F4 | 26 | F | $\downarrow$ | $\downarrow$ |
| G2 | 11 | G $\quad$ |  | G4 | 25 | G |  | , |

## Digit Assignment



* I.e. E4

Functional Block Diagram


## Functional Block Diagram



## Typical Operating Characteristics



TSC7212AM LED Segment Current as a Function of Brightness Control Voltage


## Basic Operation TSC7211AM (LCD) Decoder/Driver

The TSC7211AM drives four digit, seven segment LCD displays. The device contains 28 individual segment drivers, a backplane driver, a self contained oscillator and a divider chain to generate the backplane signal.
The 28 CMOS segment drivers and backplane driver contain ratioed N and P channel transistors for identical "ON" resistance. The equal resistances eliminate the d.c. output driver component resulting from unequal rise and fall times. This ensures maximum LCD display life.
The backplane output driver can be disabled by grounding the oscillator input (pin 36). The 28 output segment drivers can therefore be synchronized directly to an input signal at the backplane terminal (pin 5). Several slave devices may be cascaded to the backplane output of a master device. The backplane signal may also be derived from an external

TSC7212AM Operating Power
(LED Display) as a Function of Supply Voltage

source. These features permit interfacing to single backplane LCD displays with characters in multiples of four.
Each slave's backplane input represents only a 200 pF capacitive load to the master backplane driver (comparable to one additional segment). The number of slave devices driveable by a master device is therefore set by the larger display backplane capacitive load. The master backplane output will drive the display backplane of 16 one-half inch characters with rise and fall times under $5 \mu \mathrm{sec}$. This represents a system with 3 slave devices and a fourth master TSC7211AM driving the backplane (Figure 3).
If more than four devices are slaved together, the backplane signal should be derived externally and all TSC7211AM devices slaved to it. The external drive signal must drive a high capacitive load with $1-2 \mu \mathrm{sec}$ rise and fall times. The backplane frequency is normally 125 Hz . At lower display ambient temperatures the frequency may be reduced to compensate for display response time.

The on chip RC oscillator free runs at approximately 16 kHz . A divide by 128 circuit provides the 125 Hz backplane frequency. The oscillator frequency may be reduced by connecting an external capacitor between the oscillator terminal (pin 36) and V+ (see typical operating characteristic curve).
The free running oscillator may be overriden, if desired, by an external clock. The backplane driver, however, must not be disabled during the external clock's negative or low portion as this will result in a d.c. drive component being applied to the LCD display. This would limit the LCD's display's life. To prevent backplane driver disabling, the oscillator input should be driven from the positive supply to no less than onefifth the supply voltage above ground. A backplane disable signal will not be sensed if the driving signal remains above ground by one-fifth the supply voltage. An alternate method for externally driving the oscillator permits the oscillator input to swing the full supply voltage range. The oscillator input signal duty cycle is skewed so the low portion duration is less than $1 \mu \mathrm{sec}$. The backplane disable sensing circuit will not respond to such a short signal.


Figure 3: TSC7211AM Driving 8-Digit LCD Display in Master Slave Configuration.

## TSC7212AM LED Decoder/Driver

The TSC7212AM directly drives four digit, seven segment, common-anode LED displays. The 28 segment drivers are low leakage, current controlled, open drain N-channel MOS transistors.
A brightness input (pin 5) can be used in two ways to control output transistor drain current. The voltage at the brightness control input is transferred to the output transistor gate for "ON" segments. The brightness voltage directly modulates the segment drivers "ON" resistance. A variable brightness control may be implemented with a single potentiometer (Figure 4). A high value potentiometer ( $100 \mathrm{k} \Omega$ to $1 \mathrm{M} \Omega$ ) will minimize power consumption.

The brightness input may also be operated digitally as a display enable. At a logic 1 the display is fully "ON" and at a logic 0 fully "OFF." The display brightness may be controlled by a logic signal of varying duty cycle also. When operating with LEDs at higher temperatures and/or higher supply voltages, the device power dissipation may need to be reduced to prevent excessive chip temperature rise. The maximum power dissipation is 1 watt at $25^{\circ} \mathrm{C}$. Derate linearly above $35^{\circ} \mathrm{C}$ to 500 mW at $70^{\circ} \mathrm{C}\left(-15 \mathrm{~mW} /{ }^{\circ} \mathrm{C}\right.$ above $35^{\circ} \mathrm{C}$ ). Power dissipation for the device is given by:

$$
P=\left(V^{+}-V_{F L E D}\right)(I S E G)(n S E G)
$$

where $\mathrm{V}_{\text {FLED }}$ is the LED forward voltage drop, ISEG is segment current, and nSEG is the number of "ON" segments. If the device is operated at elevated temperatures, the segment current can be limited through the brightness input to keep power dissipation within the limits described above.
The display may be blanked (all segments OFF) by applying the input code 1111 or by driving the brightness pin with a logic 0 . If brightness control is not needed, pin 5 should be tied to 5.0 V .


Figure 4: Brightness Control

## Input Configuration and Output Codes

The TSC7211AM/TSC7212AM accept a four bit, true binary (positive level $=$ logic 1 ) input at pins 27 (LSB) through 30 (MSB). The output display format is 0 to $9,-, E, H, L, P$ and blank (see Table 1). Segment assignments are shown in Figure 5. The TSC7211AM and TSC7212AM will correctly decode binary and BCD true codes to a seven segment output.

The TSC7211AM and TSC7212AM are designed to interface with a data bus and display data under microprocessor control. Four data input bits (Pins 27-30) and two digit select input bits (Pins 31, 32) are written into input buffer latches. The rising edge of either chip select causes data to be latched, decoded and stored in the selected digit output data latch. The two bit digit code selects the appropriate output digit latch. The four bit display data word is decoded to the "Code B" seven segment output format.
For applications where bus compatibility is not required refer to the TSC7211A (LCD), TSC7212A (LED) and TSC700A (LED) four digit decoder driver data sheets. These devices are designed to accept multiplexed BCD/Binary input data for display under the control of four separate digit select control signals.
$\left.\begin{array}{|cccc|}\hline \text { BINARY INPUT } & \begin{array}{c}\text { CODE B } \\ \text { TSC7211AM } \\ \text { TSC7212AM }\end{array} \\ 0 & 0 & 0 & 0\end{array}\right] 0$


Figure 5: Segment Assignment

## Special Order Decoder Option

The TSC7211AM and TSC7212AM are mask programmed to give the 16 seven segment output codes. For large volume orders ( 25 k pieces minimum) custom decoder options are available. Contact factory for details.

## Applications Information

The TSC7212AM has two ground pins. These pins should be connected together.

Table 1: Output Code
Package Outline

## 40-Pin Plastic Dual-In-Line Package <br> P Package <br> (Package \#17)



Section 11
Interface ICs ..... 11-3
TSC426/427/428 Dual High Speed Power MOSFET Driver ..... 11-5
TSC450 Dual Power MOSFET Driver ..... 11-15
TSC7660 DC to DC Voltage Converter ..... 11-19TSC9403
TSC9404 Serial Input/16-Bit Parallel Output Peripheral Driver (15 V) ..... 11-31Serial Input/16-Bit Parallel Output Peripheral Driver (20 V)11-31

# *N TELEDYNE SEMICONDUCTOR 

## TSC426/427/428 Dual Power MOSFET Driver - 30 ns Rise Time - Low Power CMOS

## General Description

The TSC426/427/428 are dual CMOS high speed drivers. A TTL/CMOS input voltage level is translated into an output voltage level swing equalling the supply. The CMOS output will be within 25 mV of ground or positive supply. Bipolar designs are capable of swinging only within 1 volt of the supply.
The low impedance high current driver outputs will swing a 1000 pf load 18 V in 30 ns . The unique current and voltage drive qualities make the TSC426/427/428 ideal power MOSFET drivers, line drivers and DC to DC converter building blocks.
Input logic signals may equal the power supply voltage. Input current is a low $1 \mu \mathrm{~A}$ making direct interface to CMOS/BIPOLAR switch mode power supply control integrated circuits possible as well as open collector analog comparators.
Quiescent power supply current is 8 mA maximum. The TSC426 requires $1 / 5$ the current of the pin compatible bipolar DS0026 device. This is important in DC to DC converter applications with power efficiency constraints and high frequency switch mode power supply applications. Quiescent
Features

- High Speed Switching $\left(\mathrm{C}_{\mathrm{H}}=1000 \mathrm{pf}\right)$ ..... 30 ns
- High Peak Output Current ..... 1.5 A
- High Output Voltage Swing ..... $V_{S}-25 \mathrm{mV}$
- Low Input Current (Logic "0" or "1") ............ $1 \mu \mathrm{~A}$
- TTL/CMOS Input Compatible
- Available in Inverting \& Non-Inverting Configurations
- Wide Operating Supply Voltage .......... 4.5 V to 18 V
- Low Power Consumption (Inputs Low) ........ 0.4 mA
- Single Supply Operation
- Low Output Impedance
- Pin Out Equivalent to DSOO26 \& MMH0026
current is typically 6 mA when driving a 1000 pf load 18 V at 100 kHz .

The inverting TSC426 driver is pin compatible with the bipolar DSOO26 and MMH0026 devices. The TSC427 is noninverting; the TSC428 contains an inverting and non-inverting driver.

## Pin Configuration (See Ordering Information on Page 4)



## Functional Diagram


\$1 TELEDYNE SEMICONDUCTOR

## Dual Power MOSFET Driver <br> - 30 ns Rise Time Low Power CMOS

Input Voltage Any Terminal . . Vs +0.3 V to $\operatorname{Ground}-0.3 \mathrm{~V}$ Operating Temperature
M Version . . . . . . . . . . . . . . . . . . . . . . $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$

I Version . . . . . . . . . . . . . . . . . . . . . . . . . . $-25^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$
C Version ............................... . . . $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$
Maximum Chip Temperature ........................ . $+150^{\circ} \mathrm{C}$
Storage Temperature ................... $-55^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$
Lead Temperature ( 10 Sec ) ........................... $300^{\circ} \mathrm{C}$

TSC426
Electrical Characteristics: $T_{A}=25^{\circ} \mathrm{C}$ with $4.5 \mathrm{~V} \leq \mathrm{V}_{\mathrm{S}} \leq 18 \mathrm{~V}$ unless otherwise specified.

| TYPE | NO. | SYMBOL | PARAMETER | CONDITIONS | MIN | $\begin{gathered} \text { TSC426 } \\ \text { TYP } \end{gathered}$ | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \mathbf{I} \\ & \mathbf{N} \\ & \mathbf{P} \\ & \mathbf{U} \\ & \mathbf{T} \end{aligned}$ | 1 | $\mathrm{V}_{1} \mathrm{H}$ | Logic 1 Input Voltage | - | 2.4 | - | - | V |
|  | 2 | VIL | Logic 0 Input Voltage |  | - | - | 0.8 | V |
|  | 3 | IIN | Input Current | $0 \leq \mathrm{V}_{\text {IN }} \leq \mathrm{V}_{\text {S }}$ | -1 | - | 1 | $\mu \mathrm{A}$ |
| $\begin{aligned} & 0 \\ & \mathbf{U} \\ & \mathbf{T} \\ & \mathbf{P} \\ & \mathbf{U} \\ & \mathbf{T} \end{aligned}$ | 4 | VOH | High Output Voltage |  | Vs -0.025 | - | - | V |
|  | 5 | VOL | Low Output Voltage |  | - | - | 0.025 | V |
|  | 6 | Ro | Output Resistance | $\begin{aligned} & V_{I N}=0.8 \mathrm{~V} \\ & \text { IOUT }=10 \mathrm{~mA}, \mathrm{~V}_{\mathrm{S}}=18 \mathrm{~V} \end{aligned}$ | - | 10 | 15 | $\Omega$ |
|  | 7 | Ro | Output Resistance | $\begin{aligned} & \mathrm{V}_{\mathrm{IN}}=2.4 \mathrm{~V} \\ & \text { IOUT }=10 \mathrm{~mA}, \mathrm{~V}_{\mathrm{S}}=18 \mathrm{~V} \end{aligned}$ | - | 6 | 10 | $\Omega$ |
|  | 8 | IPK | Peak Output Current |  | - | 1.5 | - | A |
| $S$$W$$I$$T$$C$$C$$H^{M}$$I$$N$$G$ | 9 | $T_{R}$ | Rise Time | Test Figure 1 | - | - | 30 | ns |
|  | 10 | TF | Fall Time | Test Figure 1 | - | - | 20 | ns |
|  | 11 | TD1 | Delay Time | Test Figure 1 | - | - | 40 | ns |
|  | 12 | TD2 | Delay Time | Test Figure 1 | - | - | 75 | ns |
| $\begin{aligned} & P S \\ & O U \\ & W_{P} \\ & E P \\ & R L \\ & \hline \end{aligned}$ | 13 | Is | Power Supply Current | $\mathrm{VIN}=3.0 \mathrm{~V}$ (Both Inputs) | - | - | 8.0 | mA |
|  | 14 | is | Power Supply Current | $V_{i N}=0.0 \mathrm{~V}$ (Both Inputs) | - | - | 0.4 | mA |

## TSC426

Electrical Characteristics: Over operating temperature range with $4.5 \mathrm{~V} \leq \mathrm{V}_{\mathrm{S}} \leq 18 \mathrm{~V}$ unless otherwise specified.

| TYPE | NO. | SYMBOL | PARAMETER | CONDITIONS | MIN | $\begin{gathered} \text { TSC426 } \\ \text { TYP } \end{gathered}$ | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \mathbf{I} \\ & \mathbf{N} \\ & \mathbf{P} \\ & \mathbf{U} \\ & \mathbf{T} \end{aligned}$ | 1 | VIH | Logic 1 Input Voltage |  | 2.4 | - | - | V |
|  | 2 | VIL | Logic 0 Input Voltage |  | - | - | 0.8 | V |
|  | 3 | lin | Input Current | $0 \leq \mathrm{V}_{\text {IN }} \leq \mathrm{V}_{\text {S }}$ | -10 | - | 10 | $\mu \mathrm{A}$ |
| $\begin{aligned} & \hline \mathbf{O} \\ & \mathbf{U} \\ & \mathbf{T} \\ & \mathbf{P} \\ & \mathbf{U} \end{aligned}$ | 4 | VOH | High Output Voltage |  | Vs -0.025 | - | - | V |
|  | 5 | Vol | Low Output Voltage |  | - | - | 0.025 | V |
|  |  |  |  |  |  |  |  |  |

TSC426
Electrical Characteristics: Over operating temperature range with $4.5 \mathrm{~V} \leq \mathrm{V}_{\mathrm{S}} \leq 18 \mathrm{~V}$ unless otherwise specified.

| TYPE | NO. | SYMBOL | PARAMETER | CONDITIONS | MIN | $\begin{gathered} \hline \text { TSC426 } \\ \text { TYP } \end{gathered}$ | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| O U $\mathbf{T}$ | 6 | Ro | Output Resistance | $\begin{aligned} & \mathrm{V}_{\mathrm{IN}}=0.8 \mathrm{~V} \\ & \text { IOUT }=10 \mathrm{~mA}, \mathrm{VS}_{\mathrm{S}}=18 \mathrm{~V} \end{aligned}$ | - | 13 | 20 | $\Omega$ |
| U | 7 | Ro | Output Resistance | $\begin{aligned} & \mathrm{V}_{\mathrm{IN}}=2.4 \mathrm{~V} \\ & \text { IOUT }=10 \mathrm{~mA}, \mathrm{~V}_{\mathrm{S}}=18 \mathrm{~V} \end{aligned}$ | - | 8 | 15 | , |
| S | 8 | TR | Rise Time | Test Figure 1 | - | - | 60 | ns |
| $\begin{aligned} & I T \\ & \mathrm{~T} \\ & \mathrm{C} \\ & \hline \end{aligned}$ | 9 | TF | Fall Time | Test Figure 1 | - | - | 40 | ns |
| $\underset{i}{H_{E}^{M}}$ | 10 | TD1 | Delay Time | Test Figure 1 | - | - | 60 | ns |
| $\begin{aligned} & \mathbf{N} \\ & \mathbf{G} \end{aligned}$ | 11 | TD2 | Delay Time | Test Figure 1 | - | - | 120 | ns |
| $\begin{aligned} & \mathbf{p} \mathbf{S} \\ & \mathbf{O} \mathbf{U} \end{aligned}$ | 12 | Is | Power Supply Current | V IN $=3.0 \mathrm{~V}$ (Both Inputs) | - | - | 12.0 | mA |
| $\begin{aligned} & \mathbf{W} \mathbf{E} \\ & \mathbf{R}_{\mathbf{Y}} \\ & \hline \end{aligned}$ | 13 | Is | Power Supply Current | $\mathrm{V}_{\mathrm{IN}}=0.0 \mathrm{~V}$ (Both Inputs) | - | - | 0.6 | mA |

## TSC427

Electrical Characteristics: $T_{A}=25^{\circ} \mathrm{C}$ with $4.5 \mathrm{~V} \leq \mathrm{V}_{\mathrm{S}} \leq 18 \mathrm{~V}$ unless otherwise specified.

| TYPE | NO. | SYMBOL | PARAMETER | CONDITIONS |  TSC427  <br> MIN TYP MAX |  |  | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \mathbf{I} \\ & \mathbf{N} \\ & \mathbf{P} \\ & \mathbf{U} \\ & \mathbf{T} \end{aligned}$ | 1 | $\mathrm{V}_{1} \mathrm{H}$ | Logic 1 Input Voltage |  | 2.4 | - | - | V |
|  | 2 | VIL | Logic 0 Input Voltage |  | - | - | 0.8 | V |
|  | 3 | IIN | Input Current | $0 \leq \mathrm{V}_{1 N} \leq \mathrm{V}_{S}$ | -1 | - | 1 | $\mu \mathrm{A}$ |
| $\begin{aligned} & O \\ & U \\ & T \\ & P \\ & U \\ & T \end{aligned}$ | 4 | VOH | High Output Voltage |  | Vs -0.025 | - | - | V |
|  | 5 | VOL | Low Output Voltage |  | - | - | 0.025 | V |
|  | 6 | Ro | Output Resistance | $\begin{aligned} & \mathrm{V}_{\text {IN }}=2.4 \mathrm{~V} \\ & \mathrm{IOUT}_{\mathrm{OU}}=10 \mathrm{~mA}, \mathrm{~V}_{\mathrm{S}}=18 \mathrm{~V} \end{aligned}$ | - | 10 | 15 | $\Omega$ |
|  | 7 | Ro | Output Resistance | $\begin{aligned} & \mathrm{V}_{\text {IN }}=0.8 \mathrm{~V} \\ & \text { IOUT }=10 \mathrm{~mA}, \mathrm{~V}_{\mathrm{S}}=18 \mathrm{~V} \end{aligned}$ | - | 6 | 10 | § |
|  | 8 | IPK | Peak Output Current |  | - | 1.5 | - | A |
| S$W$$I$$T$$C$$C$$H$$H$$I$$N$$G$ | 9 | TR | Rise Time | Test Figure 1 | - | - | 30 | ns |
|  | 10 | TF | Fall Time | Test Figure 1 | - | - | 20 | ns |
|  | 11 | TD1 | Delay Time | Test Figure 1 | - | - | 40 | ns |
|  | 12 | TD2 | Delay Time | Test Figure 1 | - | - | 75 | ns |
| $\begin{aligned} & p_{S}^{S} \\ & O_{U} \\ & W_{p} \\ & E_{Y} \\ & R \end{aligned}$ | 13 | Is | Power Supply Current | V IN $=3.0 \mathrm{~V}$ (Both Inputs) | - | - | 8.0 | mA |
|  | 14 | Is | Power Supply Current | $\mathrm{V}_{\text {IN }}=0.0 \mathrm{~V}$ (Both Inputs) | - | - | 0.4 | mA |
| NOTES: <br> 1. Functional operation above the absolute maximum stress ratings is not implied. |  |  |  |  | device. Unus $t$ devices from uaranteed by | vices mus ic dischar n. | stored d static | nductiv |

## Dual Power MOSFET Driver - 30 ns Rise Time

## TSC427

Electrical Characteristics: Over operating temperature range with $4.5 \mathrm{~V} \leq \mathrm{V}_{\mathrm{s}} \leq 18 \mathrm{~V}$ unless otherwise specified.

| TYPE | NO. | SYMBOL | PARAMETER | CONDITIONS | MIN | $\begin{gathered} \text { TSC427 } \\ \text { TYP } \end{gathered}$ | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \mathbf{I} \\ & \mathbf{N} \\ & \mathbf{P} \\ & \mathbf{U} \\ & \mathbf{T} \end{aligned}$ | 1 | $\mathrm{V}_{1}$ | Logic 1 Input Voltage |  | 2.4 | - | - | V |
|  | 2 | VIL | Logic 0 Input Voltage |  | - | - | 0.8 | V |
|  | 3 | lin | Input Current | $0 \leq \mathrm{V}_{\text {IN }} \leq \mathrm{V}_{\text {S }}$ | -10 | - | 10 | $\mu \mathrm{A}$ |
| $\begin{aligned} & \mathbf{O} \\ & \mathbf{U} \\ & \mathbf{T} \\ & \mathbf{P} \\ & \mathbf{U} \\ & \mathbf{T} \end{aligned}$ | 4 | VOH | High Output Voltage |  | Vs -0.025 | - | - | V |
|  | 5 | Vol | Low Output Voltage |  | - | - | 0.025 | V |
|  | 6 | Ro | Output Resistance | $\begin{aligned} & \mathrm{V}_{\mathrm{IN}}=2.4 \mathrm{~V} \\ & \text { Iout }=10 \mathrm{~mA}, \mathrm{~V}_{\mathrm{S}}=18 \mathrm{~V} \end{aligned}$ | - | 13 | 20 | $\Omega$ |
|  | 7 | Ro | Output Resistance | $\begin{aligned} & \mathrm{V}_{\mathrm{IN}}=0.8 \mathrm{~V} \\ & \text { lout }=10 \mathrm{~mA}, \mathrm{~V}_{\mathrm{S}}=18 \mathrm{~V} \end{aligned}$ | - | 8 | 15 | $\Omega$ |
|  | 8 | TR | Rise Time | Test Figure 1 | - | - | 60 | ns |
|  | 9 | TF | Fall Time | Test Figure 1 | - | - | 40 | ns |
|  | 10 | TD1 | Delay Time | Test Figure 1 | - | - | 60 | ns |
|  | 11 | TD2 | Delay Time | Test Figure 1 | - | - | 120 | ns |
|  | 12 | Is | Power Supply Current | $\mathrm{V}_{\text {IN }}=3.0 \mathrm{~V}$ (Both Inputs) | - | - | 12.0 | mA |
|  | 13 | Is | Power Supply Current | V IN $=0.0 \mathrm{~V}$ (Both Inputs) | - | - | 0.6 | mA |

TSC428
Electrical Characteristics: $T_{A}=25^{\circ} \mathrm{C}$ with $4.5 \mathrm{~V} \leq \mathrm{V}_{\mathrm{S}} \leq 18 \mathrm{~V}$ unless otherwise specified.

| TYPE | NO. | SYMBOL | PARAMETER | CONDITIONS | MIN | $\begin{gathered} \hline \text { TSC428 } \\ \text { TYP } \end{gathered}$ | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \mathbf{I} \\ & \mathbf{N} \\ & \mathbf{P} \\ & \mathbf{U} \\ & \mathbf{T} \end{aligned}$ | 1 | $V_{1 H}$ | Logic 1 Input Voltage |  | 2.4 | - | - | V |
|  | 2 | VIL | Logic 0 Input Voltage |  | - | - | 0.8 | V |
|  | 3 | lin | Input Current | $0 \leq V_{\text {IN }} \leq \mathrm{V}_{\text {S }}$ | -1 | - | 1 | $\mu \mathrm{A}$ |
| $\begin{aligned} & \mathbf{O} \\ & \mathbf{U} \\ & \mathbf{T} \\ & \mathbf{P} \\ & \mathbf{U} \\ & \mathbf{T} \end{aligned}$ | 4 | VOH | High Output Voltage |  | VS -0.025 | - | - | v |
|  | 5 | VoL | Low Output Voltage |  | - | - | 0.025 | v |
|  | 6 | Ro | Output Resistance | Output High $\text { lout }=10 \mathrm{~mA}, \mathrm{~V}_{\mathrm{S}}=18 \mathrm{~V}$ | - | 10 | 15 | $\Omega$ |
|  | 7 | Ro | Output Resistance | $\begin{aligned} & \text { Output Low } \\ & \text { Iout }=10 \mathrm{~mA}, \mathrm{~V}_{\mathrm{S}}=18 \mathrm{~V} \end{aligned}$ | - | 6 | 10 | $\Omega$ |
|  | 8 | IPK | Peak Output Current |  | - | 1.5 | - | A |

## NOTES:

1. Functional operation above the absolute maximum stress ratings is not implied.
2. Static Sensitive device. Unused devices must be stored in conductive material to protect devices from static discharge and static fields.
3. Switching times guaranteed by design.

TSC428
Electrical Characteristics: $T_{A}=25^{\circ} \mathrm{C}$ with $4.5 \mathrm{~V} \leq \mathrm{V}_{S} \leq 18 \mathrm{~V}$ unless otherwise specified.

| TYPE | NO. | SYMBOL | PARAMETER | CONDITIONS | MIN | $\begin{gathered} \text { TSC428 } \\ \text { TYP } \end{gathered}$ | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \mathbf{S} \\ & \mathbf{w} \end{aligned}$ | 9 | TR | Rise Time | Test Figure 1 | - | - | 30 | ns |
| $\begin{aligned} & 1 \\ & { }^{\top} \\ & \hline \end{aligned}$ | 10 | TF | Fall Time | Test Figure 1 | - | - | 20 | ns |
| ${\underset{I}{C}}_{\mathrm{H}}^{\mathrm{M}}$ | 11 | TD1 | Delay Time | Test Figure 1 | - | - | 40 | ns |
| $\begin{aligned} & \dot{\mathbf{N}} \\ & \mathbf{G} \end{aligned}$ | 12 | TD2 | Delay Time | Test Figure 1 | - | - | 75 | ns |
| ${ }_{\text {P }}^{\text {P }}$ | 13 | Is | Power Supply Current | $\mathrm{V}_{\text {IN }}=3.0 \mathrm{~V}$ (Both Inputs) | - | - | 8.0 | mA |
| $\begin{aligned} & W \\ & E \\ & \mathcal{E}_{\mathrm{Y}} \\ & \hline \end{aligned}$ | 14 | Is | Power Supply Current | $\mathrm{V}_{1 \times}=0.0 \mathrm{~V}$ (Both Inputs) | - | - | 0.4 | mA |

## TSC428

Electrical Characteristics: Over operating temperature range with $4.5 \mathrm{~V} \leq \mathrm{V}_{\mathrm{S}} \leq 18 \mathrm{~V}$ unless otherwise specified.

| TYPE | NO. | SYMBOL | PARAMETER | CONDITIONS | MIN | $\begin{gathered} \text { TSC428 } \\ \text { TYP } \end{gathered}$ | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \mathbf{I} \\ & \mathbf{N} \\ & \mathbf{P} \\ & \mathbf{U} \\ & \mathbf{T} \end{aligned}$ | 1 | $\mathrm{V}_{1}$ | Logic 1 Input Voltage |  | 2.4 | - | - | V |
|  | 2 | VIL | Logic 0 Input Voltage |  | - | - | 0.8 | V |
|  | 3 | lin | Input Current | $0 \leq \mathrm{V}_{\text {IN }} \leq \mathrm{V}_{\text {S }}$ | -10 | - | 10 | $\mu \mathrm{A}$ |
| $\begin{aligned} & \mathbf{O} \\ & \mathbf{U} \\ & \mathbf{T} \\ & \mathbf{P} \\ & \mathbf{U} \end{aligned}$ | 4 | VOH | High Output Voltage |  | VS -0.025 | - | - | V |
|  | 5 | Vol | Low Output Voltage |  | - | - | 0.025 | V |
|  | 6 | Ro | Output Resistance | $\begin{aligned} & \text { Output High } \\ & \text { lout }=10 \mathrm{~mA}, \mathrm{~V}_{\mathrm{S}}=18 \mathrm{~V} \end{aligned}$ | - | 13 | 20 | $\Omega$ |
|  | 7 | Ro | Output Resistance | Output Low $\text { lout }=10 \mathrm{~mA}, \mathrm{~V}_{\mathrm{S}}=18 \mathrm{~V}$ | - | 8 | 15 | $\Omega$ |
| $\begin{aligned} & \hline S_{1} \\ & W^{\prime} \\ & I^{T} \\ & \mathbf{C}_{1} \\ & C_{M} \\ & H_{E} \\ & N^{\prime} \\ & G \end{aligned}$ | 8 | TR | Rise Time | Test Figure 1 | - | - | 60 | ns |
|  | 9 | TF | Fall Time | Test Figure 1 | - | - | 40 | ns |
|  | 10 | TD1 | Delay Time | Test Figure 1 | - | - | 60 | ns |
|  | 11 | TD2 | Delay Time | Test Figure 1 | - | - | 120 | ns |
|  | 12 | Is | Power Supply Current | V IN $=3.0 \mathrm{~V}$ (Both Inputs) | - | - | 12.0 | mA |
|  | 13 | Is | Power Supply Current | V IN $=0.0 \mathrm{~V}$ (Both Inputs) | - | - | 0.6 | mA |
| NOTES: <br> 1. Functional operation above the absolute maximum stress ratings is not implied. |  |  |  |  | device. Unus devices fro guaranteed by | vices mus ic dischar gn. | stored d static | nductive |

# Dual Power MOSFET Driver <br> - 30 ns Rise Time <br> - Low Power CMOS 

TSC426/427/428

## Ordering Information

| Part No. | Package | Configuration | Temperature <br> Range |
| :--- | :--- | :--- | ---: |
| TSC426CPA | 8-Pin <br> Plastic Dip | Inverting | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ |
| TSC426IJA* | 8-Pin <br> CerDIP | Inverting | $-25^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
| TSC426MJA* | 8-Pin <br> CerDIP | Inverting | $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |
| TSC427CPA | 8-Pin <br> Plastic Dip | Non-Inverting | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ |
| TSC427IJA* | $8-$-Pin <br> CerDIP | Non-Inverting | $-25^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
| TSC427MJA* | $8-$-Pin <br> CerDIP | Non-Inverting | $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |

Switching Time Test Circuits


Figure 1: Inverting Driver Switching Time

| Part No. | Package | Configuration | Temperature <br> Range |
| :--- | :--- | :--- | ---: |
| TSC428CPA | 8-Pin <br> Plastic Dip | Non-Inv. \& Inv. | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ |
| TSC428IJA* | 8-Pin <br> CerDIP | Non-Inv. \& Inv. | $-25^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
| TSC428MJA* | 8-Pin <br> CerDIP | Non-Inv. \& Inv. | $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |
| TSC426C/Y | CHIP | Inverting | $25^{\circ} \mathrm{C}$ |
| TSC427C/Y | CHIP | Non-Inverting | $25^{\circ} \mathrm{C}$ |
| TSC428C/Y | CHIP | Non-Inv. \& Inv. | $25^{\circ} \mathrm{C}$ |

* For devices with $125^{\circ} \mathrm{C}, 160$ Hour Burn In add /BI to part number suffix.


Figure 2: Non-Inverting Driver Switching Time


TSC426 Switching Speed


## Typical Characteristic Curves

Rise and Fall Time vs Supply Voltage


Delay Time vs Temperature


Supply Current vs Frequency


Delay TIme vs Supply Voltage


## Supply Current vs Capacitive Load



High Output vs Voltage


Rise and Fall Time vs Temperature


Rise and Fall Time vs Capacitive Load


# Dual Power MOSFET Driver - 30 ns Rise Time 

## Typical Characteristic Curves



Delay Time vs Supply Voltage


Supply Current vs Frequency


Delay Time vs Temperature


## Supply Current vs

 Capacitive Load

High Output Voltage


Rise and Fall Time vs Supply Voltage


Rise and Fall Time vs Capacitive Load


Low Output Voltage


## Typical Characteristic Curves

## Quiescent Power Supply Current

 vsSupply Voltage


Package Power
Dissipation Dissipation


Quiescent Power Supply Current vs
Supply Voltage


## Supply Bypassing

Charging and discharging large capacitive loads quickly requires large currents. For example, changing a 1000 pf load 18 volts in 25 ns requires a 0.8 A current from the device power supply.
To guarantee low supply impedance over a wide frequency range, a parallel capacitor combination is recommended for supply bypassing. Low inductance ceramic disk capacitors with short lead lengths (<0.5 inch) should be used. A $4.7 \mu \mathrm{f}$ solid tantalum capacitor in parallel with one or two 0.1 uf ceramic disk capacitors normally provides adequate bypassing.

## Grounding

The TSC426 and TSC428 contain inverting drivers. Ground potential drops developed in common ground impedances from input to output will appear as negative feedback and degrade switching speed characteristics.
Individual ground returns for the input and output circuits or a ground plane should be used.

## Input Stage

The input voltage level changes the no load or quiescent supply current. The N channel MOSFET input stage transistor drives a 2.5 mA current source load. With a logic "1" input, the maximum quiescent supply current is 8 mA . Logic " 0 " input level signals reduce quiescent current to $400 \mu \mathrm{~A}$ maximum. Minimum power dissipation occurs for logic " 0 " inputs for the TSC426/427/428; unused driver inputs must be grounded or tied to the positive supply.
The drivers are designed with 100 mV of hysteresis. This provides clean transitions and minimizes output stage current spiking when changing states. Input voltage thresholds are approximately 1.5 V making the device TTL compatible over the 4.5 V to 18 V operating supply range. Input current is less than $1 \mu \mathrm{~A}$ over this range.

The TSC426/427/428 may be directly driven by the TL494, SG1526/1527, SG1524, SE5560 and similar switch mode power supply integrated circuits.

## Power Dissipation

The supply current vs frequency and supply current vs capacitive load characteristic curves will aid in determining power dissipation calculations.
The TSC426/427/428 CMOS drivers have greatly reduced quiescent DC power consumption. Maximum quiescent current is 8 mA compared to the DS 002640 mA specification. For a 15 V supply, power dissipation is typically 40 mW .
Two other power dissipation components are:

- Output stage AC and DC load power.
- Transition state power.

Output stage power is:

$$
\begin{aligned}
P O & =P D C+P_{A C} \\
& =V_{O}(I D C)+f C_{L} V_{S}^{2}
\end{aligned}
$$

Where:

$$
\begin{aligned}
& \text { Vo }=\text { DC output voltage } \\
& \text { IDC }=\text { DC output load current } \\
& \text { f }=\text { Switching frequency } \\
& \text { Vs }=\text { Supply voltage }
\end{aligned}
$$

In power MOSFET drive applications the PDC term is negligible. MOSFET power transistors are high impedance, capacitive input devices. In applications where resistive loads or relays are driven the PDC component will normally dominate.

The magnitude of $P_{A C}$ is readily estimated for several cases:
A.

1. $f=200 \mathrm{kHz}$
B. $1 . \mathrm{f}=200 \mathrm{kHz}$
2. $C_{L}=1000 \mathrm{pf}$
3. $C_{L}=1000 \mathrm{pf}$
4. $\mathrm{V}_{\mathrm{S}}=18 \mathrm{~V}$
5. $V_{S}=15 \mathrm{~V}$
6. $\mathrm{P}_{\mathrm{AC}}=65 \mathrm{~mW}$

During output level state changes, a current surge will flow through the series connected N and P channel output MOSFETS as one device is turning "ON" while the other is turning "OFF." The current spike flows only during output transitions. The input levels should not be maintained
between the logic " 0 " and logic " 1 " levels. Unused driver Inputs must be tied to ground and not be allowed to float. Average power dissipation will be reduced by minimizing input rise times. As shown in the characteristic curves, average supply current is frequency dependent.

## Voltage Doubler




## Voltage Inverter




## Package Information



## General Description

The TSC450 is a low cost bipolar dual driver with TTL compatible inputs and high voltage outputs. Each device may be configured in an inverting or non-inverting configuration. The active pullup, high voltage outputs will drive power MOSFET gates. See the TSC426/427/428 for higher speed power MOSFET drivers.

The TSC450 also serves as a logic level translator and discrete analog switch driver.

## Ordering Information

| Part No. | Supply <br> Voltage | Temp. <br> Range | Package |
| :--- | :---: | :---: | :--- |
| TSC450AIJE | 15 V | $-25^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 16 Pin CerDIP |
| TSC450ACPE | 15 V | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ | 16 Pin Epoxy |
| TSC450BIJE | 12 V | $-25^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 16 Pin CerDIP |
| TSC450BCPE | 12 V | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ | 16 Pin Epoxy |
| TSC450AMJE | 15 V | $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 16 Pin CerDIP |
| TSC450BMJE | 12 V | $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 16 Pin CerDIP |

## Features

- Dual Device for High Packing Density
- User Selectable Inverting or Non-Inverting Operation
- Single Supply Operation
- TTL Compatible Inputs
- High Output Sink Current . ........................... 12 mA
- High Output Source Current ....................... 6 mA
- Fast Switching ......................................... 125 ns


## Pin Configuration



Functional Diagram (1/2 Circuit)


Absolute Maximum Ratings

|  | J Package, <br> CerDIP | P Package, <br> Plastic |
| :--- | :---: | :---: |
| Storage Temperature | $-65^{\circ} \mathrm{C}$ <br> to $+150^{\circ} \mathrm{C}$ | $-55^{\circ} \mathrm{C}$ <br> to $+100^{\circ} \mathrm{C}$ |
| Lead Temperature <br> (1/16 inch from case, <br> 10 sec max) | $300^{\circ} \mathrm{C}$ | $300^{\circ} \mathrm{C}$ |
| Continuous Supply <br> Voltage |  |  |
| Type B Device <br> Type A Device | +15.0 V | +15.0 V |


|  | J Package, <br> CerDIP | P Package, <br> Plastic |
| :--- | :---: | :---: |
| Pulsed Supply Voltage <br> (less than 100 msec) | +18.0 V | +18.0 V |
| Input Voltage (any input) <br> Type B Device <br> Type A Device | -0.5 to +15 V | -0.5 to +15 V |
| Surge Sink Current <br> (less than 100 msec at | -0.5 to +18 V | -0.5 to +18 V |
| $\mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ ) | 20 mA | 20 mA |

Note: Exceeding the absolute maximum ratings may cause permanent damage. Operation at the absolute maximum ratings or beyond the
conditions guaranteed is not implied.

Electrical Characteristics: Specifications apply over full operating temperature range. $\mathrm{V}_{\mathrm{cc}}=+15 \mathrm{~V}$ for type A devices and $\mathrm{V}_{\mathrm{cc}}=12 \mathrm{~V}$ for type B devices unless otherwise indicated.

| TYPE | NO. | SYMBOL | PARAMETER | TEST CONDITIONS | MIN | $\begin{aligned} & \text { TSC450 } \\ & \text { TYP } \end{aligned}$ | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \mathbf{I} \\ & \mathbf{N} \\ & \mathbf{P} \\ & \mathbf{U} \\ & \mathbf{T} \end{aligned}$ | 1 | Vinh | Input High Voltage | $\mathrm{I}_{\text {IN }} \leq 40 \mu \mathrm{~A}$ | 2.0 | - | - | v |
|  | 2 | $V_{\text {INL }}$ | Input Low Voltage |  | - | - | 0.8 | v |
|  | 3 | İnh | Input High Current |  | - | - | 10 | $\mu \mathrm{A}$ |
|  | 4 | 1 INL | Input Low Current | $\mathrm{V}_{\mathrm{IN}}=0.4 \mathrm{~V}$ | - | - | 1.6 | mA |
| $\begin{aligned} & 0 \\ & U \\ & \mathbf{U} \\ & \mathbf{P} \\ & \mathbf{U} \\ & \mathbf{T} \end{aligned}$ | 5 | $\mathrm{V}_{\text {OHL }}$ | Loaded Output High Voltage | $\begin{gathered} \hline \mathrm{V}_{\mathrm{cc}}=12 \mathrm{~V}, \mathrm{I}_{\text {OH }}=5 \mathrm{~mA} \\ \text { (Type B Device) } \end{gathered}$ | 6.0 | - | - | V |
|  | 6 | Vон | Output High Voltage | $\begin{gathered} \mathrm{V}_{\mathrm{cc}}=11 \mathrm{~V} \\ \text { (Type B Device) } \\ \hline \end{gathered}$ | 9.0 | - | - | V |
|  | 7 | Vohl | Loaded Output High Voltage | $\begin{gathered} \mathrm{V}_{\mathrm{cc}}=15 \mathrm{~V}, \text { Ioh }_{\text {on }}=5 \mathrm{~mA} \\ \text { (Type A Device) } \end{gathered}$ | 9.0 | - | - | V |
|  | 8 | Vон | Output High Voltage | $\begin{gathered} \mathrm{V}_{\mathrm{cc}}=14 \mathrm{~V} \\ \text { (Type A Device) } \end{gathered}$ | 12.0 | - | - | V |
|  | 9 | VoL | Output Low Voltage | loL $\leq 10 \mathrm{~mA}$ | - | - | 0.4 | v |
| $\begin{aligned} & \hline \mathbf{S} \\ & \mathbf{Y} \\ & \mathbf{S} \\ & \mathbf{T} \\ & \mathbf{~ M} \end{aligned}$ | 10 | $t_{\text {poi }}$ | Inverting Input to Output Propagation Delay |  | - | - | 235 | ns |
|  | 11 | $t_{\text {PDN }}$ | Non-Inverting Input to Output Propagation Delay |  | - | - | 125 | ns |
| $\begin{aligned} & \hline \mathbf{s} \\ & \mathbf{U} \\ & \mathbf{p} \\ & \mathbf{p} \\ & \mathbf{L} \\ & \mathbf{y} \end{aligned}$ | 12 | Icc | Supply Current | Type A Device $V_{c c}=16 \mathrm{~V}$ | - | - | 13 | mA |
|  | 13 | Icc | Supply Current | $\begin{gathered} \text { Type B Device } \\ V_{c c}=13 \mathrm{~V} \end{gathered}$ | - | - | 10 | mA |

## Switching Time Definitions



## Operating Characteristics




## Application Information

## TSC450 Drives Power MOS FET



TSC450 Driving VMOS FET in Inverting Mode (Pin 4)


TSC450 Driving VMOS FET in Non-Inverting Mode (Pin 2)


## Package Outlines



## General Description

The TSC7660 DC to DC converter will generate a negative voltage from a positive source. With two external capacitors the TSC7660 will convert a 1.5 V to 10.0 V input signal to -1.5 V to -10.0 V level. The TSC7660 easily generates -5 V in +5 V digital systems.
Many analog to digital converters, digital to analog converters, operational amplifiers, and multiplexers require negative supply voltages. The TSC7660 allows +5 V digital logic systems to incorporate these analog components without adding an additional main power source. The TSC7660 can lower total system cost, ease engineering development and save space, power and weight.

The TSC7660 charges a capacitor to the applied supply voltage. Internal analog gates connect the capacitor across the output. Charge is transferred to an output storage capacitor completing the voltage conversion. Operation requires only two external capacitors for supply voltage $<6.5 \mathrm{~V}$.
Contained on-chip are a series DC power supply regulator, RC oscillator, voltage level translator, four output power MOS switches, and a unique logic eiement which senses the most negative voltage in the device and ensures that the output N-channel switches are not forward biased. This assures latch-up free operation.
The oscillator, when unloaded, oscillates at a nominal frequency of 10 kHz for an input supply voltage of 5.0 volts. This frequency can be lowered by the addition of an external capacitor to the "OSC" terminal, or the oscillator may be overdriven by an external clock.
The "LV" terminal may be tied to GROUND to bypass the internal series regulator and improve low voltage (LV) operation. At medium to high voltages ( +3.5 to +10.0 volts), the LV pin is left floating to prevent device latchup.

## Features

- Converts +5 V Logic Supply to $\pm 5 \mathrm{~V}$ System
- Wide Input Voltage Range 1.5 V to 10.0 V
- Efficient Voltage Conversion ...................... 99.9\%
- Excellent Power Efficiency 98\%
- Low Supply Current ........................ 500 $\mu \mathrm{A}$ Max.
- Cascade for Output Voltage Multiplication
- Low Cost and Easy to Use
- Only 2 External Capacitors Required
- RS232 Negative Power Supply
- Available in Small Outline SO Package

Ordering Information

| Part No. | Package | Temperature Range |
| :--- | ---: | ---: |
| TSC7660CPA | 8-Pin Plastic DIP | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ |
| TSC7660IJA | 8-Pin CerDIP | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
| TSC7660MJA | 8 -Pin CerDIP | $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |
| TSC7660COA | 8-Pin SO | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ |
| TSC7660/Y | Chip | $25^{\circ} \mathrm{C}$ |


| Devices with MIL-STD-883 Processing |  |  |
| :--- | :--- | :--- |
| TSC7660MJA/883 | 8-Pin CerDIP | $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |

The TSC7660 open circuit output voltage is equal to the input voltage to within $0.1 \%$. The TSC7660 has a $98 \%$ power conversion efficiency for a 2-5 mA load currents.
Pin Configuration

## Block Diagram



## Absolute Maximum Ratings



| TSC7660M | $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |
| :---: | :---: |
| TSC7660C | $0^{\circ} \mathrm{C}$ to $70^{\circ} \mathrm{C}$ |
| Storage Temperature Range (Soldering, 10 sec .) | $\begin{aligned} & -65^{\circ} \mathrm{C} \text { to } 150^{\circ} \mathrm{C} \\ & \ldots \ldots . .300^{\circ} \mathrm{C} \end{aligned}$ |

Stresses above those listed under Absolute Maximum Ratings may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions above those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

Operating Characteristics $\mathrm{V}^{+}=5 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{Cosc}=0$, Test Circuit Figure 1 (unless otherwise specified)

| NO. | SYMBOL PARAMETER | CONDITIONS | MIN | LIMITS <br> TYP | MAX | UNIT |
| :---: | :--- | :--- | :--- | :--- | :--- | :--- |

## Notes:

1. Connecting any input terminal to voltages greater than C+ or less than GROUND may cause destructive latchup. It is recommended that no inputs from sources operating from external supplies be applied prior to "power up" of the TSC7660.
2. Derate linearly above $50^{\circ} \mathrm{C}$ by $5.5 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$.
3. TSC7660M only.

Typical Performance Characteristics (Circuit of Figure 1)


Power Conversion Efficiency as a Function of Osc. Frequency


Output Voltage vs Current


Output Source Resistance as a Function of Supply Voltage


Frequency of Oscillation as a Function of External Osc. Capacitance


Output Voltage vs Current - Diode In Circult -


Output Source Resistance as a Function of Temperature


Unloaded Oscillator Frequency as a Function of Temperature
 of Output Current


## Typical Performance Characteristics (Circuit of Figure 1)

Output Voltage as a Function of Output Current


## Test Clrcuit


#### Abstract

Supply Current \& Power Conversion Efficiency as a Function of Load Current




Note 4.
Note that the curves on the right include in the supply current that current fed directly into the load ( $\mathrm{RL}_{\mathrm{L}}$ ) from $\mathrm{V}^{+}$(see Figure 1). Thus, approximately half the supply current goes directly to

## Supply Current Power Conversion Efficiency as a Function of Load Current


the positive side of the load, and the other half, through the TSC7660, to the negative side of the load. Ideally, $\mathrm{VOUt}^{2}=2 \mathrm{~V}$ IN, Is $\simeq 2 \mathrm{IL}$, so $\mathrm{VIN}_{\mathrm{IN}} \cdot$ Is $\simeq$ Vout • IL.


Figure 1: TSC7660 Test Circuit

## Circuit Description

The TSC7660 contains all the necessary circuitry to complete a voltage doubler, with the exception of two external capacitors which may be inexpensive $10 \mu \mathrm{~F}$ polarized electrolytic capacitors. Operation is best understood by considering Figure 3, which shows an idealized voltage doubler. Capacitor $\mathrm{C}_{1}$ is charged to a voltage, $\mathrm{V}^{+}$, for the half cycle when switches $S_{1}$ and $S_{3}$ are closed. (Note: Switches $S_{2}$ and $S_{4}$ are open during this half cycle.) During the second half cycle of operation, switches $S_{2}$ and $S_{4}$ are closed, with $S_{1}$ and $S_{3}$ open, thereby shifting capacitor $\mathrm{C}_{1}$ negatively by $\mathrm{V}^{+}$volts. Charge is then transferred from $\mathrm{C}_{1}$ to $\mathrm{C}_{2}$ such that the voltage on $\mathrm{C}_{2}$ is exactly $\mathrm{V}^{+}$, assuming ideal switches and no load on $\mathrm{C}_{2}$.

The 4 switches in Figure 3 are MOS power switches; $\mathrm{S}_{1}$ is a P-channel device and $S_{2}, S_{3}$ and $S_{4}$ are $N$-channel devices. The main difficulty with this approach is that in integrating


Figure 2: Chip Topography


Figure 3: Idealized Switched Capacitor
the switches, the substrates of $\mathrm{S}_{3}$ and $\mathrm{S}_{4}$ must always remain reverse biased with respect to their sources, but not so much as to degrade their "ON" resistances. In addition, at circuit startup, and under output short circuit conditions (VOUT $=\mathrm{V}^{+}$), the output voltage must be sensed and the substrate bias adjusted accordingly. Failure to accomplish this would result in high power losses and probable device latchup.
This problem is eliminated in the TSC7660 by a logic network which senses the output voltage (VOUT) together with the level translators and switches the substrates or $\mathrm{S}_{3}$ and $\mathrm{S}_{4}$ to the correct level to maintain necessary reverse bias.
The voltage regulator portion of the TSC7660 is an integral part of the anti-latchup circuitry. It's inherent voltage drop can, however, degrade operation at low voltages. To improve low voltage operation the "LV" pin should be connected to GND, disabling the regulator. For supply voltages greater than 3.5 volts the LV terminal must be left open to insure latchup proof operation, and prevent device damage.

## Theoretical Power Efficiency Considerations

In theory a voltage multiplier can approach 100\% efficiency if certain conditions are met:

- The drive circuitry consumes minimal power
- The output switches have extremely low ON resistance and virtually no offset.
- The impedances of the pump and reservoir capacitors are negligible at the pump frequency.
The TSC7660 approaches these conditions for negative voltage multiplication if large values of $\mathrm{C}_{1}$ and $\mathrm{C}_{2}$ are used. Energy is lost only in the transfer of charge between capacitors If a change in voltage occurs. The energy lost is defined by:

$$
E=1 / 2 C_{1}\left(V_{1}^{2}-V_{2}^{2}\right)
$$

$\mathrm{V}_{1}$ and $\mathrm{V}_{2}$ are the voltages on $\mathrm{C}_{1}$ during the pump and transfer cycles. If the impedances of $\mathrm{C}_{1}$ and $\mathrm{C}_{2}$ are relatively high at the pump frequency (refer to Figure 3) compared to the value of $R_{L}$, there will be a substantial difference in the voltages $V_{1}$ and $\mathrm{V}_{2}$. Therefore, it is not only desirable to make $\mathrm{C}_{2}$ as large as possible to eliminate output voltage ripple, but also to employ a correspondingly large value for $\mathrm{C}_{1}$ in order to achieve maximum efficiency of operation.

## Do's And Don'ts

- Do not exceed maximum supply voltages.
- Do not connect LV terminal to GROUND for supply voltages greater than 3.5 volts.
- Do not short circuit the output to $\mathrm{V}^{+}$supply for supply voltages above 5.5 volts for extended periods, however, transient conditions including startup are okay.
- When using polarized capacitors, the + terminal of $\mathrm{C}_{1}$ must be connected to pin 2 of the TSC7660 and the + terminal of $\mathrm{C}_{2}$ must be connected to GROUND.
- Add diode Dx as shown in Figure 1 for high-voltage, elevated temperature applications. A1N914 diode is suitable.


## Considerations for High Voltage and Elevated Temperature

The TSC7660 will operate efficiently over its specified temperature range with only two external passive components (storage and pump capacitors), provided the operating supply voltage does not exceed 6.5 volts at $+70^{\circ} \mathrm{C}$ and 5.0 volts at $+125^{\circ} \mathrm{C}$. Exceeding these maximums at the temperatures indicated may result in desctructive latch-up of the TSC7660 (Ref: Graph "Operating Voltage Vs. Temperature")
Operation at supply voltages of up to 10.0 volts over the full temperature range without danger of latch-up can be achieved by adding a general purpose diode in series with the TSC7660 output, as shown by "Dx" in the circuit diagrams. The effect of this diode on overall circuit performance is the reduction of output voltage by one diode drop (approximately 0.6 volts).

## Typical Applications Simple Negative Voltage Converter

Figure 4 shows typical connections to provide a negative supply where a positive supply is available. A similar scheme may be employed for supply voltages anywhere in the operating range of +1.5 V to +10.0 V , keeping in mind that pin 6 (LV) is tied to the supply negative (GND) only for supply voltages below 3.5 volts, and that diode Dx must be included for proper operation at higher voltage and/or elevated temperatures.
The output characteristics of the circuit in Figure 4 are those of a nearly ideal voltage source in series with 70 ohms. Thus for a load current of -10 mA and a supply voltage of +5 volts, the output voltage would be -4.3 volts. The dynamic output impedance due to the capacitor impedances is approximately $1 / \omega \mathrm{C}$ where:

$$
C=C_{1}=C_{2}
$$

$$
\text { giving } \frac{1}{\omega C}=\frac{1}{2 \pi \text { fosc } \times 10-5}=3 \text { ohms }
$$

for $\mathrm{C}=10 \mu \mathrm{~F}$ and fosc $=5 \mathrm{kHZ}$ (1/2 of oscillator frequency)


Figure 4: Simple Negative Converter

## Paralleling Devices

Any number of TSC7660 voltage convertors may be paralleled to reduce output resistance. The reservoir capacitor, $\mathrm{C}_{2}$, serves all devices while each device requires its own pump
capacitor, $\mathrm{C}_{1}$. The resultant output resistance would be approximately

$$
\text { Rout }=\frac{\text { Rout (of TSC7660) }}{\mathrm{n} \text { (number of devices) }}
$$



Figure 5: Paralleling Devices Lowers Output Impedance

## Cascading Devices

The TSC7660 may be cascaded as shown to produce larger negative multiplication of the initial supply voltage, however, due to the finite efficiency of each device, the practical limit is 10 devices for light loads. The output voltage is defined by:

$$
\text { VOUT }=-n\left(V_{\text {IN }}\right), \cdot
$$

where n is an integer representing the number of devices cascaded. The resulting output resistance would be approximately the weighted sum of the individual TSC7660 ROUT values.


Figure 6: Increased Output Voltage By Cascading Devices

## Changing the TSC7660 Oscillator Frequency

It may be desirable in some applications, due to noise or other considerations, to increase the oscillator frequency. This is achieved by overdriving the oscillator from an external clock, as shown in Figure 7. In order to prevent possible device latchup, a $1 \mathrm{k} \Omega$ resistor must be used in series with the clock output. In the situation where the designer has generated the external clock frequency using TTL logic, the addition of a $10 \mathrm{k} \Omega$ pullup resistor to $\mathrm{V}^{+}$supply is required. Note that the pump frequency with external clocking, as with internal clocking, will be $1 / 2$ of the clock frequency. Output transitions occur on the positive-going edge of the clock.


Figure 7: External Clocking

It is also possible to increase the conversion efficiency of the TSC7660 at low load levels by lowering the oscillator frequency. This reduces the switching losses, and is achieved by connecting an additional capacitor, Cosc, as shown in Figure 8. Lowering the oscillator frequency will cause an undesirable increase in the impedance of the pump $\left(C_{1}\right)$ and the reservoir $\left(\mathrm{C}_{2}\right)$ capacitors. To overcome this increase the values of $C_{1}$ and $C_{2}$ by the same factor that the frequency has been reduced. For example, the addition of a 100 pf capacitor between pin 7 (Osc) and $\mathrm{V}^{+}$will lower the oscillator frequency to 1 kHz from its nominal frequency of 10 kHz (a multiple of 10), and necessitate a corresponding increase in the value of $\mathrm{C}_{1}$ and $\mathrm{C}_{2}$ (from $10 \mu \mathrm{~F}$ to $100 \mu \mathrm{~F}$ ).


Figure 8: Lowering Oscillator Frequency

## Positive Voltage Multiplication

The TSC7660 may be employed to achieve positive voltage multiplication using the circuit shown in Figure 9. In this application, the pump inverter switches of the TSC7660 are used to charge $\mathrm{C}_{1}$ to a voltage level of $\mathrm{V}^{+}-\mathrm{V}_{\mathrm{F}}$ (where $\mathrm{V}^{+}$is the supply voltage and $V_{F}$ is the forward voltage drop of diode $D_{1}$ ). On the transfer cycle, the voltage on $\mathrm{C}_{1}$ plus the supply voltage $\left(\mathrm{V}^{+}\right)$is applied through drode $\mathrm{D}_{2}$ to capacitor $\mathrm{C}_{2}$. The voltage thus created on $\mathrm{C}_{2}$ becomes $\left(2 \mathrm{~V}^{+}\right)-\left(2 \mathrm{~V}_{\mathrm{F}}\right)$ or twice the supply voltage minus the combined forward voltage drops of diodes $\mathrm{D}_{1}$ and $\mathrm{D}_{2}$.
The source impedance of the output (VOUT) will depend on the output current, but for $\mathrm{V}^{+}=5$ volts and an output current of 10 mA it will be approximately 60 ohms.


Figure 9: Positive Voltage Multiplier

## Combined Negative Voltage Conversion and Positive Supply Multiplication

Figure 10 combines the functions shown in Figures 4 and 9 to provide negative voltage conversion and positive voltage multiplication simultaneously. This approach would be, for example, suitable for generating +9 volts and -5 volts from an existing +5 volt supply. In this instance capacitors $C_{1}$ and $C_{3}$ perform the pump and reservoir functions respectively for the generation of the negative voltage, while capacitors $\mathrm{C}_{2}$ and $\mathrm{C}_{4}$ are pump and reservoir respectively for the multiplied positive voltage. There is a penalty in this configuration which combines both functions, however, in that the source impedances of the generated supplies will be somewhat higher due to the finite impedance of the common charge pump driver at pin 2 of the device.


Figure 10: Combined Negative Converter and Positive Multiplier

## Efficient Positive Voltage Multiplication/Conversion

Since the switches that allow the charge pumping operation are bidirectional, the charge transer can be performed backwards as easily as forwards. Figure 11 shows a TSC7660 transforming -5 V to +5 V (or +5 V to +10 V , etc.). The only problem here is that the internal clock and switch-drive section will not operate until some positive voltage has been generated. An initial inefficient pump, as shown in Figure 10, could be used to start this circuit up, after which it will bypass the other (D1 and D2 in Figure 10 would never turn on) or else the diode and resistor shown dotted in Figure 11 can be used to "force" the internal regulator on.


Figure 11: Positive Voltage Conversion

## Voltage Splitting

The same bidirectional characteristics used in Figure 11 can also be used to split a higher supply in half, as shown in Figure 12. The combined load will be evenly shared between the two sides. Once again, a high value resistor to the LV pin ensures start-up. Because the switches share the load in parallel, the output impedance is much lower than in the standard circuits, and higher currents can be drawn from the device. By using this circuit, and then the circuit of Figure 6, +15 V can be converted (via +7.5 , and -7.5 V ) to a nominal -15 V , though with rather high series resistance ( $\sim 250 \Omega$ ).


Figure 12: Splitting a Supply in Half.

## Negative Voltage Generation for Display ADCs

The TSC7106 is designed to work from a 9 V battery. With fixed power supply system the TSC7106 will perform conversions with input signals referenced to power supply ground.


Figure 13a: Fixed Power Supply Operation of TSC7106 ADC.


Figure 13b: Negative Power Supply Generation for TSC7107A ADC

## Negative Supply Generation for 4 1/2 Digit Data Acquisition System

The TSC7136 is a $41 / 2$ Digit ADC operating from $\pm 5 \mathrm{~V}$ supplies. The TSC7660 inexpensively provides a $\mathbf{- 5} \mathrm{V}$ source.
see AN16 and AN17 for TSC7135 interface details and software routines.


Figure 14: TSC7660 Supplies -5 V for Converters in Microprocessor Controlled Data Acquisition Systems.

Negative Supply Generation for TSC94XX Frequency to Voltage Converters.


Figure 15: TSC7660 Supplies Negative Supply for TSC9400/9401/9402 Frequency to Voltage Converters.

## Package Outline



## General Description

The Teledyne Semiconductor TSC9403 and TSC9404 are serial input, 16 -bit parallel output shift registers. High output power MOS switching transistors make the TSC9403 and TSC9404 ideal interface circuits between microprocessor I/O ports and high current/voltage peripherals. The CMOS construction limits quiescent power dissipation to 20 mW .
The TSC9403 common source, open drain MOS outputs sustain 20 V in the OFF state and maintain leakage currents under $100 \mu \mathrm{~A}$. The TSC9404 outputs are rated at 15 V . The 16 parallel outputs will continuously sink 60 mA . (VSAT $\leq 0.5 \mathrm{~V}$ ).
Successive connection of serial data outputs to serial data inputs make longer length serial to parallel conversions possible. Device cascading makes the TSC9403 and TSC9404 ideal thermal printhead or high resolution LED bar graph drivers.

## Ordering Information

| Part | Package | Temperature <br> Range | Output <br> Voltage |
| :--- | :--- | :--- | :--- |
| TSC9403CJ | 24-Pin <br> Epoxy Dip | $0^{\circ} \mathrm{C}$ to $70^{\circ} \mathrm{C}$ | 20 V |
| TSC9403IL | 24-Pin <br> CerDIP | $-25^{\circ} \mathrm{C}$ to $85^{\circ} \mathrm{C}$ | 20 V |
| TSC9404CJ | 24-Pin <br> Epoxy Dip | $0^{\circ} \mathrm{C}$ to $70^{\circ} \mathrm{C}$ | 15 V |
| TSC9404IL | $24-$ Pin <br> CerDIP | $-25^{\circ} \mathrm{C}$ to $85^{\circ} \mathrm{C}$ | 15 V |
| TSC9404ML | $24-P i n$ <br> CerDIP | $-55^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ | 15 V |

## Features

- High Voltage Outputs: 20 V (TSC9403), 15 V (TSC9404)
- High Output Current Sink Capability: 60 mA
- Low Standby Power: 20 mW
- High Speed Operation: 3.0 MHz
- 16 Parallel Outputs
- Cascading Possible for Longer Data Words


## Applications

- Incandescent Lamp Driver
- Thermal Printhead Driver
- LED Bar Graph Driver
- High Current, Microprocessor Serial Port Expander
- Relay/Solenoid Driver
- Tungsten Lamp Driver
- SCR Gate Driver


## Pin Configuration



Simplified Schematic


# Serial Input/16-Bit Parallel Output Peripheral Driver <br> - High Voltage, High Current Outputs 

## Absolute Maximum Ratings



| CerDIP Package ................... $0.4 \mathrm{~W} @+125^{\circ} \mathrm{C}$ |  |
| :---: | :---: |
| Epoxy Package | $1 \mathrm{~W} @ 70^{\circ} \mathrm{C}$ |
| Operating Temperature |  |
| CerDIP Package (IL) | $-25^{\circ} \mathrm{C} \leq \mathrm{T}_{A} \leq+85^{\circ} \mathrm{C}$ |
| CerDIP Pacakge (ML) | $-55^{\circ} \mathrm{C} \leq \mathrm{T}_{A} \leq+125^{\circ} \mathrm{C}$ |
| Epoxy Package (CJ) | $0^{\circ} \mathrm{C} \leq \mathrm{T}_{A} \leq+70^{\circ} \mathrm{C}$ |
| Storage Temperature | $-65^{\circ} \mathrm{C} \leq \mathrm{T}_{A} \leq+150^{\circ} \mathrm{C}$ |
| Lead Temperature (Sol | $+300^{\circ} \mathrm{C}$ |

Electrical Characteristics ( $\mathrm{V}_{\mathrm{S}}=5.0 \mathrm{~V}, 0^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+70^{\circ} \mathrm{C}$ for TSC9403CJ, TSC9404CJ and $-25^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}}+85^{\circ} \mathrm{C}$ for TSC9403IL, TSC9404IL, and $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ for TSC9404ML unless otherwise stated).

| PARAMETER | SYMBOL | CONDITIONS | TSC9403/TSC9404 |  |  | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | MIN | TYP | MAX |  |
| Output ON Voltage | VSAT | $\begin{aligned} & 1 \mathrm{IO}=60 \mathrm{~mA} \\ & \mathrm{~V}_{\mathrm{S}}=4.75 \mathrm{~V} \end{aligned}$ | - | 0.35 | 0.5 | V |
| Output OFF Voltage | $V_{B}$ | TSC9403 | - | - | 20 | V |
|  |  | TSC9404 | - | - | 15 | V |
| Output Sink Current | 1/O | $\begin{aligned} & \text { VSAT } \leq 0.5 \mathrm{~V} \\ & \text { (Note 1) } \end{aligned}$ | 60 | - | - | mA |
| Output Leakage Current | Iox | $\begin{aligned} & V_{S}=4.75 \mathrm{~V} \\ & V_{B}=20 \mathrm{~V} \text { (TSC9403) } \\ & V_{B}=15 \mathrm{~V} \text { (TSC9404) } \end{aligned}$ | - | - | 100 | $\mu \mathrm{A}$ |
| Logic "1" Input Voltage | VINH | $\mathrm{V}_{\mathrm{S}}=5.25 \mathrm{~V}$ | 3.3 | - | - | V |
| Logic "0" Input Voltage | VINL | V S $=5.25 \mathrm{~V}$ | - | - | 0.8 | V |
| Logic "1" Input Current | IINH | $\mathrm{V}_{\mathrm{S}}=5.25 \mathrm{~V}$ | - | - | 20 | $\mu \mathrm{A}$ |
| Logic "0" Input Current | IINL | $\begin{aligned} & \mathrm{V}_{\mathrm{INL}}=0.4 \mathrm{~V} \\ & \mathrm{~V}_{\mathrm{S}}=5.25 \mathrm{~V} \end{aligned}$ | - | - | 400 | $\mu \mathrm{A}$ |
| Input Capacitance | CIN | $\mathrm{V}_{\text {INL }}=0 \mathrm{~V}$ | - | 15 | - | pF |
| Serial Output Logic "1" Voltage | VOH | $\begin{aligned} & \mathrm{IOH}=400 \mu \mathrm{~A} \\ & \mathrm{IOH}=10 \mu \mathrm{~A} \end{aligned}$ | $\begin{aligned} & 2.4 \\ & 4.5 \end{aligned}$ | - | - | V |
| Serial Output Logic "0" Voltage | Vol | $\mathrm{lOL}=5 \mathrm{~mA}$ | - | - | 0.4 | V |
| Serial Input Data Hold Time | toh |  | 20 | 0 | - | ns |
| Serial Input Data Set-up Time | tos |  | 100 | 70 | - | ns |
| Clock Frequency | tcP |  | 3 | 5 | - | MHz |
| Clock Pulse Width | tpw |  | 150 | 100 | - | ns |
| Parallel Output Low to High Transition Time | tplH | $\begin{aligned} & \mathrm{V}_{\mathrm{B}}=20 \mathrm{~V}(\mathrm{TSC} 9403) \\ & \mathrm{V}_{\mathrm{B}}=15 \mathrm{~V}(\mathrm{TSC} 9404) \\ & \mathrm{R}_{\mathrm{L}}=330 \Omega \\ & \mathrm{C}_{\mathrm{L}}=25 \mathrm{pF} \end{aligned}$ | - | - | 150 | ns |
| Parallel Output High to Low Transition Time | tPHL | $\begin{aligned} & \mathrm{V}_{\mathrm{B}}=20 \mathrm{~V}(\mathrm{TSC} 9403) \\ & \mathrm{V}_{\mathrm{B}}=15 \mathrm{~V}(\mathrm{TSC} 9404) \\ & \mathrm{R}_{\mathrm{L}}=330 \Omega \\ & \mathrm{C}_{\mathrm{L}}=\mathrm{pF} \end{aligned}$ | - | - | 200 | ns |
| Serial Output Low to High Transition Time | tsLH | $\begin{aligned} & \mathrm{IOH}=400 \mu \mathrm{~A} \\ & \mathrm{CL}=25 \mathrm{pF} \end{aligned}$ | - | - | 150 | ns |

## Electrical Characteristics (Cont.)

| PARAMETER | SYMBOL | CONDITIONS | TSC9403/TSC9404 |  |  | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | MIN | TYP | MAX |  |
| Serial Output High to Low Transition Time | tSHL | $\begin{aligned} & \mathrm{IOL}=5 \mathrm{~mA} \\ & \mathrm{CL}=25 \mathrm{pF} \end{aligned}$ | - | - | 75 | ns |
| Operating Supply Voltage | Vs |  | 4.75 | 5.0 | 5.25 | V |
| Quiescent Power Supply | Is | $\begin{aligned} & \mathrm{V}_{\mathrm{S}}=5.25 \mathrm{~V} \\ & \mathrm{fC}=0 \mathrm{~Hz} \\ & \mathrm{~V}_{\mathrm{IHL}}=0 \mathrm{~V} \\ & 10=0 \mathrm{~mA} \\ & \text { Pin } 22 \mathrm{Open} \\ & \hline \end{aligned}$ | - | 1.0 | 4.0 | mA |

Note 1: Maintain Chip Temperature $\leq 150^{\circ} \mathrm{C}$.
Timing Diagrams


Function Table

| DATA <br> INPUT <br> $D_{N}$ | CLOCK <br> INPUT | PARALLEL OUTPUTS |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\mathbf{Q}_{2}$ | $\mathbf{Q}_{3}$ | $\ldots \mathbf{Q}_{16}$ |  |
| X | L | $\overline{\mathrm{D}_{1}}$ | $\overline{\mathrm{D}_{2}}$ | $\overline{\mathrm{D}_{3}}$ | $\ldots \overline{\bar{D}_{16}}$ |
| H | $\sim \sim$ | $\mathrm{L}^{*}$ | $\overline{\mathrm{D}_{1}}$ | $\overline{\mathrm{D}_{2}}$ | $\ldots \overline{\mathrm{D}_{15}}$ |
| L | $\sim \sim$ | $\mathrm{H}^{*}$ | $\overline{\mathrm{D}_{1}}$ | $\overline{\mathrm{D}_{2}}$ | $\overline{\mathrm{D}_{15}}$ |

[^7]
## Applications

## Microprocessor Controlled LED Bar

Graph Display


Thermal Printhead Driver


## Package Outline


Section 12References12-3
TSC9491 1.22 V Bandgap Voltage Reference ..... 12-5
TSC9495 +5 V Bandgap Voltage Reference/Temperature Transducer ..... 12-7
TSC9496 +10 V Bandgap Voltage Reference ..... 12-11

## Features

- Guaranteed temperature coefficient: 50 or $100 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$
- Low bias current: $50 \mu \mathrm{~A}$
- Low breakdown voltage: 1.22 V
- Low dynamic impedance $2 \Omega$ max.
- TO-18 or TO-92 package
- Low Cost


## Applications

- Reference for $A / D$ and $D / A$ converters
- Threshold detectors
- Voltage Regulators
- VOM and VTVM's
- Amplifier biasing
- Battery operated equipment


## General Description

The TSC9491 is a 1.22 V temperature compensated voltage reference. It uses the band-gap principal to achieve extremely tight regulation over a wide range of operating currents. The use of thin film resistors assures long term stability and low noise.

## Connection Diagram

Bottom Views


TO-18


TO-92

## Ordering Information

|  | Temperature Range |  |
| :--- | :---: | :---: |
| Temp. Coeff. | $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ <br> (TO-18) | $0^{\circ} \mathrm{C}$ to $70^{\circ} \mathrm{C}$ <br> (TO-92) |
| $50 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | TSC9491AM | TSC9491AJ |
| $100 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | TSC 9491 BM | TSC9491BJ |

## Packaging Information



All dimensions in inches (millimeters)

## Absolute Maximum Ratings

|  | TO-18 | TO-92 |
| :--- | :---: | :---: |
| Storage Temperature | $-65^{\circ} \mathrm{C}$ to $+200^{\circ} \mathrm{C}$ | $-55^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
| Operating Temperature | $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ |
| Forward Current, Max. | 5 mA | 5 mA |
| Reverse Current, Max. | 1 mA | 1 mA |
| Power Dissipation | Limited by max forward $/$ reverse current |  |
| Lead Temperature <br> (Soldering, 10 seconds) | $300^{\circ} \mathrm{C}$ | $260^{\circ} \mathrm{C}$ |

Electrical Characteristics $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ unless otherwise noted)

| Parameters |  | Min | Typ | Max | Units | Conditions |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Reverse Breakdown <br> Voltage | $\mathrm{B}_{\mathrm{VR}}$ | 1.20 | 1.22 | 1.25 | V | $\mathrm{I}_{\mathrm{R}}=500 \mu \mathrm{~A}$ |
| Reverse Breakdown <br> Voltage Change | $\Delta \mathrm{B}_{\mathrm{VA}}$ | - | 15 | 20 | mV | $50 \mu \mathrm{~A}<\mathrm{I}_{\mathrm{R}}<500 \mu \mathrm{~A}$ |
| Temp. Coefficient <br> TSC9491B <br> TSC9491A | $\frac{\Delta \mathrm{B}_{\mathrm{VR}}}{\Delta \mathrm{T}}$ |  |  | .003 | 0.01 | $\% /{ }^{\circ} \mathrm{C}$ |
| TSC | $\mathrm{I}_{\mathrm{R}}=500 \mu \mathrm{~A}$ |  |  |  |  |  |
| Reverse Current | $\mathrm{I}_{\mathrm{R}}$ | 0.05 | - |  | mA |  |

## Applications/Design Circuits

## Adjustable Voltage Reference



$$
\begin{aligned}
& V_{0}=V_{\text {REF }}\left(\frac{R_{2}+R_{3}}{R_{2}}\right) \\
& I_{\text {REF }}=\frac{V_{0}-V_{\text {REF }}}{R_{1}} \\
& R_{4}=\frac{R_{2} \cdot R_{3}}{R_{2}+R_{3}}
\end{aligned}
$$

## General Description

The TSC9495, Precision Voltage Reference, uses the band gap principle to generate an extremely stable 5 volt reference. Included in the TSC9495 are a band gap reference, an output amplifier and a voltage which varies linearily with temperature. The reference is ideal because of its low cost, low output noise and low power requirement. The TSC9495 is exceptionally stable over wide variations in temperature, line voltage and load current. The reference operates on a single supply with voltages of 7 volts to 40 volts.

The TSC9495 is available with an initial accuracy of $\pm 1 \%$. An external potentiometer can be used to vary the output voltage $\pm 6 \%$ with little effect on the temperature coefficient. The potentiometer can also be used to adjust the voltage for binary applications such as 5.12 volts.
Pin 3 of the TSC9495 has available a voltage which varies linearily with temperature. The typical change is $2.1 \mathrm{mv} /{ }^{\circ} \mathrm{C}$. By using a buffer amplifier, the output voltage can be scaled to the desired resolution and range.

## Ordering Information

|  |  | Max. |  | Initial | Temp. |
| :--- | :--- | :--- | :--- | :--- | ---: | | Max. Temp |
| :--- |
| Part No. |$\quad$ Package Voltage | Accuracy | Range |
| :--- | :--- |

## Schematic Diagram



## Features

- Excellent Temperature Stability: $20 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$
- Tight Output Tolerance: $1 \%$
- Adjustable Output
- Input Voltage Range: 7 V to 40 V
- Low Noise: $15 \mu \mathrm{Vpp}$ max.
- 10 mA Output Current
- Short Circuit Proof
- Low Power: 1.4 mA
- Temperature Output
- Replaces REF-02


## Applications

- A/D Reference
- D/A Reference
- Current Source
- Transducer Reference
- Calibration Standard
- Thermometer


## Pin Configuration



> 8 Pin Plastic Mini Dip

## Output Adjustment

The output voltage of the TSC9495 can easily be adjusted by connecting a potentiometer to pin 5 as shown in the adjacent figure. Changing the output voltage does affect the overall temperature coefficient, however, this effect is small being typically only $0.7 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ per 100 mV of adjustment.


## Absolute Maximum Ratings

| Input Voltage | 30 V | Operating Temperature . . . . . . . . . . . . $0^{\circ} \mathrm{C}$ to $70^{\circ} \mathrm{C}$ |
| :---: | :---: | :---: |
| Power Dissipation | 500 mW | Storage Temperature . . . . . . . . . . . . $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
| Derating: Mini Dip, | $5.6 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ | Lead Temperature (Soldering, 60 sec.$)$. . . . . . . . $300^{\circ} \mathrm{C}$ |

Electrical Characteristics: These specifications apply for $\mathrm{V}_{\mathrm{IN}}=+15 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, unless otherwise noted.

| PARAMETER | SYMBOL | TEST CONDITION | MIN | TSC949 | X | TS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Output Voltage | $\mathrm{V}_{0}$ | $\mathrm{IL}_{\mathrm{L}}=0 \mathrm{~mA}$ | 4.950 | 5.000 | 5.050 | V |
| Output Adjustment Range | $\Delta V_{\text {trim }}$ | $\mathrm{R}_{\mathrm{p}}=10 \mathrm{k} \Omega$ | $\pm 2.7$ | $\pm 6.0$ | - | \% |
| Output Voltage Noise | $e_{\text {np-p }}$ | 0.1 Hz to 10 Hz | - | 12 | 18 | $\mu \mathrm{Vp-p}$ |
| Input Voltage Range | $\mathrm{V}_{\mathrm{IN}}$ |  | 7 | - | 30 | V |
| Line Regulation (Note 1) |  | $\mathrm{V}_{\text {IN }}=8$ to 30 V | - | 0.009 | 0.015 | 5/V |
| Load Regulation (Note 1) |  | $\mathrm{I}_{\mathrm{L}}=0$ to 8 mA | - | 0.006 | 0.015 | \%/mA |
| Load Regulation (Note 1) |  | $\mathrm{I}_{\mathrm{L}}=0$ to 4 mA | - | - | - | \%/mA |
| Turn-on-Settling Time | $\mathrm{t}_{\text {on }}$ | To $\pm 0.1 \%$ of final value | - | 5.0 | - | $\mu \mathrm{sec}$ |
| Quiescent Supply Current | $\mathrm{I}_{\text {SY }}$ | No Load | - | 1.0 | 1.6 | mA |
| Load Current | $I_{L}$ |  | 8 | 21 | - | mA |
| Sink Current | $\mathrm{I}_{5}$ |  | -0.2 | -0.5 | - | mA |
| Short Circuit Current | $I_{\text {SC }}$ | $V_{0}=0$ | - | 30 | - | mA |
| Temp Voltage Output | $\mathrm{V}_{\mathrm{T}}$ | (Note 2) | - | 630 | - | mV |

The following specifications apply for $\mathrm{V}_{\mathrm{IN}}==15 \mathrm{~V}, 0^{\circ} \mathrm{C} \leqslant \mathrm{T}_{\mathrm{A}} \leqslant=70^{\circ} \mathrm{C}$ and $\mathrm{I}_{\mathrm{L}}=0 \mathrm{~mA}$, unless otherwise noted.

| Output Voltage Change <br> with Temperature | $\Delta \mathrm{V}_{\mathrm{OT}}$ | (Note 3) |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Output Voltage <br> Temperature Coefficient | $\mathrm{TCV}_{\mathrm{O}}$ | (Note 4) | - | 0.14 | 0.45 | $\%$ |
| Change in $\mathrm{V}_{\mathrm{O}}$ Temperature <br> Coefficient with Output <br> Adjustment |  | $\mathrm{R}_{\mathrm{p}}=10 \mathrm{k} \Omega$ | - | 20 | 65 | $\mathrm{ppm} /{ }^{\circ} \mathrm{C}$ |
| Line Regulation (Note 1) |  | $\mathrm{V}_{\mathrm{IN}}=8$ to 30 V |  |  |  |  |
| Load Regulation (Note 1) |  | $\mathrm{I}_{\mathrm{L}}=0$ to 5 mA | - | 0.7 | - | $\mathrm{ppm} / \%$ |
| Temp Voltage Output |  | (Note 2) | - | 0.011 | 0.018 | $\% / \mathrm{V}$ |
| Temperature Coefficient | $\mathrm{TCV}_{\mathrm{T}}$ |  | - | 0.008 | 0.018 | $\% / \mathrm{mA}$ |

## Notes:

1. Line and Load Regulation specifications include the effects of self heating
2. Limit current in or out of pin 3 to 50 nA and capacitance on pin 3 to 30 pF
3. $\Delta \mathrm{V}_{\mathrm{OT}}$ is defined as the absolute difference between the maximum output voltage and the minimum output voltage over the specified temperature range expressed as a percentage of 5 v :

$$
\Delta V_{O T}=\frac{V_{M A X}-V_{M I N}}{5 V} \times 100
$$

4. $T C V_{O}$ is defined as $\Delta V_{O T}$ divided by the temperature range, i.e.

$$
\mathrm{TCV}_{\mathrm{O}}=\frac{\Delta \mathrm{V}_{\mathrm{OT}}}{70^{\circ} \mathrm{C}}
$$

## Package Information



## General Description

The TSC9496, Precision Voltage Reference, uses the band gap principle to generate an extremely stable 10 volt reference. Included in the TSC9496 are a band gap reference, and an output amplifier, which delivers 10 mA of output current. The reference is ideal because of its low cost, low output noise and low power requirement. The TSC9496 is exceptionally stable over wide variations in temperature, line voltage and load current. The reference operates on a single supply with voltages of 12 volts to 40 volts.
The 9496 is available with an initial accuracy of $\pm 1 \%$. An external potentiometer can be used to vary the output voltage $\pm 3 \%$ with little effect on the temperature coefficient. The potentiometer can also be used to adjust the voltage for binary applications such as 10.24 volts.

## Ordering Information

| Part No. | Package | Max. <br> Voltage | Initial Accuracy | Temp. Range | Max. Temp Coefficient |
| :---: | :---: | :---: | :---: | :---: | :---: |
| TSC9496CJ | 8-Pin Mini-Dip | 30 V | 1.0\% | $0-70^{\circ} \mathrm{C}$ | 65 ppm |

## Schematic Diagram



## Features

- Excellent Temperature Stability: $20 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$
- Tight Output Tolerance: 1\%
- Adjustable Output
- Input Voltage Range: 12 V to 40 V
- Low Noise: $30 \mu \mathrm{Vp}-\mathrm{p}$ max.
- 10mA Output Current
- Short Circuit Proof
- Low Power: 1.4 mA
- Replaces REF-01


## Applications

- A/D Reference
- D/A Reference
- Current Source
- Transducer Reference
- Calibration Standard


## Pin Configuration



8 Pin Plastic Mini Dip

## Output Adjustment

The output voltage of the TSC9496 can easily be adjusted by connecting a potentiometer to pin 5 as shown in the figure below. Changing the output voltage does affect the overall temperature coefficient, however, this effect is small being typically only $0.7 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ per 100 mV of adjustment.


## Absolute Maximum Ratings

Input Voltage . . . . . . . . . . . . . . . . . . . . . . . . . . . . 30 V
Power Dissipation . . . . . . . . . . . . . . . . . . . . . 500 mW
Derating: Mini Dip, above $30^{\circ} \mathrm{C}$ ambient . . . . . $5.6 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$

Operating Temperature . . . . . . . . . . . . . . $0^{\circ} \mathrm{C}$ to $70^{\circ} \mathrm{C}$
Storage Temperature . . . . . . . . . . . . . $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ Lead Temperature (Soldering, 60 sec.) . . . . . . . . . $300^{\circ} \mathrm{C}$

Electrical Characteristics:These specifications apply for $\mathrm{V}_{1 \mathrm{~N}}=+15 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, unless otherwise noted.

| PARAMETER | SYMBOL | TEST CONDITION | MIN | TSC9496CJ TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Output Voltage | $V_{0}$ | $\mathrm{I}_{\mathrm{L}}=0 \mathrm{~mA}$ | 9.90 | 10.000 | 10.10 | V |
| Output Adjustment Range | $\Delta V_{\text {trim }}$ | $\mathrm{R}_{\mathrm{p}}=10 \mathrm{k} \Omega$ | $\pm 2.7$ | $\pm 3.3$ | - | \% |
| Output Voltage Noise | $e_{\text {np-p }}$ | 0.1 Hz to 10 Hz | - | 25 | 35 | $\mu \vee p-p$ |
| Input Voltage Range | $\mathrm{V}_{\text {IN }}$ |  | 12 | - | 30 | V |
| Line Regulation (Note 1) |  | $\mathrm{V}_{\text {IN }}=13$ to 30 V | - | 0.009 | 0.015 | \%/V |
| Load Regulation (Note 1) |  | $\mathrm{I}_{\mathrm{L}}=0$ to 8 mA | - | 0.006 | 0.015 | \%/mA |
| Load Regulation (Note 1) |  | $\mathrm{I}_{\mathrm{L}}=0$ to 4 mA | - | 0.006 | 0.015 | \%/mA |
| Turn-on-Settling Time | $t_{0}$ | To $\pm 0.1 \%$ of final value | - | 5.0 | - | $\mu \mathrm{sec}$ |
| Quiescent Supply Current | ISY | No Load | - | 1.0 | 1.6 | mA |
| Load Current | $\mathrm{I}_{\mathrm{L}}$ |  | 8 | 21 | - | mA |
| Sink Current | $\mathrm{I}_{5}$ |  | -0.2 | -0.5 | - | mA |
| Short Circuit Current | Isc | $\mathrm{V}_{0}=0$ | - | 30 | - | mA |

The following specifications apply for $\mathrm{V}_{\text {IN }}=+15 \mathrm{~V}, 0^{\circ} \mathrm{C} \leqslant \mathrm{T}_{\mathrm{A}} \leqslant+70^{\circ} \mathrm{C}$, unless otherwlse noted.

| Output Voltage Change <br> with Temperature | $\Delta \mathrm{V}_{\text {OT }}$ | (Note 3) | - | 0.14 | 0.45 | $\%$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Output Voltage |  |  |  |  |  |  |
| Temperature Coefficient | $\mathrm{TCV}_{0}$ | (Note 4) | - | 20 | 65 | $\mathrm{ppm} /{ }^{\circ} \mathrm{C}$ |

Change in $\mathrm{V}_{0}$ Temperature
Coefficient with Output

| Adjustment | $R_{p}=10 \mathrm{k} \Omega$ | - | 0.7 | - | $\mathrm{ppm} / \%$ |
| :--- | :--- | :--- | ---: | :--- | ---: |
| Line Regulation (Note 1) | $\mathrm{V}_{\mathrm{IN}}=13$ to 30 V | - | 0.011 | 0.018 | $\% / \mathrm{V}$ |
| Load Regulation (Note 1) | $\mathrm{I}_{\mathrm{L}}=0$ to 5 mA | - | 0.008 | 0.018 | $\% / \mathrm{mA}$ |

## Notes:

1. Line and Load Regulation specifications include the effects of self heating.
2. $T C V_{O}$ is defined as $\Delta V_{O T}$ divided by the temperature range, i.e.
$T C V_{O}=\frac{\Delta V_{O T}}{70^{\circ} \mathrm{C}}$
3. $\Delta V_{O T}$ is defined as the absolute difference between the maximum output voltage and minimum output voltage over the specified temperature range expressed as a percentage of 10 V :

$$
\Delta V_{O T}=\frac{V_{M A X}-V_{M I N}}{10 \mathrm{~V}} \times 100
$$

## Package Information



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## General Description

The TSC900 is a low power precision operational amplifier. The $200 \mu \mathrm{~A}$ maximum supply current reduces device power requirement by over fifteen times when compared to the pin compatible ICL7650 device.
Offset voltage is a low $5 \mu \mathrm{~V}$ with drift at $0.05 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$. Vos errors are removed and adjustment potentiometers made unnecessary. The chopper stabilized error correction technique keeps offset voltage errors near zero throughout the device operating temperature range.
The TSC900 performance advantages are achieved without the additional manufacturing complexity and cost incurred with laser or "zener zap" Vos trim techniques. The TSC900 is one of the lowest cost low power precision operational amplifiers available.
The TSC900 nulling scheme corrects both DC Voserrors and Vos drift errors with temperature. A nulling amplifier alternately corrects its own Vos errors and the main amplifier Vos error. Offset nulling voltages are stored on two user supplied external capacitors. The capacitors connect to the internal amplifier Vos null points. The main amplifier input signal is never switched. Switching spikes are not present at the TSC900 output. The null scheme keeps Vos errors low throughout the operating temperature range. Laser and "zener zap" trimming can correct for Vos at only one temperature.
The nulling circuit oscillator and control circuits are integrated on chip. Only two external Vos error storage capacitors are required. The TSC900 operates as a conventional operational amplifier with vastly improved input specifications. The low Vos and Vos drift errors make the TSC900 ideal for thermocouple, thermistor, and strain gauge applications. Low dc errors and high open loop gain make the TSC900 an excellent preamplifier for precision analog to digital converters like the TSC7135, TSC800 and TSC7109.
The 14 -pin dual-in-line package (DIP) has an external oscillator input to drive the nulling circuitry. Both the 8 and 14 -pin DIP have an output voltage clamp circuit to minimize overload recovery time.

## Pin Configuration



## Features

- Low Power Supply Current ..................... $140 \mu \mathrm{~A}$
- Low Input Offset Voltage ................... $5 \mu \mathrm{~V}$ Max.
- Low Input Offset Voltage Drift ........ $0.05 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ Max.
- High Impedance Differential CMOS Inputs ..... $1012 \Omega$
- High Open Loop Voltage Gain ............ 120 dB Min.
- Low Input Noise Voltage ...................... $0.3 \mu \mathrm{Vp}-\mathrm{p}$
- High Slew Rate ................................. $0.2 \mathrm{~V} / \mu \mathrm{s}$
- Compensated Internally for Stable Unity Gain Operation
- Available in 8-Pin Dip
- Pin Compatible to ICL7650/TSC7650A/TSC7650

Ordering Information

| Part No. | Package | Temp. <br> Range | Max. <br> Vos | Max. <br> Supply <br> Current |
| :--- | :--- | :---: | :---: | :---: |
| "TSC900ACPA | 8-Pin <br> Plastic Dip | COM | $5 \mu \mathrm{~V}$ | $200 \mu \mathrm{~A}$ |
| "TSC900AIJA | 8-Pin <br> CerDIP | IND | $5 \mu \mathrm{~V}$ | $200 \mu \mathrm{~A}$ |
| "TSC900ACPD | 14-Pin <br> Plastic Dip | COM | $5 \mu \mathrm{~V}$ | $200 \mu \mathrm{~A}$ |
| *TSC900AIJD | 14-Pin <br> CerDIP | IND | $5 \mu \mathrm{~V}$ | $200 \mu \mathrm{~A}$ |
| *TSC900BCPA | 8-Pin <br> Plastic Dip | COM | $15 \mu \mathrm{~V}$ | $400 \mu \mathrm{~A}$ |
| *TSC900BIJA | 8-Pin <br> CerDIP | IND | $15 \mu \mathrm{~V}$ | $400 \mu \mathrm{~A}$ |
| *TSC900BCPD | 14-Pin <br> Plastic Dip | COM | $15 \mu \mathrm{~V}$ | $400 \mu \mathrm{~A}$ |
| *TSC900BIJD | 14-Pin <br> CerDIP | IND | $15 \mu \mathrm{~V}$ | $400 \mu \mathrm{~A}$ |

*Available with 160 hour, $+125^{\circ} \mathrm{C}$ burn-in. Add $/ \mathrm{BI}$ to part number suffix.

## Functional Diagram



か TELEDYNE SEMICONDUCTOR

# Low Power Chopper-Stablized Operational Amplifier - 2 mW Power Dissipation $0.05 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ Offset Voltage Drift 

TSC900

## Absolute Maximum Ratings



| Current into Any Pin ........ While Operating (Note 4) | $\begin{aligned} & . . \quad 10 \mathrm{~mA} \\ & . \quad 100 \mu \mathrm{~A} \end{aligned}$ |
| :---: | :---: |
| Operating Temp. Range |  |
| 1 Device | $-25^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
| C Device | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ |
| Package Power Dissipation |  |
| CerDIP Package | 500 mV |
| Plastic Package | 500 mW |

Electrical Characteristics: $\mathrm{V}_{\mathrm{S}}^{+}=+5 \mathrm{~V}, \mathrm{~V}_{\mathrm{S}}^{-}=-5 \mathrm{~V}, \mathrm{C}_{A}=\mathrm{C}_{\mathrm{B}}=0.1 \mu \mathrm{f} . \mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$.

| TYPE | NO. | SYMBOL | PARAMETER | TEST CONDITIONS | TSC900A |  |  | TSC900B |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | MIN | TYP | MAX | MIN | TYP | MAX | UNIT |
| $\begin{aligned} & \mathbf{I} \\ & \mathbf{N} \end{aligned}$ | 1 | Vos | Input Offset Voltage | $\mathrm{T}_{\text {A }}=+25^{\circ} \mathrm{C}$ | - | - | 5 | - | - | 15 | $\mu \mathrm{V}$ |
|  | 2 | $\frac{\Delta V_{O S}}{\Delta T}$ | Input Offset Voltage Average Temp. Coefficient | Operating Temp <br> Range (Note 1) | - | 0.02 | 0.05 | - | 0.1 | 0.3 | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
| P | 3 | IbIAS | Average | $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ | - | - | 50 | - | - | 80 | pA |
| U |  |  | Input Bias Current | $0^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+70^{\circ} \mathrm{C}$ | - | - | 70 | - | - | 100 |  |
| T |  |  | (Note 7) | $-25^{\circ} \mathrm{C} \leq \mathrm{T}_{A} \leq+85^{\circ} \mathrm{C}$ | - | - | 100 | - | - | 140 |  |
|  | 4 | los | Input Offset Current | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ | - | 0.5 | - | - | 0.5 | - | pA |
|  | 5 | enp-p | Input Noise Voltage | $\begin{aligned} & \mathrm{Rs}=100 \Omega \\ & 0.1 \text { to } 10 \mathrm{~Hz} \end{aligned}$ | - | 4 | - | - | 4 | - | $\mu \mathrm{V}_{\mathrm{p}-\mathrm{p}}$ |
|  | 6 | Enp-p | Input Noise Voitage | $\begin{aligned} & \text { Rs }=100 \Omega \\ & 0.1 \mathrm{~Hz} \text { to } 1 \mathrm{~Hz} \end{aligned}$ | - | 0.3 | - | - | 0.3 | - | $\mu \mathrm{V}$ p-p |
|  | 7 | Rin | Input Resistance |  | - | 1012 | - | - | 1012 | - | $\Omega$ |
|  | 8 | CMVR | Common-Mode Voltage Range |  | -5.0 |  | +1.5 V | -5.0 | - | +1.5 | V |
|  | 9 | CMRR | Common-Mode Rejection Ratio | CMVR $=-5 \mathrm{~V}$ to +1.5 V | 110 | 130 | - | 100 | - | - | dB |
| $\begin{aligned} & \mathbf{O} \\ & \mathbf{U} \\ & \mathbf{T} \\ & \mathbf{P} \\ & \mathbf{U} \end{aligned}$ | 10 | Av | Large-Signal Voltage Gain | $\mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega$ | 120 | 130 | - | 100 | - | - | dB |
|  | 11 | Vout | Output Voltage Swing | $\mathrm{R} \mathrm{L}=10 \mathrm{k} \Omega$ | -4.7 | - | +3.5 | -4.7 | - | +3.5 | V |
|  |  |  | (Note 3) | $\mathrm{RL}_{\mathrm{L}}=100 \mathrm{k} \Omega$ | -4.9 | - | +3.9 | -4.9 | - | +3.9 |  |
|  | 12 |  | Clamp ON Current (Note 2) | $\mathrm{R}_{\mathrm{L}}=100 \mathrm{k} \Omega$ | 20 | 90 | 200 | 20 | 90 | 200 | $\mu \mathrm{A}$ |
|  | 13 |  | Clamp OFF Current (Note 2) | -4.0 V < VOUT $<+4.0 \mathrm{~V}$ | - | 1 | - | - | 1 | - | pA |
| $\begin{aligned} & \mathbf{D} \\ & \mathbf{Y} \\ & \mathbf{N} \\ & \mathbf{A} \\ & \mathbf{M} \\ & \mathbf{I} \\ & \mathbf{C} \end{aligned}$ | 14 | Bw | Unity Gain Bandwidth | Unity Gain ( +1 ) | - | 0.7 | - | - | 0.7 | - | MHz |
|  | 15 | $S_{R}$ | Slew Rate | $C_{L}=50 \mathrm{pF}, \mathrm{R}_{\mathrm{L}}=100 \mathrm{k}$ | - | 0.2 | - | - | 0.2 | - | $\mathrm{V} / \mu \mathrm{s}$ |
|  | 16 |  | Rise Time |  | - | 0.5 | - | - | 0.5 | - | $\mu \mathrm{s}$ |
|  | 17 |  | Overshoot |  | - | 18 | - | - | 18 | - | \% |
|  | 18 | $f$ foh | Internal Chopping Frequency | Pins 12-14 open (DIP) | - | 150 | - | - | 150 | - | Hz |
| $\begin{aligned} & \mathbf{S} \\ & \mathbf{U} \\ & \mathbf{P} \\ & \mathbf{P} \\ & \mathbf{L} \\ & \mathbf{Y} \end{aligned}$ | 19 | $\mathrm{Vs}^{+}$to $\mathrm{Vs}^{-}$ | Operating Supply Range |  | 4.5 | - | 16 | 4.5 | - | 16 | V |
|  | 20 | Is | Supply Current | No Load | - | 140 | 200 | - | - | 400 | $\mu \mathrm{A}$ |
|  | 21 | PSRR | Power Supply Rejection Ratio | $\mathrm{Vs}= \pm 3 \mathrm{~V}$ to $\pm 8 \mathrm{~V}$ | 120 | - | - | 100 | - | - | dB |

## Notes:

1. Operating temperature range is $-25^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ for "I" grade and $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ for "C" grade.
2. See OUTPUT CLAMP discussion.
3. OUTPUT CLAMP not connected.
4. Limiting input current to $100 \mu \mathrm{~A}$ is recommended to avold latch-up problems.
5. Static Sensitive Device. Unused devices must be stored in conductive material to protect devices from possible static damage.
6. Stresses above those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only and functional operation of the device at these or any other conditions above those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum ratIng conditions for extended periods may affect device rellability.
7. Average current caused by switch charge transfer at input.

## Low Power Chopper-Stablized Operational Amplifier

- 2 mW Power Dissipation
- $0.05 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ Offset Voltage Drift


## Chopper Stabilized Operational Amplifiers

The TSC900 is the first low power chopper stabilized amplifier commercially available. The TSC900 maximum supply current is 15 times lower than the pin compatible TSC7650 amplifier. As Figure 1 shows the low supply current is achieved without sacrificing offset voltage or offset voltage drift performance.

## Nulling Capacitor Connection

The offset voltage correction capacitors are connected to $\mathrm{C}_{\mathrm{A}}$ and $\mathrm{C}_{\mathrm{B}}$. The common capacitor connection is made to $\mathrm{V}_{\bar{S}}$ (Pin 4) on the 8-pin packages and to capacitor return ( $C_{R}$, Pin 8) on the 14-pin packages. The common connection should be made through either a separate pc trace or wire to avoid voltage drops.
Internally $\mathrm{V}_{\mathrm{S}}^{-}$is connected to $\mathrm{C}_{\mathrm{R}}$.


Figure 1


Figure 2: Nulling Capacitor Connection

## Clock Operation

The internal oscillator is set for a 150 Hz nominal chopping frequency on both the 8 and 14 -pin dual in line packages. With the 14-pin DIP TSC900, the 150 Hz internal chopping frequency is available at the internal clock output (Pin 12). A 300 Hz nominal signal will be present at the external clock input pin (Pin 13) with EXT/INT high or open. This is the internal clock signal before a divide by two operation.
The 14 -pin DIP device can be driven by an external clock. The INT/EXT input (Pin 14) has an internal pull-up and may be left open for internal clock operation. If an external clock is used INT/EXT must be tied to $\mathrm{V}_{\bar{s}}^{-\bar{s}}$ (Pin 7) to disable the internal clock. The external clock signal is applied to the external clock input (Pin 13).
The external clock amplitude should swing between $V_{S}^{+}$and ground for power supplies up to $\pm 6 \mathrm{~V}$ and between $\mathrm{V}_{S}^{+}$and $\mathrm{V}_{S}^{+}$ -6 V for higher supply voltages.
At low frequencies the external clock duty cycle is not critical since an internal divide by two gives the desired $50 \%$ switching duty cycle. The offset storage correction capacitors are charged only when the external clock input is high. A $50-80 \%$ external clock positive duty cycle is desired for frequencies above 500 Hz to guarantee transients settle before the internal switches open.
The external clock input can also be used as a strobe input. If a strobe signal is connected at the external clock input so that it is low during the time an overload signal is applied, neither capacitor will be charged. The leakage currents at the capacitor pins are very low.

## Output Clamp

Chopper-stabilized systems can show long recovery times from overloads. If the output is driven to either supply rail, output saturation occurs. The inputs are no longer held at a "virtual ground." The Vos null circuit treats the differential signal as an offset and tries to correct it by charging the external capacitors. The nulling circuit also saturates. Once the input signal returns to normal, the response time is lengthened by the long recovery time of the nulling amplifier and external capacitors.
Through an external clamp connection, the TSC900 eliminates the overload recovery problem by reducing the feedback network gain before the output voltage reaches either supply rail.
The output clamp circuit is shown in Figure 3 with typical inverting and non-inverting circuit connections shown in Figure 4 and 5 . Output voltage vs clamp circuit current characteristics are shown in the typical operating curves. For the clamp to be fully effective, the impedance across the clamp output should be greater than $100 \mathrm{k} \Omega$.


Figure 3: Internal Clamp Circuit


Figure 4: Non-Inverting Amplifier with Optional Clamp


Figure 5: Inverting Amplifier with Optional Clamp

## Static Protection

All device pins are static-protected. Strong static fields and discharges should be avoided, however, as they can degrade diode junction characteristics and increase input-leakage currents.
Many companies are actively involved in providing services, educational material, and supplies to aid electronic manufacturers in establishing "static safe" work areas where CMOS components are handled. A partial company listing is:

- 3M

Static Control Systems Division
223-25W EM Center
St. Paul, MN 55101
(800) 792-1072

- Semtronics
P.O. Box 592

Martinsville, NJ 08836
(210) 561-9520

## Input Bias Current

The TSC900 inputs are never disconnected from the main internal amplifier. The null amplifier samples the input offset voltage and corrects DC errors and drift by storing compensating voltages on external capacitors. The sampling causes, however, charge transfer at the inputs. The charge transfer represents a peak impulse current of 200 to 290 nA at the inputs when the internal clock makes a transition.

## Latch-Up Avoidance

Junction-isolated CMOS circuits inherently include a parasitic 4-layer (p-n-p-n) structure which has characteristics similar to an SCR. Under certain circumstances this junction may be triggered into a low impedance state, resulting in excessive supply current. To avoid the condition, no voltage greater than 0.3 V beyond the supply rails should be applied to any pin. In general, the amplifier supplies must be established either at the same time or before any input signals are applied. If this is not possible, the drive circuits must limit input current flow to under 0.1 mA to avoid latchup.

## Thermo-Electric Potentials

Precision dc measurements are ultimately limited by thermo-electric potentials developed in thermocouple junctions of dissimilar metals, alloys, silicon, etc. Unless all junctions are at the same temperature, thermoelectric voltages typically around $0.1 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$, but up to tens of $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ for some materials, will be generated. In order to realize the benefits extremely low offset voltages provide, it is essential to take special precautions to avoid temperature gradients. All components should be enclosed to eliminate air movement, especially those caused by power-dissipating elements in the system. Low thermoelectric-coefficient connections should be used where possible and power supply voltages and power dissipation should be kept to a minimum. Highimpedance loads are preferable, and separation from surrounding heat-dissipating elements is advised.

## Pin Compatibility

On the 8-pin mini-dip TSC900 the external null storage capacitors are connected to pins 1 and 8 . On most other operational amplifiers these are left open or are used for offset potentiometer or compensation capacitor connections.
For OP05 and OP07 operational amplifiers, the replacement of the offset null pot between pins 1 and 8 by two capacitors from the pins to $V \bar{s}$ will convert the OP05/07 pin configuration for TSC900 operation. For LM108 devices the compensation capacitor is replaced by the external nulling capacitors. The LM101/748/709 pin outs are modified similarly by also removing any circuit connections to pin 5 . On the TSC900 pin 5 is the output clamp connection. Other operational amplifiers may use this pin as an offset or compensation point.
The minor modifications needed to retrofit a TSC900 into existing sockets operating at reduced power supply voltages make prototyping and circuit verification straight forward.

## Component Selection

The two required capacitors, $\mathrm{C}_{\mathrm{A}} \mathrm{C}_{\mathrm{B}}$, have optimum values depending on the clock or chopping frequency. For the present internal clock, the correct value is $0.1 \mu \mathrm{~F}$. To maintain the same relationship between the chopping frequency and the nulling time constant, the capacitor values should be scaled in proportion to the external clock if used. Highquality film-type capacitors such as mylar are preferred. Ceramic or other lower-grade capacitors may be suitable in some applications. For fast settling on initial turn-on, low dielectric absorption capacitors (such as polypropylene) should be used. With ceramic capacitors, several seconds may be required to settle to microvolt levels.

## Typical Characteristic Curves



Positive Clamp Current


Output Voltage Swing vs Load Resistance


Negative Clamp Current


Slew Rate


## Typical Characteristic Curves



Supply Current vs Supply Voltage


Gain and Phase vs Frequency


Package Outline


TSC911

## General Description

The CMOS TSC911 auto-zeroed operational amplifier is the first complete monolithic chopper-stabilized amplifier. Chopper operational amplifiers like the ICL7650/7652 and LTC1052 require user supplied, external, offset compensation storage capacitors. EXTERNAL CAPACITORS ARE NOT REQUIRED WITH THE TSC911. Just as easy to use as the conventional 741 type amplifier, the TSC911 significantly reduces offset voltage errors. Pin-out matches the OP07/ 741/7650 8-pin mini-dip configuration.
Several system benefits arise by eliminating the external chopper capacitors. Lower system part count. Reduced assembly time and cost. Greater system reliability. Reduced printed circuit board layout effort and greater pc board area utilization. Space savings can be significant in multiple amplifier designs.
Electrical specifications include a $15 \mu \mathrm{~V}$ maximum offset voltage, $0.15 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ maximum offset voltage temperature coefficient. Offset voltage error is five times lower than the premium OP07E bipolar device. In offset drift the TSC911 improves performance by eight times.
Low offset voltage errors eliminate trim procedures during manufacturing, periodic re-calibrations, and reliability problems caused by damaged or misadjusted trim potentiometers.
The TSC911 automatically corrects offset voltage drift with time also. Operational amplifier long term drift is less easily controlled and more expensive to maintain when low offset errors are obtained by trimming thin film resistors. The TSC911 internal circuits correct errors repetitively at a 200 Hz rate. Long term drift is effectively eliminated.
The TSC911 operates from dual or single power supplies. Supply current is typically $350 \mu \mathrm{~A}$. Single 4.5 V to 16 V supply operation is possible. This makes single 9 V battery operation possible. The TSC7660 DC to DC converter can easily supply a negative potential in dual supply applications where only a +5 V system supply is available.
Open-loop voltage gain is 115 dB minimum with a $10 \mathrm{k} \Omega$ load. Unity gain bandwidth is 1.5 MHz . Slew rate is $2.5 \mathrm{~V} / \mu \mathrm{s}$. Com-mon-mode rejection ratio is 110 dB . Input common-mode range extends from 2 V below the positive supply to the negative supply.
The TSC911 is available in an 8-pin plastic or cerDIP package. Dice are available for hybrid applications.
For precision dual and quad monolithic chopper-stabilized amplifiers see the TSC913 dual and TSC914 quad data sheets.

## Features

- First Monolithic Chopper-Stabilized Amplifier - External Capacitors Not Required
- Chopper Amplifier Performance Without External Capacitors
$-5 \mu \mathrm{~V}$ Offset Voltage
$-0.05 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ Offset Voltage Drift
- Low Supply-Current ........................... $350 \mu \mathrm{~A}$
- High Common-Mode Rejection ................. 116 dB
- Single Supply Operation .................. 4.5 V to 16 V
- High Slew Rate .................................. $2.5 \mathrm{~V} / \mu \mathrm{s}$
- Wide Bandwidth ............................... 1.5 MHz
- High Open Loop Voltage Gain ( $\mathrm{RL}_{\mathrm{L}}=10 \mathrm{k} \Omega$ ) ... 120 dB
- Low Input Voltage Noise ( 0.1 to 1 Hz ) ...... $0.65 \mu \mathrm{~V}$ P-p
- Pin Compatible with ICL7650
- Lower System Part Count


## Ordering Information

| Part No. | Package | Temperaaure <br> Range | Max. Offset <br> Voltage |
| :--- | :--- | ---: | ---: |
| *TSC911ACPA | 8-Pin <br> Plastic DIP | $0^{\circ} \mathrm{C}$ to $70^{\circ} \mathrm{C}$ | $15 \mu \mathrm{~V}$ |
| *TSC911BCPA | 8 -Pin <br> Plastic DIP | $0^{\circ} \mathrm{C}$ to $70^{\circ} \mathrm{C}$ | $30 \mu \mathrm{~V}$ |
| *TSC911AIJA | 8 -Pin <br> CerDIP | $-25^{\circ} \mathrm{C}$ to $85^{\circ} \mathrm{C}$ | $15 \mu \mathrm{~V}$ |
| *TSC911BIJA | 8 -Pin <br> CerDIP | $-25^{\circ} \mathrm{C}$ to $85^{\circ} \mathrm{C}$ | $30 \mu \mathrm{~V}$ |
| TSC911AY | Chip | $25^{\circ} \mathrm{C}$ | $15 \mu \mathrm{~V}$ |
| TSC911BY | Chip | $25^{\circ} \mathrm{C}$ | $30 \mu \mathrm{~V}$ |

* Parts Available with 160 Hour, $+125^{\circ} \mathrm{C}$ Burn-In. Add /BI to Part Number Suffix.


## Pin Configuration



Absolute Maximum Ratings


Operating Temp. Range
I Device ............................. $-25^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$
C Device ................................ $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$
Package Power Dissipation ( $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ )
CerDIP Package ...................................... 500 mW
Plastic Package ........................................ 375 mW

Electrical Characteristics: $\mathrm{V}_{\mathrm{S}}= \pm 5 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ unless otherwise indicated.

| NO. | SYMBOL | PARAMETER | TEST CONDITIONS | MIN | TSC911A | MAX | MIN | $\begin{gathered} \text { TSC9111 } \\ \text { TYP } \end{gathered}$ | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Vos | Input Offset Voltage | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ | - | 5 | 15 | - | 15 | 30 | $\mu \mathrm{V}$ |
| 2 | Vos/T | Average Temperature Coefficient of Input Offset Voltage | $\begin{aligned} & 0^{\circ} \mathrm{C} \leq T_{A} \leq 70^{\circ} \mathrm{C} \\ & -25^{\circ} \mathrm{C} \leq T_{A} \leq 85^{\circ} \mathrm{C} \end{aligned}$ | - | $\begin{aligned} & 0.05 \\ & 0.05 \end{aligned}$ | $\begin{aligned} & 0.15 \\ & 0.15 \end{aligned}$ | - | $\begin{aligned} & 0.1 \\ & 0.1 \end{aligned}$ | $\begin{aligned} & 0.25 \\ & 0.25 \end{aligned}$ | $\begin{aligned} & \mu \mathrm{V} /{ }^{\circ} \mathrm{C} \\ & \mu \mathrm{~V} /{ }^{\circ} \mathrm{C} \end{aligned}$ |
| 3 | IB | Average Input Bias Current | $\begin{aligned} & T_{A}=25^{\circ} \mathrm{C} \\ & 0^{\circ} \mathrm{C} \leq T_{A} \leq 70^{\circ} \mathrm{C} \\ & -25^{\circ} \mathrm{C} \leq T_{A} \leq 85^{\circ} \mathrm{C} \end{aligned}$ | - | 二 | $\begin{array}{r} 70 \\ 3 \\ 4 \end{array}$ | - | - | 120 4 6 | pA nA nA |
| 4 | los | Average Input | Offset Current | - | 5 | 20 | - | 10 | 40 | pA |
| 5 | en | Input Voltage Noise | 0.1 to $1.0 \mathrm{~Hz}, \mathrm{Rs} \leq 100 \Omega$ | - | 0.65 | - | - | 0.65 | - | $\mu \mathrm{VP-P}$ |
| 6 | en | Input Voltage Noise | 0.1 to $10 \mathrm{~Hz}, \mathrm{Rs} \leq 100 \Omega$ | - | 11 | - | - | 11 | - | $\mu \mathrm{VP-P}$ |
| 7 | CMRR | Common-Mode Rejection Ratio | $\mathrm{V}_{\mathrm{S}}^{-} \leq \mathrm{V}_{\mathrm{CM}} \leq \mathrm{V}_{\mathrm{S}}^{+}-2.2$ | 110 | 116 | - | 105 | 110 | - | dB |
| 8 | CMVR | Common-Mode Voltage Range |  | $\mathrm{V}_{s}^{-}$ |  | $\mathrm{V}_{\mathrm{s}}^{+}-2.0$ | Vs |  | $\mathrm{V}_{S}^{+}-2.0$ | V |
| 9 | Aol | Open-Loop Voltage Gain | $\mathrm{RL}_{\mathrm{L}}=10 \mathrm{k} \Omega, \mathrm{V}_{\mathrm{O}}= \pm 4 \mathrm{~V}$ | 115 | 120 | - | 110 | 120 | - | dB |
| 10 | Vout | Output Voltage Swing | $\mathrm{RL}=10 \mathrm{k} \Omega$ | V - +3 V |  | $\mathrm{V}_{s}^{+}-.9 \mathrm{~V}$ | V - +.3 V |  | ${ }_{s}^{+}-.9 \mathrm{~V}$ | V |
| 11 | BW | Closed Loop Bandwidth | Closed Loop Gain $=+1$ | - | 1.5 | - | - | 1.5 | - | MHz |
| 12 | SR | Slew Rate | $\mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega, \mathrm{C}_{\mathrm{L}}=50 \mathrm{pf}$ | - | 2.5 | - | - | 2.5 | - | $\mathrm{V} / \mu \mathrm{s}$ |
| 13 | PSRR | Power Supply Rejection | $\pm 3.3 \mathrm{~V}$ to $\pm 5.5 \mathrm{~V}$ | 112 | - | - | 105 | - | - | dB |
| 14 | Vs | Operating Supply Voltage | Range ( Note 3) | $\pm 3 \mathrm{~V}$ | - | $\pm 8 \mathrm{~V}$ | $\pm 3 \mathrm{~V}$ | - | $\pm 8 \mathrm{~V}$ | V |
| 15 | Is | Quiescent Supply Current | $\mathrm{V}_{\mathrm{s}}= \pm 5 \mathrm{~V}$ | - | 350 | 600 | - | - | 800 | $\mu \mathrm{A}$ |

## Notes:

1. Static Sensitive Device. Unused devices should be stored in conductive material.
2. Stresses above those listed under "Absolute Maximum Ratings" may cause permanent damage to the devices. These are stress ratings only and functlonal operation of the device at these or any other conditions above those indicated in the operational sections of the specifications is not implied.
3. Single Supply Operation: $\mathrm{V}_{\mathrm{S}}^{+}=+4.5 \mathrm{~V}$ to +16 V .

## Auto-Zeroed Monolithic

Operational Amplifier

- No External Chopper Capacitors
- 3.5 mW Power Dissipation
- $5 \mu \mathrm{~V}$ Offset Voltage


## Functional Diagram



## Typical Characteristic Curves



Supply Current vs Temperature


Gain vs Phase


## Typical Characteristic Curves (Cont.)

Large Signal Output
Switching Wave Form


HORIZONTAL SCALE $=2 \mu \mathrm{~s} /$ DIV

Input Offset Voltage vs Common-Mode Voltage


Positive Overload Recovery Time


Negative Overload Recovery Time


HORIZONTAL SCALE $=\mathbf{2 0} \mathbf{~ m s} /$ DIV

Output Voltage Swing vs Load Resistance


## Pin Compatibility

The CMOS TSC911 is pin compatible with the GE/Intersil ICL7650 chopper-stabilized amplifier. The ICL7650 must use external $0.1 \mu \mathrm{~F}$ capacitors connected at pins 1 and 8 . With the TSC911 operational amplifier, however, external offset voltage error cancelling capacitors are not required. TSC911 pins 1 and 8 are not connected internally. Pin 5 is also not internally connected. The ICL7650 uses pin 5 as an optional output clamp connection. The external chopper capacitors and clamp conections are not necessary when the TSC911 is used. External circuits connected to pins 1,8 , and 5 will have no effect on the TSC911. The TSC911 can be quickly evaluated in existing ICL7650 designs. Since external capacitors are not required system part count, assembly time, and total system cost are reduced. Reliabilty is increased and printed circuit board layout eased by having the error storage capacitors integrated on the TSC911 chip.
The TSC911 pin-out matches many popular operational amplifiers - OP07, OP05, ICL7650, ICL7652, 741, LM101, LM108, OP20, OP21, OP08 and OP06. In many applications that operate from +5 V power supplies the TSC911 will offer superior electrical performance and be a functional pin compatible replacement. Offset voltage correction potentiometers, compensation capacitors, and chopper-stabilization capacitors can be removed when retro-fitting existing equipment designs.


Figure 1: Unwanted Thermocouple Errors Eliminated by Reducing Thermal Gradients and Balancing Junctions.

## Thermocouple Errors

Heating one joint of a loop made form two different metallic wires causes current flow. This is known as the Seebeck effect. By breaking the loop an open circuit voltage (Seebeck Voltage) can be measured. Junction temperature and metal type set the magnitude. Typical values are $0.1 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ to $10 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$. Thermal induced voltages can be many times larger than the TSC911 offset voltage drift. Unless the unwanted thermocouple potentials can be controlled system performance will be less than optimum.
Unwanted thermocouple junctions are created when leads are soldered or sockets/connectors used. Low thermo-electric coefficient solder can reduce errors. A $60 \% \mathrm{Sn} / 36 \% \mathrm{~Pb}$ solder has one tenth the thermal voltage of common $64 \% \mathrm{Sn} /$ $36 \% \mathrm{~Pb}$ solder at a copper junction.
The number and type of dissimilar metallic junctions in the input circuit loop should be balanced. If the junctions are kept at the same temperature their summation will add to zero cancelling errors (Figure 1 ).
Shielding precision analog circuits from aircurrents - especially those caused by power dissipating components and fans - will minimize temperature gradients and minimize thermocouple induced errors.

## Avoiding Latch-Up

Junction isolated CMOS circuits inherently contain a parasitic p-n-p-n transistor circuit. Voltages exceeding the supplies by 0.3 V should not be applied to the device pins. Larger voltages can turn the p-n-p-n device on causing excessive device power supply current and excessive power dissipation. TSC911 power supplies should be established either at the same time or before input signals are applied. If this is not possible input current should be limited to 1 mA to avoid triggering the p-n-p-n structure.

## Static Protection

Input pins are protected against electrostatic fields. Static handling procedures should be used with all CMOS devices. Many companies provide services, educational material, and supplies to aid electronic equipment manufacturers establish "static safe" CMOS component handling areas. A partial company list is:

- 3M
Static Control Systems Div 223-23W EM Center St. Paul, MN 55101
(800) 792-1072
- Semtronics
P.O. Box 592 Martinsville, NJ 08836
(201) 561-9520


## Overload Recovery

The TSC911 recovers quickly from output saturation. Typical recovery time from positive output saturation is 20 msec . Negative output saturation recovery time is typically 5 msec .

## Typical Applications

## 10 Volt Precision Reference



Thermometer Circuit


Programmable Gain Amplifier with Imput Multiplexer


## Auto-Zeroed Monolithic

Operational Amplifier

- No External Chopper Capacitors
- 3.5 mW Power Dissipation
- $5 \mu \mathrm{~V}$ Offset Voltage


## Package Outline



## Chip Pad Layout



## General Description

The TSC913 is the world's first complete monolithic dual auto-zeroed operational amplifier. The TSC913 sets a new standard for low power precision dual operational amplifiers. Chopper-stabilized or auto-zeroed amplifiers offer low offset voltage errors by periodically sampling offset error and storing correction voltages on capacitors. Previous single amplifier designs required two user supplied external $0.1 \mu \mathrm{~F}$ error storage correction capacitors - much too large for on-chip integration. The unique TSC913 architecture requires smaller capacitors making on-chip integration possible. Microvolt offset levels are achieved and External Capacitors Are Not Required.

The TSC913 system benefits are apparent when contrasted with a 7650 chopper amplifier circuit implementation. A single TSC913 replaces two 7650s and four capacitors. Five components and assembly steps are eliminated.

The TSC913 pinout matches many popular dual operational amplifiers. The OP04, TLC322, LM358, and ICL7621 are typical examples. In many applications operating from dual five volt power supplies or single supplies, the TSC913 offers superior electrical performance and can be a functional, drop-in replacement. Printed circuit board rework is not necessary. The TSC913 low offset voltage error eliminates offset voltage trim potentiometers often needed with bipolar and low accuracy CMOS operational amplifiers.

The TSC913 takes full advantage of Teledyne's proprietary CMOS technology. The TSC913 $650 \mu \mathrm{~A}$ supply current ( $250 \mu \mathrm{~A}$ per amplifier) makes the TSC913 the lowest power, precision dual operational amplifier available. The 250 microampere amplifier supply current does not compromise AC performance. Unity gain bandwidth is 1.5 MHz and slew rate is $2.5 \mathrm{~V} / \mu \mathrm{s}$.

For single and quad operational amplifiers see the TSC911 and TSC914 data sheets.

## Features

- First Monolithic Dual Auto-Zeroed Operational Amplifier
- Chopper Amplifier Performance Without External Capacitors
- $15 \mu \mathrm{~V}$ Vos Maximum
$-0.15 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ Vos Drift Maximum
- Saves Cost/Assembly of Four "Chopper" Capacitors
- High DC Gain ........................................ 120 dB
- Low Supply Current .............................. $650 \mu \mathrm{~A}$
- Low Input Voltage Noise ( 0.1 to 10 Hz ) .................. $0.65 \mu \mathrm{Vp-p}$
- Wide Common-Mode Voltage Range $\ldots \mathrm{V}_{\mathrm{S}}^{-}$to $\mathrm{V}_{\mathrm{S}}^{+}-2 \mathrm{~V}$
- High Common-Mode Rejection ................. 116 dB
- Dual or Single Supply Operation ........ $\pm 3 \mathrm{~V}$ to $\pm 8 \mathrm{~V}$ +4.5 V to +16 V
- Excellent AC Operating Characteristics
$-2.5 \mathrm{~V} / \mu \mathrm{s}$ Slew Rate
- 1.5 MHz Unity Gain Bandwidth
- Pin Compatible to LM358, OP14, MC1458, ICL7621, TL082, TLC322


## Pin Configuration



# Dual Auto－Zeroed Operational Amplifier － $15 \mu \mathrm{~V}$ Offset Voltage － $650 \mu \mathrm{~A}$ Supply Current 

## Absolute Maximum Ratings

| Total Supply Voltage（ $\mathrm{V}_{s}^{+}$to $\mathrm{V}_{\bar{s}}$ ） $\qquad$ 18 Volts Input Voltage $\ldots \ldots \ldots \ldots . .\left(V_{s}^{+}+0.3\right)$ to $\left(V_{s}^{-}-0.3\right)$ Volts <br> Storage Temp．Range $\qquad$ ．．．．．．．．．$-55^{\circ} \mathrm{C}$ to $150^{\circ} \mathrm{C}$ <br> Lead Temperature（Soldering， 10 sec ） $\qquad$ $300^{\circ} \mathrm{C}$ <br> Current into Any Pin $\qquad$ 10 mA |
| :---: |
|  |  |
|  |  |
|  |  |

```
Operating Temp. Range
    I Device ........................... - -25 }\textrm{C}\mathrm{ to +85 }\mp@subsup{}{}{\circ}\textrm{C
    C Device .............................. 0 0 }\mp@subsup{0}{}{\circ}\textrm{C}\mathrm{ to }+7\mp@subsup{0}{}{\circ}\textrm{C
Package Power Dissipation ( }\mp@subsup{T}{A}{}=25\mp@subsup{}{}{\circ}\textrm{C}\mathrm{ )
CerDIP Package ................................... }500\textrm{mW
Plastic Package ...............................................
```

Electrical Characteristics： $\mathrm{V}_{\mathrm{S}}= \pm 5, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ unless otherwise indicated．

| NO． | SYMBOL | PARAMETER | TEST CONDITIONS | MIN | $\begin{gathered} \hline \text { TSC913A } \\ \text { TYP } \end{gathered}$ | MAX | MIN | $\begin{gathered} \text { TSC913B } \\ \text { TYP } \end{gathered}$ | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Vos | Input Offset Voltage | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ | － | 5 | 15 | － | 15 | 30 | $\mu \mathrm{V}$ |
| 2 | Vos／T | Average Temperature Coefficient of Input Offset Voltage | $\begin{aligned} & 0^{\circ} \mathrm{C} \leq T_{A} \leq 70^{\circ} \mathrm{C} \\ & -25^{\circ} \mathrm{C} \leq T_{A} \leq 85^{\circ} \mathrm{C} \end{aligned}$ | － | $\begin{aligned} & 0.05 \\ & 0.05 \end{aligned}$ | $\begin{aligned} & 0.15 \\ & 0.15 \end{aligned}$ | － | － | $\begin{aligned} & 0.25 \\ & 0.25 \end{aligned}$ | $\begin{aligned} & \mu \mathrm{V} /{ }^{\circ} \mathrm{C} \\ & \mu \mathrm{~V} /{ }^{\circ} \mathrm{C} \end{aligned}$ |
| 3 | IB | Average Input Bias Current | $\begin{aligned} & T_{A}=25^{\circ} \mathrm{C} \\ & 0^{\circ} \mathrm{C} \leq T_{A} \leq 70^{\circ} \mathrm{C} \\ & -25^{\circ} \mathrm{C} \leq T_{A} \leq 85^{\circ} \mathrm{C} \end{aligned}$ | － | 二 | 90 3 4 | 二 | 二 | 120 4 6 | pA nA nA |
| 4 | los | Average Input | Offset Current | － | 5 | 20 | － | 10 | 40 | pA |
| 5 | en | Input Voltage Noise | 0.1 to $1.0 \mathrm{~Hz}, \mathrm{Rs} \leq 100 \Omega$ | － | 0.6 | － | － | 0.6 | － | $\mu \mathrm{V}$ P－P |
| 6 | en | Input Voltage Noise | 0.1 to $10 \mathrm{~Hz}, \mathrm{Rs} \leq 100 \Omega$ | － | 11 | － | － | 11 | － | $\mu \mathrm{VP-P}$ |
| 7 | CMRR | Common－Mode Rejection Ratio | $\mathrm{V}_{\mathrm{s}}^{-} \leq \mathrm{VCM} \leq \mathrm{V}_{\mathrm{S}}^{+}-2.2 \mathrm{~V}$ | 110 | 116 | － | 100 | 110 | － | dB |
| 8 | CMVR | Common－Mode Voltage Range |  | Vs |  | $V_{S}^{+}-2.0$ | Vs |  | $\mathrm{V}_{s}^{+}-2.0$ | V |
| 9 | AoL | Open－Loop Voltage Gain | $R_{L}=10 \mathrm{k} \Omega, \mathrm{V}_{0}= \pm 4 \mathrm{~V}$ | 115 | 120 | － | 110 | 120 | － | dB |
| 10 | Vout | Output Voltage Swing | $\mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega$ | $V \bar{s}+.3 \mathrm{~V}$ |  | $\mathrm{V}_{\mathbf{+}}^{+}-9 \mathrm{~V}$ | $\mathrm{Vs}+3 \mathrm{~V}$ |  | －-.9 V | V |
| 11 | BW | Closed Loop Bandwidth | Closed Loop Gain＝＋1 | － | 1.5 | － | － | 1.5 | － | MHz |
| 12 | SR | Slew Rate | $\mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega, \mathrm{C}_{\mathrm{L}}=50 \mathrm{pf}$ | － | 2.5 | － | － | 2.5 | － | $\mathrm{V} / \mu \mathrm{s}$ |
| 13 | PSRR | Power Supply Rejection | $\pm 3.3 \leq \mathrm{Vs}_{s} \leq \pm 5.5 \mathrm{~V}$ | 110 | － | － | 100 | － | － | dB |
| 14 | Vs | Operating Supply Voltage Range（Note 3） |  | $\pm 3 \mathrm{~V}$ | － | $\pm 8 \mathrm{~V}$ | $\pm 3 \mathrm{~V}$ | － | $\pm 8 \mathrm{~V}$ | V |
| 15 | Is | Quiescent Supply Curr （Both Amplifiers） | ${ }^{t} V_{s}= \pm 5 \mathrm{~V}$ | － | 0.65 | 0.85 | － | － | 1.1 | mA |

## Notes：

1．Static Sensitive Device．Unused devices should be stored in conductive material．
2．Stresses above those listed under＂Absolute Maximum Ratings＂may cause permanent damage to the devices．These are stress ratings only and func－ tional operation of the device at these or any other conditions above those indicated in the operational sections of the specifications is not implied．
3．Single Supply Operation： $\mathrm{V}_{\mathrm{S}}^{+}=+4.5 \mathrm{~V}$ to +16 V ．
4．Advance product information．

## General Description

The TSC914 is the world's first complete monolithic quad auto-zeroed operational amplifier. The TSC914 sets a new standard for low power precision quad operational amplifiers. Chopper-stabilized or auto-zeroed amplifiers offer low offset voltage errors by periodically sampling offset error and storing correction voltages on capacitors. Previous single amplifier designs required two user supplied external $0.1 \mu \mathrm{~F}$ error storage correction capacitors - much too large for on-chip integration. The unique TSC914 architecture requires smaller capacitors making on-chip integration possible. Microvolt offset levels are achieved and External Capacitors Are Not Required.

The TSC914 system benefits are apparent when contrasted with a 7650 chopper amplifier circuit implementation. A single TSC914 replaces four 7650s and eight capacitors. Eleven components and assembly steps are eliminated.

The TSC914 pinout matches many popular quad operational amplifiers. The OP11, TLC274, LTC1014, LM348, and ICL7642/ 41 are typical examples. In many applications operating from dual five volt power supplies or single supplies, the TSC914 offers superior electrical performance and can be a functional, drop-in replacement. Printed circuit board rework is not necessary. The TSC914 low offset voltage error eliminates offset voltage trim potentiometers often needed with bipolar and low accuracy CMOS operational amplifiers.

The TSC914 takes full advantage of Teledyne's proprietary CMOS technology. The TSC914 1.5 mA supply current ( 250 $\mu$ A per amplifier) makes the TSC914 the lowest power, precision quad operational amplifier available. The 250 microampere amplifier supply current does not compromise AC performance. Unity gain bandwidth is 1.5 MHz and slew rate is $2.5 \mathrm{~V} / \mu \mathrm{s}$.

For single and dual operational amplifiers see the TSC911 and TSC913 data sheets.

## Features

- First Monolithic Quad Auto-Zeroed Operational Amplifier
- Chopper Amplifier Performance Without External Capacitors
$-15 \mu \mathrm{~V}$ Vos
$-0.15 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ Vos Drift
- Saves Cost/Assembly of Eight "Chopper" Capacitors
- High DC Gain .................................... 110 dB
- Low Supply Current ................................. 1.5 mA
- Wide Common-Mode Voltage Range .... $\mathrm{V}_{\mathrm{S}}^{-}$to $\mathrm{V}_{\mathrm{S}}^{+}-2 \mathrm{~V}$
- High Common-Mode Rejection ................. 110 dB
- Dual or Single Supply Operation ........ $\pm 3 \mathrm{~V}$ to $\pm 8 \mathrm{~V}$
+4.5 V to +16 V
- Excellent AC Operating Characteristics
- $2.5 \mathrm{~V} / \mu \mathrm{s}$ Slew Rate
- 1.5 MHz Unity Gain Bandwidth
- Pin Compatible to LM348, TLC274, LM324, OP11, ICL7641/42


## Pin Configuration



## Absolute Maximum Ratings

| Total Supply Voltage（ $\mathrm{V}_{\mathrm{s}}^{+}$to V s ） 18 Volts Input Voltage $\left(V_{s}^{+}+0.3\right)$ to $\left(V_{s}^{-}-0.3\right)$ Volts |
| :---: |
| Storage Temp．Range ．．．．．．．．．．．．．．．．．－ $55^{\circ} \mathrm{C}$ to $150{ }^{\circ} \mathrm{C}$ |
| Lead Temperature（Soldering， 10 sec ）．．．．．．．．．．．． $300^{\circ} \mathrm{C}$ |
| into Any Pin |

Operating Temp．Range
I Device $-25^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ C Device ．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．． $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$
Package Power Dissipation（ $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ ）CerDIP Package500 mW
Plastic Package ..... 375 mW

Electrical Characteristics： $\mathrm{V}_{\mathrm{S}}= \pm 5, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ unless otherwise indicated．

| NO． | SYMBOL | PARAMETER | TEST CONDITIONS | MIN | $\begin{aligned} & \text { TSC914A } \\ & \text { TYP } \end{aligned}$ | MIN | $\begin{array}{cc} \text { TSC914B } \\ \text { TYP } \end{array} \text { MAX }$ | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Vos | Input Offset Voltage | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ | － | 515 | － | 1530 | $\mu \mathrm{V}$ |
| 2 | Vos／T | Average Temperature Coefficient of Input Offset Voltage | $\begin{aligned} & 0^{\circ} \mathrm{C} \leq T_{A} \leq 70^{\circ} \mathrm{C} \\ & -25^{\circ} \mathrm{C} \leq T_{A} \leq 85^{\circ} \mathrm{C} \end{aligned}$ | － | $\begin{array}{ll} 0.05 & 0.15 \\ 0.05 & 0.15 \end{array}$ | － | $\begin{array}{ll}- & 0.25 \\ - & 0.25\end{array}$ | $\begin{aligned} & \mu \mathrm{V} /{ }^{\circ} \mathrm{C} \\ & \mu \mathrm{~V} /{ }^{\circ} \mathrm{C} \end{aligned}$ |
| 3 | $\mathrm{I}_{\mathrm{B}}$ | Average Input Bias Current | $\begin{aligned} & T_{A}=25^{\circ} \mathrm{C} \\ & 0^{\circ} \mathrm{C} \leq T_{A} \leq 70^{\circ} \mathrm{C} \\ & -25^{\circ} \mathrm{C} \leq T_{A} \leq 85^{\circ} \mathrm{C} \end{aligned}$ | － | $\begin{array}{rr} \\ - & 90 \\ - & 3\end{array}$ | 三－ | $\begin{array}{lr} \\ - & 120 \\ - & 4 \\ - & 6\end{array}$ | $\begin{aligned} & \mathrm{pA} \\ & \mathrm{nA} \\ & \mathrm{nA} \end{aligned}$ |
| 4 | los | Average Input | Offset Current | － | 520 | － | $10 \quad 40$ | pA |
| 5 | en | Input Voltage Noise | 0.1 to $1.0 \mathrm{~Hz}, \mathrm{R}_{\mathrm{s}} \leq 100 \Omega$ | － | 0.6 | － | 0.6 | $\mu \mathrm{V}$ P－P |
| 6 | en | Input Voltage Noise | 0.1 to $10 \mathrm{~Hz}, \mathrm{Rs} \leq 100 \Omega$ | － | 11 | － | 11 | $\mu V_{\text {P－P }}$ |
| 7 | CMRR | Common－Mode Rejection Ratio | $\mathrm{V}_{\mathrm{S}}^{-} \leq \mathrm{V}_{\text {CM }} \leq \mathrm{V}_{S}^{+}-2.2 \mathrm{~V}$ | 110 | 116 | 100 | 110 | dB |
| 8 | CMVR | Common－Mode Voltage Range |  | vs | － $\mathrm{V}_{\mathrm{S}}^{+}-2.0$ | $\mathrm{V}_{s}^{-}$ | － $\mathrm{V}_{S}^{+}-2.0$ | V |
| 9 | Aol | Open－Loop Voltage Gain | $\mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega, \mathrm{V}_{\mathrm{O}}= \pm 4 \mathrm{~V}$ | 115 | 120 | 110 | 120 | dB |
| 10 | Vout | Output Voltage Swing | $\mathrm{RL}=10 \mathrm{k} \Omega$ | $\mathrm{Vs}+.3 \mathrm{~V}$ | － $\mathrm{V}_{S}^{+}-.9 \mathrm{~V}$ | $\mathrm{V}_{\mathrm{s}}^{-}+.3 \mathrm{~V}$ | $-\mathrm{V}_{\mathrm{S}}^{+}-.9 \mathrm{~V}$ | V |
| 11 | BW | Closed Loop Bandwidth | Closed Loop Gain＝＋1 | － | 1.5 | － | 1.5 | MHz |
| 12 | SR | Slew Rate | $\mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega, \mathrm{C}_{\mathrm{L}}=50 \mathrm{pf}$ | － | 2.5 | － | 2.5 | $\mathrm{V} / \mu \mathrm{s}$ |
| 13 | PSRR | Power Supply Rejection | $\pm 3.3 \leq \mathrm{Vs}^{5} \pm 5.5 \mathrm{~V}$ | 110 | － | 100 | － | dB |
| 14 | Vs | Operating Supply Voltage Range（Note 3） |  | $\pm 3 \mathrm{~V}$ | $-\quad \pm 8 \mathrm{~V}$ | $\pm 3 \mathrm{~V}$ | －$\pm 8 \mathrm{~V}$ | V |
| 15 | Is | Quiescent Supply Current （Four Amplifiers） | $\mathrm{V}_{\mathrm{S}}= \pm 5 \mathrm{~V}$ | － | － 1.6 | － | － 2.2 | mA |

## Notes：

1．Static Sensitive Device．Unused devices should be stored in conductive material．
2．Stresses above those listed under＂Absolute Maximum Ratings＂may cause permanent damage to the devices．These are stress ratings only and func－ tional operation of the device at these or any other conditions above those indicated in the operational sections of the specifications is not implied．
3．Single Supply Operation： $\mathrm{V}_{\mathrm{S}}^{+}=+4.5 \mathrm{~V}$ to +16 V ．
4．Advance product information．

## General Description

The TSC918 is a general purpose, low cost CMOS operational amplifier. By sampling input offset voltage periodically and storing compensating voltages on external capacitors low offset voltage errors are possible. The correction circuits compensate offset voltage drift with temperature and time. Offset voltage temperature coefficient is $0.8 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ maximum. Maximum Vos is $50 \mu \mathrm{~V}$.

The TSC918 performance advantages are achieved without the manufacturing complexity and cost incurred with laser or "zener zap" Vos trim techniques. The TSC918 offers a $0.2 \mathrm{~V} / \mu \mathrm{s}$ slew rate and a 700 kHz unity gain bandwidth. Open loop voltage gain is 100 dB .

Operating from $\pm 5 \mathrm{~V}$ supplies the CMOS TSC918 power dissipation is under 10 mW . In +5 V only systems the TSC7660 DC-to-DC converter can supply the TSC918 negative supply potential. The TSC918 will also operate from a single +5 supply.

For lower power dissipation and offset voltage errors, see the TSC900 and TSC7650/7650A specifications.

## Functional Diagram



## Features

- Low Power Supply Current ................ . $800 \mu \mathrm{~A}$ Max.
- Low Input Offset Voltage .................... $50 \mu \mathrm{~V}$ Max.
- Low Input Offset Voltage Drift ......... $0.8 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ Max.
- High Impedance Differential CMOS Inputs ..... 1012 ת
- High Open Loop Voltage Gain ............ 100 dB Min.
- Low Input Noise Voltage ....................... $0.3 \mu \mathrm{Vp}-\mathrm{p}$
- Compensated internally for Stable Unity Gain Operation
- High Common Mode Rejection ............. 98 dB Min.


## Ordering Information

| Part No. | Package | Temp. <br> Range | Max. <br> VoS |
| :--- | :--- | :---: | :---: |
| TSC918CPA | 8-Pin <br> Plastic Dip | COM | $50 \mu \mathrm{~V}$ |
| TSC918IJA | 8-Pin <br> CerDIP | IND | $50 \mu \mathrm{~V}$ |
| TSC918CPD | 14-Pin <br> Plastic Dip | COM | $50 \mu \mathrm{~V}$ |
| TSC918IJD | 14-Pin <br> CerDIP | IND | $50 \mu \mathrm{~V}$ |

## Pin Configuration



## Absolute Maximum Ratings

Total Supply Voltage ( $V_{S}^{+}$to $V_{\bar{s}}^{-}$) $\ldots . . . . . . . . . . . .$.
Input Voltage $\ldots . . . . . . . . .\left(V_{s}^{+}+0.3\right)$ to $\left(\mathrm{V}_{s}^{-}-0.3\right)$ Volts
Storage Temp. Range ..................... $-55^{\circ} \mathrm{C}$ to $150^{\circ} \mathrm{C}$
Lead Temperature (Soldering, 10 sec ) .............. $300^{\circ} \mathrm{C}$
Voltage on Oscillator Control Pins ............... $\mathrm{V}_{\mathrm{S}}^{+}$to $\mathrm{V}_{\mathrm{s}}^{-}$
Output Short Circuit Duration .................... Indefinite

Current into Any Pin ............................... 10 mA
While Operating (Note 4) ...................... $100 \mu \mathrm{~A}$
Operating Temp. Range
I Device ............................... $-25^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$
C Device . ................................. $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$
Package Power Dissipation ( $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ )
CerDIP Package
500 mW
Plastic Package ........................................ 500 mW

Electrical Characteristics: $\mathrm{V}_{S}^{+}=+5 \mathrm{~V}, \mathrm{~V}_{S}^{-}=-5 \mathrm{~V}, \mathrm{C}_{A}=\mathrm{C}_{B}=0.1 \mu \mathrm{~F} . \mathrm{T}_{A}=25^{\circ} \mathrm{C}$.

| TYPE | NO. | SYMBOL | PARAMETER | TEST CONDITIONS | MIN | $\begin{gathered} \text { TSC918 } \\ \text { TYP } \end{gathered}$ | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \mathbf{I} \\ & \mathbf{N} \\ & \mathbf{P} \\ & \mathbf{U} \\ & \mathbf{T} \end{aligned}$ | 1 | Vos | Input Offset Voltage | $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ | - | - | 50 | $\mu \mathrm{V}$ |
|  | 2 | $\frac{\Delta V_{\text {OS }}}{\Delta T}$ | Input Offset Voltage Average Temp. Coefficient | Operating Temp <br> Range (Note 1) | - | 0.4 | 0.8 | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
|  | 3 | IBIAS | Average Input Bias Current (Note 7) | $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ | - | - | 100 | pA |
|  | 4 | los | Input Offset Current | $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ | - | 0.5 | - | pA |
|  | 5 | enp-p | Input Noise Voltage | $\begin{aligned} & \text { Rs }=100 \Omega \\ & 0 \text { to } 10 \mathrm{~Hz} \end{aligned}$ | - | 4 | - | $\mu \mathrm{V}_{\mathrm{p}-\mathrm{p}}$ |
|  | 6 | enp-p | Input Noise Voltage | $\begin{aligned} & \text { Rs }=100 \Omega \\ & 0 \text { to } 1 \mathrm{~Hz} \end{aligned}$ | - | 0.3 | - | $\mu V_{p-p}$ |
|  | 7 | RIN | Input Resistance |  | - | 1012 | - | $\Omega$ |
|  | 8 | CMVR | Common-Mode Voltage Range |  | -5.0 |  | +2.0 V | V |
|  | 9 | CMRR | Common-Mode Rejection Ratio | CMVR $=-5 \mathrm{~V}$ to +2.0 V | 98 | 115 | - | dB |
| $\begin{aligned} & \hline \mathbf{O} \\ & \mathbf{U} \\ & \mathbf{T} \\ & \mathbf{P} \\ & \mathbf{U} \\ & \mathbf{T} \end{aligned}$ | 10 | Av | Large-Signal Voltage Gain | $\mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega$ | 100 | 130 | - | dB |
|  | 11 | Vout | Output Voltage | $R_{L}=25 \mathrm{k} \Omega$ | -4.7 | - | +3.5 | V |
|  |  |  | Swing (Note 3) | $\mathrm{R}_{\mathrm{L}}=100 \mathrm{k} \Omega$ | -4.9 | - | +3.9 |  |
|  | 12 |  | Clamp ON Current (Note 2) | $\mathrm{R}_{\mathrm{L}}=100 \mathrm{k} \Omega$ | 20 | 90 | 200 | $\mu \mathrm{A}$ |
|  | 13 |  | Clamp OFF Current (Note 2) | $-4.0 \mathrm{~V}<$ VOUT $<+4.0 \mathrm{~V}$ | - | 1 | - | pA |
| D $\mathbf{Y}$ $\mathbf{N}$ $\mathbf{A}$ $\mathbf{M}$ | 14 | Bw | Unity <br> Gain <br> Bandwidth | Unity Gain (+1) | - | 0.7 | - | MHz |
| $\begin{gathered} \mathbf{M} \\ \mathbf{1} \\ \mathbf{C} \\ \hline \end{gathered}$ | 15 | $S_{R}$ | Slew Rate | $\begin{aligned} & \mathrm{C}_{\mathrm{L}}=50 \mathrm{pF}, \\ & \mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega \end{aligned}$ | - | 0.2 | - | $\mathrm{V} / \mu \mathrm{s}$ |
| S $\mathbf{U}$ | 16 | $V_{S}^{+}$to $V_{S}$ | Operating Supply Range |  | 4.5 | - | 16 | V |
| P | 17 | Is | Supply Current | No Load | - | 300 | 800 | $\mu \mathrm{A}$ |
| $\begin{aligned} & \mathrm{L} \\ & \mathbf{Y} \end{aligned}$ | 18 | PSRR | Power Supply Rejection Ratio | $V_{S}= \pm 3 \mathrm{~V}$ to $\pm 8 \mathrm{~V}$ | 105 | - | - | dB |

## Notes:

1. Operating temperature range is $-25^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ for " l " grade and $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ for "C" grade.
2. See OUTPUT CLAMP discussion.
3. OUTPUT CLAMP not connected.
4. Limiting input current to $100 \mu \mathrm{~A}$ is recommended to avoid latch-up problems.
5. Static Sensitive Device. Unused devices must be stored in conductive material to protect devices from possible static damage.
6. Stresses above those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only and functional operation of the device at these or any other conditions above those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.
7. Average current caused by switch charge transfer at input.

## Low Cost Operational Amplifier

## OP Amp Performance Comparison

The TSC918 is a low cost, low power, precision amplifier. A comparison between the TSC918 and other amplifiers is shown in Figure 1 below.


Figure 1

## Nulling Capacitors

The offset voltage correction capacitors are connected to $\mathrm{C}_{\mathrm{A}}$ and $\mathrm{C}_{\mathrm{B}}$. The common capacitor connection is made to $\mathrm{V}_{\mathrm{S}}$ (Pin 4) on the 8-pin packages and to capacitor return ( $\mathrm{C}_{\mathrm{R}}$, Pin 8 ) on the 14 -pin packages. The common connection should be made through either a separate pc trace or wire to avoid voltage drops.
Internaliy $V_{s}^{-}$is connected to $C_{R}$.
$C_{A}$ and $C_{B}$ should be $0.1 \mu \mathrm{~F}$ film capacitors. Mylar capacitors are suitable.


Figure 2: Nulling Capacitor Connection

## Clock Operation

The internal oscillator is set for a 150 Hz nominal frequency on both the 8 and 14-pin dual in line packages. With the 14pin DIP TSC918, the 150 Hz internal frequency is available at the internal clock output (Pin 12). A 300 Hz nominal signal will be present at the external clock input pin (Pin 13) with EXT/INT high or open. This is the internal clock signal before a divide by two operation.

The 14-pin DIP device can be driven by an external clock. The INT/EXT input (Pin 14) has an internal pull-up and maybe left open for internal clock operation. If an external clock is used INT/EXT must be tied to $\mathrm{V}_{\bar{s}}^{-\bar{E}}(\mathrm{Pin} 7)$ to disable the internal clock. The external clock signal is applied to the external clock input (Pin 13).
The external clock amplitude should swing between $V_{S}^{+}$and ground for power supplies up to $\pm 6 \mathrm{~V}$ and between $\mathrm{V}_{S}^{+}$and $\mathrm{V}_{S}^{+}$ -6 V for higher supply voltages.

At low frequencies the external clock duty cycle is not critical since an internal divide by two gives the desired $50 \%$ switching duty cycle. The offset storage correction capacitors are charged only when the external clock input is high. A 50-80\% external clock positive duty cycle is desired for frequencies above 500 Hz to guarantee transients settle before the internal switches open,
The external clock input can also be used as a strobe input. If a strobe signal is connected at the external clock input so that it is low during the time an overload signal is applied, neither capacitor will be charged. The leakage currents at the capacitor pins are very low.

## Output Clamp

If the output is driven to either supply rail output saturation occurs. The inputs are no longer held at a "virtual ground." The Vos null circuit treats the differential signal as an offset and tries to correct it by charging the external capacitors. The nulling circuit also saturates. Once the input signal returns to normal, the response time is lengthened by the long recovery time of the internal correction circuit and external capacitors.
Through an external clamp connection, the TSC918 eliminates the overload recovery problem by reducing the feedback network gain before the output voltage reaches either supply rail.
Normally the clamp pin is not connected.


Figure 3: Internal Clamp Circuit


Figure 4: Non-Inverting Amplifier with Optional Clamp

## Input Bias Current

The TSC918 inputs are never disconnected from the main internal amplifier. The null amplifier samples the input offset voltage and corrects DC errors and drift by storing compensating voltages on external capacitors. The sampling causes, however, charge transfer at the inputs. The charge transfer represents a peak impulse current of 200 to 290 nA at the inputs when the internal clock makes a transition.


Figure 5: Inverting Amplifier with Optional Clamp

## Latch-Up Avoidance

Junction-isolated CMOS circuits inherently include a parasitic 4-layer ( $p-n-p-n$ ) structure which has characteristics similar to an SCR. Under certain circumstances this junction may be triggered into a low impedance state, resulting in excessive supply current. To avoid the condition, no voltage greater than 0.3 V beyond the supply rails should be applied to any pin. In general, the amplifier supplies must be established either at the same time or before any input signals are applied. If this is not possible, the drive circuits must limit input current flow to under 0.1 mA to avoid latchup.

## Typical Characteristic Curve



## General Description

The TSC7650A CMOS chopper-stabilized operational amplifier practically removes offset voltage error terms from system error calculations. The $5 \mu \mathrm{~V}$ maximum Vos specification, for example, represents a fifteen times improvement over the industry standard OP07E. The $0.2 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ Max. offset drift specification is six times lower than the OP07E. The increased performance eliminates Vos trim procedures, periodic potentiometer adjustment and the reliability problems caused by damaged trimmers. The TSC7650A features lower maximum power supply current and higher slew rate than the ICL 7650. The TSC7650A power supply current is 2.5 mA maximum.
The TSC7650A performance advantages are achieved without the additional manufacturing complexity and cost incurred with laser or "zener zap" Vos trim techniques. The TSC7650A is one of the lowest cost precision operational amplifiers available.
The TSC7650A nulling scheme corrects both dc Vos errors and Vos drift errors with temperature. A nulling amplifier alternately corrects its own Vos errors and the main amplifier Vos error. Offset nulling voltages are stored on two user supplied external capacitors. The capacitors connect to the internal amplifier Vos null points. The main amplifier input signal is never switched. Switching spikes are not present at the TSC7650A output. The null scheme keeps Vos errors low throughout the operating temperature range. Laser and "zener zap" trimming can correct for Vos at only one temperature.
The nulling circuit oscillator and control circuits are integrated on chip. Only two external Vos error storage capacitors are required. The TSC7650A operates as a conventional operational amplifier with vastly improved input specifications. The low Vos and Vos drift errors make the TSC7650A ideal for thermocouple, thermistor, and strain gauge applications. Low dc errors and high open loop gain make the TSC7650A an excellent preamplifier for precision analog to digital converters like the TSC7135, TSC800, and TSC7109.
The 14-pin dual in line package (DIP) has an external oscillator input to drive the nulling circuitry for optimum noise performance. Both the 8 and 14-pin DIP have an output voltage clamp circuit to minimize overload recovery time.

## Pin Configuration



## Features

- Low Input Offset Voltage .................... $5 \mu \mathrm{~V}$ Max.
- Low Input Offset Voltage Drift ......... $0.2 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ Max.
- Low Input Bias Current .................... 15 pA Max.
- High Impedance Differential CMOS Inputs ..... $1012 \Omega$
- High Open Loop Voltage Gain ........... 120 dB Min.
- High Slew Rate .................................... . . $4.0 \mathrm{~V} / \mu \mathrm{s}$
- Low Power Operation ...................... ...... 17 mW
- Output Clamp Speeds Recovery Time
- Compensated Internally for Stable Unity Gain Operation
- Pin Compatible Replacement for ICL7650

Ordering Information

| Part No. | Package | Temp. <br> Range | Max. <br> VOS |
| :--- | :--- | :--- | :--- |
| *TSC7650ACPA | 8-Pin <br> Plastic Dip | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ | $5 \mu \mathrm{~V}$ |
| *TSC7650AIJA | 8 -Pin <br> CerDIP | $-25^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | $5 \mu \mathrm{~V}$ |
| *TSC7650ACPD | $14-$-Pin <br> Plastic Dip | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ | $5 \mu \mathrm{~V}$ |
| *TSC7650AIJD | $14-$ Pin <br> CerDIP | $-25^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | $5 \mu \mathrm{~V}$ |

*Available with 160 hour, $+125^{\circ} \mathrm{C}$ burn-in. Add /BI to part number suffix.

Functional Diagram


## Absolute Maximum Ratings

Total Supply Voltage (V't to Vs̄)
18 Volts Input Voltage ............... ( $V_{s}^{+}+0.3$ ) to $\left(V_{s}^{-}-0.3\right)$ Volts Storage Temp. Range ..................... $-55^{\circ} \mathrm{C}$ to $150^{\circ} \mathrm{C}$
Lead Temperature (Soldering, 10 sec ) .............. $300^{\circ} \mathrm{C}$
Voltage on Oscillator Control Pins ............... $\mathrm{V}^{+}$to $\mathrm{V}_{\mathrm{s}}^{-}$
Output Short Circult Duration ................... Indefinite
Current into Any Pin

Electrical Characteristics: $\mathrm{V}_{\mathrm{S}}^{+}=+5 \mathrm{~V}, \mathrm{~V}_{\mathrm{S}}^{-}=-5 \mathrm{~V}, \mathrm{C}_{A}=\mathrm{C}_{\mathrm{B}}=0.1 \mu \mathrm{~F} . \mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$.

| TYPE | NO. | SYMBOL | PARAMETER | TEST CONDITIONS | MIN | $\begin{gathered} \text { TSC7850A } \\ \text { TYP } \end{gathered}$ | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| I | 1 | Vos | Input Offset Voltage | $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ | - | $\pm 0.7$ | $\pm 5.0$ | $\mu \mathrm{V}$ |
|  | 2 | $\frac{\Delta V O S}{\Delta T}$ | Input Offset Voltage Average Temp. Coefficient | Operating Temp Range (Note 1) | - | 0.08 | 0.2 | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
| N | 3 | Ibias | Input Bias Current | $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ | - | 1.5 | 15 | pA |
| P |  |  |  | $0^{\circ} \mathrm{C} \leq \mathrm{T}_{A} \leq+70^{\circ} \mathrm{C}$ | - | 35 | 150 |  |
| U |  |  |  | $-25^{\circ} \mathrm{C} \leq \mathrm{T}_{A} \leq+85^{\circ} \mathrm{C}$ | - | 100 | 400 |  |
| T | 4 | los | Input Offset Current | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ | - | 0.5 | - | pA |
|  | 5 | enp-p | Input Noise Voltage | $\begin{aligned} & R s=100 \Omega \\ & 0.1 \text { to } 10 \mathrm{~Hz} \end{aligned}$ | - | 4.0 | - | $\mu V_{\text {p-p }}$ |
|  | 6 | In | Input Noise Current | $f=10 \mathrm{~Hz}$ | - | 0.01 | - | $\mathrm{pA} / \sqrt{ } \mathrm{Hz}$ |
|  | 7 | RIN | Input Resistance |  | - | 1012 |  | $\Omega$ |
|  | 8 | CMVR | Common-Mode Voltage Range |  | -5.0 | $\begin{array}{r} -5.2 \text { to } \\ +2.0 \\ \hline \end{array}$ | +1.5 V | V |
|  | 9 | CMRR | Common-Mode Rejection Ratio | $C M V R=-5 V$ to +1.5 V | 120 | 130 | - | dB |
| $\begin{aligned} & 0 \\ & \mathbf{U} \\ & \mathbf{T} \\ & \mathbf{P} \\ & \mathbf{T} \end{aligned}$ | 10 | Av | Large-Slgnal Voltage Gain | $\mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega$ | 120 | 130 | - | dB |
|  | 11 | Vout | Output Voltage Swing (Note 3) | $R_{L}=10 \mathrm{k} \Omega$ | $\pm 4.7$ | $\pm 4.85$ | - | V |
|  |  |  |  | $\mathrm{R}_{\mathrm{L}}=100 \mathrm{k} \Omega$ | - | $\pm 4.95$ | - |  |
|  | 12 |  | Clamp ON Current (Note 2) | $\mathrm{R}_{\mathrm{L}}=100 \mathrm{k} \Omega$ | 25 | 70 | 200 | $\mu \mathrm{A}$ |
|  | 13 |  | Clamp OFF Current (Note 2) | $-4.0 \mathrm{~V}<\mathrm{VOUT}^{<+4.0 ~ V}$ | - | 1 | - | pA |
| D | 14 | Bw | Unity Gain Bandwidth | Unity Gain ( +1 ) | - | 1.0 | - | MHz |
| Y | 15 | $\mathrm{S}_{\mathrm{R}}$ | Slew Rate | $\mathrm{C}_{\mathrm{L}}=50 \mathrm{pF}, \mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega$ | - | 4.0 | - | $\mathrm{V} / \mu \mathrm{s}$ |
| A | 16 | $t_{r}$ | Rise Time |  | - | 0.2 | - | $\mu \mathrm{s}$ |
| $\underset{1}{M}$ | 17 |  | Overshoot |  | - | 30 | - | \% |
| c | 18 | fch | Internal Chopping Frequency | Pins 12-14 Open (DIP) | 120 | 300 | 420 | Hz |
| S U | 19 | $V_{S}^{+}$to $V_{s}^{-}$ | Operating Supply Range |  | 4.5 | - | 16 | V |
| P | 20 | Is | Supply Current | No Load | - | 1.7 | 2.5 | mA |
| $\underset{Y}{\mathbf{Y}}$ | 21 | PSRR | Power Supply Rejection Ratio | $\mathrm{Vs}_{s}= \pm 3 \mathrm{~V}$ to $\pm 8 \mathrm{~V}$ | 120 | 130 | - | dB |

## Notes:

1. Operating temperature range is $-25^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ for " I " grade and $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ for " C " grade.
2. See OUTPUT CLAMP discussion.
3. OUTPUT CLAMP not connected. See characteristic curves for output swing vs clamp current.
4. Limilting input current to $100 \mu \mathrm{~A}$ is recommended to avoid latch-up problems.
5. Static Sensitive Device. Unused devices must be atored in conductive material to protect devices from possible static damage.
6. Stresses above those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only and functional operation of the device at these or any other conditions above those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for exiended perlods may affect device rellablilty.

## Chopper-Stabilized Operational Amplifier

- Low Offset Voltage $5 \mu \mathrm{~V}$ Max.
- Low Supply Current 1.7 mA


## Theory of Operation

Figure 1 shows the major elements of the TSC7650A. There are two amplifiers, the main amplifier and the nulling amplifier; both have offset-null capability. The main amplifier is connected full-time from the input to the output. The nulling amplifier, under the control of the chopping frequency oscillator and clock circuit, alternately nulls itself and the main amplifier. Two external capacitors provide the required storage of the nulling potentials and the necessary nulling-loop time constants. The nulling arrangement operates over the full common-mode and power-supply ranges, and is also independent of the output level, thus giving exceptionally high CMRR, PSRR, and Avol.


Figure 1: TSC7650A Contains a Nulling and Main Amplifier. Offset Correction Voltages are Stored on Two External Capacitors.

Careful balancing of the input switches minimizes chopper frequency charge injection at the input terminals, and the feed forward-type injection into the compensation capacitor that can cause output spikes in this type of circuit.
The circuits offset voltage compensation is easily shown. With the nulling inputs shorted a voltage almost identical to the nulling amplifier offset voltage is stored on $\mathrm{C}_{\mathrm{A}}$. The effective offset voltage at the null amplifier input is:
(1) VOSE $=\frac{1}{A_{N}+1} \operatorname{VOSN}$

After the nulling amplifier is zeroed the main amplifier is zeroed; the A switches open and B switches close.
The output voltage equation is:
(2) $V_{O}=A_{M}\left[V_{O S M}+\left(V^{+}-V^{-}\right)+A_{N}\left(V^{+}-V^{-}\right)+A_{N} V_{\text {OSE }}\right]$

Substituting (1) $\rightarrow(2)$ and assuming $A_{N} \gg 1$.
(3)


As desired the device offset voltages are reduced by the high open-loop gain of the nulling amplifier.

## Output Stage/Load Driving

The output circuit is a high-impedance stage (approximately $18 \mathrm{k} \Omega$ ). With loads less than this the chopper amplifier behaves in some ways like a transconductance amplifier whose open-loop gain is proportional to load resistance. For example, the open-loop gain will be 17 dB lower with a $1 \mathrm{k} \Omega$ load than with a $10 \mathrm{k} \Omega$ load. If the amplifier is used strictly for dc the lower gain is of little consequence since the dc gain is typically greater than 120 dB even with a $1 \mathrm{k} \Omega$ load. In wideband applications, the best frequency response will be achieved with a load resistor of $10 \mathrm{k} \Omega$ or higher. This will result in a smooth $6 \mathrm{~dB} /$ octave response from 0.1 Hz to 2 MHz , with phase shifts of less than $10^{\circ}$ in the transition region where the main amplifier takes over from the null amplifier. The clock frequency sets the transition region.

## Intermodulation

Previous chopper-stabilized amplifiers have suffered from intermodulation effects between the chopper frequency and input signals. These arise because the finite ac gain of the amplifier results in a small ac signal at the input. This is seen by the zeroing circuit as an error signal, which is chopped and fed back, thus injecting sum and difference frequencies and causing disturbances to the gain and phase vs. frequency characteristics near the chopping frequency. These effects are substantially reduced in the TSC7650A by feeding the nulling circuit with a dynamic current, corresponding to the compensation capacitor current, in such a way as to cancel that portion of the input signal due to a finite ac gain. The intermodulation and gain/phase disturbances are held to very low values, and can generally be ignored.

## Nulling Capacitor Connection

The offset voltage correction capacitors are connected to $\mathrm{C}_{A}$ and $C_{B}$. The common capacitor connection is made to $V_{\bar{s}}^{-}$ (Pin 4) on the 8-pin packages and to capacitor return ( $\mathrm{C}_{\mathrm{R}}$, Pin 8) on the 14-pin packages. The common connection should be made through either a separate pc trace or wire to avoid voltage drops. The capacitors outside foil, if possible, should be connected to $\mathrm{C}_{\mathrm{R}}$ or $\mathrm{V}_{\overline{\mathrm{s}}}^{-}$.


Figure 2: Nulling Capacitor Connection

## Clock Operation

The internal oscillator is set for a 300 Hz nominal chopping frequency on both the 8 and 14 -pin dual in line packages. With the 14 -pin DIP TSC7650A, the 300 Hz internal chopping frequency is available at the internal clock output (Pin 12). A 600 Hz nominal signal will be present at the external clock input pin (Pin 13) with EXT/INT high or open. This is the internal clock signal before a divide by two operation.
The 14-pin DIP device can be driven by an external clock. The INT/EXT input (Pin 14) has an internal pull-up and may be left open for internal clock operation. If an external clock is used INT/EXT must be tied to $V_{\bar{s}}^{-}(\operatorname{Pin} 7)$ to disabie the internal clock. The external clock signal is applied to the external clock input (Pin 13).
The external clock amplitude should swing between $\mathrm{V}_{\mathrm{S}}^{+}$and ground for power supplies up to $\pm 6 \mathrm{~V}$ and between $\mathrm{V}^{+}$and $\mathrm{V}^{+}$ -6 V for higher supply voltages.
At low frequencies the external clock duty cycle is not critical since an internal divide by two gives the desired $50 \%$ switching duty cycle. The offset storage correction capacitors are charged only when the external clock input is high. A $50-80 \%$ external clock positive duty cycle is desired for frequencies above 500 Hz to guarantee transients settle before the internal switches open.
The external clock input can also be used as a strobe input. If a strobe signal is connected at the external clock input so that it is low during the time an overload signal is applied, neither capacitor will be charged. The leakage currents at the capacitor pins are very low. At $25^{\circ} \mathrm{C}$ a typical TSC7650A will drift less than $10 \mu \mathrm{~V} / \mathrm{sec}$.

## Output Clamp

Chopper-stabilized systems can show long recovery times from overloads. If the output is driven to either supply rail, output saturation occurs. The inputs are no longer held at a "virtual ground." The Vos null circuit treats the differential signal as an offset and tries to correct it by charging the external capacitors. The nulling circuit also saturates. Once the input signal returns to normal, the response time is lengthened by the Jong recovery time of the nulling amplifier and external capacitors.
Through an external clamp connection, the TSC7650A eliminates the overload recovery problem by reducing the feedback network gain before the output voltage reaches either supply rail.
The output clamp circuit is shown in Figure 3 with typical inverting and non-inverting circuit connections shown in Figure 4 and 5 . Output voltage vs clamp circuit current characteristics are shown in the typical operating curves. For the clamp to be fully effective, the impedance across the clamp output should be greater than $100 \mathrm{k} \Omega$.


Figure 3: Internal Clamp Circuit


Figure 4: Non-Inverting Amplifier with Optional Clamp


Figure 5: Inverting Amplifier with Optional Clamp

## Static Protection

All device pins are static-protected. Strong static fields and discharges should be avoided, however, as they can degrade diode junction characteristics and increase input-leakage currents.

Many companies are actively involved in providing services, educational material, and supplies to aid electronic manufacturers in establishing "static safe" work areas where CMOS components are handied. A partial company listing is:

- 3M

Static Control Systems Division
223-25W EM Center
St. Paul, MN 55101
(800) 792-1072

- Semtronics
P.O. Box 592

Martinsville, NJ 08836
(210) 561-9520

- American Convertors

1919 South Butlerfield Road
Mundelein, IL 60060
(312) 362-9000

- ACL

1960 East Devon Avenue
Elk Grove Village, IL 60007
(312) 981-9212

## Latch-Up Avoidance

Junction-isolated CMOS circuits inherently include a parasitic 4-layer (p-n-p-n) structure which has characteristics similar to an SCR. Under certain circumstances this junction may be triggered into a low impedance state, resulting in excessive supply current. To avoid the condition, no voltage greater than 0.3 V beyond the supply rails should be applied to any pin. In general, the amplifier supplies must be established either at the same time or before any input signals are applied. If this is not possible, the drive circuits must limit input current flow to under 0.1 mA to avoid latchup.

## Thermo-Electric Potentials

Precision dc measurements are ultimately limited by thermoelectric potentials developed in thermocouple junctions of dissimilar metals, alloys, silicon, etc. Unless all junctions are at the same temperature, thermoelectric voltages typically around $0.1 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$, but up to tens of $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ for some materials, will be generated. In order to realize the benefits extremely low offset voltages provide, it is essential to take special precautions to avoid temperature gradients. All components should be enclosed to eliminate air movement, especially those caused by power-dissipating elements in the system. Low thermoelectric-coefficient connections should be used where possible and power supply voltages and power dissipation should be kept to a minimum. High-impedance loads are preferable, and separation from surrounding heat-dissipating elements is advised.

## Pin Compatibility

On the 8-pin mini-dip TSC7650A the external null storage capacitors are connected to pins 1 and 8 . On most other operational amplifiers these are left open or are used for offset potentiometer or compensation capacitor connections.
For OP05 and OP07 operational amplifiers, the replacement of the offset null pot between pins 1 and 8 by two capacitors from the pins to $\mathrm{V}_{\mathrm{s}}^{-}$will convert the OP05/07 pin configuration for TSC7650A operation. For LM108 devices the compensation capacitor is replaced by the external nulling capacitors. The LM101/748/709 pin outs are modified similarly by also removing any circuit connections to pin 5. On the TSC7650A pin 5 is the output clamp connection. Other operational amplifiers may use this pin as an offset or compensation point.
The minor modifications needed to retrofit a TSC7650A into existing sockets operating at reduced power supply voltages make prototyping and circuit verification straight forward.

## Input Guarding

High impedance, low leakage CMOS inputs allow the TSC7650A to make measurements of high impedance sources. Stray leakage paths can increase input currents and decrease input resistance unless inputs are guarded. A guard is a conductive pc trace surrounding the input terminals. The ring connects to a low impedance point as the same potential as the inputs. Stray leakages are absorbed by the low impedance ring. The equal potential between ring and inputs prevents input leakage currents. Typical guard connections are shown in Figure 6.
The 14-pin DIP configuration has been specifically designed to ease input guarding. The pins adjacent to the inputs are unused.

In applications requiring low leakage currents, boards should be cleaned thoroughly and blown dry after soldering. Protective coatings will prevent future board contamination.

Chopper-Stabilized Operational Amplifier


Figure 6: Input Guard Connection


Gain $=1000,1$ Div $=20 \mu V_{p-p}$
Figure 7: TSC7650A Peak to Peak Noise (0.1 to 10Hz)

Chopper-Stabilized
Operational Amplifier

- Low Offset Voltage $5 \mu \mathrm{~V}$ Max.
- Low Supply Current 1.7 mA


## Typical Characteristic Curves

Positive Clamp Current vs Output Voltage


## Supply Current vs

Supply Voltage


Negative Clamp Current vs Output Voltage



Package Outline


# が TELEDYNE SEMICONDUCTOR 

## General Description

The TSC7650 CMOS chopper－stabilized operational ampli－ fier practically removes offset voltage error terms from sys－ tem error calculations．The $5 \mu \mathrm{~V}$ maximum Vos specification， for example，represents a fifteen times improvement over the industry standard OPO7E．The $50 \mathrm{nV} /{ }^{\circ} \mathrm{C}$ offset drift speci－ fication is over twenty－five times lower than the OPO7E．The increased performance eliminates Vos trim procedures， periodic potentiometer adjustment and the reliability prob－ lems caused by damaged trimmers．
The TSC7650 performance advantages are achieved without the additional manufacturing complexity and cost incurred with laser or＂zener zap＂Vos trim techniques．The TSC7650 is one of the lowest cost precision operational amplifiers available．
The TSC7650 nulling scheme corrects both dc Vos errors and Vos drift errors with temperature．A nulling amplifier al－ ternately corrects its own Vos errors and the main amplifier Vos error．Offset nulling voltages are stored on two user supplied external capacitors．The capacitors connect to the internal amplifier Vos null points．The main amplifier input signal is never switched．Switching spikes are not present at the TSC7650 output．The null scheme keeps Vos errors low throughout the operating temperature range．Laser and ＂zener zap＂trimming can correct for Vos at only one tem－ perature．
The nulling circuit oscillator and control circuits are inte－ grated on chip．Only two external Vos error storage capaci－ tors are required．The TSC7650 operates as a conventional operational amplifier with vastly improved input specifica－ tions．The low Vos and Vos drift errors make the TSC7650 ideal for thermocouple，thermistor，and strain gauge applica－ tions．Low dc errors and high open loop gain make the TSC7650 an excellent preamplifier for precision analog to digital converters like the TSC7135 and TSC800．
The 14－pin dual in line package（DIP）has an external oscillator input to drive the nulling circuitry for optimum noise performance．Both the 8 and 14 －pin DIP have an output voltage clamp circuit to minimize overload recovery time．

## Pin Configuration



## Features

－Low Input Offset Voltage ．．．．．．．．．．．．．．．．．．．．．．．．． $0.7 \mu \mathrm{~V}$
－Low Input Offset Voltage Drift ．．．．．．．． $0.05 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ Max．
－Low Input Bias Current ．．．．．．．．．．．．．．．．．．． 10 pA Max．
－High Impedance Differential CMOS Inputs ．．．．． $10^{12} \Omega$
－High Open Loop Voltage Gain ．．．．．．．．．．．． 120 dB Min．
－Low Input Noise Voltage ．．．．．．．．．．．．．．．．．．．．． $2.0 \mu \mathrm{Vp}$－p
－High Slew Rate ．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．． $2.5 \mathrm{~V} / \mu \mathrm{s}$
－Low Power Operation
20 mW
－Output Clamp Speeds Recovery Time
－Compensated Internally for Stable Unity Gain Operation
－Direct Replacement for ICL7650
－Available in 8－Pin Dip

## Ordering Information

| Part No． | Package | Temp． Range | Max． <br> Offset Voltage |
| :---: | :---: | :---: | :---: |
| ＊TSC7650CPA | 8－Pin <br> Plastic Dip | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ | $5 \mu \mathrm{~V}$ |
| ＊TSC7650IJA | $\begin{aligned} & \text { 8-Pin } \\ & \text { CerDIP } \end{aligned}$ | $-25^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | $5 \mu \mathrm{~V}$ |
| ＊TSC7650CPD | $\begin{aligned} & \text { 14-Pin } \\ & \text { Plastic Dip } \end{aligned}$ | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ | $5 \mu \mathrm{~V}$ |
| ＊TSC7650IJD | $\begin{aligned} & \text { 14-Pin } \\ & \text { CerDIP } \end{aligned}$ | $-25^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | $5 \mu \mathrm{~V}$ |

＊Available with 160 hour，$+125^{\circ} \mathrm{C}$ burn－in．Add／BI to part number suffix．
Functional Diagram
－FOR 8 PIN DIP CONNECT TO VĒ

Absolute Maximum Ratings
Total Supply Voltage ( $V_{s}^{+}$to $V_{\bar{s}}$ ) $\ldots \ldots . . . . . . . . .$. Input Voltage $\ldots \ldots . . . . . .\left(V_{s}^{+}+0.3\right)$ to $\left(V_{s}^{-}-0.3\right)$ Volts Storage Temp. Range $\ldots . . . . . . . . . . . . . .-55^{\circ} \mathrm{C}$ to $150^{\circ} \mathrm{C}$ Lead Temperature (Soldering, 10 sec ) ............. $300^{\circ} \mathrm{C}$ Voltage on Oscillator Control Pins .............. $V_{s}^{+}$to $\mathrm{V}_{s}{ }^{-}$
Output Short Circuit Duration .................. Indefinite
Current into Any Pin ............................... 10 mA

While Operating (Note 4) .......................... $100 \mu \mathrm{~A}$ Operating Temp. Range

| Device | $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |
| :---: | :---: |
| 1 Device | $-25^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
| C Device | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ | Package Power Dissipation ( $T_{A}=25^{\circ} \mathrm{C}$ )

CerDIP Package
500 mV
Plastic Package ................................... 375 mW

Electrical Characteristics: $\mathrm{V}_{\mathrm{S}}^{+}=+5 \mathrm{~V}, \mathrm{~V}_{\mathrm{S}}^{-}=-5 \mathrm{~V}, \mathrm{C}_{A}=\mathrm{C}_{\mathrm{B}}=0.1 \mu \mathrm{~F} . \mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$.

| TYPE | NO. | SYMBOL | PARAMETER | TEST CONDITIONS | MIN | $\begin{gathered} \text { TSC7650 } \\ \text { TYP } \\ \hline \end{gathered}$ | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \mathrm{I} \\ & \mathrm{~N} \\ & \mathbf{P} \\ & \mathbf{U} \\ & \mathbf{T} \end{aligned}$ | 1 | Vos | Input Offset Voltage | $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ | - | $\pm 0.7$ | $\pm 5.0$ | $\mu \mathrm{V}$ |
|  |  |  |  | Over Operating Temp. Range (Note 1) | - | $\pm 1.0$ | - |  |
|  | 2 | $\frac{\Delta V_{\text {OS }}}{\Delta T}$ | Input Offset Voltage Average Temp. Coefficient | Operating Temp <br> Range (Note 1) | - | 0.01 | 0.05 | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
|  | 3 |  | Offset Voltage vs Time |  | - | 100 | - | $\frac{n V}{\sqrt{\text { month }}}$ |
|  | 4 | IBIAS | Input Bias Current | $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ | - | 1.5 | 10 | pA |
|  |  |  |  | $0^{\circ} \mathrm{C} \leq T_{A} \leq+70^{\circ} \mathrm{C}$ | - | 35 | 150 |  |
|  |  |  |  | $-25^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+85^{\circ} \mathrm{C}$ | - | 100 | 400 |  |
|  | 5 | los | Input Offset Current | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ | - | 0.5 | - | pA |
|  | 6 | Enp-p | Input Noise Voltage | $\begin{aligned} & \text { Rs }=100 \Omega \\ & 0 \text { to } 10 \mathrm{~Hz} \end{aligned}$ | - | 2 | - | $\mu \mathrm{V}_{\mathrm{p}-\mathrm{p}}$ |
|  | 7 | in | Input Noise Current | $f=10 \mathrm{~Hz}$ | - | 0.01 | - | $\mathrm{pA} / \sqrt{ } \mathrm{Hz}$ |
|  | 8 | RIN | Input Resistance |  | - | 1012 |  | $\Omega$ |
|  | 9 | CMVR | Common-Mode Voltage Range |  | -5.0 | $\begin{array}{r} -5.2 \text { to } \\ +2.0 \end{array}$ | +1.6 V | V |
|  | 10 | CMRR | Common-Mode Rejection Ratio | $C M V R=-5 \mathrm{~V}$ to +1.5 V | 120 | 130 | - | dB |
| 0 | 11 | Av | Large-Signal Voltage Gain | $\mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega$ | 120 | 130 | - | dB |
| U | 12 | Vout | Output Voltage Swing (Note 3) | $\mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega$ | $\pm 4.7$ | $\pm 4.85$ | - | V |
| P |  |  |  | $R_{L}=100 \mathrm{k} \Omega$ | - | $\pm 4.95$ | - |  |
| $\mathbf{U}$ | 13 |  | Clamp ON Current (Note 2) | $\mathrm{R}_{\mathrm{L}}=100 \mathrm{k} \Omega$ | 25 | 70 | 200 | $\mu \mathrm{A}$ |
|  | 14 |  | Clamp OFF Current (Note 2) | -4.0 V < VOUT < + 4.0 V | - | 1 | - | pA |
| D | 15 | BW | Unity Gain Bandwidth | Unity Gain (+1) | - | 2.0 | - | MHz |
| Y | 16 | $S_{R}$ | Slew Rate | $\mathrm{C}_{\mathrm{L}}=50 \mathrm{pF}, \mathrm{R}_{\mathrm{L}}=10 \mathrm{k}$ | - | 2.5 | - | $\mathrm{V} / \mu \mathrm{s}$ |
| A | 17 | tr | Rise Time |  | - | 0.2 | - | $\mu \mathrm{s}$ |
| $\xrightarrow{\mathbf{M}}$ | 18 |  | Overshoot |  | - | 20 | - | \% |
| C | 19 | foh | Internal Chopping Frequency | Pins 12-14 Open (DIP) | 120 | 200 | 375 | Hz |
| S $\mathbf{U}$ $\mathbf{p}$ | 20 | $V_{S}^{+}$to $V_{S}^{-}$ | Operating Supply Range |  | 4.5 | - | 16 | V |
| P | 21 | Is | Supply Current | No Load | - | 2.0 | 3.5 | mA |
| $\underline{L}$ | 22 | PSRR | Power Supply Rejection Ratio | $V_{S}= \pm 3 \mathrm{~V}$ to $\pm 8 \mathrm{~V}$ | 120 | 130 | - | dB |

## Notes:

1. Operating temperature range is $-25^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ for " $I$ " grade and $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ for "C" grade.
2. See OUTPUT CLAMP discussion.
3. OUTPUT CLAMP not connected. See characteristic curves for output swing vs clamp current.
4. Limiting input current to $100 \mu \mathrm{~A}$ is recommended to avoid latch-up problems.
5. Static Sensitive Device. Unused devices must be stored in conductive material to protect devices from possible static damage.
6. Stresses above those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only and functional operation of the device at these or any other conditions above those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

# Precision Chopper-Stabilized Operational Amplifier 

## Theory of Operation

Figure 1 shows the major elements of the TSC7650. There are two amplifiers, the main amplifier and the nulling amplifier; both have offset-null capability. The main amplifier is connected full-time from the input to the output. The nulling amplifier, under the control of the chopping frequency oscillator and clock circuit, alternately nulls itself and the main amplifier. Two external capacitors provide the required storage of the nulling potentials and the necessary nullingloop time constants. The nulling arrangement operates over the full common-mode and power-supply ranges, and is also independent of the output level, thus giving exceptionally high CMRR, PSRR, and Avol.


Figure 1: TSC7650 Contains a Nulling and Main Amplifier. Offset Correction Voltages are Stored on Two External Capacitors.

Careful balancing of the input switches minimizes chopper frequency charge injection at the input terminals, and the feed forward-type injection into the compensation capacitor that can cause output spikes in this type of circuit.

The circuits offset voltage compensation is easily shown. With the nulling inputs shorted a voltage almost identical to the nulling amplifier offset voltage is stored on $\mathrm{C}_{A}$. The effective offset voltage at the null amplifier input is:
(1) $V_{\text {OSE }}=\frac{1}{A_{N}+1} \operatorname{VOSN}$

After the nulling amplifier is zeroed the main amplifier is zeroed; the A switches open and B switches close.

The output voltage equation is:
(2) $\mathrm{V}_{\mathrm{O}}=\mathrm{A}_{\mathrm{M}}\left[\mathrm{VOSM}_{\mathrm{O}}+\left(\mathrm{V}^{+}-\mathrm{V}^{-}\right)+\mathrm{AN}_{\mathrm{N}}\left(\mathrm{V}^{+}-\mathrm{V}^{-}\right)+\mathrm{AN}_{\mathrm{N}} \mathrm{V}_{\text {OSE }}\right]$

Substituting $(1) \rightarrow(2)$ and assuming $A_{N} \gg 1$.


As desired the device offset voltages are reduced by the high open-loop gain of the nulling amplifier.

## Output Stage/Load Driving

The output circuit is a high-impedance stage (approximately $18 \mathrm{k} \Omega$ ). With loads less than this the chopper amplifier behaves in some ways like a transconductance amplifier whose open-loop gain is proportional to load resistance. For example, the open-loop gain will be 17 dB lower with a $1 \mathrm{k} \Omega$ load than with a $10 \mathrm{k} \Omega$ load. If the amplifier is used strictly for dc the lower gain is of little consequence since the dc gain is typically greater than 120 dB even with a $1 \mathrm{k} \Omega$ load. In wideband applications, the best frequency response will be achieved with a load resistor of $10 \mathrm{k} \Omega$ or higher. This will result in a smooth 6 dB /octave response from 0.1 Hz to 2 MHz , with phase shifts of less than $10^{\circ}$ in the transition region where the main amplifier takes over from the null amplifier. The clock frequency sets the transition region.

## Intermodulation

Previous chopper-stabilized amplifiers have suffered from intermodulation effects between the chopper frequency and input signals. These arise because the finite ac gain of the amplifier results in a small ac signal at the input. This is seen by the zeroing circuit as an error signal, which is chopped and fed back, thus injecting sum and difference frequencies and causing disturbances to the gain and phase vs. frequency characteristics near the chopping frequency. These effects are substantially reduced in the TSC7650 by feeding the nulling circuit with a dynamic current, corresponding to the compensation capacitor current, in such a way as to cancel that portion of the input signal due to a finite ac gain. The intermodulation and gain/phase disturbances are held to very low values, and can generally be ignored.

## Nulling Capacitor Connection

The offset voltage correction capacitors are connected to $\mathrm{C}_{A}$ and $\mathrm{C}_{\mathrm{B}}$. The common capacitor connection is made to $\mathrm{VS}_{\mathrm{S}}^{-}$ ( $\operatorname{Pin} 4$ ) on the 8-pin packages and to capacitor return ( $C_{R}$, $\operatorname{Pin}$ 8) on the 14-pin packages. The common connection should be made through either a separate pc trace or wire to avoid voltage drops. The capacitors outside foil, if possible, should be connected to $\mathrm{C}_{\mathrm{R}}$ or $\mathrm{V}_{\mathrm{s}}^{-}$.


Figure 2: Nulling Capacitor Connection

## Clock Operation

The internal oscillator is set for a 200 Hz nominal chopping frequency on both the 8 and 14 -pin dual in line packages. With the 14 -pin DIP TSC7650, the 200 Hz internal chopping frequency is available at the internal clock output (Pin 12). A 400 Hz nominal signal will be present at the external clock input pin (Pin 13) with EXT/INT high or open. This is the internal clock signal before a divide by two operation.
The 14-pin DIP device can be driven by an external clock. Offset voltage and noise characteristics vs chopping frequency are shown in the typical operating characteristic curves. The INT/EXT input (Pin 14) has an internal pull-up and maybe left open for internal clock operation. If an external clock is used INT/EXT must be tied to $\mathrm{V}_{\mathrm{s}}^{-1}$ ( Pin 7 ) to disable the internal clock. The external clock signal is applied to the external clock input (Pin 13).
The external clock amplitude should swing between $V_{S}^{+}$and ground for power supplies up to $\pm 6 \mathrm{~V}$ and between $\mathrm{V}^{+}$and $\mathrm{V}^{+}$ -6 V for higher supply voltages.
At low frequencies the external clock duty cycle is not critical since an internal divide by two gives the desired $50 \%$ switching duty cycle. The offset storage correction capacitors are charged only when the external clock input is high. A $50-80 \%$ external clock positive duty cycle is desired for frequencies above 500 Hz to guarantee transients settle before the internal switches open.
The external clock input can also be used as a strobe input. If a strobe signal is connected at the external clock input so that it is low during the time an overload signal is applied, neither capacitor will be charged. The leakage currents at the capacitor pins are very low. At $25^{\circ} \mathrm{C}$ a typical TSC7650 will drift less than $10 \mu \mathrm{~V} / \mathrm{sec}$.

## Output Clamp

Chopper-stabilized systems can show long recovery times from overloads. If the output is driven to either supply rail, output saturation occurs. The inputs are no longer held at a "virtual ground." The Vos null circuit treats the differential signal as an offset and tries to correct it by charging the external capacitors. The nulling circuit also saturates. Once the input signal returns to normal, the response time is lengthened by the long recovery time of the nulling amplifier and external capacitors.
Through an external clamp connection, the TSC7650 eliminates the overload recovery problem by reducing the feedback network gain before the output voltage reaches either supply rail.
The output clamp circuit is shown in Figure 3 with typical inverting and non-inverting circuit connections shown in Figure 4 and 5 . Output voltage vs clamp circuit current characteristics are shown in the typical operating curves. For the clamp to be fully effective, the impedance across the clamp output should be greater than $100 \mathrm{k} \Omega$.


Figure 3: Internal Clamp Circuit


Figure 4: Non-Inverting Amplifier with Optional Clamp


Figure 5: Inverting Amplifier with Optional Clamp

## Static Protection

All device pins are static-protected. Strong static fields and discharges should be avoided, however, as they can degrade diode junction characteristics and increase input-leakage currents.

Many companies are actively involved in providing services, educational material, and supplies to aid electronic manufacturers in establishing "static safe" work areas where CMOS components are handled. A partial company listing is:

- 3M

Static Control Systems Division
223-25W EM Center
St. Paul, MN 55101
(800) 792-1072

- Semtronics
P.O. Box 592

Martinsville, NJ 08836
(210) 561-9520

- American Convertors

1919 South Butlerfield Road
Mundelein, IL 60060
(312) 362-9000

- ACL

1960 East Devon Avenue
Elk Grove Village, IL 60007
(312) 981-9212

## Latch-Up Avoidance

Junction-isolated CMOS circuits inherently include a parasitic 4-layer (p-n-p-n) structure which has characteristics similar to an SCR. Under certain circumstances this junction may be triggered into a low impedance state, resulting in excessive supply current. To avoid the condition, no voltage greater than 0.3 V beyond the supply rails should be applied to any pin. In general, the amplifier supplies must be established either at the same time or before any input signals are applied. If this is not possible, the drive circuits must limit input current flow to under 0.1 mA to avoid latchup.

## Thermo-Electric Potentials

Precision dc measurements are ultimately limited by thermoelectric potentials developed in thermocouple junctions of dissimilar metals, alloys, silicon, etc. Unless all junctions are at the same temperature, thermoelectric voltages typically around $0.1 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$, but up to tens of $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ for some materials, will be generated. In order to realize the benefits extremely low offset voltages provide, it is essential to take special precautions to avoid temperature gradients. All components should be enclosed to eliminate air movement, especially those caused by power-dissipating elements in the system. Low thermoelectric-coefficient connections should be used where possible and power supply voltages and power dissipation should be kept to a minimum. High-impedance loads are preferable, and separation from surrounding heat-dissipating elements is advised.

## Pin Compatibility

On the 8-pin mini-dip TSC7650 the external null storage capacitors are connected to pins 1 and 8 . On most other operational amplifiers these are left open or are used for offset potentiometer or compensation capacitor connections.
For OPO5 and OPO7 operational amplifiers, the replacement of the offset null pot between pins 1 and 8 by two capacitors from the pins to $\mathrm{V}_{\mathrm{s}}^{-}$will convert the OPO5/07 pin configuration for TSC7650 operation. For LM108 devices the compensation capacitor is replaced by the external nulling capacitors. The LM101/748/709 pin outs are modified similarly by also removing any circuit connections to pin 5 . On the TSC7650 pin 5 is the output clamp connection. Other operational amplifiers may use this pin as an offset or compensation point.
The minor modifications needed to retrofit a TSC7650 into existing sockets operating at reduced power supply voltages make prototyping and circuit verification straight forward.

## Input Guarding

High impedance, low leakage CMOS inputs allow the TSC7650 to make measurements of high impedance sources. Stray leakage paths can increase input currents and decrease input resistance unless inputs are guarded. A guard is a conductive pc trace surrounding the input terminals. The ring connects to a low impedance point as the same potential as the inputs. Stray leakages are absorbed by the low impedance ring. The equal potential between ring and inputs prevents input leakage currents. Typical guard connections are shown in Figure 6.
The 14-pin DIP configuration has been specifically designed to ease input guarding. The pins adjacent to the inputs are unused.
In applications requiring low leakage currents, boards should be cleaned thoroughly and blown dry after soldering. Protective coatings will prevent future board contamination.

## Precision Chopper-Stabilized Operational Amplifier



Figure 6: Input Guard Connection

## Typical Characteristic Curves



Positive Clamp Current vs Output Voltage

## Negative Clamp Current vs Output Voltage



Supply Current vs Supply Voltage


Gain/Phase vs Frequency


## Package Outline



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# Bipolar Interface Logic 

## Purpose of Bipolar Interface Logic

## PROTECTING CMOS AND $\mu$ P SYSTEMS

Bipolar Interface Logic - the 300 Series - is a remarkably simple solution to interfacing your CMOS and $\mu$ p systems (which operate on 12 or 15 V power supplies) with the outside world.

## OPERATION ON 11V TO 16V

These bipolar circuits have the unique ability to operate on 11 V to 16 V power supplies with an input threshold of 6 V , which allows noise margins from 3.5 V up to 6.5 V . This eliminates worry about the high-voltage spikes or noise generated by bouncing switches, SCR's, relays, solenoids or large motors. Also, the rugged bipolar construction of the 300 series minimizes catastrophic failures often caused by high voltage spikes or improper maintenance.

## LOW OUTPUT IMPEDANCE

With low output impedances, the 300 series can handle high drive currents of up to 250 mA , which makes them ideal for driving relays, solenoids, SCR's, displays or long lines.

## MANY SOLUTIONS OFFERED BY THE 300 SERIES

Teledyne Semiconductor's Bipolar Interface Logic line includes buffer gates, power drivers, timing elements and much more.


A detailed explanation of High Noise Immunity Bipolar Interface Logic and its uses can be found in Application Note 1.

## Bipolar Interface Logic Most Popular 300 Series Devices

POWER GATES

GATES
10mA SINK CURRENT


GND $=8$

HEX BUFFERS 10mA SINK CURRENT


334 STROBED


GND $=8$

VOLTAGE LEVEL TRANSLATORS

(15V TO 5V)

(5V TO 15 V )
$V_{C C}=16$
GND $=8$

## Most Popular 300 Series Devices



| DUAL RETRIGGERABLE ONE SHOT | TIMER FROM MICROSECONDS TO HOURS |
| :---: | :---: |
| $\begin{aligned} & V_{c c}=16 \\ & G N D=8 \end{aligned}$ |  |

## Additional Products:

- Digital Multiplexers
- Four Blt Comparators
- Decade Counters
- Up/Down Counters
- Quad D Flip Flops
- AND-OR-Invert Gates
- Dual, Triple and Quad Gates


# Bipolar Interface Logic Electrical Summary Data 

| Parameter | Definition | $\begin{gathered} \text { Type } \mathrm{C}^{*} \\ \left(\mathrm{~V}_{\mathrm{cc}}=+12 \mathrm{~V} \pm 1 \mathrm{~V}\right) \\ -30^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+85^{\circ} \mathrm{C} \\ \hline \end{gathered}$ | Test Conditions |
| :---: | :---: | :---: | :---: |
| V CC | Supply Voltage | 13 V max <br> 12 V nominal <br> 11 V min | (Voltage for other tests - see below) |
| VINL | Input Threshold Voltage, Low | 5.0 V min | Guaranteed input low threshold for all inputs except $311 \mathrm{~T}_{2}=$ 4.8 V min @ 15 V |
| VINH | Input Threshold Voltage, High | 6.5V max | Guaranteed input high threshold for all inputs except $311 \overline{\mathrm{~S}} \& \overline{\mathrm{R}}$ inputs $=$ 7.0V max |
| lint | Input Current, Low; 1 Unit Load (U) | UL) 2.1 mA max | At $\mathrm{V}_{\text {cc }}$ max with $\mathrm{V}_{\text {IN }}=\mathrm{V}_{\text {OL }}$ |
| IINH | Input Leakage Current; 1 Unit Load (UL) | $10 \mu \mathrm{~A}$ max | At $V_{C C C}=\max$ with $V_{I N}=V_{C C}$ max |
| Imax 382 | Output High Breakdown Current (Open Collector Devices) | 2 mA max | $\mathrm{V}_{\text {CEX }}=+65 \mathrm{~V}$ |
| Vol | Output Low Voltage (see Loading Table on Data Sheet) | 1.5 V max | IOL = F.O. $x$ UL at $V_{C C}$ min with $\mathrm{V}_{\mathrm{INL}}=5.0 \mathrm{~V}$ and $\mathrm{V}_{\mathrm{INH}}=6.5 \mathrm{~V}$ |
|   <br> VOL 302 <br>  323 <br>  332 <br>  334 <br>  380 <br>  382 <br>  383 <br>  383 | Output Low Voltage (Open Collector Devices) | .4 V max <br> 4 V max <br> 4 V max <br> 4 V max <br> 1.2V max <br> 2.5V max <br> .7V max <br> 1.2V max | $\begin{aligned} & \text { loL }=16 \mathrm{~mA}(10 \mathrm{TTL} \mathrm{UL}) \\ & \mathrm{lOL}=6.4 \mathrm{~mA}(4 \mathrm{TTL} \mathrm{UL}) \\ & \mathrm{lOL}=6.4 \mathrm{~mA}(4 \mathrm{TTL} \mathrm{UL}) \\ & \mathrm{lOL}=6.4 \mathrm{~mA}(4 \mathrm{TTL} \mathrm{UL}) \\ & \mathrm{loL}=30 \mathrm{~mA} \\ & \mathrm{loL}=7 \mathrm{~mA} \\ & \mathrm{loL}=20 \mathrm{~mA}(100 \% \text { Duty Cycle }) \\ & \text { loL }=40 \mathrm{~mA}(50 \% \text { Duty Cycle }) \end{aligned}$ |
| VOH | Output High Voltage of all Devices Without Open Collector Except 362 and 396 | s 10.0 V min | At $\mathrm{V}_{\mathrm{CC}} \min , \mathrm{V}_{\mathrm{INL}}=5.0 \mathrm{~V}, \mathrm{~V}_{\mathrm{INH}}=6.5 \mathrm{~V}$; IOH = F.O. $\times$ UL |
| $V_{\text {MAX }} 302,323$ 332,334 380 381 $390-395$ | Output High Breakdown Voltage (Open Collector Devices) | 13.0 V min 20.0 V min 24.0 V min 15.0 V min 30.0 V min | $\begin{aligned} & \operatorname{IMAX}=4 \mathrm{~mA} \\ & \text { IMAX }=4 \mathrm{~mA} \\ & \text { IMAX }=0.5 \mathrm{~mA} \\ & \text { IMAX }=0.5 \mathrm{~mA} \end{aligned}$ |
| VOHL | Output High Voltage, Loaded, of Active Pullup Devices Except 362 and 306 | 7.0 V min | $\begin{aligned} & \text { At } V_{\text {CC }} \text { nominal, } V_{I N L}=5.0 \mathrm{~V}, \\ & V_{I N H}=6.5 \mathrm{~V} ; \text { IOH }=-5 \mathrm{~mA} \text { (except } \\ & -15 \mathrm{~mA} \text { for } 301 \text { and }-12 \mathrm{~mA} \text { for } 350,351 \end{aligned}$ |
| ICEX $302,323,307$ <br> 332,334  <br> 380,381  <br> 382  <br>  383 <br>  $390-395$ | Output High Leakage Current (Open Collector Devices) | $25 \mu \mathrm{~A}$ max <br> $25 \mu \mathrm{~A}$ max <br> $25 \mu \mathrm{~A}$ max <br> $50 \mu \mathrm{~A}$ max <br> $25 \mu \mathrm{~A}$ max <br> $100 \mu \mathrm{~A}$ max | $\begin{aligned} & V_{C E X}=V_{C C} \text { max } \\ & V_{C E X}=V_{C C} \text { max } \\ & V_{C E X}=V_{C C} \text { max } \\ & V_{C E X}=+55 \mathrm{~V} \\ & V_{C E X}=V_{C C} \text { max } \\ & V_{\text {CEX }}=30 V \end{aligned}$ |
| "0" N.I. | Zero State Noise Immunity | 3.5 V min | Guaranteed zero state noise immunity across temp range and $V_{C C} \pm 1 \mathrm{~V}$. $\mathrm{V}_{\mathrm{INL}}$ - $\mathrm{V}_{\mathrm{OL}}$ |
| "I" N.I. | One State Noise Immunity | 3.5 V min | Guaranteed one state noise immunity across temp range and $\mathrm{Vcc} \pm 1 \mathrm{~V}$. $\mathrm{VOH}-\mathrm{V}_{\mathrm{INH}}$ |

Notes: F.O. is fanout in unit loads (UL). Unit loadings are given in the pin tables on the individual data sheets. A unit load for High Noise Immunity Logic is defined by the above input specifications.

See individual data sheets for additional specifications.
*Military spec Type $B(V C c=12 V)$ and Type $M(V C C=15 V)$ are available to meet $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ temperature requirements. Available in ceramic package only. See ordering data.

## Electrical Summary Data (Continued)

Absolute Maximum Ratings

| Storage Temperature | L Package, Ceramic | J Package, Plastic |
| :--- | :---: | :---: |
| Lead Temperature (1/16 inch from case, 10 sec max) | $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ | $-55^{\circ} \mathrm{C}$ to $+100^{\circ} \mathrm{C}$ |
| Continuous Supply Voltage | $300^{\circ} \mathrm{C}$ | $300^{\circ} \mathrm{C}$ |
| Type $\mathrm{C}^{*}, \mathrm{~B}^{*}$ |  |  |
| Type $\mathrm{A}^{*}, \mathrm{M}^{*}$ | +15.0 V | +15.0 V |
| Pulsed Supply Voltage (less than 100 msec ) | +16.5 V | +16.5 V |
| Input Voltage (any input) | +18.0 V | +18.0 V |
| Type $\mathrm{C}^{*}, \mathrm{~B}^{*}$ |  |  |
| Type A*, M | -0.5 to +15 V | -0.5 to +15 V |
| Surge Sink Current (less than 100 msec at $25^{\circ} \mathrm{C} \mathrm{TA)}$ | -0.5 to +18 V | -0.5 to +18 V |
| Standard Outputs |  |  |
| 301,302 and 303 | 20 mA | 20 mA |
| $306,307,332$ through $335,350,351,380,381,383$ | 100 mA | 100 mA |
| $390-395$ | 35 mA | 35 mA |
| 355 | 300 mA | - |
| Expander Input Currents | 150 mA | 150 mA |

Note: Exceeding the absolute maximum ratings may cause permanent damage. Function of HiNIL devices at the absolute maximum ratings or beyond the conditions guaranteed is not implied.

## Digital Logic - $\mathbf{3 0 0}$ Series Ordering Information

4. PACKAGE TYPE $\qquad$

L - Ceramic Package (CerDIP)
EXAMPLE: 303AL Operates Over an Industrial Temperature Range at 15 V and is a CerDIP Package

```
Product List - Digital Logic
301 Power NAND Gates Dual 5-Input
302 Power NAND Gates Quad 2-Input
303 Power NAND Gates Quad 2-Input
304 Power NAND Gates Triple 4, 3, 4-Input
3 0 6 ~ N O R ~ G a t e ~ Q u a d ~ 2 , ~ 2 , ~ 3 , ~ 3 - I n p u t ~
3 0 7 \text { NOR Gate Quad 2, 2, 3, 3-Input}
311 Flip Flops Master/Slave RST
312 Flip Flops Dual J-K Edge Triggered
313 Flip Flops Dual J-K Master/Slave
3 2 1 ~ N A N D ~ G a t e s ~ Q u a d ~ 2 - I n p u t
3 2 2 ~ N A N D ~ G a t e s ~ D u a l ~ 5 - I n p u t
3 2 3 ~ N A N D ~ G a t e s ~ Q u a d ~ 2 - I n p u t
3 2 4 ~ N A N D ~ G a t e s ~ Q u a d ~ 2 - I n p u t
325 NAND Gates 2, 2, 3, 3-Input
3 2 6 ~ N A N D ~ G a t e s ~ 2 , ~ 2 , ~ 3 , ~ 3 - I n p u t
331 Gate Expander Dual 5-Input
332 Hex Inverter Gates 4-Inverter, 2-NAND
333 Hex Inverter Gates 4-Inverter, 2-NAND
334 Hex Inverter Gates Strobed Hex NAND
335 Hex Inverter Gates Strobed Hex NAND
341 Multifunction Gates Dual 2-Wide, 2-Input
    and/or Invert
342 Dual Monostable Multivibrator
343 Digital Comparator 4-Bit
344 Multifunction Gates Dual Expandable AND-NOR
347 Dual Retriggerable Monostable Multivibrator
```

| 350 | Multiplexers 8-Bit |
| :--- | :--- |
| 351 | Multiplexers Dual 4-Bit |
| 355 | Timer |
| 361 | Dual 11 -16V to 5V Interface Voltage Translator |
| 362 | $5 V$ to 11-16V Interface Dual Translator |
| 363 | 5 V to 11-16V Interface Quad 2-Input NAND |
| 367 | Schmitt Trigger Quad(Active Pullup) |
| 368 | Schmitt Trigger Quad(Open Collector) |
| 370 | Flip Flop Quad D |
| 371 | Counters Decade |
| 372 | Counters Hexadecimal |
| 373 | Up-Down Counters Decade |
| 374 | Up-Down Counters Hexadecimal |
| 375 | Shift Register 4-Bit |
| 380 | BCD-to-Decade Decoder/Drivers Lamp Driver |
| 381 | BCD-to-Decade Decoder/Drivers Logic Driver |
| 382 | BCD-to-Decade Decoder/Drivers Gas Tube Driver |
| 383 | Decoder/Driver BCD-to-7 Segment |
| 390 | Dual Interface Buffers 4-Input Expandable AND |
| 391 | Dual Interface Buffers 2-Input AND |
| 392 | Dual Interface Buffers 2-Input NAND |
| 393 | Dual Interface Buffers 2-Input OR |
| 394 | Dual Interface Buffers 2-Input NOR |
| 395 | Dual Interface Buffers 4-Input Expandable NAND |
| 396 | Line Driver/Receiver Dual Differential |

## Input Current Requirements

Device
Number
$I_{\text {INL }} @ V_{C C}=12 \mathrm{~V}$
$\mathrm{~V}_{\mathrm{IL}}=1.5 \mathrm{~V}$ (mA)
$\mathrm{I}_{\mathrm{INL}} @ \mathrm{~V}_{\mathrm{cc}}=15 \mathrm{~V}$
$\mathrm{~V}_{\mathrm{IL}}=1.5 \mathrm{~V}(\mathrm{~mA})$

$$
\mathrm{I}_{\mathrm{INH}} @ V_{C C}=12 \text { or 15V, }
$$

$\frac{\mathrm{V}_{\mathrm{IL}}=1.5 \mathrm{~V}(\mathrm{~mA})}{2.6}$
$\frac{V_{\text {INH }}=V_{\text {CC }}(\mathrm{mA})}{10}$

302
2.1
2.6

10
303
$2.1 \quad 2.6$
10
304
2.1
2.6

10
306
1.3
1.6

10
307
1.3
1.6

10
311
312
313
2.1-4.2
2.6-5.2

10-20
2.6-5.2 10-20
2.6-5.2 10-20

321
322
2.1-4.2
2.1-4.2
2.6 10

323
2.1
$2.6 \quad 10$
324
2.1
2.6 10

325
2.1
2.6

10
326
2.1 2.6 10

332
2.1 2.6 10

333
2.1 2.6 10

334
$2.1 \quad 2.6 \quad 10$
335
2.1 $2.6 \quad 10$

341
2. 2.6 10

342
2.1
2.6

10
10

343
2.1
2.6

10
2.1-4.2
2.6-5.2
$10-20$
347
2.1-4.2
2.6-5.2

10-20
349
350
2.1
2.6

10
351
2.1
2.6

10
355
2.
2.6 10

361
0.01
0.01 10
$\begin{array}{lll}2.1 & 2.6 & 10\end{array}$
362
$0.47 \quad 0.47$
10
363
367
1.6
1.6

10
$\begin{array}{lll}2.1 & 2.6 & 40\end{array}$
$2.1 \quad 2.6 \quad 40$
370
371
372
373
374
375
2.1-4.2
2.1-4.2
2.6-5.2

10-20
$\begin{array}{lll}2.1-4.2 & 10-20 \\ 2.6-5.2 & 10-20\end{array}$
2.1
2.6 10
2.1
$2.6 \quad 10$
380
2.1
2.6 10

381
382
383
390
2.1
2.1
2.6 10
2.
2.6 10
2.1
2.6

10
2.1-6.3
2.6-7.8

10-30
0.7

391
0.7
1.0

10
392
0.7
1.0

10

393
0.7
1.0

10

394
0.7
1.0

10
0.7
1.0

10
395
0.7
1.0

10
396
0.4
1.0

10
Notes:

1. If there are several types of inputs on a device, then the currents listed above are the range of values for the various inputs.

Check the individual data sheets to determine what the input current requirements are for each input.
2. A unit load is defined as liNL @ $12 \mathrm{~V}=2.1 \mathrm{~mA}$ max, $\operatorname{liNL} @ 15 \mathrm{~V}=2.6 \mathrm{~mA}$ max and $\operatorname{liNH}=10 \mu \mathrm{~A}$ max at 12 or 15 V .
3. CMOS operated at 12 or 15 V can be used to drive these devices even if the VOL rating of the CMOS device does not appear to give enough sink current. This is possible since the 300 series of devices has input low rated at $\leq 5 \mathrm{~V}$ instead of 0.8 V as is common with TTL parts. The result is the CMOS output will be operated at a VoL larger than is typical for CMOS or TTL systems.

## Bipolar Interface Logic

## Output Sink Current vs. Output Voltage

| Device Number | $\mathrm{V}_{\text {OL }}$ (V) | $\mathrm{loL}(\mathrm{mA})$ | Device Number | $\mathrm{V}_{\text {OL }}(\mathrm{V})$ | 1 OL (mA) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 301 | 1.5 | 42 | 350 | 1.5 | 16 |
| 302 | . 4 | 42 | 351 | 1.5 | 16 |
| 303 | . 4 | 42 | 355 | 2.0 | 75 |
| 304 | . 4 | 42 | 361 | . 4 | 10 |
| 306 | 1.5 | 18 | 362 | . 4 | 10 |
| 307 | . 4 | 10 | 363 | . 4 | 30 |
| 311 | 1.5 | 12 | 367 | 1.5 | 10 |
| 312 | 1.5 | 10 | 368 | . 4 | 10 |
| 313 | 1.5 | 10 | 370 | . 4 | 10 |
| 321 | 1.5 | 10 | 371 | . 4 | 10 |
| 322 | 1.5 | 10 | 372 | . 4 | 10 |
| 323 | . 4 | 10 | 373 | 1.5 | 10 |
| 324 | . 4 | 10 | 374 | 1.5 | 10 |
| 325 | 1.5 | 10 | 375 | 1.5 | 6 |
| 326 | . 4 | 10 | 380 | . 4 | 20 |
| 332 | . 4 | 10 | 381 | . 4 | 10 |
| 333 | . 4 | 10 | 382 | 2.5 | 7 |
| 334 | . 4 | 10 | 383 | . 7 | 20 |
| 335 | . 4 | 10 | 390 | . 7 | 250 |
| 341 | 1.5 | 10 | 391 | . 7 | 250 . |
| 342 | 1.5 | 10 | 392 | . 7 | 250 |
| 343 | 1.5 | 10 | 393 | . 7 | 250 |
|  |  |  | 394 | . 7 | 250 |
| 347 | 1.5 | 10 | 395 | . 7 | 250 |
| 349 | 1.5 | 10 | 396 | 1.5 | 12 |

## Power Supply Current and Delay Times

| Device Number | $\begin{aligned} & \text { ICC } \\ & \text { 13V } \end{aligned}$ |  | ay Time 50\% | (W0\% Point Case) |
| :---: | :---: | :---: | :---: | :---: |
|  |  | $\underset{16 \mathrm{~V}}{(\mathrm{~mA})}$ | Low to High (ns) | High to Low (ns) |
| 301 | 48 | 68 | 340 | 400 |
| 302 | 40 | 60 | 600 | 240 |
| 303 | 49 | 70 | 600 | 240 |
| 304 | 49 | 70 | 600 | 240 |
| 306 | 34 | 40 | 600 | 100 |
| 307 | 34 | 40 | 600 | 100 |
| 311 | 18 | 25 | 820 | 610 |
| 312 | 30 | 40 | 300 | 230 |
| 313 | 30 | 40 | 300 | 230 |
| 321 | 15 | 20 | 300 | 200 |
| 322 | 8 | 11 | 550 | 190 |
| 323 | 5.5 | 8 | 400 | 160 |
| 324 | 28 | 40 | 600 | 200 |
| 325 | 15 | 20 | 300 | 200 |
| 326 | 28 | 40 | 600 | 200 |
| 332 | 28 | 42 | 350 | 140 |
| 333 | 42 | 60 | 350 | 140 |
| 334 | 28 | 42 | 350 | 140 |
| 335 | 42 | 60 | 350 | 140 |
| 341 | 11 | 15 | 410 | 150 |
| 342 | 17 | 23 | 260 | 160 |
| 343 | 42 | 56 | 1000 | 1000 |
| 344 | 11 | 15 | 600 | 200 |
| 347 | 40 | 50 | 650 | 750 |
| 350 | 33 | 40 | 400 | 250 |
| 351 | 33 | 40 | 400 | 250 |
| 361 | 8 | 11 | 325 | 230 |
| 362 | 10 | 13 | 400 | 160 |
| 363 | 51 | 64 | 600 | 240 |
| 367 | 36 | 54 | 400 | 300 |
| 368 | 33 | 50 | 600 | 340 |
| 370 | 38 | 48 | 750 | 750 |
| 371 | 41 | 53 | 800 | 300 |
| 372 | 41 | 53 | 800 | 300 |
| 373 | 50 | 55 | 1 mHz | Toggle |
| 374 | 50 | 55 | 1 mHz | Toggle |
| 375 | 48 | 64 | 600 | 550 |
| 380 | 24 | 31 | 500 | 400 |
| 381 | 30 | 38 | 500 | 400 |
| 382 | 24 | 31 | - | - |
| 383 | 24 | 31 | - | - |
| 390 | 38 | 40 | 500 | 200 |
| 391 | 38 | 40 | 500 | 200 |
| 392 | 38 | 40 | 500 | 200 |
| 393 | 38 | 40 | 500 | 200 |
| 394 | 38 | 40 | 500 | 200 |
| 395 | 38 | 40 | 500 | 200 |
| 396 | 23 | 25 | 650 | 80 |

## Bipolar Interface Logic



304 TRIPLE 4, 3, 4 INPUT NAND (PASSIVE PULL-UP)
$I_{C C}=40 \mathrm{~mA}(304 \mathrm{C}), 60 \mathrm{~mA}(304 \mathrm{~A})$
1 UL 20 UL 1 UL 1 UL 1 UL 1 UL 20 UL



311 MASTER/SLAVE FLIP-FLOP (ACTIVE PULL-UP)
${ }^{\prime} \mathrm{cC}=18 \mathrm{~mA}(311 \mathrm{C}) 25 \mathrm{~mA}(311 \mathrm{~A})$


1 UL 1 UL 1 UL 2 UL 1 UL 1 UL 1 UL


302 QUAD TWO INPUT POWER GATE (OPEN COLLECTOR)
${ }^{I} C C=40 \mathrm{~mA}$ (302C), 60 mA (302A) $\left.1 \mathrm{UL} 1 \mathrm{UL} 1 \mathrm{UL}{ }_{23} 28 \mathrm{UL}(\mathrm{C}) 1 \mathrm{~A}\right) 1 \mathrm{UL} 1 \mathrm{UL}$


306 2, 2, 3, 3 INPUT NOR GATE (ACTIVE PULL-UP)
$\mathrm{I}_{\mathrm{CC}}=34 \mathrm{~mA}(306 \mathrm{C}), 40 \mathrm{~mA}(306 \mathrm{~A})$


322 DUAL FIVE INPUT NAND GATE (ACTIVE PULL-UP)
${ }^{\prime} \mathrm{CC}=8 \mathrm{~mA}$ (322C), 11 mA (322A)
5 UL 1 UL 1 UL 1 UL 1 UL 1 UL


303 QUAD TWO INPUT POWER GATE (PASSIVE PULL-UP)
${ }^{\circ} \mathrm{CC}=49 \mathrm{~mA}(303 \mathrm{C}), 70 \mathrm{~mA}(303 \mathrm{~A})$ 1 UL IUL


307 2, 2, 3, 3 INPUT NOR GATE (OPEN COLLECTOR)
$\mathrm{I}_{\mathrm{CC}}=23 \mathrm{~mA}(307 \mathrm{C}), 28 \mathrm{~mA}(307 \mathrm{~A})$
1 UL 1UL $1 \mathrm{UL} 5 \mathrm{UL} \quad 1 \mathrm{UL} \quad 1 \mathrm{UL} 5 \mathrm{UL}$



313 DUAL J-K FLIP. FLOP
(ACTIVE PULL-UP)
${ }^{\prime} \mathrm{CC}=30 \mathrm{~mA}(312 \mathrm{C}) 40 \mathrm{~mA}(312 \mathrm{~A})$ 2 UL 5 UL 1 UL 1 UL 1 UL 5 UL 2 UL


323 QUAD TWO INPUT NAND GATE (OPEN COLLECTOR)
${ }^{\prime} \mathrm{CC}=5.5 \mathrm{~mA}$ (323C), 8 mA (323A)


324 QUAD TWO INPUT NAND GATE
(PASSIVE PULL-UP)
${ }^{1} \mathrm{CC}=28 \mathrm{~mA}(324 \mathrm{C}), 40 \mathrm{~mA}$ (324A)


331 dual five input gate expander ${ }^{\prime} \mathrm{CC}=4.2 \mathrm{~mA}(331 \mathrm{C}), 5.2 \mathrm{~mA}(331 \mathrm{~A})$


334 strobed hex inverter gate (OPEN-COLLECTOR) ${ }^{\prime} \mathrm{CC}=28 \mathrm{~mA}(334 \mathrm{C}) .42 \mathrm{~mA}(334 \mathrm{~A})$


342
DUAL MONOSTABLE MULTIVIBRATOR (ACTIVE PULL-UP)
${ }^{\prime} \mathrm{CC}=17 \mathrm{~mA}(342 \mathrm{C}), 23 \mathrm{~mA}(342 \mathrm{~A})$

$$
5 \mathrm{UL} \quad 5 \mathrm{UL} 1 \mathrm{UL}
$$



325 2, 2, 3, 3-INPUT NAND GATE
(ACTIVE PULL-UP)
${ }^{1} \mathrm{CC}=15 \mathrm{~mA}(325 \mathrm{C}), 20 \mathrm{~mA}(325 \mathrm{~A})$
1 UL 1 UL 1 UL 5 UL 1 UL 1 UL 5 UL


332 hex inverter gate (OPEN COLLECTOR)
ICC $=28 \mathrm{~mA}(332 \mathrm{C}), 42 \mathrm{~mA}(332 \mathrm{~A})$
1 UL 1 UL 7 UL 1 UL 7 UL 1 UL 7 UL



335 STROBED HEX INVERTER GATE (PASSIVE PULL-UP)
${ }^{1} \mathrm{CC}=42 \mathrm{~mA}(335 \mathrm{C}), 60 \mathrm{~mA}(335 \mathrm{~A})$ 2 UL 1 UL 5 UL 1 UL 5 UL 1 UL 5 UL


343 FOUR BIT COMPARATOR (ACTIVE PULL-UP)
${ }^{\prime} \mathrm{CC}=42 \mathrm{~mA}(343 \mathrm{C}), 56 \mathrm{~mA}(343 \mathrm{~A})$
$\mathrm{V}_{\mathrm{CC}} \overbrace{1 \mathrm{UL} 1 \mathrm{UL} 1 \mathrm{UL} 1 \text { UL } 1 \mathrm{UL} 2 \mathrm{UL} 2 \mathrm{UL}}$






368 QUAD SCHMITT TRIGGER (OPEN COLLECTOR) ${ }^{\prime} \mathrm{CC}=33 \mathrm{~mA}(368 \mathrm{C}), 50 \mathrm{~mA}(368 \mathrm{~A})$


## 349 dual retriggerable pulse stretcher (ACTIVE PULL-UP) $I_{\mathrm{CC}}=40 \mathrm{~mA}(349 \mathrm{C}), 50 \mathrm{~mA}(349 \mathrm{~A})$



355 TIMER
$\operatorname{lcc}^{\approx}=20 \mathrm{~mA}$


370 QUAD D FLIP.FLOP (PASSIVE PULL-UP)
${ }^{1} \mathrm{CC}=38 \mathrm{~mA}(370 \mathrm{C}), 48 \mathrm{~mA}(370 \mathrm{~A}$


350 EIGHT BIT MULTIPLEXER (ACTIVE PULL-UP)
${ }^{1} \mathrm{CC}=33 \mathrm{~mA}(350 \mathrm{C}), 40 \mathrm{~mA}(350 \mathrm{~A})$


361 dUAL INPUT INTERFACE (PASSIVE PULL.UP) ${ }^{\circ} \mathrm{CC}=8 \mathrm{~mA}(361 \mathrm{C}), 11 \mathrm{~mA}(361 \mathrm{~A})$


367 QUAD SCHMITT TRIGGER (ACTIVE PULL-UP) ${ }^{\circ} \mathrm{CC}=36 \mathrm{~mA}(367 \mathrm{C}), 54 \mathrm{~mA}(367 \mathrm{~A})$


371 DECADE COUNTER (PASSIVE PULL-UP) ${ }^{1} \mathrm{CC}=41 \mathrm{~mA}(371 \mathrm{C}), 53 \mathrm{~mA}(371 \mathrm{~A})$



375 FOUR BIT SHIFT REGISTER (ACTIVE PULL-UP)
${ }^{\prime} \mathrm{CC}=48 \mathrm{~mA}(375 \mathrm{C}), 64 \mathrm{~mA}(375 \mathrm{~A})$


382 bCD TO DECADE DECODER/GAS DISCHARGE (OPEN-COLLECTOR) TUBE DRIVER ${ }^{\prime} \mathrm{CC}=24 \mathrm{~mA}(382 \mathrm{C}), 31 \mathrm{~mA}(382 \mathrm{C})$


383 bCD TO SEVEN SEGMENT DECODER/DRIVER (OPEN-COLLECTOR) ${ }^{\prime} \mathrm{CC}=40 \mathrm{~mA}(383 \mathrm{C}), 44 \mathrm{~mA}(383 \mathrm{~A})$


374 HEXADECIMAL UP-DOWN COUNTER
$\mathrm{I}_{\mathrm{CC}}=50 \mathrm{~mA}(374 \mathrm{C}), 55 \mathrm{~mA}(373 \mathrm{~A})$
1 UL 1 UL 5 UL 1 UL 1 UL 5 UL 1 UL
COUNT COUNT
$\mathrm{V}_{\mathrm{CC}}$ COUNT COUNT $\mathrm{a}_{A}$ INA INB $\mathrm{a}_{B}$ LOAD


381 BCD TO DECADE DECODER/LOGIC DRIVER (OPEN COLLECTOR) ${ }^{\prime} \mathrm{CC}=30 \mathrm{~mA}(383 \mathrm{C}), 38 \mathrm{~mA}(383 \mathrm{~A})$


390 dual 4 INPUT POWER AND ${ }^{\prime} \mathrm{cc}=40 \mathrm{~mA}$


## Pin-Out Guide



39 DUAL 2 INPUT POWER NOR ${ }^{\prime} \mathrm{cc}=40 \mathrm{~mA}$


392 DUAL 2 INPUT POWER NAND $\mathrm{I}_{\mathrm{CC}}=40 \mathrm{~mA}$


395 DUAL 4 INPUT POWER NAND ${ }^{\prime} \mathrm{Cc}=40 \mathrm{~mA}$


393 DUAL 2 INPUT POWER OR ${ }^{\prime} \mathrm{Cc}=40 \mathrm{~mA}$


## 396 dUAL DIFF. LINE DRIVER/RECEIVER

 $I_{C C}=25 \mathrm{~mA}$

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## INTERFACING THE 8700 A/D CONVERTER WITH THE $8080 \mu \mathrm{P}$ SYSTEM

The growth of microcomputers has included an expansion into process monitoring and control systems, as well as other applications requiring interaction with "real world" physical variables. At the same time, advances in semiconductor technology have allowed complex datá conversión functions (A/D, D/A, V/F, etc.) to be performed by small and inexpensive IC's. By integrating these monolithic converter circuits into his microcomputer system, the designer thus can retain the same low cost and small size advantages which make the microprocessor so attractive.
In particular, the popular Intel 8080A microprocessor and Teledyne Semiconductor's 8700 series analog-to-digital converters are well suited to such a combination. This paper describes the basic techniques for interfacing the two, as well as ways to handle some more sophisticated situations.


Figure 1. 8700 Series Internal Elements

## THE 8700 A/D CONVERTER

Teledyne Semiconductor's 8700 series is a family of monolithic CMOS analog-to-digital converter IC's. All versions - the 87008 -bit, 8701 10-bit and 8702 12-bit - are integrating converters which can accept an unlimited input voltage range (changed to a current input by external scaling resistor) and provide a latched parallel binary digital output. All are available in 24 -pin ceramic DIP, and the 8 -bit version is also offered in a low-cost 24 -pin plastic package. As may be seen from the block diagram (Fig. 1), each device contains all of the essential elements for a complete A/D converter; only minimal support components are needed.

In addition to the 8, 10 or 12 buffered data output lines, three handshaking signals are provided to ease the interface to the host system. All outputs are CMOS and LPTTL compatible. The DATA VALID output signal is normally high, indicating that the data in the output latches is valid, for the entire cycle except for approximately $5 \mu \mathrm{~s}$ before the end of the conversion, when the data is being updated. Notice that the latches maintain the data from the previous conversion even while the next conversion is being performed. A second output, BUSY, is high whenever a conversion is being performed. Finally, an input to the device, INITIATE CONVERSION, allows the function to be operated under system control. A positive-going pulse of at least 500 ns duration causes the conversion to begin. If this input is tied high, the conversion will occur in a free-running mode at approximately 800 conversions per second for the 8700 (200 conv/sec for the 8701 and 50 conv/sec for the 8702).
Since the 8700 series devices operate from +5 V and -5 V supplies, they are particularly easy to interface with the 8080A microprocessor system. Fig. 2 shows a possible hook-up for the 8700's analog inputs and power supply; also


Figure 2. 8700 Analog Input and Power Supply Hook-up Circuits, Including VREF Derived from 8080A System
incorporated is a circuit to supply the necessary negative reference, using a temperature-compensated zener diode and an inverting op amp. Note that the $\pm 5 \mathrm{~V}$ supplies needed for the 8700 , as well as the additional +12 V used in the reference circuit, are all available from the 8080A system.
In order to simplify the hardware and software for illustrative purposes, this paper concentrates on interfacing the 8 -bit 8700 converter and the 8 -bit 8080A microprocessor system. The same principles apply to inter-connecting the 8080A with the higher-resolution 8701 and 8702 A/D converters.

## THE 8080A MICROPROCESSOR

The 8080A, an 8 -bit microprocessor, communicates within the microcomputer system over two buses, a 16 -bit address bus and an 8 -bit data bus. During each machine cycle the current contents of the program counter are sent out over the address bus; the memory receives the address and returns the contents of the selected memory location to the 8080A via the data bus. During an instruction fetch cycle, the returning data is interpreted as an instruction.
Communications between the microcomputer and the outside world are via Input/Output (I/O) ports addressed by the address bus. I/O instructions utilize 8 -bit addresses; the port address is duplicated on both the low order address lines and the high order address lines of the address bus.

In addition to the address and data buses, the 8080A communicates with the memory and I/O ports via a set of control signals. In particular two control lines, $\overline{\mathrm{IN}}$ and $\overline{\mathrm{OUT}}$, are used to enable the I/O ports. A logic 0 on the $\overline{\mathrm{N}}$ line will
enable the Input port that corresponds to the address on the address bus at that time. The OUT line functions in a similar fashion.

## THE BASIC 8700 I/O PORT

A basic approach to interfacing the 8080A and the 87008 -bit A/D converter is shown in Fig. 3. The conversion is started on command of the 8080A, using the INITIATE CONVERSION input of the 8700 . When the conversion is complete, the DATA VALID output of the A/D requests an interrupt; the interrupt service routine transfers the current data from the working registers to the stack memory, and the $A / D$ input port is read. A control signal then is sent to the INITIATE CONVERSION input to restart the conversion, and the main program activity is resumed.

It is assumed that the data bus will be shared by many devices, both in the ports and in memory, and that inverting drivers/receivers (such as 8228 ) will be included in the 8080 A system to service this bus. Therefore, 80 L 98 buffers have been provided at the 8700 to drive an inverted input over the data bus, as well as to provide a three-state function, electrically removing the $A / D$ from the bus when its input port has not been selected. (For applications where inverted signal and high bus-driving capability are not needed, Teledyne is offering a version of the 8700 with three-state outputs.)
Each port of the system is assigned an address by virtue of the way the address bus is decoded to select the port. In the basic input port of Fig. 3, the output of the 7430 gate is low only when all of its inputs are high. This corresponds to address $\mathrm{FFH}_{\mathrm{H}}$.


Figure 3. Basic 8700/8080A Interface

| IINITIATION |  |  |
| :---: | :---: | :---: |
| MVI | A, 98H | f THE CONVERSION |
| OUT | AFF4 | IIS INITIATED |
| MU: | A) 1 | f BY SENDING A |
| OUT | OFFH | ; BRIEF PULSE |
|  |  | ; TO PORT FF |
| I INTERRIJPT |  |  |
| PUSH | 8 | STHE PROCESSOR |
| PISH | D | BREGISTERS AND |
| Prst | H | ; STATUS ARE SAVED |
| PUSH | PSU | IIN THE STACK, AND THE |
| in | OFFH | j DATA IS READ AND |
| MOV | Q, $A$ | ; STORED IN REG B. |
| MUI | A, 30 H | ; THE CONVERSION IS |
| OUT | OFFH | IINITIATED AND |
| MVI | A, 8 | 1THE DATA 15 |
| OUT | GFFH | PPROCESSED. |
| - |  |  |
| - |  |  |
| - |  |  |
| POP PST 3 WHEN COMPLETE, |  |  |
| POP | H | ; THE REGISTERS |
| POP | D | ; ARE RESTORED, THE |
| POP B $\quad$ P INTERRUPTS ENABLED |  |  |
|  |  |  |
|  |  | ; CONTROL RETURNED |
| 3A |  | ; TO THE MAIN PROGRAM. |

To initiate a conversion in the $A / D$, an output port, also address $\mathrm{FFH}_{\mathrm{H}}$, is used. By defining both the input and output ports as address $\mathrm{FFH}_{\mathrm{H}}$, the same address decoder, the 7430, may be used for both functions. In this case the output of the 7430 and the OUT signal are gated by 7402 to clock half of a 74 C 74 flip-flop. The D input of the flip-flop is tied to the $\mathrm{D}_{7}$ line of the data bus. The flip-flop is, in effect, a one-bit output port. Sending the data word 80 H to port FFH with an output (OUT) instruction will cause the flip-flop to be set, thus supplying an INITIATE CONVERSION signal to the 8700. A second output instruction, sending $00_{\mathrm{H}}$ to the same port, will reset the flip-flop and remove the INITIATE CONVERSION signal. Since an output instruction requires ten $0.5 \mu \mathrm{sec}$ clock cycles to execute, the INITIATE conversion pulse will be approximately $5 \mu \mathrm{sec}$ long. After beginning the conversion process by the double output instructions, the 8080 A is free to perform other processing operations.
When the 8700 completes its conversion cycle and latches the result onto its internal output latches. the DATA VALID output goes high. This triggers the other half of the 74C74 flip-flop, clocking a logic one from the $D$ input (tied high) onto the INTERRUPT REQUEST line. The result is that the microprocessor is interrupted when the conversion is complete. The interrupt service routine (See Fig. 3A) saves the CPU's working register contents by pushing them onto the stack and then reads the output of the 8700.
To read the 8700 input port, it is necessary to supply the address of port $\mathrm{FFH}_{H}$ on the address bus while simultaneously sending out a logic zero on the $\overline{\mathbb{N}}$ control line. The combination of the 7430 and 7402 gates supplies a logic zero to the enabling input of the 80L98 three-state buffers on the outputs of the 8700 and to the clear input of the 74 C 74 flip-flop on the INTERRUPT line; this puts the 8700 data on the data bus and removes the interrupt request.
After reading the converter data and saving it in one of the registers, the system again pulses the INITIATE CONVERSION input to start the next conversion, restores the stack with a series of POP instructions, and resets the internal interrupt-enable flip-flop. Thus the 8080A only reads the 8700 when the new information becomes available; the rest of the time is spent in processing activities.

## HANDLING MULTIPLE A/D CONVERTERS

When multiple analog inputs are involved, conventional system designs have tended to use an analog multiplexer feeding a single high-speed $A / D$ converter. With the increasing availability of low-cost converter IC's, the approach of using a separate $A / D$ for each analog line becomes more attractive. Fig. 4 illustrates a system of eight 8700 converters all supplying data in parallel to an 8080A system.
The system illustrated in Fig. 4 contains many of the same elements as the basic input port of Fig. 3. As before, the data outputs of the 8700 s are buffered with 80L98 three-state buffers to drive the bus and to allow them to be disconnected. The decoding circuitry is slightly more complex. The five high-order address lines form the inputs to a 7430 gate which is used to enable a 7442 BCD to decimal decoder. The 7442 performs the final decoding by selecting the appropriate 8700 whenever an INPUT instruction is executed to one of the output ports $\mathrm{F8}$ H to FFH . Also, the 8700 s have their INITIATE CONVERSION inputs tied high so the devices operate in the free-running mode.
The interrupt scheme in this system is far more versatile than that previously illustrated. The user may assign priorities to each of the input ports, so that if one port has already interrupted the system and is being serviced, only a higher priority port can interrupt it. Lower priority interrupts will be delayed until the first port has been serviced.
Each of the eight interrupt input ports is constructed of a 74 L 74 flip-flop with its $D$ inputs wired high. Each flip-flop is clocked independently by lines from the appropriate 8700 DATA VALID output, transferring the logic one on the D input to the Q output. The $\overline{\mathrm{Q}}$ output of each flip-flop is gated onto the $\overline{\mathrm{NTT}} \overline{\mathrm{REO}}$ line producing an interrupt whenever one of the 8700's completes its cycle. The Q outputs of the flip-flops are buffered by the 8098 and tied to the data bus; this buffer is enabled by a 7430 and 7400 gates to respond to the INPUT instruction at address $7 \mathrm{~F}_{\mathrm{H}}$. The 8080A thus can determine which flip-flop has caused the interrupt and which of the 8700s has completed its conversion cycle.
The interrupt service routine (See Fig. 4A) saves the contents of the working registers with a series of PUSH instructions, and then proceeds to determine which port caused the interrupt. This is done with an input (IN) instruction to address 7 FH , which loads the status of the DATA VALID outputs from the 8098 into the accumulator. Here the word can be tested, bit by bit, until a logic one is found. This is then converted to the address of the correct 8700 input port and that port read with an input instruction. At the conclusion of the service routine, the flip-flop is reset by sending a zero to the appropriate bit position of the output port $7 \mathrm{~F}_{\mathrm{H}}$ which shares the same decoding circuitry as the input status port. Finally the stack is restored, and the internal interrupt enable flip-flop is reset.
There is nothing to prevent one of the 8700s from completing its conversion cycle and sending out a DATA VALID signal at the very time that another 8700 port has caused an interrupt and is in the process of being read. If this occurs, the flip-flop tied to the second port will be set and an additional interrupt signal generated. This will have no effect, however, since the


Figure 4. Eight Port A/D Converter System with Maskable Priority Interrupt

| ; THIS IS A PROGRAM FOR RESPONDING |  |  |  |
| :---: | :---: | :---: | :---: |
| ; TO AND SERUICING EIGHT INTERRUPTING |  |  |  |
| ; INPUT <br> POLLED: | PORTS ON A PRIORI |  | TY BASIS. |
|  | PUSH | B | ; SAVE PROCESSOR |
|  | PUSH | D | ; REGISTERS AND |
|  | PUSH | H | ; STATUS. |
|  | PUSH | PSW |  |
|  | IN | 7FH | PREAD INPUT PORT |
|  | MUI | D, $\varnothing$ | 3 TO FIND WHICH |
|  | STC |  | ; CAUSED INTERRUPT. |
|  | CMC |  | ; SET D TO ZERO |
|  |  |  | ; AND CARRY TO ZERO. |
| LOOP1: | RAL |  | ; DETERMINE WHICH |
|  | INR | D | ; PORT CAUSED INTERRUPT |
|  | JNC | LOOP1 | ; BY ROTATING ACCUMULATOR |
|  |  |  | ;LEFT AND TESTING |
|  |  |  | ; FOR PRESENCE OF |
|  |  |  | ; CARRY. INCREMENT |
|  |  |  | ; D EACH TIME. |
|  | $\begin{aligned} & \mathrm{L} \times \mathrm{I} \\ & \mathrm{~L} \times \mathrm{I} \end{aligned}$ | H. STABL$B, 3$ | ;LOAD H AND L WITH |
|  |  |  | ; STARTING ADDRESS |
|  |  |  | ; OF JUMP TABLE AND |
|  |  |  | ; AND C WITH 3. |
| LOOP2: | DAD | B | ; ADD B AND C TO |
|  | DCR | D | ; H AND L, DECREMENT D |
|  | $\begin{aligned} & \mathrm{JN} ? \\ & \mathrm{PCHL} \end{aligned}$ | LOOP2 | ; AND TEST FOR |
|  |  |  | ; ZERO. EXIT LOOP |
|  |  |  | ; BY TRANSFERRING |
|  |  |  | ITO APPROPRIATE |
|  |  |  | ; JUMP COMMAND |
|  |  |  | ; IN JUMP TABLE. |
| STABL: | $J M P$ | ONE | ; JUMP TABLE |
|  | JMP | TWO | ; CONSISTING OF |
|  | JMP | THREE | ; 3-BYTE JUMP |
|  | JMP | FOUR | ; INSTRUCTIONS. |
|  | JMP | FIVE |  |
|  | JMP | SIY |  |
|  | JMP | SEVEN |  |
|  | JMP | EIGHT |  |


| RSTR: |  | POP |  | PSW | ; RESTORE REGISTERS |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | POP |  | H | ; AND EXIT. |
|  |  | POP |  | D |  |
|  |  | POP |  | B |  |
|  |  | RET |  |  |  |
| ONE: |  | IN |  | 9FSH | ; THIS IS THE |
|  |  | MOV |  | B, A | ; SERUICE ROUTINE |
|  |  | MUI |  | OFEH | ;FOR PORT I. |
|  |  | OUT |  | 7FH | ; IT LOADS THE |
|  |  | EI |  |  | ; PRIORI TY MASK |
|  |  | - |  |  | ; WITH 1111 1110, |
|  |  | - |  |  | ; ENABLES INTERRUPTS |
|  |  | - |  |  | ; AND PROCESSES |
|  |  | - |  |  | ; DATA. AT CONCLUSION, |
|  |  |  |  |  | ; THE PROGRAM JUMPS |
|  |  | JMP |  | RSTR | ; TO RSTR. |
| TWO: |  | IN |  | OF9H | ; THIS IS THE |
|  |  | MOV |  | B, $A$ | ; ROUTINE FOR |
|  |  | MUI |  | DFCH | ; PORT *2. THE |
|  |  | OUT |  | 7 FH | ; PRIORI TY MASK |
|  |  | EI |  |  | 3 IS 11111100 WHICH |
|  |  | - |  |  | ; KEEPS PORT 1 |
|  |  | - |  |  | ; FROM INTERRUPTING. |
|  |  | - |  |  |  |
|  |  | - |  |  |  |
|  |  | MP |  |  |  |
|  |  | JMP |  | RSTR |  |
| $\begin{aligned} & \text {; THE } \\ & \text {; ARE } \end{aligned}$ |  | BALANCE | OF | THE | ICE ROUTINES |
|  |  | OMI TTED | FOR | R BREV |  |

Figure 4A

8080A's internal-interrupt enable flip-flop is automatically disabled when the first interrupt is received, locking out any further interrupts. (This flip-flop must be reset with an EI instruction, Enable Interrupts.) The first interrupt service routine ends with the resetting of the status flip-flop and the enabling of the internal interrupt enable flip-flop. This removes the source of the first interrupt, but the second status flip-flop now causes a new interrupt which must be serviced in turn. The 8080A will respond to each of the input ports as they complete their cycles, even if several occur in a short period.

So far we have assumed that each of the 8700 ports is of equal importance. When we wish to assign priorities to the ports, it is only necessary to make a slight change in the program - no hardware changes are needed. This is done by holding the reset inputs of selected data valid flip-flops low, which effectively serves to inhibit those ports from causing interrupts. The output port 7F accomplishes this by having its latches loaded with a binary word called a priority mask. Each interrupt service routine begins by loading a different priority mask into the output port and resetting the internal enable interrupt flip-flop. For example, if the priority mask for port number 3 is 11111100, port number 1 and 2 cannot interrupt the processing of port number 3 data; ports number 4 through number 8, however, can cause further interrupts.

If it is necessary to guarantee that no data is ever lost, a slight modification places the conversion cycle under the control of the CPU. This is done by tying the reset inputs of the status flip-flops to the INITIATE CONVERSION inputs of the corresponding 8700's. The process of resetting the status flip-flop after the port has been read will cause the cycle to restart. This has the effect of holding the data on the output latches of the 8700's until it has been read.

## INCREASING THE THROUGHPUT

If a great deal of data manipulation is to be done by the 8080 A or a large number of 8700 input ports are to be connected to the bus, it is possible to feed data to the system faster than it can be processed. If the analog inputs on some of the ports are changing slowly, additional logic can be added to increase the effective capacity of the system. This involves adding a latching output port with the same address as the 8700 input port corresponding to it. (See Fig. 5) After the input port is read initially, an output instruction to the same
address causes the data to be duplicated in the 74175 latches. The open collector feature of the 9386 allows them to be collector-ORed; logic ones at all of their outputs signify that the data in the 8700 latches matches that in the output port. This condition means there has been no change in the analog input voltage and there is no need to reprocess the data. If one of the bits of the 8700 does not match the corresponding bit in the 74175, a zero will be produced on the outputs of the 9386. This will deliver a clock pulse to the 7474 status flip-flop which will in turn interrupt the 8080A. From this point the operation is similar to the system already discussed.


Figure 5. Significant Change Interrupt for 8700 Input Port

# Application Note 9 Applications of the TSC8700 Series CMOS A/D Converters By Michael O. Paiva \& John Blake 

## LED PANEL METER

| 12345678 | 16 | 24 | 32 | 40 | 48 | 56 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |

000000000000000000000000000000000000000000000000000000000000000


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## RATIOMETRIC APPLICATIONS



3½ DIGIT AID WITH GAS DISCHARGE DISPLAY


## OVERRANGE INDICATOR



## UNDERRANGE INDICATOR



## AID WITH TWO STEP AUTORANGE



DUAL $3 ½$ DIGIT LED DISPLAY



## ANALOG PEAK DETECTOR WITH DIGITAL HOLD



Analog peak detection is accomplished by repeatedly measuring the input signal with an A/D converter and comparing the current reading with the previous reading. If the current reading is larger than the previous, the current reading is stored in the latch and becomes the new peak value. Since the peak is stored in a CMOS latch, the peak can be stored indefinitely.

The TELEDYNE 8700 A/D converter measures the analog input at a 1 KHz rate and computes the binary value of the input. After each 1 ms measurement, the binary value is
ched in the output of the A/D. This value is then presented to both the 4585 comparators and the 45088 -bit latch. If the A/D's value is greater than that of the 4508 memory, pin $13(A>B)$ of the 4585 goes high. This allows the strobe
pulse to go through the 4001 NOR gate to the 4508 memory. The new value is then stored and becomes the reference for subsequent readings. Each time the A/D has a value greater than that stored in the latch, the latch is updated with the larger peak. The system is reset by pulsing the 4508 reset pin high, causing the output to go to 0000 0000.

This system uses an 8 -bit A/D to give $0.4 \%$ resolution. If greater resolution is required, the 8700 can be replaced by the 8701 (10-bit) for $0.1 \%$ resolution or the 8702 (12-bit) for $0.025 \%$ resolution. Since this will require 10 or 12 bits to be compared instead of 8 , the memory and comparator need to be expanded by adding one additional 4508 and one 4585.

## 8-CHANNEL DATA ACQUISITION SYSTEM



A low-cost data acquisition system with 8 inputs and 8 bits ( $0.4 \%$ ) of resolution at the ouput can be built by using the TELEDYNE 8700 CMOS A/D converter and adding the 4051 8 channel CMOS multiplexer and the 4024 binary counter.

Each input is measured for 1 ms , then the digital value is placed in the output latch and remains for 1 ms while the next input is being measured. After each 1 ms measurement (conversion), the data valid line goes low for $5 \mu \mathrm{~s}$ to indicate that the output latch is being updated. (The data must not be read during this period.) The negative edge of the data valid pulse is used to advance the binary counter by one. So after each conversion the 4051, via the 4024, automatically advances to the next input. The sampling sequence is therefore $\mathrm{V}_{1}, \mathrm{~V}_{2}, \ldots \mathrm{~V}_{7}, \mathrm{~V}_{0}$ and then back to $\mathrm{V}_{1}$. The 8700 resets itself for $2.5 \mu \mathrm{~s}$ after the data valid pulse so the analog switch has a total of $7.5 \mu \mathrm{~s}$ to settle down. This is more than adequate to assure that the A/D will ignore any switching transients.

For the circuit shown, the input voltage range is limited by the 4051 to $\pm 5$ volts (VDD, VEE). If more input voltage range
is needed, then $V_{S S}$ and $V_{E E}$ can be increased or the $1 M \Omega$ resistor can be replaced by individual resistors in front of each analog input. The exact value of each resistor is determined by dividing the maximum input voltage by $5 \mu \mathrm{~A}$. $\left(R_{I N}=V_{\text {max }} \div 5 \mu \mathrm{~A}\right)$.

The 950 K and 100 K resistor are used to provide an offset current of $5 \mu \mathrm{~A}$, allowing the analog input voltage to be negative as well as positive. If the input voltage does not go negative, then these two resistors can be deleted.

By adding additional 4051's, the number of analog inputs can be increased in multiples of eight. The additional binary outputs of the 4024 are then simply decoded to control the inhibit (1) input of each 4051.

If three-state outputs are needed for interfacing to a data buss, then the 8700 can be replaced by the 8703 . The 8703 is identical to the 8700 except that the digital data outputs are three-state outputs controlled by pin 24 (ENABLE).

$\vec{v}$

## 8700 PC BOARD METAL PATTERN

 PC BOARD FOR 1, 8, 16 CHANNEL DATA ACQUISITION SYSTEMREDUCE TO $5.000 \pm .005$

BACK SIDE

Note: PC board can be ordered from Teledyne as part \#8700PC


STANDARD TEST CIRCUIT


A/D WITH 8-CHANNEL ANALOG INPUT SELECTOR


## ASSEMBLY INFORMATION

8-CHANNEL DATA ACQUISITION SYSTEM


16-CHANNEL DATA ACQUISITION SYSTEM


| Ref \# | Part Number | Description |
| :---: | :---: | :---: |
| IC1, IC2 | 4051 | CMOS - 8 CHANNEL ANALOG SWITCH |
| IC3 | 8700 TYPE | CMOS - TELEDYNE AID CONVERTER |
| IC4 | 4024 | CMOS - 7 bit BINARY COUNTER |
| IC5 | 4011 | CMOS - QUAD 2-INPUT NAND GATE |
| C1 | $68 \mathrm{pF} \pm 10 \%$ | Low leakage mica, ceramic, etc. |
| C2 | 270pF $\pm 20 \%$ | Ceramic, mica, etc. |
| C3, C4, C5 | $0.1 \mu \mathrm{~F} \pm 20 \%$ | Ceramic, mylar, electrolytic, tantalum, etc. |
| R1 | * 953K $\pm 1 \%$ | Carbon, carbon film, metal film, etc. |
| R2 | * 100K $\pm 10 \%$ | Trimmer resistor |
| R3 | * $1 \mathrm{M} \Omega \pm 1 \%$ | Carbon, carbon film, metal film, etc. |
| R4 | 100 $\pm 10 \%$ | Carbon resistor |
| R5 | 20K $\pm 10 \%$ | Trimmer resistor |
| R6 | $100 \mathrm{~K} \pm 5 \%$ | Carbon resistor |
| R7 | $1 \mathrm{~K} \pm 5 \%$ | Carbon resistor |
| R8 | 100K $\pm 10 \%$ | Carbon resistor |
| R9 | * 20K $\pm 10 \%$ | Trimmer resistor |
| R10 | * 243K $\pm 1 \%$ | Carbon, carbon film, metal film, etc. |


#### Abstract

$\star$ The stability of these components directly affects the accuracy of the overall system. Choose components whose stability is consistent with the accuracy and temperature range required. For example, if an 8 -bit $\mathrm{A} / \mathrm{D}$ is used at a constant temperature, then $5 \%$ carbon resistors may be adequate since an 8 -bit A/D's resolution is only $0.4 \%$. However, if a 12 -bit A/D ( $0.025 \%$ resolution) is to be used over the $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ temperature range, then these components will be verg' critical and shouid have a stability of 5 to 15 ppm for fixed resistors and 25 to 50 ppm for variable resistors.


The following parts list of possible suppliers is intended to be of assistance in putting a converter design into production. It should not be interpreted as a comprehensive list of suppliers, nor does it constitute an endorsement by Teledyne Semiconductor.

## TYPICAL COMPONENT SOURCES FOR PRECISION APPLICATION

A. Precision fixed resistors

| Value | Tol. |  | Typical Source |  | Type |
| :--- | :--- | :--- | :--- | :--- | :--- |

B. Variable resistors

| $20 \mathrm{~K} / 100 \mathrm{~K}$ | $\pm 10 \%$ | Mepco/Electra | 8035 | $\pm 100 \mathrm{ppm}$ |
| :--- | :--- | :--- | :--- | :--- |
| $20 \mathrm{~K} / 100 \mathrm{~K}$ | $\pm 10 \%$ | Spectrol | 43 P | $\pm 100 \mathrm{ppm}$ |

C. Capacitors

| 68 pF | $\pm 10 \%$ | Union Carbide | C114K680K1X1CA | $\pm 800 \mathrm{ppm}$ |
| :--- | :--- | :--- | :--- | :--- |
| 68 pF | $\pm 10 \%$ | Union Carbide | C114G680K565CM | $\pm 30 \mathrm{ppm}$ |
| 68 pF | $\pm 5 \%$ | Corning | CY06C680G | $\pm 25 \mathrm{ppm}$ |

## DESIGN INFORMATION

## 1. AVOID INTRODUCING ERRORS:

Proper design procedures are necessary to obtain best accuracy from 8700 series converters.
a. Do not route logic signals under the 8700 or near any of the three analog terminals IIN, IREF, and Zero Adjust (pins 13, 14, 15, 16).
b. Plan your grounding. Keep the analog ground isolated from the logic ground by making the two electrically common only at the system ground.
c. Filter the supply voltages by using bypass capacitors of value $0.1 \mu \mathrm{~F}$ or greater connected in shunt between the supply line and the logic ground (pin 20). Locate the capacitors as close as to the 8700 as practical.
d. Provide a reference as stable as the conversion accuracy you expect. Remember:

DIGITAL COUNTS $=\frac{I_{I N}}{I_{\text {REF }}} \bullet A=\frac{V_{I N} \div R_{I N}}{V_{\text {REF }} \div R_{R E F}} \bullet A$

The conversion accuracy is a direct function of the $V_{\text {REF }}$. In terms of $V_{\text {REF }}$ voltage regulation, the 8-bit requires $\pm .04 \%$, the $10-\mathrm{bit}, \pm .01 \%$, the 12 -bit, $\pm .0025 \%$, and the $31 / 2$ digit BCD, $\pm .005 \%$,to introduce less than $1 / 10$ LSB error.
e. Choose a full scale voltage range as large as possible; this will minimize the effect of zero drift and input noise. For example, a $50 \mu \mathrm{~V}$ zero drift or noise voltage on the 8701 (10-bit) will produce a $\pm 1 / 2$ LSB error at 500 mV full scale, but only $\pm 1 / 40$ LSB at 10 V full scale.
2. OTHER SUGGESTIONS FOR IMPROVING PERFORMANCE:
a. For CINT, virtually any type of non-polarized 68pF $\pm 10 \%$ is acceptable. Locate as near to the converter as possible and away from noisy lines.
b. Locate RDAMP and CDAMP as near the converter as possible and away from noisy lines. The value of RDAMP $=100 \Omega$ and $C_{D A M P}=270 \mathrm{pF}$ are nominal; these two elements stabilize the input op amp to prevent oscillations.
3. CAUTION: WHEN USING ZENERS, OP AMPS AND VOLTAGE REGULATORS:

These devices are often used as input amplifiers, voltage references and power supplies for A/D converters. It is worth noting that these devices can generate quite a bit of "High Frequency" noise. Normally, this noise does not interfere with the operation of the A/D converter. However, excessive noise from zeners, used as voltage references for example, have been found to be the cause of strange counting sequences and non-linear A/D operation. It should therefore be standard practice to bypass all zeners and voltage regulators with at least $0.1 \mu \mathrm{~F}$ capacitors. (If the zener is exceptionally noisy, 1 to $10 \mu \mathrm{~F}$ capacitors may be required. Remember that zeners are often used as white noise sources in noise generators.)

If erratic operation is still observed, then either the op amp's feedback resistor or the output should be bypassed. Note also that the noise level of zeners, op amps and voltage regulators varies from lot to lot and especially from one manufacturer to another. Bypassing these devices during the design stage will prevent the noise level variation from becoming a possible production problem.



## NEGATIVE SUPPLY GENERATOR



OUTPUT VOLTAGE VS OUTPUT CURRENT

A negative voltage for $V_{S S}$ and $V_{\text {REF }}$ can be generated from the positive supply by using a hex inverter as a free running oscillator to drive a voltage doubler. The five inverters are paralleled to provide a low output impedance. Since the 4049 is a standard 4000 CMOS part, the circuit can be operated from 3 to 15 volts. $10 \mu \mathrm{~F}$ capacitors were used in order to minimize output ripple at low $\mathrm{V}+$ voltages.

When higher input voltages ( $\mathrm{V}+$ ) are available the $10 \mu \mathrm{~F}$ capacitors can be lowered to 1 or $0.1 \mu \mathrm{~F}$ depending on the output loading. If this circuit generates more voltage than is needed, one half of the diodes and capacitors can be eliminated to reduce cost. The output voltage will then be one half of that shown in the graph and is available on the negative side of the $10 \mu \mathrm{~F}$ capacitor connected to ground.


The Teledyne Semiconductor 8700 series are integrating AID converters. These are available with 8-, 10-, or 12-bit resolutions, with or without three-state outputs, and
also in a $31 / 2$ digit parallel BDC format. Individual data sheets are available from Teledyne Semiconductor.

Application Note 10 Applications of the TSC9400 Voltage to Frequency Frequency to Voltage Converter By Michael O. Paiva

## RATIOMETRIC MEASUREMENT

(ANALOG DIVISION)


OUTPUT $=N \frac{V_{1}}{V_{2}}$

One of the most difficult circuits to build is one which will divide one analog signal by another. Two V/F converters can
do such division with ease. The numerator is counted directly as a signal, while the denominator forms the time base.


Flow rates and revolutions per second are nothing more than frequency signals since they measure the number of events per time period. Optical and magnetic sensors will convert these flows and revolutions into a digital signal which in turn can be
converted to a proportional voltage by the use of an $\mathrm{F} / \mathrm{V}$ converter. A simple voltmeter will then give a visual indication of the speed.


The motor's speed is measured with the F/V, which converts RPM into a proportional voltage. This voltage is used in a
negative feedback system to maintain the motor at the controlled setting.


A $9400 \mathrm{~F} / \mathrm{V}$ can be used to regulate the amount of liquid or gas flowing through a pipeline.

The flow rate detector generates a pulse train whose frequency is proportional to the rate of flow through it. The F/V con-
verts this frequency to a proportional analog voltage which is used to drive the valve controller. The valve controller regulates the valve so that the flow is steady even though pipeline pressure goes up and down. A voltmeter connected to the F/V output will indicate the actual instantaneous flow rate.

## TEMPERATURE METER



A temperature meter using the voltage output of a probe, such as one of the three shown, can be economically and straightforwardly implemented with the $9400 \mathrm{~V} / \mathrm{F}$. The V/F output is simply counted to display the temperature.

For long distance data transmission, the 9400 can be used to modulate an RF transmitter.

## A/D CONVERSION WITH A MICROPROCESSOR



There are two schemes that can be utilized to accomplish $A / D$ conversion with a microprocessor:

1. Depending on the number of digits of resolution required, VOUT is measured by counting the V/F frequency for 1 ms , $10 \mathrm{~ms}, 100 \mathrm{~ms}$, or 1 second. The final count is then directly proportional to the input voltage. (The microprocessor provides the time base.)
2. $V_{I N}$ is measured by determining the time between two pulses (negative edges). The FOUT signal is used as a gate
for counting the microprocessor's clock. The final count will then be inversely proportional to the input signal.

By taking the one's complement (changing 1's to 0 's and 0 's to 1 's) of the final binary count a value directly proportional to the input will result.

This technique will give a faster conversion time when resolution is very important, but dynamic range is limited.

13 BIT A/D CONVERTER


A 13 bit binary or 4 digit BCD A/D converter can be built by combining the $9400 \mathrm{~V} / \mathrm{F}$ with a counter, latch and time
base. When the V/F is set up for 10 KHz full scale a 1 second time base will provide one conversion per second.

## 4 DIGIT VOLTMETER W/OPTO-ISOLATED INPUT



The use of a frequency counter will give a display of the $\mathrm{V} / \mathrm{F}^{\prime} \mathrm{s}$ frequency which is directly proportional to the input voltage.

When the $\mathrm{V} / \mathrm{F}$ is running at 10 KHz full scale, a 0.1 second time base will give 3 digit resolution with 10 readings per second.

The opto isolator is used for transmitting the frequency so that there is no DC path to the frequency counter. This is especially handy in medical applications where a voltage probe should not be directly connected to a human body.

LONG TERM INTEGRATOR WITH INFINITE HOLD


This system will integrate an input signal for minutes or days and hold its output indefinitely. The data is held in a digital counter and will stay there until the counter is reset. Typical
applications involve controlling the amount of surface metal deposited in a plating system or how much charge a battery has taken on.


When the input signal is negative as well as positive there needs to be a way of generating "negative" frequencies. An absolute value circuit accomplishes this by giving the V/F a
positive voltage only; and also telling the counter to count up for a positive voltage and to count down for a negative voltage.


The 9400's square wave output is ideal for transmitting analog data over telephone lines. A square wave is actually preferred over a pulse waveform for data transmission since the square wave takes up less frequency spectrum than a pulse waveform.

At the other end of the telephone line a $9400 \mathrm{~F} / \mathrm{V}$ converts the frequency signial back into a voltage output which is linearly proportional to the original input voltage.

The square wave's spectrum can be further reduced by use of low pass filters.

## TELEMETRY



In a telemetry system the 9400 converts the analog input ( $V_{\text {IN }}$ ) into frequencies $(10 \mathrm{~Hz}$ to 100 KHz$)$ which can be used to modulate an RF transmitter.

At the other end a receiver picks up the RF signal and modulates it back into the 10 Hz to 100 KHz spectrum. A frequency
counter connected to this signal will then give a count which is linearly proportional to the original analog voltage ( $\mathrm{V}_{\mathrm{IN}}$ ).

If a linearly proportional analog output voltage is required, then the counter can be replaced by a 9400 used in the F/V mode.

## HIGH NOISE IMMUNITY DATA TRANSMISSION



When transmitting analog data over long distances it is advantageous to convert the analog signal into a digital signal which will be less susceptible to noise pick-up.

In the above system the 9400 converts the input voltage into
either a pulse or square wave which is transmitted on a pair or wires by use of a line driver and receiver. At the other end the original voltage ( $\mathrm{V}_{\mathrm{IN}}$ ) can be digitally displayed on a frequency counter or converted back to an analog voltage by use of a $9400 \mathrm{~F} / \mathrm{V}$ converter.


Low frequency analog data (DC to 10 KHz ) can be recorded anywhere, stored and then reproduced. By varying the play-
back speed, the frequency spectrum of the original data can be shifted up or down.

FSK GENERATION AND DECODING


Frequency shift keying (FSK) is a simple means of transmitting digital data over a signal path (two wires, telephone lines, AM transmitters or FM transmitters).

Typically only two frequencies are transmitted. One corresponds to a logical " 0 " while the other corresponds to a logical " 1 ".
the lower frequency. The digital input will then determine which frequency is selected. $A$ " $O$ " selects the lower frequency while a " 1 " selects the upper frequency.

The digital frequency signal is converted back into a digital format by a 9400 used in the F/V mode.

A $9400 \mathrm{~V} / \mathrm{F}$ will generate these two frequencies when connected as shown above. The potentiometer sets the $\mathrm{V} / \mathrm{F}$ to

## ULTRA LINEAR FREQUENCY MODULATOR



Since the 9400 is a very linear V/F converter an FM modulator is very easy to build.
tion) around the center frequency. $V_{\text {IN }}$ can be negative as well as positive.

The potentiometer determines the center frequency while VIN will determine the amount of modulation (FM devia-

## FREQUENCY METER



The 9400 will convert any frequency below 100 KHz into an output voltage, which is linearly proportional to the input frequency. The equivalent frequency is then displayed on an analog meter.

If the incoming frequency is above 100 KHz a frequency divider in front of the 9400 can be used to scale the frequency down to the 100 KHz region.


A tachometer can be constructed by using the 9400 in the F/V mode to convert the frequency information (RPM) into a linearly proportional voltage. This voltage is then compared to one of n comparators ( 8 in this example). When the voltage
exceeds the trip point of a comparator the respective LED will light up and continue to stay lit as long as the voltage exceeds the trip point. This will give a bar graph type display with the height of the bar being proportional to RPM.

## FREQUENCY/TONE DECODER



The frequency or tone to be detected is converted into a proportional analog voltage by the 9400 F/V converter. The quad comparators sense when the voltage (frequency) exceeds any of the four preset frequency limits. A logical " 1 " at any of the five outputs indicates that the frequency is within those limits.

This system is useful for determining which frequency band a signal is in or for remote control where each frequency band corresponds to a different command.


The high linearity of the $9400(0.01 \%)$ is used to greatly
very precise tracking of $V_{O}$ with respect to $F_{I N}$.
improve the performance of a phase locked loop, resulting in

ANALOG DATA TRANSMISSION ON DC SUPPLY LINES (TWO WIRE TRANSMITTER)


By converting an analog voltage to a linearly proportional pulse train of short duration, it is possible to transmit this data on the same wires that are used to energize the V/F converter.

The. $9400 \mathrm{~V} / \mathrm{F}$ shorts out the DC supply for $3 \mu \mathrm{~s}$ out of each period. At 100 KHz the supply line is down $30 \%$ of the $10 \mu \mathrm{~s}$ period. As the frequency is lowered the down time decreases so that at 1 KHz the line is down only $0.3 \%$ of the time.

Two precautions are necessary to assure that the system does not stop functioning during the shorting period. At the power supply end a 1.2 K resistor limits the current to 10 mA on a 15V supply line. This prevents the 9400 from being operated beyond its output rating and at the same time it prevents the supply from being shorted out. At the V/F end a capacitor
is used to keep the 9400 energized while the diode keeps the capacitor from being discharged.

Since the 9400 requires only 2 mA of current, a $1 \mu \mathrm{~F}$ capacitor ensures a stable voltage (the ripple is only 6 mV ). Since the $3 \mu \mathrm{~s}$ pulses appear at the left side of the 1.2 K resistor, it is easy to sense the signal here and convert the data back into a recognizable format. A frequency counter connected at this point will directly display the input voltage by counting the frequency.

If an analog output is required, a 9400 in the $F / V$ mode can be used to convert the frequency back into a voltage. The overall linearity is in the order of $0.03 \%$, when both $V / F$ and $F / V$ are used. If only the $V / F$ is used, then $0.01 \%$ linearity can easily be achieved.

DIGITALLY CONTROLLED FREQUENCY SOURCE


This system generates frequencies which are controlled by a microprocessor counter, register, or by thumb-wheel switches.

Applications for such a system include computer controlled test equipment and numerically controlled machine tools.


The $9400 \mathrm{~V} / \mathrm{F}$ is useful in the laboratory as a portable, battery operated low cost frequency source. The 9400 provides both pulse and square wave outputs. By adding an Op Amp inte-
grator, a triangular waveform can also be generated. The outputs can be frequency modulated via the FM input.

FREQUENCY MULTIPLIER/DIVIDER WITH INFINITE RESOLUTION


$$
\text { FOUT }=K_{1} K_{2}\left(\frac{R_{2}}{R_{1}+R_{2}}\right) F_{\text {IN }}
$$

Frequency scaling can easily be performed by first converting the incoming frequency into a proportional DC voltage. This is accomplished by using the 9400 in the $F / V$ mode. Once the frequency is in a voltage format it is easy to scale this voltage up or down by use of a single potentiometer. The resultant
voltage is then applied to a $9400 \mathrm{~V} / \mathrm{F}$ which generates a proportional output frequency.

Since the potentiometer is infinitely variable, the division/ multiplication factor can be any number, including fractions, ( $K_{1}$ is simply $V_{O} / F_{\text {IN }}$ while $K_{2}$ is $F_{O} / V_{I N}$ ).

FREQUENCY DIFFERENCE MEASUREMENT


Frequency difference measurement is accomplished by using two 9400's in the F/V mode to convert both frequencies into two proportional analog voltages $\left(\mathrm{V}_{1}\right.$ and $\left.\mathrm{V}_{2}\right) . \mathrm{V}_{2}$ is inverted by a unity gain inverter. $\mathrm{V}_{1}$ and $-\mathrm{V}_{2}$ are then added by the summing Op Amp to give a voltage proportional to the frequency difference between $F_{2}$ and $F_{1}$.

Since the $9400 \mathrm{~V} / \mathrm{F}$ input is actually the summing junction to an Op Amp, $V_{1}$ and $-V_{2}$ can be summed at the 9400 input to generate a frequency output which is proportional to the difference between $\mathrm{F}_{1}$ and $\mathrm{F}_{2}$.

## CONVERTERS SIMPLIFY DESIGN OF FREQUENCY MULTIPLIER*

By using a programmable digital-to-analog converter in combination with frequency-to-voltage and voltage-to-frequency converters, this circuit can multiply an input frequency by any number. Because it needs neither combinational logic nor a high-speed counter, it is more flexible than competing designs, uses fewer parts, and is simpler to build.

As shown in the figure, the V/F converter, a Teledyne 9400, transforms the input frequency into a corresponding voltage. An inexpensive device, the converter requires only a few external components for setting its upper operating frequency as high as 100 kilohertz.

Next the signal is applied to the reference port of the DAC-03
d -a converter, where it is amplified by the frequency-multiplying factor programmed into the converter by thumbwheel switches or a microprocessor. The d-a converter's output is the product of the analog input voltage and the digital gain factor.
$R_{3}$ sets the gain of the 741 op amp to any value, providing trim adjustment or a convenient way to scale the d-a converter's output to a much higher or lower voltage for the final stage, a 9400 converter that operates in the voltage-to-frequency mode. The 741 and $R_{3}$ can also be used to set circuit gain to noninteger values. The V/F device then converts the input voltage into a proportionally higher or lower frequency.


[^8][^9]
## Instructions for the LCD and LED Kits

Two kits are offered; the TSC7106 EV/Kit and the TSC7107 EV/Kit. Each kit contains the appropriate IC, a circuit board, a display (LCD/TSC7106, LED/TSC7107), passive components and miscellaneous hardware.


Figure 1: TSC7106 with Liquid Crystal Display
The TSC7106 and TSC7107 contain all the acive circuitry for a 3-1/2 digit panel meter on a single chip. The TSC7106 is designed to interface with a liquid crystal display (LCD), while the TSC7107 is intended for the light-emitting diode (LED) display. Both circuits contain BCD to seven segment decoders, display drivers, a clock and a reference. To build a high-performance panel meter, (with auto-zero and auto polarity features) it is only necessary to add a display, four resistors, four capacitors, and an input filter if required.


Figure 2: TSC7107 with LED Display

## Assembly

The circuit board layouts and assembly drawings are shown in Figure 17 (TSC7106) and Figure 18 (TSC7107). Pin strips are used to provide a low-cost socket. One IC board can thus be used to evaluate several IC's. Solder terminals are provided for the first five test points and for the $\pm 5 \mathrm{~V}$ input on the TSC7107 kit. A provision has been made for separating REF LO from COMMON when using an external reference zener. Provision has also been made for connecting an external clock. A value of 150 ohms is used for decimal point (TSC7107 EV/Kit).

## Liquid Crystal Display (TSC7106)

The TSC7106 generates the symmetrical square wave to the back plane (B.P.) internally. The user should generate the decimal point from the plane drive by inverting the B.P. (pin 21) output.

In some displays, a satisfactory decimal point can be achieved by tying the decimal plane to COMMON (pin 32). This pin is internally regulated at about 2.8 volts below $\mathrm{V}^{+}$. Prolonged use of this technique, however, may permanently burn-in the decimal, because COMMON is not exactly midway between B.P. high and B.P. Iow. In applications where the decimal point remains fixed, a simple MOS inverter can be used (Figure 3). For instruments where the decimal point


Figure 3: Simple Inverter for Fixed Decimal Point

Figure 4: Exclusive 'OR' Gate for Decimal Point Drive
must be shifted, a quad exclusive OR gate is recommended (Figure 4). Note that in both instances, TEST (pin 37, TP1) is used as $\mathrm{V}^{-}$for the inverters. This pin is capable of sinking about 1 mA and is approximately 5 volts below $\mathrm{V}^{+}$. The B.P. output (pin 21) oscillates between $\mathrm{V}^{+}$and TEST.

## Light Emitting Diode Display (TSC7107)

The TSC7107 will sink 8 mA per segment. This drive produces a bright display suitable for most applications. A fixed decimal point can be turned on by tying the appropriate cathode to ground through a 150 ohm resistor. The circuit boards supplied with the kits will accommodate either HP 0.3 displays or the MAN 3700 types. Note that the HP has the decimal point cathode on pin 6, whereas the MAN 3700 has the decimal point cathode on pin 9. Not all the decimal points are brought out to jumper pads. It may be necessary to wire directly from the 150 ohm resistor to the display. For multiple range instruments, a 7400 series CMOS quad gate should be used.

## Full-Scale Readings

200 mV Full-Scale - The kits have been optimized for 200 mV Full-Scale. The component values supplied are those specified in Figures 1 and 2.

2,000 V Full-Scale - The component values in Table 1 change the integrator time constant and reference and the auto-zero capacitor time constant. These extra components are not supplied in the kits. In addition, the decimal point jumper should be changed so that the display reads 1.999.

## Table 1: Component Values for Full Scale Options

| Component <br> (Type) | 200.0 mV <br> Full Scale | 2.000 V <br> Full Scale |
| :---: | :---: | :---: |
| $\mathrm{C}_{2}$ (mylar) | $0.47 \mu \mathrm{~F}$ | $.047 \mu \mathrm{~F}$ |
| $\mathrm{R}_{1}$ | $24 \mathrm{~K} \Omega$ | $1.5 \mathrm{~K} \Omega^{*}$ |
| $\mathrm{R}_{2}$ | $47 \mathrm{~K} \Omega$ | $470 \mathrm{~K} \Omega$ |

 of the 7106 kit. As an alternative, the potentiometer can be changed to $25 \mathrm{~K} \Omega$.

## Clock

Setting the clock oscillator at precisely 48 kHz will result in the optimum line frequency $(60 \mathrm{~Hz})$ noise rejection (Figure $5)$. Since the integration period is an integral number of the line frequency period, the RC oscillator supplied in the kit runs at approximately 48 kHz giving a measurement frequency of three readings per second. Countries with 50 Hz line frequencies should set the clock to 40 kHz by increasing the value of the 100 k ohm resistor across pins 39 and 40 to 120 k ohms.
An external clock can also be used. In the TSC7106, the internal logic is referenced to TEST. External clock waveforms should therefore swing between TEST and $\mathrm{V}^{+}$(Figure

6A). In the TSC7107, the internal logic is referenced to GND so any generator whose output swings from ground to +5 V will work well, (Figure 6b).


Figure 5: TSC7106/7107 Internal Oscillator/Clock


Figure 6: External Clock Options

## Capacitors

The dual slope technique cancels the effects of long term stability and temperature coefficient. The integration capacitor should have low dielectric loss. Inexpensive polypropelene capacitors have the low dielectric loss characteristics and are recommended. Mylar capacitors may be used for C1 (reference) and C2 (auto-zero).

## Reference

The voltage between $\mathrm{V}^{+}$and COMMON is internally regulated at about 2.8 volts. This reference is adequate for many applications. For improved performance use TSC7106A/7107A devices.
For 200 mV Full-Scale, the voltage applied between REF HI and REF LO should be set at about 100 mV . For 2.000 V Full-Scale, set the reference voltage at 1.0.V. The reference inputs are floating, and the only restriction on the applied voltage is that it should lie in the range $\mathrm{V}^{-}$to $\mathrm{V}^{+}$. For calibration, place 190.0 mV on input and adjust REF pot $\left(\mathrm{R}_{4}\right)$ for 1900 readout.
For greater temperature stability, an external reference can be added as shown in Figures 7a and 7b.


Figure 7: Using an External Reference

## Power Supplies

The TSC7106 kit is intended to be operated from a 9 V battery. INPUT LO is shorted to COMMON, causing $\mathrm{V}^{+}$to sit at 2.8 volts positive with respect to INPUT LO, and $\mathrm{V}^{-}$at 6.2 volts negative with respect to INPUT LO.
The TSC7107 kit should be operated from $\pm 5$ volts. Noisy supplies should be bypassed with $6.8 \mu \mathrm{~F}$ tantalum capacitors to ground at the point where the supplies enter the board.
If $a-5$ volt supply is unavailable, a suitable negative rail can be generated locally using the circuit shown in Figure 8.


Figure 8: Generating Negative Supply from $+5 \mathbf{V}$

## Input Filters

With the leakage current in the order of 1 pA at $25^{\circ} \mathrm{C}$, high impedance passive filters may be used. The RC filter used in the evaluation kits ( 1 megohm $-0.01 \mu \mathrm{~F}$ ) introduces a negligible $1 \mu \mathrm{~V}$ error.

## Sources of Supply

The following list of suppliers is intended to help with the development of production meters. It should not be interpreted as a comprehensive list of suppliers, nor does it constitute an endorsement by Teledyne Semiconductor:

## Suppliers of LCD's

1. Hamlin Inc., WI (414) 648-2361
2. Crystalloid Electronics, $\mathrm{OH}(216) 688-1180$
3. Printed Circuits Integrated, CA (408) 733-4603
4. IEE Inc., CA (213) 787-0311

## Suppliers of LED's

1. AND, CA (415) 347-9916
2. Litronix Inc., CA (408) 257-7910
3. Hewlett-Packard, CA (415) 493-1212
4. General Instruments, CA (415) 493-0400

## Suppliers of Polypropelene Capacitors

1. Plessey Capacitors, CA (213) 889-4120
2. IMB Electronic Products, CA (213) 921-3407
3. Elcap Electronics, CA (714) 979-4400
4. TRW Capacitors, NB (308) 284-3611

## Preliminary Tests

1. Solder flux or other impurities on PC boards may cause leakage paths between IC pins and board traces, reducing performance. Rubbing alcohol or another appropriate cleaning agent should be used to remove impurities.
2. In order to insure that unused segments on the LCD displays do not turn on, tie them to the Back Plane pin (pin 22).
3. Auto-Zero - With the inputs shorted the display should read zero. The negative sign will be on about one half of the time, showing the input to be exactly zero volts.
4. Polarity - A negative sign indicates a negative reading. No sign indicates a positive reading.
5. Overrange - For inputs greater than Full-Scale, only 1 or -1 will be displayed. The three least significant digits will be suppressed.
6. Calibration - The instrument should be calibrated at 1900 counts by using a high-quality $41 / 2$ digit DVM.

## Applications Input Attenuator

There are times it is desirable to have full scale readings other than 199.9 mV or 1.999 V . To measure voltages greater than 2 V , an input attenuator is needed as shown in Figure 9.

The Full-Scale sensitivity is given by:

$$
\mathrm{V}_{\mathrm{IN}}(\text { Full-Scale })=1.999 \mathrm{~V}_{\text {REF }} \times \frac{R_{2}}{\left(R_{1}+R_{2}\right)}
$$

It is important that $R_{1}$ and $R_{2}$ remain fixed for the calibration period of the instrument. Metal film resistors with good longterm drift characteristics, and low temperature coefficients are recommended.

The input attenuator reduces the input resistance of the circuit from $>10^{12}$ ohms to $\left(R_{1}+R_{2}\right)$. This places an upper limit of about 10 megohms on the input resistance that can readily be achieved when using an attenuator before the $A / D$ input current causes offset errors.
To measure Full-Scale voltage less than 199.9 mV , an operational amplifier is used prior to the TSC7106/7 inputs. Note that the auto-zero circuitry within the IC can not take care of the op amp offset or voltage drift. For this reason the use of a low power low offset Op Amp such as the TSC900 is recommended.

Figure 10 shows a circuit with $\pm 20 \mathrm{mV}$ Full-Scale and an input resistance greater than 10 megohms.
For scale factors between 100 mV and 1 mV per least significant digit (LSD), simply determine the reference voltage required for the following equation:
$\mathrm{V}_{\text {REF }}=\left(\right.$ Voltage Change represented by one LSD) $\times 10^{3}$
For scale factors greater than $1 \mathrm{mV} / \mathrm{LSD}$, the most straight forward approach is to use an input attenuator in conjunction with a 1 volt reference.


Figure 9: Input Attenuator for $\mathrm{V}_{\text {IN }} \geqslant 2.0 \mathrm{~V}$


Figure 10:

## AC Voltage Measurements

It is necessary to build an AC to DC converter to measure AC voltages with the TSC7106/7. Figure 11 shows a circuit used extensively in commercial $31 / 2$ digit DVM's. The circuit responds to the average value of the sinusoidal waveform and assumes low distortion. It has 10 megohms input impedance, 20 Hz to 5 kHz bandwidth, and is AC coupled to the kit introducing to DC errors.

## Multl-Range DVM's

Two schemes commonly used are shown in Figures 12a and 12b. The circuit of Figúre 12a has the advantage that any switch contact resistance appears in series with the TSC7106/7 input resistance. Since the input resistance is $>10^{12}$ ohms, errors due to the switch are negligible. Precision voltage attenuators ( $R_{1}$ through $R_{5}$ ) are available from a number of manufacturers. Allen Bradley, for example, makes a thin film network which contains $1 \mathrm{k}, 9 \mathrm{k}, 90 \mathrm{k}, 900 \mathrm{k}$ and 9 M
resistors in one package (FN207) - ideal for a five range voltmeter. However, it is less expensive to use meaıum precision resistors in series with potentiometers for the attenuator. Then the schematic of Figure $12 b$ has some of the advantages because the resistors in the attenuator are noninteractive. It is also more amenable to solid state range switching. An analog switch or FETs may be used in place of the mechanical switch. Then, by adding a couple of zener diodes (or ordinary silicon diodes in the case of a 200 mV F.S. panel meter) the solid state switch is totally protected against overvoltages. By contrast, the configuration of Figure 12a exposes the switch to the full-input voltage, which may be several hundred volts. However, in Figure 12b the switch resistance forms part of the attenuator and could contribute an error.

## Resistance Measurements

The ratiometric technique is used. The unknown resistance is put in series with a known standard and a current passed through the pair. The voltage developed across the unknown is applied to the input (between IN HI and IN LO), and the voltage across the known resistor applied to the reference input (REF HI and REF LO). If the unknown equals the standard, the display will read 1000. The displayed reading can be determined from the following expression:
Displayed Reading $=\frac{\text { R Unknown }}{\text { R Standard }} \times 1000$
Figure 13 shows a typical measurement circuit. Note that due to its ratiometric nature, the technique does not require an accurately defined reference voltage. The display will overrange for $R$ Unknown $\geqslant 2 \times R$ Standard.

## Current Measurements

The use of a shunt resistor converts the current to a voltage. The relationship between the current and the displayed reading for the circuit of Figure 14 is found by:
Displayed Reading $=\frac{\mathrm{I}_{\mathbb{N}} \times R_{\mathrm{S}}}{\mathrm{V}_{\text {REF }}} \times 1000$
When measuring current the 199.9 mV scale is used. This limits the voltage drop to $100 \mu \mathrm{~V}$ per count. A multi-range current meter circuit is shown in Figure 15. Note that although the input current passes through the selector switch, IR drops across the switch do not contribute to the measured voltage.

## Temperature Measurements

A diode connected transistor may be used as the temperature sensing element. $\mathrm{V}_{\mathrm{BE}}$ has a temperature coefficient of $-2.1 \mathrm{mV} /{ }^{\circ} \mathrm{C}$. A scale factor of $0.1^{\circ} \mathrm{C} /$ count may be obtained by setting the reference at 210 mV .
At $0^{\circ} \mathrm{C}$ and $100 \mu \mathrm{~A}$ bias current, the diode connected transistor will have a forward voltage drop of approximately 550 mV . A fixed 500 mV source is set up to offset the diode drop. In the circuit of Figure 16, adjust R5 to give 000.0 output reading with Q1 at $0^{\circ} \mathrm{C}$. Then adjust for R 4 for a 100.0 reading with Q1 at $100^{\circ} \mathrm{C}$.


Figure 11: AC to DC Converter


Figure 12a: Multirange Voltmeter


Figure 12b: Multirange Voltmeter, Alternative Scheme


Figure 13: Resistance Measurement* (*Requires some modification to the kit)


Figure 14: Current Measurement


Figure 15: Multirange Current Meter


Figure 16: Digital Thermometer*
(*Requires some modification to the kit)


Pin Configuration


ACTUAL SIZE NOT SHOWN
Figure 17: TSC7106 - Circuit Board Layout and Component Placement


ACTUAL SIZE NOT SHOWN

## LEGEND

| C1 | 0.1 Mf | R1 | 24 K | $1 / 4 \mathrm{~W}$ | $5 \%$ |
| :--- | :--- | :--- | :--- | :--- | :--- |
| C2 | 0.47 Mf | R2 | 47 K | $1 / 4 \mathrm{~W}$ | $5 \%$ |
| C3 | 0.22 Mf | R3 | 100 K | $1 / 4 \mathrm{~W}$ | $5 \%$ |
| C4 | 100 pf | R4 | 1 K | POT |  |
| C5 | 0.01 Mf | R5 | 1 M | $1 / 4 \mathrm{~W}$ | $5 \%$ |
|  |  | R6 | $150 \Omega$ | $1 / 4 \mathrm{~W}$ | $5 \%$ |


a313w unvd vyito asi 2014
TRTELEDYNE SEMICONDUCTOR
actual size not shown
Figure 18: TSC7107 - Circuit Board Layout and Component Placement

Due to the extremely low input noise characteristics of the TSC7106/7107, the user may build a digital thermocouple thermometer with only one active component and fifteen passive components. With this circuit, both type $J$ and type $K$ thermocouples may be used. The type $J$ will measure over the temperature range of 10 to $530^{\circ} \mathrm{C}$ with a conformity of $\pm 2^{\circ} \mathrm{C}$. The type K will measure over a temperature range of $0^{\circ} \mathrm{C}$ to $1000^{\circ} \mathrm{C}$ with a conformity of $\pm 3^{\circ} \mathrm{C}$.
In operation, the TSC7106 provides all A/D functions including seven segment decoder, display drive, reference, and a clock. True differential low noise input allows the bridge circuit shown in Figure 2 with no other active components. This circuit will give a three month life when operated from a normal alkaline 9 volt battery.
The circuit using a type $J$ thermocouple will be discussed here. (The circuit for the type K thermocouple is similar except for the changing of component values and the replacement of the type J thermocouple with type K). The extremely low noise front-end of the TSC7106/7107 allows the IC to operate reliably at one-half its minimum reference voltage specifications, approximately 50 microvolts per count.
A thermocouple is made by the junction of two dissimilar metals. Figure 1 shows the type $J$ (iron and constantan) thermocouple in a temperature measuring mode.


Figure 1.
A voltage is generated as a function of the difference in temperature between the two iron - constantan thermocouples - TC 1 and TC 2. If TC 1 is kept at a constant temperature (such as the freezing temperature of water), the voltage generated as a function of temperature of TC 2 is displayed in the normal type $J$ thermocouple charts. The sensitivity at room temperature is approximately $50.4 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$.
Figure 2 shows the circuit for a portable battery operated thermocouple thermometer using the TSC7106. The clrcuit uses six components in addition to those required for the standard TSC7106 circultry. The TSC7106 is designed for normal 200 mV operation. Then the reference voltage is readjusted to 50.4 mV which corresponds to 1,000 times the one degree sensitivity of the type J thermocouple.


Figure 2.
Since the thermocouple reference can not be easily maintained at a constant temperature, a circuit is used which provides a voltage that changes with temperature in an equal and opposite manner to the thermocouple. When combined with the thermocouple this has the effect of simulating the reference at a constant temperature over the normal ambient.


Figure 3.

## Application Note 12

The circuit generating the compensating voltage is composed of Q1, R6 and R7. Q1 may be any small signal transistor.
A voltage equal and opposite to that generated by the thermocouple occurs as follows: Q1 base and collector leads are tied together allowing Q1 to operate as a diode. In this mode, the forward voltage drop of the diode connected transistor is -2.1 millivolts per degree centegrade. R7 is returned to the TSC7106 reference. The junction of R6 and R7 will vary by the ratio of
$2.1 \mathrm{mV} /{ }^{\circ} \mathrm{C} \frac{720}{30,000}=50.4 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$.
One end of the thermocouple is attached to this point. The thermocouple reference and the transistor should be thermally bonded. In this manner, temperature changes of the
thermocouple will be compensated by the transistor and resistor divider R6 and R7. R8, R9 and R10 form the other leg of a bridge. The $200 \Omega$ pot (R9) center arm is fed to the negative or reference section of the input amplifier. The thermocouple output is fed to the positive section.
Calibration is accomplished by the use of an ice water bath and millivolt source as shown in Figure 3. The ice water bath is used as a $\mathrm{O}^{\circ} \mathrm{C}$ reference. The millivolt source is used to simulate thermocouple temperature over the range of 10 to $530^{\circ}$ C. R9 is used for zero adjustment and R4 is used for full-scale. The thermocouple temperature curve is calibrated for best accuracy over the user's temperature range. Type K thermocouple is fabricated in a similar manner by changing the thermocouple type and resistor values and readjusting 0 and full-scale. The TSC7107 may also be used as a laboratory thermometer with similar circuitry.

Application Note 16 TSC7135 Microprocessor Interface By Wes Freeman

Many data acquisition systems require both a visual display and a computer interface. The TSC7135 from Teledyne Semiconductor is a 4-1/2 digit Analog-to-Digital converter (ADC) which can easily provide both of these functions. The TSC7135's multiplexed BCD outputs interface easily to low cost LED or LCD decoder/drivers, such as the TSC7211A (LCD) and TSC7212A (LED) or TSC700A (high-current LED). Also, the TSC7135's data outputs simplify computer interfacing.
This application note will present both the hardware and software required to interface the TSC7135 to a microprocessor. The circuit was developed for a $6502 \mu \mathrm{P}$ and $6522 \mathrm{I} / \mathrm{O}$ port, but the design can easily be modified for other $\mu \mathrm{Ps}$ and I/O ports.
The TSC7135 has several features which make it an attractive choice for data acquisition where speed is not an overriding consideration. The analog features include:

- High resolution . ............................. . . 20,000 counts
- High accuracy . . . . . . . . . . . . . . . . . . . . . . . . . . . . . $\pm 1$ count
- Low roll-over error ............................. $\pm 1$ count
- Valid polarity at 000 reading (the + and - zero states give an extra bit of resolution)
- Negligible zero drift - definitely not the case with a bipolar DAC/SAR type ADC


## Timing Relationship Between TSC7135 Outputs



- The dual-slope conversion method rejects $50 \mathrm{~Hz}, 60 \mathrm{~Hz}$, and 400 Hz noise.
- The ratiometric reference and differential inputs provide flexible transducer interfacing.

The TSC7135 also has features that simplify system design:

- Easy $\mu \mathrm{P}$ Interfacing
- Overrange and underrange flags for autoranging and process control decisions
- Operation from $\pm 5 \mathrm{~V}$ supplies, with only 10 mW typical power dissipation
- TTL compatible outputs ( 1.6 mA sink current)

The TSC7135 provides output signals which, together with one port of an LSI I/O chip, simplify a microprocessor interface. The relationship between the various TSC7135 outputs is shown in Figure 1. The specific function of these outputs are as follows:

## TSC7135 Pin Function

- B1-B8 BCD coded data is output on the B1-B8
- DS5-DS1 Digit Select 5 (most significant digit) through Digit Select 1 (least significant) go high as data on B1-B8 becomes valid for that digit.
- STROBE For the first digit scan after a conversion STROBE goes low (for $1 / 2$ clock period) in the middle of each digit strobe. After five pulses, STROBE stays high until the next conversion is complete.
- BUSY BUSY is high while the TSC7135 is in Integrate or Deintegrate phases of a conversion. The falling of BUSY can, therefore, be used as an end of conversion signal.
- POL POLARITY is high if the analog input polarity is positive.
- OR OVERRANGE goes high if the analog input is greater than full scale (reading $>20,000$ ), while UNDERRANGE goes high if the reading is 1,800 or less.

The TSC7135 also has a RUN/HOLD input. If RUN/HOLD is held low, the converter will remain in the auto-zero phase. A new conversion will not begin until RUN/FOLD goes high. This input can be used to generate conversions on command.

Figure 1

## Interface Hardware

The complete TSC7135 to SYP6522 interface schematic is shown in Fiqure 2. BCD data, POL, OR, UR, and DS5 a re connected to the 6522's PAO through PA7 inputs. The TSC7135's STROBE output interrupts the microprocessor via the 6522's CA1 interrupt. RUN/HOLD can be controlled by programming CA2 as an output.
At first glance, the circuit may appear incomplete because digit selects DS4 through DS1 are not connected. However, DS5 is the only digit select required. As mentioned previously, there are only 5 STROBE pulses per conversion cycle, with the first STROBE occurring during DS5. The $\mu \mathrm{P}$ decodes the logical "AND" of DS5 and STROBE (DS5 - STROBE) as a conversion complete signal.
If the $\mu \mathrm{P}$ finds (DS • STROBE) true upon responding to an interrupt, an "end of conversion" is assumed and assembling of BCD data from the TSC7135 begins. Each of the next four interrupts will provide another BCD digit. The $\mu \mathrm{P}$ counts interrupts in a register and stores the corresponding BCD data in successive memory locations. After five STROBE pulses, all BCD data has been transferred to the $\mu \mathrm{P}$ and conversion is complete.
One constraint of this interface method is that the $\mu \mathrm{P}$ must respond to each digit's interrupt before the next digit becomes valid. The 6522's CA1 input can be programmed to latch data into Port A, as well as provide an interrupt to the $\mu \mathrm{P}$. Since latched data remains valid until the next STROBE pulse, the $\mu \mathrm{P}$ has the full interval between STROBE pulses to service each interrupt. STROBE pulses are 200 clock cycles apart. A

TSC7135 clock frequency of 100 kHz will allow the $\mu \mathrm{P}$ two milliseconds ( $10 \mu \mathrm{sec} \times 200$ clock cycles) to respond to each interrupt without losing data.

## Interface Software

Software for the TSC7135 to 6502 interface can be divided into three routines: (1) Programming the 6522's Port A for latched input and interrupt from pin CA1; (2) the interrupt service routine which actually acquires and stores BCD data from the TSC7135; (3) display or manipulation of the acquired data. Figure 3 is a 6502 assembly language listing of the first two routines. An interrupt service routine flow chart is shown in Figure 4. Since the end of a digit scan leaves 5 digits of BCD data in successive memory locations, the user will find the interface software easy to incorporate into a specific display or manipulation routine.

The 6522 I/O port must be programmed before data can be received from the TSC7135. The code in Figure 3, beginning at location "SET-UP", writes data into the 6522's control registers to enable the following functions: (1) Port A will be a latched input, controlled by input CA1; (2) CA2 will be an output, programmed high (TSC7135 in "RUN" mode); (3) Interrupt enabled on the falling edge of CA1. The function of data written to each 6522 register is defined in Figure 5.
When programmed for interrupt operation, the 6522 will pull its IRQ output low on the falling edge of each STROBE pulse from the TSC7135. Assuming interrupts are enabled, IRQ going low will cause the $6502 \mu \mathrm{P}$ to load the address of an interrupt service routine from memory locations FFFE and

TSC7135 to $6502 \mu$ P Interface Schematic


## Flgure 2

FFFF. This routine will typically identify the interrupting device, determine its priority and jump to a program to service the interrupt. The user must provide software to vector interrupts coming from the TSC7135 to the service routine located at location "INTVEC" of Figure 3. The TSC7135-6522 hardware can accommodate interrupt service delays of up to two msec , so a relatively low-priority interrupt status can be used.

## 6502 - Assembly Language Listing



Figure 3
Once the 6522's interrupt has been recognized and vectored to location "INTVEC", a read of Port A loads the TSC7135 data into the 6502 accumulator. Reading Port A also sets the $\mu \mathrm{P}$ 's status flags and resets the 6522's interrupt flag.
The $\mu \mathrm{P}$ now tests whether the accumulator contains the TSC7135's most significant digit by testing for DS5 being high. Connecting DS5 to PA7 (MSB) of the I/O port allows testing DS5 with a single branch on plus instruction.
If DS5 is high, this data signals the beginning of a new display
scan (i.e., an end of conversion has occurred.) The $\mu \mathrm{P}$ zerns its $X$ index register, which will be used both to count the digits and to provide an offset for storing each digit in zero page memory. Register X is also stored in zero page memory at location XSTOR, since its contents will probably be lost upon returning from interrupt.

An early indication of an overrange condition can be obtained at this time. A bit mask, stored in memory, is used to test for the TSC7135's OVERRANGE output. If OR is high, the program branches to an error routine. An alternative for overrange testing is to wait until all digits have been scanned and then test bit 4 of any digit.

TSC7135 to $6502 \mu$ P Interface Program Flow Chart


Figure 4

If DS5 is not high, or after register X is zeroed, program execution proceeds to location "NXTDIG". The BCD data is stored in zero page memory, beginning at location "DIGSTOR" and indexed by register $X$. After each digit is stored, register $X$ is incremented and compared to five. If register $X$ equals five, the digit scan is complete and data can be processed or displayed.

Register $X$ less than five indicates the digit scan is not complete, so an RTI instruction returns operation to the main program to await another digit strobe. Other programs can use memory location XSTOR as a "Data Valid" indication: if XSTOR $=5$, then 5 consecutive memory locations begining at DIGSTOR contain the results of the latest TSC7135 conversion.

## 6522 I/O Port Control Register Functions



Application Note 17 Simplify A/D Converter Interface With Software By Gary Grandbois \& Wes Freeman

Integrating ADCs featuring BCD outputs for display interface offer a number of excellent features as well as high resolution at a very low cost. These advantages which include auto-zeroing, sign-magnitude coding, noise averaging and high impedance inputs are also attractive for microprocessor based systems. Unfortunately many of the display-oriented A/D converters are difficult to interface due to the multiplexed BCD format of the outputs. An exception to this problem is the $41 / 2$ digit TSC7135 ADC which provides a "strobe" output.
This output allows the number of $1 / O$ port pins required to interface a $41 / 2$ digit analog to digital converter chip to a microprocessor to be reduced from 15 lines (see ref.) to only 10 lines by counting the digit strobes in a software register. Besides freeing I/O pins for other applications, this method also results in slightly faster interrupt response because the $\mu \mathrm{P}$ does not have to loop while identifying each digit. Although the hardware and software shown are designed for the 8080 , 8085 or $\mathbf{Z - 8 0}$, the same method can be applied to 6502 or 6800 I/O devices.

## Interface Hardware

The complete TSC7135 to 18255A hardware interface is shown in Figure 1. The only digit strobe used is DS5 (the MSD), and the BUSY output is ignored. To understand why the other digit strobes are not required refer to the TSC7135 output timing diagram in Figure 2. The STROBE output goes low five times per conversion cycle. The first STROBE pulse occurs in the middle of DS5, when BCD data for the most significant digit is available on outputs B1-B8. STROBE also pulses LOW during the following DS4 through DS1 signals, after which STROBE remains high until the next conversion cycle. Therefore, only one STROBE pulse occurs for each digit select, and each STROBE corresponds to a BCD digit in MSD to LSD order. To read the A/D converter's data the $\mu \mathrm{P}$ simply reads BCD data during each STROBE pulse and stores that data in memory locations that correspond to the number of STROBE pulses received.


Figure 1: TSC7135 to I/O Port Interface

## Synchronizing Data Transfer

The microprocessor must be able to identify an end-of-conversion, so that each digit will be stored in its proper location. Since the TSC7135 has a BUSY output, the processor could simply monitor this output for end-of-conversion status. However, this method would require an extra input bit, as well as processor time to test for BUSY status. By using software to identify the end-of-conversion, both software and hardware can be simplified.
In order to synchronize data transfer between $\mu \mathrm{P}$ and $\mathrm{A} / \mathrm{D}$ converter, the $\mu \mathrm{P}$ tests the most significant bit of I/O port A for the presence of DIGIT STROBE 5(DS5). If DS5 is true then an end-of-conversion has occured. The data pointer is then initialized and assembly of five BCD digits begins. The next four STROBE pulses will find DS5 false, so the BCD digits are simply stored in successive memory locations. The fifth STROBE pulse signals an end of data transfer, so the user can display or manipulate the data as desired.


Figure 2: Timing Relationships Between TSC7135 Outputs

## Initializing the I8255A I/O Port

At power up, or after a microprocessor reset, the I8255A is initialized for unlatched (Mode 0) input operation. In order to interface to the TSC7135, the 18255A must be programmed to latch data, and generate an interrupt, from Port A (Mode I operation). In addition, one bit of Port $C$ can be utilized for controlling the TSC7135's RUN/ $\overline{\text { HOLD }}$ input, if conversions on command are required.
Programming the 18255A is accomplished by writing data to the control register. Figure 3 outlines the function of each control bit. Writing "OB2H" to the control register, for example, configures Port A as a latched input, Port B as a nonlatched input, and remaining Port $C$ bits as outputs.

In the Port A strobed input mode, bit PC3 becomes the interrupt output. In a large system with many interrupting devices, this output would typically go to a priority interrupt controller such as the 18259A. Smaller systems can simply use a single interrupt input, with polling in software to identify the source of the interrupt. To determine whether the TSC7135 has caused the interrupt in a polled system, Port A Input Buffer Full (IBFA) is tested for a HIGH state. If IBFA is high, then data has been latched into Port A by the TSC7135. Reading Port A will clear the interrupt and reset IBFA.
Programming Port A for strobed operation will define bit PC3 as an interrupt output, but a separate operation is required to enable the output. Bit PC4 is the interrupt enable bit for Port A. This bit must be set, using the Port $C$ bit set/reset function, before the 18255A will respond to interrupts.
The circuit of Figure 1 also shows the TSC7135's RUN/HOLD input controlled by bit PC6. Setting PC6 high will result in continuous conversions. When PC6 is low, the TSC7135 will remain in its auto-zero cycle. If PC6 pulses high, the TSC7135 will perform a conversion, output the new data, and return to auto-zero.


Figure 3: 8255 I/O Port Register Functions

## Interface Software

Listing 1 contains software for acquiring data from the A/D converter. Two separate routines are required to program the I/O port and to respond to interrupts. Code at location "SETUP" will configure the 18255A for strobed input and enable Port A's interrupt.
The user must provide software for vectoring interrupts from port A of the 8255A to interrupt service routine "SVC." As mentioned previously, "SVC" will test for digit strobe 5 being high (i.e. beginning of a new digit scan). If DS5 is high then data pointer HL is loaded with the digit storage address.
If DS5 is not high, or after HL has been initialized, the BCD digits are stored in memory. If five digits have not been received, register HL is incremented to point to the next digit storage location. After five STROBE pulses, locations STORAG through STORAG +4 will contain five BCD digits that represent the latest TSC7135 conversion, plus sign, polarity, overrange, and underrange flags.


Listing 1: TSC7135 to TSC8250 Interface Software

## Converting Multiplexed BCD Numbers to 2's Complement Format

BCD data is very convenient for driving LED or LCD displays, but 2's complement format is usually preferred for computer arithmetic operations. Listing 2 is a program which will convert five BCD digits to 2's complement. This program multiplies the MSD by 10, adds the next digit, multiplies the sum again, etc., until all 5 digits have been converted. The sign bit is then tested and, if negative, a 2's complement adjustment (complement all data bits and add one) is performed. Finally, the 2's complement data is stored at location AD2SCM.

| $i$ <br> ;BCD TO 2. 5 COMPLEMENT CONVERSION SOFTWARE <br> ; THIS ROUTINE CONVERTS 5 BCD DIBITS LOCATED AT "STOR' TO 2'S COMP AND STORES RESULT AT "ADZSCM" |  |  |  |
| :---: | :---: | :---: | :---: |
|  | ORG | 20404 |  |
| BCD2BI: | LD | HL, 0000 | 3 ZERD HL REG |
|  | LD | BC, STOR | ;POINT TO 1ST (MSD) BCD DIGIT |
| DIGIT: | LD | A, (BC) | [GET DIEIT |
|  | AND | OFH | ; MASK DSS, POL, OR, AND UR FLAGS |
|  | LD | D, 0 | ; ZERO D |
|  | LD | E, A | ;DIEIT TOE |
|  | ADD | HL, DE | ;16 BIT ADD |
|  | LD | A, C | : LO BYTE OF DIGIT POINTER |
|  | SUB | ENDSTR. MOD. 256 | COMPARE TO END: IF DONE, |
|  | JP | P, DONE | ; BC POINTS TO LAST DIEIT |
|  | INC | BC | ; NOT DONE |
|  | ADD | HL, HL | ; MULTIPLY HL BY 10; START |
|  | PUSH | HL | ; WITH HL- 2; SAVE ON STACK |
|  | ADD | HL, HL | ; (HL*2) *2mHL*4 |
|  | ADD | HL, HL | ; TIMES 2 AGAIN=HL*B |
|  | POP | DE | GET BACK HL*2 |
|  | ADD | HL, DE | ; $\mathrm{HL} * 8+\mathrm{HL} * 2=H 2 * 10$ |
|  | JP | DIGIT | ; NEXT BCD DIEIT |
| DONE: | LD | $A,(B C)$ | :BC STILL POINTS TO BCD DIEIT |
|  | AND | 4 OH | ;TEST 7135 POL -IF POSITIVE, |
|  | JP | NZ, AD2CPL | ; NO 2'S COMP CORRECTICN REQ |
|  | LD | A, H | ;RESULT NEE, SO DO A 2*S COMP |
|  | CPL |  | ; CORREECTION BY COMPLEMENTING |
|  | LD | H, A | ; THE 15 BIT RESLLLT IN HL, |
|  | LD | A, L | ; AND COMPLEMENTING THE |
|  | CPL |  | ; SIGN BIT |
|  | LD | L, A | ; RESULT NOW IS 1'S COMP IN HL |
|  | INC | HL | ; ADD ONE FOR 2's COMPLEMENT |
| AD2CPL: | LD | (AD2SCM), HL | ;STORE RESULT AND DONE |
|  | RET |  |  |
| ; |  |  |  |
| ; RESERVE STORAGE FOR POINTER AND RESULTS |  |  |  |
|  |  |  |  |
|  | ORE | OBFFCH | ;MUST BE LDCATED IN RAM |
| COUNTR: | DEFS | 2 | ; STORAGE FOR DATA POINTER |
| STOR: | DEFS | 5 | ;STORAGE FOR 5 BCD DIGITS |
| ENDSTR: | EQU | STOR+4 |  |
| AD2SCM: | DEFS | 2 | ;2'S COMPLEMENT DATA STOR |
| ; |  |  |  |
| ; |  |  |  |

Listing 2: BCD to 2's Complement Conversion Software

Reference:
Smith, M.F. Interface program links A/D chip with microprocessor Electronics Nov. 3, 1982 p. 124, 125


Flowchart 1: "SVC" Interrupt Service Subroutine


Flowchart 2: "BCD2B1" 2's Complement Conversion Subroutine

Application Note 18 TSC7211AM/TSC7212AM Display Driver Microprocessor Interface By Wes Freeman

## TSC7211AM/TSC7212AM Microprocessor Interface

The TSC7211AM and TSC7212AM are complete CMOS fourdigit display drivers which greatly simplify microprocessor display interfaces. The devices contain data latches, BCD to seven-segment decoders, and either back plane and segment drivers for liquid crystal displays (TSC7211AM) or current controlled outputs for LEDs (TSC7212AM). This application note describes interfacing these display drivers to popular microprocessors.

## TSC7211AM/TSC7212AM $\mu$ P Interface Inputs

The TSC7211AM and TSC7212AM need only eight inputs to transfer data from a $\mu \mathrm{P}$ to the display. Inputs are divided into four data inputs, two address inputs, and two chip selects. Input timing relationships are shown in Figure 1.
BCD data for display is entered on inputs BO(LSB) through B3(MSB). Data inputs from 0000B through 1001B are decoded to correct seven-segment representation, while data inputs from 1010B to 1110B are decoded to "-," "E," "L," "P," and "H" respectively. An input of 1111B results in a blank display, which permits either individual digits or the entire display to be blanked under software control without external hardware.
The digit select inputs (DS1 and DS2) select the digit written to


Flgure 1. TSC7211AM/TSC7212AM Input Timing Dlagram
when the chip select inputs become active. Normally DS1 and DS2 are connected to the low-order bits (A0 and A1, respectively) of the microprocessor address bus. The DS1 and DS2 inputs must meet the same setup-and-hold-time limits as the data inputs.
Chip select inputs $\overline{\text { CS1 }}$ and $\overline{\text { CS2 }}$ control data entry into the TSC7211AM/TSC7212AM. The two chip selects are interchangeable, since they are logically "ORed" internally. In a typical application one chip select input connects to the READ/WRITE control line and the other chip select will connect to an address decoder. If only one chip select is required the remaining input should be tied to GND.

## Microprocessor Bus Interfaces

Microprocessor bus structures can roughly be divided into two groups: the 6800-type, where data is guaranteed valid on a clock edge, and the 8080-type, where data is stable for the duration of a WRITE pulse. Since the TSC7211AM and TSC7212AM are specified in terms of data setup-and-holdtimes, elther processor type is easily accommodated.
The 6800-type edge activated I/O is used on several popular microprocessors, such as the $8048,8085,6809$ and 6502. A timing diagram for the 6502 is shown in Figure 2, and a typical 6502 to TSC7211AM interface is shown in Figure 3. To transfer data to the display simply write data to the appropriate memory location.


FIgure 2. $6502 \mu \mathrm{P}$ Output Timing Dlagram


Figure 3. TSC7211AM Interface to $\mathbf{6 5 0 2 \mu} \mathrm{P}$

The 8080 bus characteristics, shown in Figure 4, are shared by the Z-80, NSC800 and 8086, among others. A typical 8080 to TSC7212AM interface is shown in Figure 5, where the TSC7212AM is accessed as four I/O port locations. The 8080 can also treat the TSC7212AM as memory, in which case the full range of memory reference instructions can be used to transfer data to the display.


Figure 4. $8080 \mu \mathrm{P}$ Output Timing Diagram


Figure 5. TSC7212AM Interface to $\mathbf{8 0 8 0 \mu} \mathbf{P}$

## Application Note 18

## Interfacing to Multiple LCD Displays

LCD displays will be damaged if the display driver causes a DC voltage between the backplane and segment inputs. Therefore, display driver outputs must be synchronized if more than one driver is used with a display. The TSC7211AM backplane outputs can be slaved together, permitting large LCD displays to be driven.
Figure 6, for example, shows three TSC7211AMs driving two six-digit LCD displays to produce a date/time display in MM:DD:YY, HH:MM:SS format. Since the backplane outputs are synchronized, each display can be driven by two separate TSC7211AMs without any display degradation. The processor shown is a Z-80, and the displays are accessed as twelve I/O port locations beginning at address 80 H .

The Z-80 indirect output instruction (OUTI) efficiently transfers data from a twelve-byte buffer in memory to three TSC7211AMs. The OUTI instruction transfers the byte data addressed by registers H \& L to the output port addressed by reg $C$, then increments register $H L$ and decrements the buffer count register B. A typical output routine is:

| Transfer | LD | C,7FH | ; 1st I/O address -1 |
| :--- | :--- | :--- | :--- |
|  | LD | HL, |  |
|  |  | Buffer Address | ; 1st byte of data |
| Loop1 | LD $B, 12$ | ; Transfer 12 bytes |  |
|  | OUC C | Point to next I/O address |  |
|  | JR NZ, Loop1 | ; Output byte; inc HL; dec B |  |
|  |  |  |  |



Figure 6. Multiple TSC7211AM Interface to Z-80 $\mu \mathbf{P}$

TSC7211AM/TSC7212AM Pin Configuration


Output Pin Description and Function

| OUTPUT | TERMINAL |  | FUNCTION |  | OUTPUT | TERMINAL |  | FUNCTION |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A1 | 37 | A | Segment Dr. Digit 1 | (LSD) | A3 | 13 | A | Segment Dr. Digit 3 |  |
| B1 | 38 | B |  |  | B3 | 14 | B |  |  |
| C1 | 39 | C |  |  | C3 | 15 | C |  |  |
| D1 | 40 | D |  |  | D3 | 16 | D |  |  |
| E1 | 2 | E |  |  | E3 | 17 | E |  |  |
| F1 | 4 | F |  | 1 | F3 | 19 | F |  |  |
| G1 | 3 | G |  | $V$ | G3 | 18 | G |  |  |
| A2 | 6 | A | Segment Dr. Digit 2 |  | A4 | 20 | A | Segment Dr. Digit 4 | (MSD) |
| B2 | 7 | B | 1 |  | B4 | 21 | B |  | \| |
| C2 | 8 | C |  |  | C4 | 22 | C |  | . |
| D2 | 9 | D |  |  | D4 | 23 | D |  | T |
| E2 | 10 | E |  |  | E4 | 24 | E |  |  |
| F2 | 12 | F | $\downarrow$ |  | F4 | 26 | F | 1 | 1 |
| G2 | 11 | G | $\nabla$ |  | G4 | 25 | G | , | 1 |

Traditionally 3 1/2 digit analog-to-digital converters have interfaced to seven segment LED or LCD displays. Converters like the TSC7106A, TSC7126A and TSC7107A contain decoder/driver circuits to directly drive seven segment displays. Devices like the TSC14433A and $41 / 2$ digit TSC7135 offer users greater flexibility since decoder/drivers are not contained on-chip. Output data is in a multiplexed BCD format. Information can be displayed on LED, LCD, vacuum fluorescent or incandescent displays as the application and environment require. Information can simultaneously be transferred to a microprocessor.
The output data latching, decoding, and drive functions for BCD output converters, however, require external MSI devices such as the TSC700A, TSC7211A or MC14543/1413. The devices are inexpensive but do require additional board space.
In measurement applications where high reliability, small size and excellent readability are needed, the Hewlett Packard \#5082-7356 dot matrix LEDs may be used. Within the LCD case is an integrated circuit display latch, decoder and driver. The numeric display font matches the style used in alphanumeric dot matrix indicators. Instrument front panels can be designed without resorting to mixed font styles. The LEDs have operating ranges from $-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$. The family contains parts with $-55^{\circ} \mathrm{C}$ to $+100^{\circ} \mathrm{C}$ operating temperature range. When matched with similarly specified converters a very reliable, compact measurement and display module can be constructed for industrial and military applications.
A typical dot matrix LED interface is shown in Figure 1. The three LSD LEDs each contain a decoder, latch and driver. The one-half Digit MSD has only LEDs; two 4013 latches hold positive polarity information and the " 1 "MSD data. The TSC14433A encodes polarity information in the MSD BCD output as shown in Table 1.

In an overrange condition the data to the three LSDs is forced to all 1's through the 7432 OR gates. The HP\#50827356 LED display blanks when an all 1 's input is decoded. This added feature is at no additional cost since the gates are required as buffers to provide logic input drive to the LEDs. The MSD and sign bits are active in an overrange condition. A slight modification (Figure 2) causes the three LSD displays to "blink" ON and OFF for overrange analog inputs. The overrange bit (OR) remains low until an in range conversion completes. With OR $=0$ the Blink FF set is removed. The end-of-conversion (EOC) clock causes the display to blink at one-half the conversion rate. This visual blinking indicates more forcefully a measurement channel has overranged. Each display also contains a decimal point for range formatting.
Table 1: Half Digit And Polarity Coding

| Coded MSD | Data |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
|  | Q3 | Q2 | Q1 | Q0 |
| +0 | 1 | 1 | 1 | 0 |
| -0 | 1 | 0 | 1 | 0 |
| +0 UR | 1 | 1 | 1 | 1 |
| -0 UR | 1 | 0 | 1 | 1 |
| +1 | 0 | 1 | 0 | 0 |
| -1 | 0 | 0 | 0 | 0 |
| +1 OR | 0 | 1 | 1 | 1 |
| -1 OR | 0 | 0 | 1 | 1 |

## Notes

1. Q3- $1 / 2$ digit, low for " 1 ", high for " 0 "
2. Q2- Polarity: " 1 " = positive, " 0 " = negative
3. Q0- Out of range condition exists if $Q 0=1$. When used in conjunction with Q3 the type of out of range condition is indicated, i.e. $Q 3=0 \rightarrow O R$ or Q3 $=1 \rightarrow$ UR.


Figure 1: 3 1/2 Digit Multiplexed BCD Output ADC Interface to Dot Matrix LEDs with Decoder/Latches


Figure 2: Flashing Display on Overrange By David Gillooly

Many system applications require microprocessors to display data on seven segment light emitting diode (LED) displays. To minimize the number of input/output lines needed, a serial to parallel data bit conversion scheme can be used. The TSC9404 will perform a serial to 16-bit parallel output conversion. The TSC9404 outputs will each sink $60 \mathrm{~mA} @ \mathrm{~V}_{\text {SAT }} \leqslant 0.5 \mathrm{~V}$ for directly driving the LED displays.
The sixteen outputs will drive two seven segment displays plus two decimal points or annunciators. A serial output allows devices to be cascaded for more digits. Two digits, however, are adequate for many event, switch position, perceniage and temperature display applications.
A basic two digit display circuit is shown in Figure 1. The TSC9404 interfaces with a standard 6522 Versatile Interface Adapter (VIA) I/O chip. The 6522 communicates with a 6502 microprocessor. The VIA chip is widely used since it contains two configurable I/O ports, and timers. It also contains an 8-bit serial input/output shift register. The VIA shift register is configured as an output with the shift rate set by the phase 2 system clock. Data latches are not needed on the TSC9404 as the high speed data transfer is transparent to the eye. Two output shift operations will fill the TSC9404 with data for display.

Program operation is straight forward. (See program listing) The eight least significant data bits are loaded first from memory into the VIA shift register. The appropriate binary to seven segment display cude is obtained through a table look-up (Table 1) procedure. The number stored in memory is the table offset. Hex or special symbol display characters are possible by expanding the table. The VIA automatically shifts eighi data bits to the TSC9404. The program waits for a complete 8 -bit transfer before obtaining the most significant digit data from memory. The wait state is impiemented by testing the interrupt register shift complete flag bit with the shift register interrupt disabled. A memory map for the 6522
is shown in Table 2. The program/system was developed on a SYM-01 microcomputer board.

If decimal point drive is desirable the program is easily modified:

LDA Table, X
ORA LSBDP; Add \#01 for decimal point
STA SR
LDA Table, X
ORA MSBDP; Add \#01 for decimal point
STA SR
Similar programming techniques can be developed for alpha-numeric display using 14 or 16 segment LEDs. Bar graph displays are also possible.

Table 1: Decimal to Seven Segment Conversion Table

| Displayed Character | LED Segment <br> abcdefg DP | HEX Equivalent * |
| :---: | :---: | :---: |
| 0 | 11111100 | FC |
| 1 | 01100000 | 60 |
| 2 | 11011010 | DA |
| 3 | 11110010 | F2 |
| 4 | 01100110 | 66 |
| 5 | 10110110 | B6 |
| 6 | 10111110 | BE |
| 7 | 11100000 | E0 |
| 8 | 11111110 | FE |
| 9 | 11100110 | $E 6$ |
| "BLANK" | 00000000 | 00 |

* For decimal point add O1 to HEX code


Figure 1: High Current Serial I/O Port Expander

Application Note 20

## Serial I/O Port Expander; Two Digit, Seven Segment LED Drive Program Listing

| Address | Instructions |  |  | Label | Mnemonic | Operand | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{gathered} \text { Byte } \\ 1 \\ \hline \end{gathered}$ | $\begin{gathered} \text { Byte } \\ 2 \\ \hline \end{gathered}$ | $\begin{gathered} \text { Byte } \\ 3 \\ \hline \end{gathered}$ |  |  |  |  |
| 200 | A9 | 18 |  | Display | LDA | \#18 |  |
| 202 | 8D | OB | A8 |  | STA | ACR | ; Shift out under 2 Control |
| 205 | A9 | 80 |  |  | LDA | \#80 |  |
| 207 | 8D | OE | A8 |  | STA | IER | ; Disable shift register Interrupt |
| 20A | AE | 50 | 03 |  | LDX | LSB |  |
| 20D | BD | 00 | 03 |  | LDA | Table, X | ; Convert LSB decimal digit to seven segment code |
| 210 | 8D | OA | A8 |  | STA | SR | ; Send LSB to shift register |
| 213 | AD | OD | A8 | LSBTST | LDA | IFR | ; Load shift register flag |
| 216 | 29 | 04 |  |  | AND | MASK |  |
| 218 | FO | F8 |  |  | BEQ | LSBTST | ; Test for LSB shift completion |
| 21A | AE | 51 | 03 |  | LDX | MSB |  |
| 21D | BD | 00 | 03 |  | LDA | Table, X | ; Convert MSB decimal digit to seven segment code |
| 220 | 8D | OA | A8 |  | STA | SR | ; Send MSB to shift register |
| 223 | AD | OD | A8 | MSBTST | LDA | IFR | ; Load shift register flag |
| 226 | 29 | 04 |  |  | AND | MASK |  |
| 228 | FO | F8 |  |  | BEQ | MSBTST | ; Test for MSB shift completion |
| 22A | 60 |  |  |  | RTS |  | ; Return from subroutine |
| 300 | FC |  |  | Table |  | FC | ; Seven segment code 0 |
| 301 | 60 |  |  |  |  | 60 | $1$ |
| 302 | DA |  |  |  |  | DA | 2 |
| 303 | F2 |  |  |  |  | F2 | ; 3 |
| 304 | 66 |  |  |  |  | 66 | 4 |
| 305 | B6 |  |  |  |  | B6 | ; 5 |
| 306 | BE |  |  |  |  | BE | $; \quad 6$ |
| 307 | EO |  |  |  |  | EO | $; \quad 7$ |
| 308 | FE |  |  |  |  | FE | ; 8 |
| 309 | E6 |  |  |  |  | E6 | ; 9 |
| 30A | 00 |  |  |  |  | 00 | ; Blank |

Table 2: 6522 (VIA) Memory Map

| Address(Hex)* |  |
| :---: | :--- |
| A80E | IER - Interrupt Enable Register |
| A80D | IFR - Interrupt Flag Register |
| A80B | ACR - Auxiliary Control Register |
| A80A | SR - 8-Bit Shift Register |

Application Note 21 TSC700A Drives LED Display for TSC14433 ADC By Wes Freeman

The TSC700A high current driver chip can demultiplex the TSC14433 3 1/2 digit analog to digital converter data lines and drive an LED display. Because the driver powers the LED statically, the high transient currents associated with multiplexed LEDs are reduced. As a result, the design eases power supply and component layout requirements and minimizes the noise at the input.

An added feature of the TSC700A is the guaranteed 11 mA minimum LED drive current. This is over twice the current available from comparable drivers. LEDs driven by the TSC700A will be very bright and readable, an important consideration when instruments use large character height displays or operate in high ambient light environments.

The TSC14433 is a $31 / 2$ dig.t A/D converter which outputs data via four output pins ( $Q_{0}-Q_{3}$ ) and four data strobes (DS1 - DS4). The TSC700A contains four sets of 4-bit latches, $B C D$ to 7 -segment decoders, and static LED drivers with 11 mA current sink capability.

Circuit operation for the three least-significant digits is straightforward. The TSC14433 puts data on the Q0-Q3outputs and the appropriate digit strobe goes high, latching data into the TSC700A.

Table 1: TSC14433 Data Output
\(\left.$$
\begin{array}{lccccc}\hline \begin{array}{l}\text { Coded Condition } \\
\text { of Most Significant } \\
\text { Diglt (MSD) }\end{array} & \mathbf{Q}_{3} & \mathbf{Q}_{2} & \mathbf{Q}_{1} & \mathbf{Q}_{0} & \begin{array}{c}\text { Binary-coded- } \\
\text { Decimal-to-Seven- } \\
\text { Segment Decoding }\end{array}
$$ <br>
\hline+0 \& 1 \& 1 \& 1 \& 0 \& blank <br>
\hline-0 \& 1 \& 0 \& 1 \& 0 \& blank <br>
\hline+0 UR \& 1 \& 1 \& 1 \& 1 \& blank <br>
\hline-0 UR \& 1 \& 0 \& 1 \& 1 \& blank <br>
\hline+1 \& 0 \& 1 \& 0 \& 0 \& 4 \rightarrow 1 <br>
\hline-1 \& 0 \& 0 \& 0 \& 0 \& 0 \rightarrow 1 <br>
\hline+1 OR \& 0 \& 1 \& 1 \& 1 \& 7 \rightarrow 1 <br>

\hline-1 OR \& 0 \& 0 \& 1 \& 1 \& 3 \rightarrow 1\end{array}\right\}\)| hook up only |
| ---: |
| segments b |
| and c to MSD |

## Notes:

Q3: $1 / 2$ digit, low for 1 , high for 0
Q2: Polarity: $1=$ positive, $0=$ negative
$Q_{0}$ : Out-of-range condition exists if $O_{0}=1$; when used in conjunction with $Q_{3}$ the type of out-of-range condition is indicated;
$Q_{3}=0 \rightarrow O R$ or $Q_{3}=1 \rightarrow U R$

Obtaining the proper data for the half digit and polarity sign is more complex. Truth table 1 shows the TSC14433 data output when DS1 goes high. The data format was designed to be used with a discrete polarity-driver transistor and a BCD to 7-segment decoder that blanks the display when an invalid BCD digit is input. Only $Q_{3}$ and $Q_{2}$ are significant for the halfdigit display, however, so a combination of these signals can be found to light the proper segments of the TSC700A.

Truth table 2 shows the TSC700A display that results when $Q_{2}$ of the TSC14433 is inverted and shifted to $Q_{1}$, and Qo and $Q_{2}$ are always high. If outputs A1 and C1 of the TSC700A are used to light the half digit, and output F1 lights the positive polarity indicator, then additional external LED drivers are not required.

In the circuit, $Q_{2}$ is inverted by one half of the CD4013B D-type flip-flop and is then shifted to Q1 by the 74C157 quad 2-input multiplexer. When DS1 is low data passes through the multiplexer unchanged. With DS2 high, the inverted Q2 comes out instead on 2 Y and both 1 Y and 3 Y are set high. The TSC700A lecodes the inputs as shown in truth table 2 and the correct segments turn on. Because no segment is "on" for all possible inputs an external resistor is required to turn on the "-" segment of the polarity sign.

A flashing display is useful for indicating overrange, and can be implemented with the remaining 4013 flip-flop. Normally the OR output (pin 15) of the TSC14433 keeps the flip-flop reset, enabling the TSC700A display. An analog input exceeding full-scale causes OR to go low, removing the reset. The flip-flop now toggles at the end of each conversion, causing the display to flash.

Table 2: Decoded Output of the Display Driver

| Coded Condition Of Most Significant Digit | Output of TSC14433 $\mathbf{Q}_{3} \quad \mathbf{Q}_{2}$ | Input to <br> TSC700A <br> With $Q_{2}$ <br> Shifted to $\mathbf{Q}_{1}$ <br> And $Q_{0}, Q_{2}=1$ <br> $\mathrm{B}_{3} \mathrm{~B}_{2} \mathrm{~B}_{1} \mathrm{~B}_{0}$ |  |  |  | TSC700A Active Segment Drivers | Half- Digit Display |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| -1 | 00 | 0 | 1 | 1 | 1 | 5 | -1 |
| +1 | 01 | 0 | 1 | 0 | 1 | 7 | - |
| -0 | 0 | 1 | 1 | 1 | 1 | blank | - |
| +0 | 11 | 1 | 1 | 0 | 1 | L | - |



Figure 1: TSC700A Gives 3 1/2 Digit ADC a Bright LED Display with Flashing Display on Overrange

# *N TELEDYNE SEMICONDUCTOR 

Application Note 22 Software Combines With CMOS LSI to Form 3 3/4 Digit DVM By Wes Freeman

Single chip analog-to-digital (A/D) converters, with on-chip LCD or LED display drivers, have greatly simplified the design of sensor-to-human interfaces. However, the $31 / 2$ digit resolution ( 1,999 counts) typically offered is often inadequate. In particular, temperature systems suffer from a limit of 199.9 degrees farenheit with 0.1 degree resolution. In addition, direct drive outputs of single-chip converters make a microprocessor interface, which is often required for process control, very difficult. Finally, display A/D converters are usually limited to about three readings per second, which is sometimes too slow for systems applications.
By combining a 13 -bit, microprocessor-compatible, CMOSLSI A/D converter with software and a CMOS display driver, you can expand the system's measurement range to " $33 / 4$ "
digits ( 4095 counts). This system retains the low cost, low power, high accuracy and excellent noise rejection of the integrating A/D converter, while providing both sign-magnitude binary and BCD data. In addition, the system A/D converter can operate at speeds up to 30 readings per second. Also, all of the interface functions can be performed by only one LSI microprocessor interface chip. Hardware and software shown are for a 6502 microprocessor, but other processor/ interface devices can also be accommodated.
The hardware of the circuit is straightforward. Both A/D converter U2 and display driver U3 are interfaced to the microprocessor via $\cup 1$, a "versatile interface adapter" with 20 I/O lines. When the falling edge of U2's status output indicates an end of conversion, U1 generates an interrupt. The


Figure 1: 12-Bit A/D Converter with 3 3/4 Digit Display
One I/O device links both the A/D converter and decoder-display driver to a microprocessor. With data formatting in software, the circuit provides faster analog conversion speed and more resolution than $31 / 2$ digit display-oriented converters.
microprocessor then reads U2's conversion data in two bytes, selecting the high or low-order byte via the CA2 handshake output.
After converting binary data to BCD in software, the microprocessor loads LCD driver U3 via port B of U1. BCD digits are output on the lower four bits of port $B$, while the upper four bits serve as digit select outputs. The CB2 handshake output of U1 controls the polarity segment of the LCD display.
Software for the 3 3/4 digit converter consists of an interrupt service routine and a binary-to-BCD conversion subroutine. In response to a CA1 interrupt, the microprocessor jumps to the service routine of listing 1 . Using U1's peripheral control register to toggle U2's byte select inputs, the microprocessor reads and stores two bytes of binary data beginning at location BINARY. After stripping the flag bits from the most significant byte, the conversion's magnitude is stored beginning at BINSRC. The program transfers the sign bit to the display, and then tests for an overrange condition. If the $A / D$ converter is overranged, "EEEE" is sent to the LCD display. If the input is not overranged, the BCD conversion and display subroutine is called.

Binary-to-BCD conversion is accomplished by multiplying each binary bit by its equivalent decimal value and summing the bit values. Since each binary bit is some factor of two, only a multiplication by two is required. The multiplication can be reduced to a decimal add, since $A+A=2^{*} A$, and the SED (SEt Decimal) mode provides easy BCD addition.
The BCD conversion begins with the binary data in two memory locations, BINSRC and BINSRC +1 , which are used as a 16 -bit shift register. Two other locations, BCD and $B C D+1$ serve as a 4 digit BCD accumulator. The sixteen bits of binary data are shifted toward the most significant bit. Bits which are logical " 1 " are added, via the carry, to the BCD accumulator. After each shift, the BCD accumulator is added to itself (i.e. multiplied by two). On each succeeding pass, the sum of the binary bits is again multiplied by two. For example, bit 11 will go thru the multiplication loop eleven times and will then have a value of 2 11, or 2048. Bit 4 goes thru the loop four times, and ends with a value of 16. The sum of the BCD values for each bit of the binary word is the final BCD result. After sixteen shift/add cycles, the binary-to$B C D$ conversion is complete.


## Listing 2: Data Formatting and Display

This program converts binary data to $B C D$ by multiplying each binary bit by its decimal value. The LCD display is accessed one BCD digit at a time, using a shift register in memory to store the digit select bit.

## Software Combines with CMOS LSI to Form 3 3/4 Digit DVM

Although the BCD conversion program shifts data sixteen times, only twelve bits are valid. This method was chosen for compact coding. A slight speed penalty is involved, however, since the program unnecessarily loops through the multiplication routine four times. With a 1 MHz 6502 clock, the total execution time (listing 1 plus listing 2 ) is about 1.07 mSec . Program execution will be slightly faster if the binary data is shifted left four times at BIN2BCD and the $Y$ register loop counter is changed from 16 to 12.
After conversion to BCD format, the conversion result is transferred to the display via Port B of U1. The display driver


Flowchart 1: Interrupt Service Routine
The A/D converter result is read in two bytes and then is tested for polarity and overrange. If not overranged, the binary data is converted to BCD and displayed.
requires data to be stable on the $\mathrm{BO}-\mathrm{B3}$ inputs while the appropriate digit select input (D1 through D4) is strobed high. The program uses memory location DIGSEL as a shift register to sequentially address each of the four digit select inputs. BCD data is loaded into the 6502's accumulator, the digit select bit is turned on, and the accumulator contents are transferred to $\cup 1$. The digit select bit is then turned off and DIGSEL is shifted to point to the next digit. After four digits have been transferred the program is complete, and the microprocessor returns to its main program.


Flowchart 2: Binary to BCD Conversion
Bit by bit, MSB first, binary data is added to the two-byte $B C D$ accumulator. Each time through the loop the BCD accumulator is added to itself. The result is that each binary bit is multiplied by its decimal value.


Flowchart 3: Data Transfer to LCD Display
Looping twice transfers four BCD digits to the LCD display decoder-driver. For each digit transferred, the four LSBs contain the BCD data, while one of the four MSBs is turned on to function as the digit select.

Micro-processor based systems, whether they be complex process controllers, bench top instruments, portable measurement devices, or computer data acquisition systems dominate the market place of the 1980s. Microprocessors maximize creativity and innovation within engineering and marketing teams. The ability to product differentiate and efficiently manufacture products for many market segments from one basic design "customized" through software maximizes the investment return on R\&D expenditures.

The CMOS TSC800 16-bit integrating analog-to-digital converter was specifically designed for easy processor interface. The TSC800 data transfer is no more complicated than two memory read operations.
Parallel 8 or 16-bit data transfer and serial data transmission with a Universal Asynchronous Receiver Transmitter (UART) is straightforward. The serial data transfer option makes optically isolated systems practical and low cost.

The 16 -bit sign magnitude code maximizes dynamic range, resolution, and accuracy. An N bit sign magnitude ADC has twice the resolution of an $N$ bit offset binary ADC. The large

| Parameter | TSC800 | TSC7109 | Units |
| :---: | :---: | :---: | :---: |
| Resolution | 15 | 12 | Bits |
| Max. Linearity Error | 0.006 | 0.024 | \% |
| Dynamic Range | 96 | 78 | dB |
| Zero Scale Drift | 0.8 | 0.2 | $\mu \mathrm{V}$ |
|  |  |  | ${ }^{\circ} \mathrm{C}$ |
| Maximum Power Dissipation | 20 | 15 | mW |
| Conversion Technique | Integrating Dual Slope <br> (4 Phases) | Integrating Dual Slope (3 Phases) | - |
| Conversion Rate | 2.5 | 40 | Conv/ Sec |
| Differential Input | Yes | Yes | - |
| Maximum Input Current | 15 | 10 | pA |
| Sign/Magnitude Coding | Yes | Yes | - |
| UART Interface | Yes | Yes | - |
| Internal Voltage Reference | No | Yes | - |
| Automatic 60 Hz Rejection | Yes | Yes | - |
| Power Supply Voltage | $\pm 5 \mathrm{~V}$ | $\pm 5 \mathrm{~V}$ |  |
| Price Per Bit (100 pc Quantity) | \$0.95 | \$0.77 |  |

Table I: TSC800 Electrical Specifications
dynamic range can be used to eliminate expensive analog components needed to obtain full 12-bit performance with 12-bit ADCs.
The TSC800 integrating conversion technique eliminates the need for a sample hold amplifier and automatically attenuates noise. A 400 mS measurement cycle gives a 100 mSec signal integration time. This provides both $50 / 60 \mathrm{~Hz}$ line frequency rejection. The conversion time is more than adequate for process control, data logging, and physical environment monitoring applications where "real time" is measured in seconds and minutes. The converter LSB size can be as low as $100 \mu \mathrm{~V}$.

By combining digital and analog functions on a single CMOS chip, excellent resolution, accuracy, and interface capability are simultaneously achieved without a high price (Table 1). The 16-bit TSC800 costs only $12 \%$ more on a price-per-bit basis than similar 13-bit monolithic devices (Figure 1). When compared to high resolution hybrid devices, an order of magnitude cost savings results. When maximum conversion speed is not required the TSC800 offers exceptional value. With a reference, crystal and half dozen passive components, a complete, bus-compatible 16-bit ADC is available.

The TSC800 analog section contains an input buffer, integrator amplifier, comparator, and analog switches (Figure 2). The differential high impedance CMOS inputs have only a 15 pA maximum leakage current. Input common mode voltage range extends to 1 V of the supply; common mode rejection is typically 86 dB . The low noise metal gate CMOS process and design limits noise to $15 \mu \mathrm{VP}-\mathrm{P}$. A system zero phase is included in each TSC800 measurement cycle to cancel buffer, integrator, and comparator offset voltage and drift characteristics. An external potentiometer adjustment is not


Figure 1: High Resolution TSC800 Features High Performance and Low Price for Low Speed Systems.


Figure 2: Analog and digital compatible CMOS process provides single chip 16-bit converter.
needed to guarantee a zero output for zero volt input. Temperature drift at zero is automatically corrected.
The TSC800 digital section includes an RC or crystal oscillator clock generator, 15 -bit counter, 16 three-state data latches, data transfer/conversion control logic, and sign bit logic. The analog and digital compatible metal gate CMOS process allows such extensive circuitry on a single monolithic die.
The oscillator control pin selects either RC or crystal oscillator operation. Normally, crystal operation is desired. In this mode, a divide by 15 counter is inserted between the oscillator and TSC800 internal counters. The divider allows a standard 2.4576 MHz UART crystal to provide the 163.84 kHz internal clock. A 400 mSec measurement cycle results with a 100 mSec signal integrate time for $50 / 60 \mathrm{~Hz}$ noise rejection.
Sixteen three-state data latches, two control inputs, and three dual fuction input/data strobe outputs simplify the interface to peripherals. Microprocessor busses, I/O peripheral ports (with or without handshake control) and UARTs are easily supported. The data outputs are TTL-compatible and have sufficient current sink capability to drive a small processor bus directly. Data is coded in a sign magnitude format (15 bits Data + Sign Bit). The TSC800 provides twice the resolution of 15 -bit offset binary converters. The sign bit is valid for signals less than one least significant bit giving an extra bit of resolution around zero. A precision nulling scheme may be implemented under processor control.
The TSC800 adds two additional phases to the conventional two-phase dual slope integrating conversion method to achieve the given price and performance characteristics. The measurement cycle is divided into four separate phases (Figure 3).

- System Zero
- Signal Integrate
- Reference Integrate
- Integrator Zero

The system zero phase (Figure 4A) begins when the internal analog switches connect the buffer input to analog common and a feedback loop closes around the integrator and comparator. The external capacitors charge to compensate for buffer, integrator, and comparator offset errors. With a zero input at the buffer, the integrator output will remain at zero.
Since the converter's major error sources are nulled during each measurement cycle, temperature sensitivity is greatly reduced. The zero scale error drift, always a large error source in successive approximation converters, is reduced to typiclly $0.8 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$.
The signal integrate phase follows (Figure 4B). The differential input signal is applied to the integrator for 16,384 internal clock cycles. The integrator output at the end of the fixed time is proportional to the input. Since the integrate time is fixed by the clock period, the interval can be adjusted to give maximum attenuation of repetitive waveforms such as $50 / 60$ Hz power line signals. A 100 mSec integration rejects 50,60 and 400 Hz signals.
In the reference integrate or deintegrate cycle (Figure 4C), the reference capacitor, which was charged to the reference voltage during system zero, is conneced to ramp the integrator back toward zero. The 15 -bit counter is enabled and counts until a zero crossing is detected by the comparator. Data is transferred to the data latches and Data Valid (DVD) goes low. This cycle normally lasts 32,678 clock period.
The final phase is integrator output zero (Figure 4D). This phase provides a rapid recovery from overloads by connec-


Figure 3: TSC800 integrating converter updates conventional dual slope conversion with system zero and integrator zero phase.
ting the comparator output to the buffer input for 4096 clock cycles. Any charge remaining in the integration capacitor is removed, allowing an accurate system zero cycle.
The TSC800 supports either continuous or convert on command operation. When the Conv/ $\overline{\text { Stop }}$ input is low, the converter remains in the system zero phase. A new conversion
will not begin until Conv/ $\overline{\text { Stop }}$ goes high. Conv/Stop has no effect when Data Valid (DVD) is high, but pulsing the Conv/Stop low after a comparator zero will immediately terminate reference integrate and cause entry into the zero integrator phase. In this case, the conversion rate will vary with input signal magnitude.


4A: TSC800 System Zero Phase


4C: TSC800 Reference Voltage Integration Cycle


4B: TSC800 Input Signal Integration Phase


4D: TSC800 Integrator Output Zero Phase

Figure 4: Internal analog gates automatically configure analog circuits for four phases of TSC800 measurement cycle.

# TSC800 Wide Dynamic Range Eliminates System Components 

## 15-BIt Resolution Eliminates Gain Amplifiers

Along with high accuracy and resolution, the TSC800 large 96 dB dynamic range solves problems usually needing additional analog components. Since each analog component adds an error term, eliminating unnecessary devices increases system accuracy and reduces cost. Error budget calculation and allocation for the design engineer is also made easier.

A circuit capitalizing on the TSC800 wide dynamic range is shown in Figure 5. The TSC800 dynamic range eliminates a precision analog amplifier. Twelve-bit resolution and accuracy is desired for digitizing the analog signals from $\pm 0.4096$ V to $\pm 3.2768 \mathrm{~V}$. A 12-bit ADC cannot accomodate this range


Figure 5: 15-Bit Dynamic Range Converter Eliminates Programmable Gain Amplifier.
without sacrificing resolution. The 12-bit ADC based system normally resolves the dilemma by using a programmable gain amplifier with gains of $1,2,4$, and 8 . This amplifier is, unfortunately, expensive and a system error source.
The 15-bit TSC800 based system replaces the programmable gain amplifier and, through a software routine, full 12-bit resolution is achieved. The TSC800 can be viewed as a 15-bit, $\pm 0.4096 \mathrm{~V}$ full-scale ADC with a built-in gain of eight (Figure 6 ). Analog inputs up to $\pm 0.4096 \mathrm{~V}$ are correctly converted by the TSC800 to 12-bit resolution. The Data bits B15, B14, and $B 13$ will be logic " 0 ".
If the applied analog input is greater than $\pm 0.4096 \mathrm{~V}$, the host computer can divide the 15-bit output to adjust for a 12-bit full-scale input. Dividing by 2,4 , or 8 corresponds to reducing the TSC800 "internal amplifier" gain to 4, 2, or 1, respectively. The TSC800 gives full 12-bit resolution at the maximurn fullscale input, even with the non-zero starting point.

The necessary division is easily accomplished by software with a simple right shift of the TSC800 15-bit output (excluding the sign bit). Shifting right one, two, or three times divides by 2,4 , or 8 . Bits B15, B14, and B13 should be set to zero after the shift operation, since the sign bit will shift into the mosi significant bits during the operation.

## Current Loop Monitoring Benefits From Wide Dynamic Range

Another design simplification made possible by using high dynamic range converters involves the popular industrial 4 to 20 mA current loop. The task is to provide a 12-bit conversion.
A simple resistive current to voltage conversion causes a 0.1024 V output offset voltage (Figure 7A). The offset causes a problem because the maximum analog input is 0.512 V . The ADC must have a 0.512 V full-scale range; an ADC which digitizes inputs from 0 to 0.512 V with 12-bit resolution cannot provide 12-bit resolution for the reduced input span of $0.4096 \mathrm{~V}(0.512 \mathrm{~V}$ to 0.1024 V$)$.


Figure 6: TSC800 15-Bit Output is Same as 12-Bit ADC Preceded With Amplifier Gain of 1, 2, 4, or 8.

An operational amplifier can be used to cancel the 0.1024 V offset (Figure 7B). The net ADC input voltage for a 4 mA (zero signal) input is 0 V . The op amp operates at unity gain giving a 0.4096 V full-scale input. The op amp allows a 12-bit resolution conversion.

The offset cancellation scheme works, but the price paid is high; the active component and five passive components increase cost, consume board space, and lower reliability. An offset adjustment procedure must be performed during production and the potential for field misadjustment increases.

The TSC800 dynamic range allows the op amp and passive components to be eliminated by a software-generated "offset voltage." The TSC800 easily digitizes the 0.1024 V to 0.512 V input to 12 -bit accuracy. A simple 1024-count software subtraction from the 15 -bit conversion produces a 12 -bit, 0 V to 0.4096 V conversion (Figure 7C).

The reduced part count and one less calibration step will offset the additional 15-bit ADC cost. The system accuracy and increased reliability also enhance end product value.


7A: Resistive Current to Voltage Conversion Causes Offset Voltage.


7B: For 12-Bit Resolution An Offset Cancelling Op Amp is Needed.


7C: Offset Voltage Corrected in Software Subtraction Routine.
Figure 7: 16-Bit Dynamic Range ADC Provides Full 12-Bit Resolution Without Analog Offset Correcting Components.

## Automatic Tare Weighing System Eliminates Analog Components

The digital offset correction scheme is useful in digital weighing systems where automatic tare is desired. Auto-tare weighing systems automatically subtract the container's weight from a measurement; the scale displays a true reading just of the contents weight. The container's weight must be measured, stored, and subtracted from the total weight.
A strain gauge or load cell represent typical weight sensors. Strain gauge output levels are below the resolution level of ADCs; amplification is required. Amplifier-related errors are unavoidable, but become magnified in auto-tare systems. The container weight must be subtracted from the total weight to yield the true content weight.

One circuit that subtracts uses a sample/hold amplifier and operational amplifier (Figure 8A). With an empty container on the weighing platform, the sample/hold amplifier samples and holds the op amp output voltage. The voltage stored on the sample/hold amplifier hold capacitor represents the container's weight. The sample/hold output is connected to the op amp's inverting input, effectively subtracting the container's weight. The analog components to store the container's weight limit system performance. For example, the sample/hold droop rate will limit the maximum allowable time between sampling the container's weight and weighing the filled container. The operational amplifier gain must also be calibrated.


Figure 8: TSC800 Scale System Eliminates Analog Droop Errors and Precision DAC.

The droop rate problem inherent in the sample hold subtract circuit can be avoided by using a digital-to-analog converter (DAC) for the feedback subtraction voltage. Figure 8B shows the sample/hold replaced by a DAC. The host computer converts the op amp output to a digital value through an ADC. The digital value is stored and transmitted to the DAC. The reconverted subtraction voltage applied to the op amp input is not subject to droop errors. The time interval between container weighing and substance weighing is unlimited.

The DAC-based subtraction circuit has drawbacks. The DAC must be calibrated so its output exactly tracks the ADC fullscale input voltage. The container weight correction occurs in discrete steps, so the DAC dynamic range must match the range of container weights to be encountered. If not, the cancellation circuit resolution will limit system accuracy. This constraint becomes significant when the container is a significant percentage of total. Weighing gravel in a truck or aspirin in a glass bottle are two examples.
The TSC800 large dynamic range makes analog components unnecessary. In Figure 8C, the TSC800 first measures the container weight. The digital value is stored in memory and a second conversion is made with total load. A software routine subtracts the stored container weight and the result is tare weight.
The TSC800 method is conceptually the same as the DACbased system. Several advantages make the TSC800 solution better. The ADC performs both conversions, so full-scale
errors cancel. The 15-bit TSC800 gives impressive resolution and range; 20,000 pounds of gravel in a 12,000 pound truck, or 0.01 gram of aspirin in a 300 gram bottle!

## Data Bus Interface

A commercially successful analog-to-digital converter must offer more than high resolution and accuracy for wide market acceptance. The converter's data transfer capabilities are equally important. A converter able to fit easily in 8 or 16-bit data systems, as well as serial configured systems, will be widely used and offer long-term price advantages over less functional components. The TSC800 transmits data in two 8bit parallel words, or one 16-bit wide byte. Serial transmission through Universal Asynchronous Receiver Transmitters (UARTs) is possible by using the handshake data transfer mode. Continuous or convert on command conversions are possible. The TSC800 can be used in interrupt-driven data transfer applications.

Data transfer is completely under user control with the TSC800. The bus interface mode allows a direct connection to a processor data bus. The dual function LBEN (Bits 1-8) and HBEN (Sign, Bits 9-15) inputs along with chip enable $\overline{(C E)}$ activate the three state data outputs.
Figure 9 pictures a typical interface. Address bit A0 and $\overline{\mathrm{AO}}$ drive the byte select inputs. Additional decoded address bits enable the TSC800. A complete 16-bit data transfer requires


Figure 9: A low-cost interface results when you access the TSC800's 16 data bits directly by treating the converter as two memory locations.

## Application Note 23

TSC800 Wide Dynamic Range<br>Eliminates System Components

two memory read operations. All 16-bit data lines can be active for 16 -bit wide date bus (Figure 10). Monitoring the TSC800 data valid signal ( $\overline{\mathrm{DVD}}$ ) allows the user to verify data did not change during the two byte operation.


Figure 10: Three state data bus controlled by byte select and chip enable control signals.

The bus data transfer mode supports interfaces using peripheral input/output chips like the 6522 Versatile Interface Adapter and 8255 Programmable Peripheral Interface Device. Data access involves selecting and reading two I/O ports. The interface in Figure 11 does not need additional software, as the 6522 and 8255 I/O ports initialize as input ports at power-up or on reset.
A data error may result if data changes - because of a new conversion update - between the processor's high and low byte read cycles. An easy error detection scheme is implemented with the peripheral I/O chip programmed for strobed input operation. The $\overline{\mathrm{DVD}}$ signal is used to strobe data into the I/O chip. The strobe signal also sets the I/O chip interrupt flag, but a processor interrupt is prevented by clearing the interrupt enable register. To access data, the microprocessor reads port A (which resets Port A's interrupt flag), then port B, and finally the port A interrupt flag. If port A's interrupt flag is set, an output data latch update occurred during the read cycle. If the interrupt flag remained clear, then both data bytes are valid.

| $\overline{C E}$ | $\overline{\text { HBEN }}$ | $\overline{\text { LBEN }}$ | High Data Byte <br> (SGN, DB15- DB9) | Low Data Byte <br> (DB8 - DB1) |
| :--- | :--- | :--- | :--- | :--- |
| 1 | X | X | Inactive <br> (High Z State) | Inactive <br> (High Z State) |
| 0 | 0 | 0 | Active | Active |
| 0 | 0 | 1 | Active | Inactive <br> (High Z State) |
| 0 | 1 | 0 | Inactive <br> (High Z State) | Active |
| 0 | 1 | 1 | Inactive <br> (High Z State) | Inactive <br> (High Z State) |

$" X "=1$ or 0


Figure 11: Using an I/O port simplifies $\mu \mathrm{P}$ interfacing. Reading the interrupt flag register prevents data overrun.

## Serial Data Transfer <br> With Handshake Mode

The TSC800 actively controls the data transfer to peripherals in the handshake data output mode. The load strobe (LDSTRB) output signal indicates valid data is available for the peripheral receiving device. The low byte (LBFLG) and high byte (HBFLG) outputs signal which data byte is available. The data request input signal (DRQST) informs the TSC800 a peripheral is ready to accept data. A complete cycle transfers two 8-bit bytes.
The handshake mode suports remote data acquisition systems using serial data transmission through current loop, RS232 or fiber optic data links. Universal Asynchronous Receiver Transmitter (UART) communication ICs provide an inexpensive parallel to serial conversion. Start, stop, and parity bits, if required, are automatically inserted on transmission and removed on reception. Data Transmission errors are automatically flagged. The TSC800 handshake mode exactly matches UART input and control requirements, making serial data transmission a practical reality (Figure 12). The UART relieves the system engineer from designing a complex serial data transmission subsystem. The easy TSC800 to UART interface lets the design engineer focus on the data acquisition task, rather than chip interfacing details and serial interface protocols. UARTs are multi-sourced in a variety of technologies: CMOS, NMOS, and PMOS. Some devices lower system part count by including on-chip baud rate generators.
Serial data transfers, especially in high resolution systems, are often dictated on a cost basis when the ADC distance from the digital processing unit exceeds several feet. Serial transmission greatly reduces the number of cables and line driver/receiver units. When system isolation through optical couplers is desired, cost savings are magnified.
A complete serial data link is shown in Figure 13. The TSC800 handshake mode is set each time the UART receives a
character. The TSC800 automatically transmits two parallel bytes to the UART for serial transmission. The converter's 2.4576 MHz clock serves double duty by driving the F4702 baud rate generator. Serial data rates between 50 and 19,200 baud are selectable.
When the UART receives a word, the Data Received (DR) output goes high, forcing the TSC800 into the handshake data transfer mode. Once the handshake mode is entered by setting the TSC800 internal handshake flip-flop, the $\overline{B U S} / \mathrm{HAND}$ input pin state is ignored.
The DATA REQUEST (DRQST) input is tested for a high UART TRANSMIT BUFFER REGISTER EMPTY (TBRE) signal that indicates the UART is able to accept data. With TBRE high, the High Byte Data Flag (HBFLG) goes low and the sign bit plus B15-B9 data bits become active. The Load Strobe (LDSTRB) pulse latches the data into the UART transmitter holding register and resets TBRE. The TSC800 tests DRQST again for an indication the UART has sent the first data byte and is ready to accept data (TRBR = 1). $\overline{\text { LBFLG }}$ goes low and output bits B1-B8 become active. LDSTRB pulses low again, latching the final byte into the UART. The $\overline{\text { LBFLG }}$ transition also resets the UART Data Received (DR) output and ends the handshake transfer. Only one conversion is transmitted in response to each word received by the UART.
The TSC800 data latch updating is prevented during the handshake to eliminate improper data transmission. The transmitted data is always the result of the conversion completed before $\overline{B U S} / \mathrm{HAND}$ went high. Conversions can be continuously transmitted, if desired, by tying HAND high. The handshake mode is then entered at the end of each TSC800 conversion.
Access to several converters can be achieved with only one UART. Two TSC800 converters in Figure 14 give a twochannel link. Output decoding provides room for 6 more ADCs; up to 256 TSC800s can be addressed with additional decoders.


Figure 12: UART interface uses data request signal to control handshake data transfer.

The data handshake starts, as before, by the host computer sending a word to the UART. The word's three least significant bits (LSB) address the desired TSC800. The three LSBs are decoded by a three of eight decoder which drives the TSC800 BUS/HAND control input. When the word is received, the DR output also goes high. An RC network and CMOS Schmitt trigger delays the DR signal to allow the decoder outputs to settle. The delayed DR pulse enables the decoder and the selected TSC800 is pulsed into the handshake mode. Note that once the handshake mode is entered, the HAND input signal is ingored. The delayed DR output also causes the DATA RECEIVED RESET input to go low. This resets the DR output and disables the decoder until another word is transmitted from the host computer to the UART. The selected TSC800 transmits the last data conversion to the host computer.
Also shown in Figure 14 is a less expensive baud rate generation circuit. A simple CMOS counter can provide common baud rates between 300 and 9600 , since the required frequencies are multiples of the 2.4576 MHz TSC 800 clock. If more than two ADCs operate from one crystal, the BUF OSC pin should be buffered with an external CMOS buffer.

## Interrupt Data Transfer Uses Handshake Mode

The handshake mode is not limited to serial data transmission applications. A system using peripheral I/O circults like the 6522 or 8255 for interrupt-driven data transters can use the handshake mode. Only one 8-bit port is required, freeing 1/O pins for other tasks. The handshake interface guarantees
data will not be accessed as the internal data latches are updated. Two processor interrupts will transfer data.
The TSC800 to 8255 interface in Figure 15 uses HAND tied high. This forces the handshake mode whenever a new conversion is completed. The 8255 negated INPUT BUFFER FULL (IBFA) signal is the DRQST input signal. $\overline{\text { LDSTRB }}$ strobes data into the 8255 port latch and sets the data request $\left(I B F_{A}=1\right)$ signal. DRQST is removed and the TSC800 remains in the handshake mode checking DRQST for the next data byte request. Once IBF is set, the 8255 generates an interrupt request. During the interrupt service routine, port A is read resetting the IBF bit. The second data byte request is generated and the low data byte becomes active. $\overline{\text { LDSTRB }}$ initiates the second interrupt request cycle. A similar interface based on the 6522 is shown in Figure 16.

## Versatility and Performance At An Affordable Price

The TSC800 design achieves $0.006 \%$ linearity without requiring laser trimming. Self-correction circuits automatically compensate for CMOS amplifier shortcomings. This lowers process complexity and increases reliability; both factors contribute to a modest selling price and low non-delivery risk. A proven metal gate CMOS process was chosen for the TSC800 to guarantee manufacturability. The development programs focused on functional performance, technical specifications, and device producibility. The TSC800 gives the designer interface options and excellent electrical performance at a price that will make new products and systems technically feasible and financially successful.


Figure 13: Serial data transmission is easy when the ADC logic Includes UART handshaking signals. The TSC800 monitors its DATA REQUEST pIn untll the UART is ready to recelve data.

Figure 14: Accessing any one of several remote TSC800s is simple. Just send the ADC address in the word that triggers handshaking.


Figure 15: Handshake mode and peripheral I/O chip ease interrupt-driven data transfer.


Figure 16: Interrupt-driven data transfer requires only one I/O port.

## APPENDIX A

## Integrating Analog-to-Digital Converter Basics

Successive approximation converters output digital words proportional to the input voltage at a given time. If the input level shifts before all bits are resolved, the conversion will be grossly in error. To prevent this sample-hold circuits often precede the SAR ADC. Noise may also make the conversion unuseable or unrepeatable. The integrating converter digital output represents the input signals integral over a given time period; the output code is proportional to the input signal average value during the time period.
Most commercially available, integrating converters use the dual slope conversion technique (Figure A). As the name implies, two phases make up a complete measurement cycle:

- Input Signal Integrate: Integrate phase
- Reference Voltage Integrate: Deintegrate phase

The basic quantization unit for successive approximation converters is current. Integrating dual slope converters use time. Time is easily monitored by counting clock pulses. Accuracy is excellent, being limited only by short-term clock stability. Low differential and integral linearity errors are easily achieved without expensive and drift-prone laser trim techniques.
The analog input is integrated for a fixed time $T_{1}$ :

$$
\underset{\text { Time }}{\text { Integration }}=\mathrm{T}_{\mathrm{l}}=\mathrm{N}_{\mathrm{I}}\left(\frac{1}{\mathrm{f}_{\mathrm{C}}}\right)
$$

Where:

$$
\begin{aligned}
& N_{1}=\# \text { Clock Periods in Integration Phase } \\
& \mathrm{fc}=\text { Counter Clock Frequency }
\end{aligned}
$$

Following the signal integrate phase, a constant magnitude reference voltage is applied to the integrator input. With a polarity opposite to the input signal, the reference signal ramps the integrator output toward zero at a constant rate. A counter totals the number of clock pulses until a comparator signals the integrator has returned to zero volts.



Figure A: Integrating Dual Slope Converter Uses Time to Quantize Input Signal. Accuracy Set by Short Term Oscillator Clock Stability and Reference Stability.

Since the "ramp-up" and "ramp-down" voltages are equal, a simple formula characterizes the conversion:
"Ramp-Up" Voltage - "Ramp-Down" Voltage $=0$

$$
\frac{1}{R C} \quad \int_{0}^{N / T C} V_{I N}(t) d t=\frac{1}{R C} \quad \int_{0}^{N U T C} V_{R} d t
$$

Where:

$$
\begin{aligned}
& \mathrm{N}_{\mathrm{I}}=\text { \# Clock Pulses in Signal Integrate Period } \\
& \text { (Fixed) } \\
& \text { Nu = \# Clock Pulses in Reference Integrate Period } \\
& \text { (Variable) } \\
& \text { Tc = Clock Period } \\
& V_{R}=\text { Reference Voltage } \\
& V_{\text {IN }}(t)=\text { Input Signal } \\
& \int_{0}^{N / T_{C}} V_{I N}(t) d t=V_{R} N U T C \\
& \frac{1}{N_{I T C}} \int_{0}^{N / T C} V_{I N}(t) d t=\overline{V_{I N}}=\frac{N U}{N_{1}} V_{R} \\
& N U=\overline{V_{I N}}\left[\frac{N_{I}}{V_{R}}\right]
\end{aligned}
$$

Where $\mathrm{V}_{\mathrm{IN}}=$ Average Value of $\mathrm{V}_{\mathrm{IN}}(\mathrm{t})$ over the Integration Period $\mathrm{T}_{\mathrm{I}}$.
The number Nu is stored in an internal counter. The counter can be decoded to give binary, BCD, or seven-segment visual display information.

The conversion accuracy does not depend on the external RC values. Reference stability and the equality of clock periods between phases establish basic accuracy limits. Oscillator stability is only required for the 10 to 400 mSec typical conversion times.
Automatic polarity detection for sign magnitude coding is easy. The comparator output provides a polarity indication that can select the proper polarity reference during the reference deintegrate phases, as well as set a sign bit flipflop. Dual polarity converters store the reference voltage across a capacitor that is switched into the integrator with the proper polarity. Low charge injection switching and a large external reference capacitor give excellent full-scale symmetry. Differences in full-scale conversions for equal magnitude but opposite polarity signals can be as low as 1 count. An N bit + sign integration converter has twice the resolution
of an N bit offset binary ADC (Figure B). The sign bit is also accurate for signals less than 1 LSB. This can be useful in precision nulling applications.


Figure B: Sign magnitude coding gives twice the resolution of offset binary.

By adding a system zero phase to the measurement cycle input buffer, integrator and comparator offset voltage and temperature induced offset drift errors can be eliminated. Manufacturers can easily guarantee a zero digital code for zero volt input without requiring any user adjustments. This is a real advantage since integrating converters typically operate with the LSB representing $100 \mu \mathrm{~V}$.
The simplified system zero loop in Figure C shows the inputs disconnected from the analog signal inputs and grounded. A loop is closed around the comparator so its Vos error is also corrected. During the auto-zero time period, compensating error voltages are stored on the system zero capacitor CAZ and integration capacitor Cl .


Figure C: During system zero phase offset voltage error correction voltages are stored.

With $S_{1}, S_{2}$, and $S_{3}$ reconfigured for the signal integrate period, a set of simple equations explains how offset voltage error terms are cancelled.
A conversion ends when the comparator indicates a zero crossing has occurred:
$V_{\text {OSI }}-V_{\text {OSC }}-\frac{V_{R}}{R_{I} C_{I}} N_{I} T C+\frac{V_{I N}}{R_{I} C_{l}}\left(N_{U T C}\right)=\left(V_{\text {OSI }}-V_{\text {OSC }}\right)=0$
$V_{R}(N \cup T C)=V_{I N}(N \mid T C)$

$$
V_{I N}=V_{R}\left[\frac{N_{U}}{N_{I}}\right]
$$

As in the ideal circuit, VIN is directly proportional to the stored count; all offset error terms are removed.

A further refinement may be added to the dual slope converter with automatic offset voltage correction. The integrator output is assumed to be at zero volts when the system zero phase is entered. The integrator may, however, not return to zero due to an over-range input signal. This is common in multiplexed systems. In such a case, a charge proportional to the output voltage is transferred to Csz. The system will not zero offset correctly until the transferred charge has dissipated. The circuit time constant is large - $\mathrm{RI}_{\mathrm{l}}\left(\mathrm{Csz}_{\mathrm{I}}+\mathrm{C}_{\mathrm{l}}\right)$ - taking several conversion cycles to decay (Figure D).

An additional phase in the measurement cycle corrects for overrange induced errors. The comparator is reconfigured to form a feedback loop around the integrator. The circuit time constant is reduced, since the integration resistor is now driven by a signal proportional to the integrator output rather than being fixed at ground potential (Figure E).


Figure D: Non-zero integrator output causes error when system zero cycle is entered.


Figure E: Integrator zero cycle returns integrator output to zero volts before system zero cycle is entered.

Integrating converters provide noise rejection automatically with at least a $20 \mathrm{~dB} /$ decade attenuation rate. In addition, interference signals with frequencies at integral multiples of the integration period are theoretically completely removed. This intuitively makes sense, since the average value of a sine wave of frequency $1 / T$ averaged over a period $T$ is zero. The finite time integrator frequency attenuation characteristic is easily derived by doing a Fourier transform on the circuits impulse response function (Figure F).
Integrating converters often establish the integration period to reject $50 / 60 \mathrm{~Hz}$ line frequency interference signals. The ability to reject such signals is shown in a normal mode rejection plot (Figure G). Normal mode rejection is practically set to $50-65 \mathrm{~dB}$, since the $50 / 60 \mathrm{~Hz}$ line frequency can deviate by a few tenths of a percent (Figure H).


Figure G: Normal Mode Rejection Vs. Input Frequency.


Figure H : Integrating converter normal mode rejection vs. 60 Hz line frequency variations.


A: Ideal Integrator


B: Ideal Fixed Time Integrator Impulse Response

$$
H(j \omega)=\int_{0}^{T} h(t) e^{-j \omega T} d t=\frac{\operatorname{SIN}(\omega T / 2)}{\omega T / 2}\left[e^{-j \omega T / 2}\right]
$$

C: Ideal Fixed Time Integrator Frequency Response
Figure F: Frequency domain response of finite time integrator explains noise rejection characteristic of dual slope ADC.

Application Note 24 TSC7109 Records Remote Data Automatically By Wes Freeman

A Teledyne Semiconductor analog-to-digital converter, a $2 k$ byte CMOS static RAM, and some gates and counters can be combined to form a low cost, flexible, stand alone data logging system. All the ICs are CMOS and the clock frequency is low, so power supply current is only a couple of milliamperes. The unit will store a 13-bit conversion (12-bit plus sign) in two consecutive bytes of memory, with a programmable time interval between measurements. The circuit is useful for logging temperature or other process control variables in remote locations or hostile environments. It is also useful in the lab for making unattended, repetitive measurements of long term drift, component aging, etc.
The heart of the circuit is a TSC7109 (IC1), a 12-bit plus sign CMOS A/D converter. The TSC7109 has a handshake mode in which the result of the latest conversion is output, in two consecutive bytes, each time the MODE input is strobed high. The data logger stores each byte in sequential RAM locations for later processing by a host computer. The IDT 6116 CMOS static RAM stores 2048 bytes and therefore can store 1024 readings. This permits, for example, one 13-bit measurement per hour for seven weeks.

Timing for the circuit is provided by IC3, operating with an inexpensive 32 kHz crystal. The crystal can be replaced with a resistor and capacitor if precise timing is not required. The Q4 output of IC3 provides a clock frequency to the A/D converter that produces excellent $50 \mathrm{~Hz}, 60 \mathrm{~Hz}$, and 400 Hz noise rejection. The Q12 output of IC3 is a 2 Hz square wave, which is divided by two in IC4A. The resulting 1 Hz output is applied to the input of IC5, a 12-stage counter. The outputs of IC5 are decoded by a NAND gate to produce any desired interval between readings, to a maximum of 68 minutes. At the end of the time interval, IC4B generates a pulse which resets the counter and places the TSC7109 in the handshake mode.
When the TSC7109's MODE input is pulsed high, the result of the latest conversion is output in two bytes. First, HBEN goes low, outputs B9 through B12, POL and OR become active, and $\overline{C E} / \overline{L O A D}$ goes low. After one clock cycle $\overline{C E} / \overline{\mathrm{OAD}}$ goes high and the high byte of the conversion is latched into memory. The rising edge of $\overline{C E} / \overline{L O A D}$ also increments IC6, to address the next memory location. Then $\overline{\mathrm{HBEN}}$ goes high, LBEN goes low, outputs B1 through B8 become active and $\overline{C E} / \overline{L O A D}$ again goes low for one clock cycle. After $\overline{C E} /$


Figure 1: 13-Blt Remote Data Logger
$\overline{\text { LOAD goes high the low byte of the conversion is latched into }}$ memory, IC6 is again incremented, LBEN goes high and the data outputs return to their high impedance state.
Data can be read out of RAM by any micro or minicomputer. An I/O port with handshaking (6522, Z8420, 8255A, etc.) makes the task easy. The I/O port is simply programmed to prooduce a handshake strobe when the port is read. The strobe then increments IC6 after each byte is read andsequences through RAM automatically. Figure 2 shows pin connections for a 6522 I/O device.

Because of CMOS's low power requirements, battery power is ideal for the data logger. Average power dissipation of the


Figure 2: Connecting 13-Bit Remote Data Logger to 6522 1/O Port for Data Readout.

TSC7109 is only 10.5 mW , and the IDT 6116 is in its powerdown mode (Isy $=20 \mu \mathrm{~A}$ ) except for the time when $\overline{\mathrm{CS}}$ is low. Power dissipation, therefore, is only about 15 mW . On-board battery operation allows modules to be exchanged at remote locations and returned to a central location for data removal and analysis without danger of data loss.
The TSC7660, a DC to DC converter, permits the circuit to operate from a single power supply. This CMOS device contains a switch matrix and on-board oscillator which convert a positive voltage to negative polarity with a power efficiency of about $98 \%$. Using the TSC7660, as shown in figure 3, permits the circuit to operate, for example, on two small 3-volt lithium cells.


Figure 3: For Single-Supply Operation, Use the TSC7660 DC to DC Converter

The TSC426/427/428 fast switching times are made possible by a low impedance CMOS output stage. The high peak currents make 30 ns rise/fall times possible.
The rapid rise/fall times do, however, require systems be designed with adequate power supply decoupling and stray lead inductance minimization. Practices which are adequate for $1 \mu \mathrm{~s}$ rise/fall times and 20 mA peak currents will not be adequate with TSC426 family. The same laws of physics apply in both systems. The results may be negligible in one and of prime importance in another.
For example, a $0.1 \mu \mathrm{H}$ power lead inductance (4" of $0.025^{\prime \prime}$ diam. wire) can cause a voltage spike 1000 times larger in a fast system with an unbypassed supply.

Low Speed System

$$
\begin{aligned}
\mathrm{L}_{\mathrm{S}} & =0.1 \mu \mathrm{H} \\
\Delta \mathrm{~V}_{\mathrm{OUT}} & =18 \mathrm{~V} \\
\mathrm{t} & =1 \mu \mathrm{~s} \\
\mathrm{I}_{\mathrm{PK}} & =20 \mathrm{~mA} \\
\mathrm{C}_{\mathrm{L}} & =1000 \mathrm{pf} \\
\Delta \mathrm{~V}_{\text {supply }} & =\mathrm{L} \frac{\mathrm{dl}}{\mathrm{dt}} \\
& =2 \mathrm{mV}
\end{aligned}
$$

High Speed System
$L_{s}=0.1 \mu \mathrm{H}$
$\Delta V_{\text {OUT }}=18 \mathrm{~V}$
$\mathrm{t}=30 \mathrm{~ns}$
$\mathrm{I}_{\mathrm{PK}}=600 \mathrm{~mA}$
$C_{L}=1000 \mathrm{pf}$
$\Delta V_{\text {supply }}=\mathrm{L} \frac{\mathrm{dl}}{\mathrm{dt}}$
$=2.0 \mathrm{~V}$
The system design practices needed are not difficult to apply. The simple good engineering practice of bypassing the power supply, minimizing stray lead inductance, and grounding unused driver inputs will solve most system problems. Nothing new is required-just a little careful application of techniques common to any high speed CMOS system.
The TSC426 family outputs are CMOS. Low quiescent power and high output voltage drive (very important with 5 V supply operation) result. Since the outputs are CMOS the potential for activating a parasitic SCR exists. This must be avoided to prevent potential device destruction. If the


Figure 1: TSC426 Output.

TSC 426 output, like any CMOS chip, is driven below ground or above the positive power supply an internal parasitic SCR can be turned on. The high current flow can damage the device. The actual TSC426 output stage is shown in Figure 1. The IC layout and simplified equivalent SCR circuit are shown in Figures 2 and 3.


Figure 2: Output Stage IC Layout.


Figure 3: Equivalent SCR Circuit.

The IC parasitic SCR can be turned on if Dp is raised above $V_{C C}$ or if $D_{N}$ is forced below ground. An inductive load at the output can also create a voltage swing at the output that exceeds the positive supply or undershoots ground.
If the output is raised above the positive supply, current is injected into the emitter of Q1 and swept into the collector. The Q1 collector feeds the base of Q2 and R2. When the base of Q2 reaches 0.6 V Q2 turns on. This forces Q1 on. The SCR is now "fired" shorting the positive power supply to ground. A similar situation exists when the output is driven below ground.

The internal SCR can also be triggered by excessive voltage on the power supply that results in internal voltage breakdown. The current injected can trigger the SCR action.

By limiting the current injected into the TSC426 output when the output is above the positive power supply latch up is avoided. The limiting current is:
$1 \leq \frac{V_{B E}}{\text { R2 II RONP }}$
where:
$\left.\begin{array}{rl}\text { RONP }= & \text { ON resistance of } P \text { channel device. (15 ohms } \\ \text { maximum) }\end{array}\right\}$

Assuming the ON resistance dominates, the current should be limited to 40 mA . A similar analysis with the output below ground indicates the current pulled out of the TSC426 output should be limited to 60 mA . The maximum allowable latch current is temperature sensitive. At high chip temperature the base emitter voltages are reduced. A $1^{\circ} \mathrm{C}$ rise lowers $V_{B E}$ by 2.2 mV .
Current limiting with a series output resistor may not be practical in all systems. The output rise and fall times may increase. An alternate solution uses low forward voltage output clamp diodes to bypass the SCR trigger current around the device.

External output clamp diodes prevent the TSC426 output from being pulled far enough outside the power supply range to turn on the parasitic SCR.


Figure 4: Dlode Output Clamp Prevents SCR Action.
The external diodes must have a lower forward on base to emitter voltage than the parasitic translstor junctions. Schottky small signal diodes are sultable. Several possible types are:

- Hewlett Packard: P/N 5082-2303
- Motorola: P/N MBR120P
- Varo: P/N VSB52 (Four diode bridge)

To be effective the output clamp diodes must be connected close to the output, supply and ground device pins.


Figure 5: Stray Supply Lead Inductance Can Decrease Rellability.


Figure 6: Suggested Eypass Procedure.


Figure 7: TSC426 Has CMOS Inputs. Speed up Capacitors Are Not Required.

Supply bypass capacitors must also be connected between $\mathrm{V}_{\mathrm{CC}}$ (Pin 6) and Ground (Pin 3). Connections must be close to the actual device pins (approx. 0.5 "). A $0.1 \mu \mathrm{f}$ ceramic disk capacitor in parallel with a $4.7 \mu \mathrm{f}$ tantalum capacitor is suggested. Without supply bypassing, power supply lead inductance can cause voltage breakdown. The bypass capacitors also supply the transient current needed during capacitive load charging.
A 10 to 15 ohm resistor in series with the power supply filters voltage spikes present at the TSC426/427/428 supply terminal. Should latch up occur, this will also limit current. Rise and fall time will not be affected if the recommended supply bypassing is used. See Figure 8.
The DS0026 has a bipolar input. A speed up capacitor is normally used to decrease switching time. Base storage time is reduced. The capacitor causes a voltage spike drive at the input that extends beyond $V_{C C}$ or ground. The TSC426 input is CMOS and does not require a speed up capacitor. In converting DS0026 sockets to the TSC426/427/428 the capacitor should be removed. This will maximize drive to the device and minimize transition time. Benefits include fewer components and reduced insertion costs. See Figure 8.


Figure 8: $\mathrm{R}_{\mathrm{L}}$ Current Limiting Protects Device and Will Not Degrade Switching Speed.

The TSC426/427/428 outputs feature a low impedance $P$ channel pull-up MOS device and low impedance $N$ channel pull-down MOS device. The low resistance outputs are responsible for the 30 ns rise and fall times. The CMOS construction minimizes current drain.

The output $N$ and $P$ channel devices should not be forced to conduct current simultaneously. This can happen if an unused input is left floating. Unused inputs must be connected to ground or the positive supply. A ground connection will minimize steady state supply current. This is common engineering practice followed in CMOS logic system design but is sometimes overlooked during a "quick" bench evaluation. Floating inputs cause excessive current flow and may potentially destroy the driver.
The input drive signal should also have rise and fall times less than $1 \mu \mathrm{~s}$. This minimizes time spent in the output stage transition region.

## Package Power Dissipation

Input signal duty cycle, power supply voltage, and capacitive load influence package power dissipation. Given power dissipation and package thermal resistance the maximum ambient operation temperature is easily calculated. The CerDIP 8-pin package junction to ambient thermal resistance is $150^{\circ} \mathrm{C} / \mathrm{W}$. At $25^{\circ} \mathrm{C}$ the package is rated at 800 mW maximum dissipation. Maximum allowable chip temperature is $150^{\circ} \mathrm{C}$.
Three components make up total package power dissipation:

- Capacitive load dissipation ( $\mathrm{P}_{\mathrm{C}}$ )
- Quiescent power ( $\mathrm{P}_{\mathrm{Q}}$ )
- Transition power ( $\mathrm{P}_{\mathrm{T}}$ )

The capacitive load caused dissipation is a direct function of frequency, capacitive load, and supply voltage. The package power dissipation per driver is:

$$
\text { EQ. 1: } P_{C}=f C V_{S}{ }^{2}
$$

where: $F=$ switching frequency
$\mathrm{C}=$ capacitive load
$\mathrm{V}_{\mathrm{S}}=$ supply voltage
Quiescent power dissipation depends on input signal duty cycle. A logic low input results in a low power dissipation mode with only 0.4 mA total current drain. Logic high signals raise the current to 8 mA maximum. The quiescent power dissipation per driver is:
$E Q .2: P_{Q}=\frac{V_{S}}{2}\left(D\left(I_{H}\right)+(1-D) I_{L}\right)$
where: $I_{H}=$ quiescent current with both inputs high ( 8 mA Max)
$I_{L}=$ quiescent current with both inputs low ( 0.4 mA Max)
D = duty cycle

Transition power dissipation is normally not significant. It arises because the output stage N and P channel MOS transistors are on simultaneously for a very short period when the output changes. The transition package power dissipation per driver is approximately:
EQ. 3: $P_{T}=f V_{S}\left(1.63 \times 10^{-9}\right)$
An example shows the relative magnitude for each term. Both drivers are driven with a $50 \%$ duty cycle signal at the same frequency. Capacitive load is the same for each driver.
Example 1:
$C=1000 \mathrm{pf}$
$V_{S}=18 \mathrm{~V}$
$D=50 \%$
$\mathrm{f}=200 \mathrm{kHz}$
$P_{D}=$ Package power dissipation $=P_{C}+P_{T}+P_{Q}$
$=130 \mathrm{~mW}+11.7 \mathrm{~mW}+38 \mathrm{~mW}$
$=180 \mathrm{~mW}$
Max. operating temperature $=T_{J}-\theta_{J A}\left(P_{D}\right)$

$$
=123^{\circ} \mathrm{C}
$$

where:
$\mathrm{T}_{\mathrm{V}}=$ Max. allowable junction temperature $\left(150^{\circ} \mathrm{C}\right)$
$\theta_{\mathrm{JA}}=$ Junction to ambient thermal resistance $\left(150^{\circ} \mathrm{C} / \mathrm{W}\right.$, CerDIP)
Table 1 gives the total package power dissipation for several different cases using the formulas developed above. If only one driver is active divide the package power dissipation numbers by two in Table 1.

Table 1: TSC426 Package Power Dissipation

| $\begin{gathered} \text { Capacitlve } \\ \text { Load } \\ {[\mathrm{pF}]} \\ \hline \end{gathered}$ | InputFrequency$[\mathbf{k H z}]$ | Supply Voltage [V] | Package Power Dlssipation CerDIP Package [ $\theta_{\mathrm{JA}}=150^{\circ} \mathrm{C} / \mathrm{W}$ ] |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Input <br> Stage <br> Power <br> [mW] | AC Power [mW] | Splke <br> Power <br> [mW] | Total Power [mW] | Max <br> Amblent Operating Temp $\left[^{\circ} \mathrm{C}\right]$ |
| 1000 | 50 | 18 | 75 | 32 | 2 | 109 | 125 |
| 1000 | 100 | 18 | 75 | 64 | 5 | 144 | 125 |
| 1000 | 200 | 18 | 75 | 129 | 11 | 215 | 117 |
| 1000 | 400 | 18 | 75 | 259 | 23 | 357 | 96 |
| 1000 | 1000 | 18 | 75 | 648 | 58 | 781 | 32 |
| 1000 | 50 | 12 | 50 | 14 | 1 | 65 | 125 |
| 1000 | 100 | 12 | 50 | 28 | 3 | 81 | 125 |
| 1000 | 200 | 12 | 50 | 57 | 7 | 114 | 125 |
| 1000 | 400 | 12 | 50 | 115 | 15 | 180 | 122 |
| 1000 | 1000 | 12 | 50 | 288 | 39 | 377 | 93 |
| 2000 | 50 | 18 | 75 | 64 | 2 | 141 | 125 |
| 1000 | 1800 | 12 | 50 | 518 | 70 | 638 | 54 |
| 50 | 4000 | 18 | 75 | 129 | 234 | 438 | 84 |
| 1000 | 100 | 18 | 75 | 64 | 5 | 144 | 125 |
| 500 | 100 | 18 | 75 | 32 | 5 | 112 | 125 |
| 500 | 200 | 15 | 63 | 45 | 9 | 117 | 125 |
| 500 | 100 | 15 | 63 | 22 | 4 | 89 | 125 |

Notes: 1. Duty Cycle $=50 \%$.
2. Each input driven.
3. Each output with load C.
4. Ambient operating temperature should not exceed $85^{\circ} \mathrm{C}$ for "IJA" device or $125^{\circ} \mathrm{C}$ for "MJA" device.

## Application Note 26 <br> Flexible TSC500 ADC Simplifies Design Tradeoffs By Wes Freeman

 SEMICONDUCTORDesigners who need to convert analog signals to digital rapidly gain respect for the word "tradeoff." At first glance, the wide variety of analog-to-digital converter (ADC) products available would indicate that the "perfect" ADC for any application is readily available. All of these products, however, involve tradeoffs in speed, power consumption, accuracy, price, and flexibilty, among others. These trade-offs are not mere specmanship, either. Speed, price, and power consumption, for example, can vary by orders of magnitude from product to product.
The overriding ADC tradeoff is usually speed. Digitizing high speed signals typically requires a successive approximation or flash ADC. The designer must then accept the cost and power penalties which usually accompany these devices.
Many analog phenomena, however, change slowly. Commonly measured physical events, for example, include temperature, humidity, pressure, strain, and pH . The dual-slope integrating ADC is the typical choice for low speed conversion, due to its high resolution at low cost and low power. Even though a variety of dual-slope ADCs are available, tradeoffs can still occur because the analog sensors vary widely in resolution, linearity, output impedance, and output level.
One solution to converting the wide variety of analog signals can be found in a flexible ADC. The TSC500, from Teledyne Semiconductor, contains all of the analog circuitry required for an integrating ADC. By transferring the digital portion of the ADC to the counters and software of a host processor, the TSC500 can be used to solve a wide variety of data conversion problems.

The TSC500 gives the design engineer powerful control over the resolution/conversion-speed tradeoff, while adding flexible input voltage scaling. Also, this flexibilty is made available at low cost and with only 10 mW power dissipation.
A typical ADC and microprocessor interface is shown in Figure 1. Notice that the digital functions of the ADC are duplicated in the microprocessor. Replicating these circuits on the ADC simplifies software development, because the conversion result is merely read as one or more memory locations. Although the hardware interface also seems to be simple, the package size and large number of I/O lines necessary can be a real limitation in small systems or with single-chip microcomputers which are not bus oriented.
Figure 2 shows the TSC500 and microprocessor interface. The counters, control logic, and most I/O functions have been moved to the microprocessor. Only three I/O lines are required, and both the size and cost of the ADC are reduced. More importantly, the designer can now specify the ADC resolution instead of selecting whatever is available in an existing product.
The TSC500 permits control of the conversion's resolution because resolution is determined by the host processor's software. With standard ADCs, resolution is determined by hardware on the chip. The designer who needs, for example, $.04 \%$ resolution is forced to use a 12-bit ADC with . $025 \%$ resolution. By using the TSC500, however, a 2500-count fullscale output is as easy to design as a 4096 count (12-bit) output, but yields a $40 \%$ increase in conversion speed.


Figure 1: Typical ADC Interface to $\mu \mathbf{C}$


Figure 2: TSC500 Interface to $\mu \mathbf{C}$

The ability to select full-scale is useful for measuring outputs which do not fall readily into a binary sequence. One such example is the 150 degree Centigrade operating range limit of IC temperature sensors such as the LM35 from National Semiconductor. By using a 1500 count ADC, the LM35's output can be read directly in tenths of a degree Centigrade. Adjusting the ADC's full-scale range to the sensor's output in engineering units can simplify software for data analysis and display.

The functional diagram of the TSC500 is shown in Figure 3. The design features include low leakage CMOS switches, high impedance input buffer, integrator op-amp, two-stage comparator, and digital control logic. These components, packaged in a 16-pin DIP, form the analog section of an ADC whose resolution can extend from less than 8 to greater than 14 bits.


Figure 3: Functional Diagram of the TSC500

The CMOS switches permit very flexible input and reference voltage applications. During the signal integrate phase, the two SWI switches connect VIN to the input buffer and ViN to the integrator. These connections provide a fully differential signal input, within the common-mode input range. The signal input common-mode range extends from ( $\mathrm{Vs}^{+}$minus 1.5) to ( $\mathrm{V} \overline{-}$ plus 1.5 V ), providing an easy interface for bridgetype and other differential input applications.
A reference capacitor and switch matrix combine to also ease reference voltage limitations. During autozero the SWRC switches close, charging the reference capacitor to Vref. Then, during deintegrate, the SWRI switches connect CREF to the buffer input. Because CREF isolates the reference inputs from the buffer, there are no common-mode limitations on the reference voltage. The REFHI and REFLO inputs can therefore be located anywhere within the power supply range.
The differential reference is especially useful for bridge applications, because the reference can be derived from the same voltage that drives the bridge. Changes in the bridge driving voltage will not, therefore, affect the ADC's output. Since there are no common-mode limits on the reference inputs, simple ratiometric resistance measurements are also possible.
The reference capacitor also combines with CMOS switches to produce a bipolar reference from the single-polarity reference inputs. Four SWDI switches in a bridge configuration connect Cref to the buffer input. By the closure of opposing pairs of switches, Cref can be connected as either a positive or a negative voltage. When the TSC500 deintegrate phase is selected, control logic samples the integrator polarity. Internal control logic then closes the appropriate pair of SWRI switches to select correct reference polarity.
The TSC500's excellent input characteristics are also a function of the low leakage, low noise metal gate CMOS process. Input bias current is only 10 picoamperes maximum, while input noise is typically limited to 30 microvolts peak to peak. Input buffer linearity is critical for system performance, so a class A output stage is used. The buffer output can supply 20 microamperes of current with negligible nonlinearity.
The main limitation in the conversion time of an integrating ADC is comparator response time. Although the TSC500's targeted response time of four microseconds is three orders of magnitude below the speed of available bipolar products, several constraints combine to make the design task difficult. First, the comparator must resolve about 50 microvolts in a slowly changing ramp, instead of the millivolt-level step response usually specified in comparator specs. Also, the comparator must operate on less than 400 microamperes of supply current, and be fabricated in a low-noise CMOS process. Finally, the comparator should be unity gain stable to minimize oscillation during the autozero phase.

TSC designers solved the high-gain/fast-response dilemma by utilizing two comparators. The first comparator is unitygain stable, and is included in the autozero loop. The second comparator, operating open loop, provides the CMOS output levels required. In both comparators, cascade gain stages were used to minimize Miller capacitance and improve speed.

Input offset voltage (Vos) of the buffer, integrator, and comparator \#1 are unimportant because the errors are stored during the autozero phase. Comparator \#2 is not in the autozero loop, however, so its Vos must be minimized to reduce potential rollover and zero-offset problems. The input FETs of comparator \#2 were therefore implemented as a crosscoupled quad, with close matching of devices and isothermal orientation. The combination of careful layout, low power dissipation on-chip, and the fact that comparator \#2's Vos is attenuated by the gain of comparator \#1 ensure that rollover errors are held to less than . $01 \%$ maximum for a $41 / 2$ digit conversion.
The TSC500's only feedback path to its host microprocessor is via the comparator output. This output must, therefore, relay both polarity and zero crossing information. For large input signals the method is straightforward. The comparator status is read and stored prior to deintegrate, which establishes polarity. After the ADC is switched to deintegrate mode, the comparator output is monitored for the polarity reversal that signals zero crossing.
This method can fail for signals near zero, however, especially in the presence of normal mode noise. In this case, the comparator state can change several times during signal integrate. If a polarity reversal occurs between reading of polarity and start of deintegrate, the zero crossing will not be detected. This method also makes the polarity of the edge that signals zero crossing dependent on input polarity, which complicates the generation of interrupts.
A unique output circuit, shown in Figure 4a, solves both of these limitations. When the deintegrate phase is selected, comparator \#2's polarity data is latched into an internal flipflop. The inverting output of the flip-flop drives an exclusiveOR gate which ensures that, at the beginning of deintegrate, the comparator output will be driven to a logic high state.


Figure 4a: Simplified Schematic of TSC500 Comparator

Figures 4b and 4c show the TSC500's comparator output for both positive and negative polarity inputs. Notice that polarity status is still valid before deintegrate begins. Even if polarity changes while the comparator output is being read, indicating an input very near zero, the comparator will still switch states when entering the deintegrate phase. In addition, zero crossing is always signalled by a negative-going transition of the comparator output. The negative-edge output is consistent with the interrupt structure of many common microprocessors.


Figure 4b \& c: Comparator Output Waveforms
This unusual comparator circuit conveys both polarity and end of conversion information. For a positive input the comparator will be in a high state during integrate (b) while for a negative input the output is low (c). In either case, the exclusive OR gate (fig. 4a) ensures that the comparator output will go high when deintegrate begins.

Table 1: TSC500 Control Inputs, Converter State, and Internal Switch Status.

| Control Logic | Conversion Phase | Internal Analog Swltch Status |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A B |  | SW1 | $\mathrm{SW}_{\text {RI }}^{+}$ | SW ${ }_{\text {RI }}^{-}$ | SWz | SW ${ }_{\text {R }}$ | SW 1 | SWIz |
| 00 | Zero Integrator |  |  |  |  |  | Closed | Closed |
| 01 | Auto- <br> Zero |  |  |  | Closed | Closed | Closed |  |
| 10 | Signal Integrate | Closed |  |  |  |  |  |  |
| 11 | Deintegrate |  | Closed* |  |  |  | Closed |  |

*Assumes positive-polarity input signal. For negative input signal, $S^{-}{ }^{-}$is is closed.

The TSC500's two logic inputs control the phases of the integrating analog-to-digital conversion. (For further information on dual-slope A/D conversion, see appendix A of Teledyne Semiconductor Application Note AN-23). As shown in Table 1, the TSC500 adds an additional phase, zero-integrator, to the conventional autozero, signal integrate, and deintegrate phases. The zero-integrator mode can greatly reduce one of the integrating ADC's drawbacks, slow recovery from an input overrange condition. Slow overrange recovery is a problem when several inputs are multiplexed into one integrating ADC, because an overrange on one channel will affect the accuracy of other channels.
The source of the integrating ADC's slow input overrange recovery is shown in Figure 5. Under normal conditions, the integrator ramps up during signal integrate, then back to zero volts during deintegrate (Figure 5a). When the signal input exceeds full-scale, however, the integrator output does not reach zero volts before the end of deintegrate (Figure 5b). If the ensuing autozero period is not long enough to discharge the integrator to zero volts, succeeding conversions will provide erroneous data. The zero-integrator phase, on the other hand, provides a rapid discharge of the integrator error voltage (Figure 5c). This speedup occurs because, during zerointegrator, the integrator is actively driven toward zero volts.


Figure 5: TSC500 Integrator Output Waveforms During:
(a) Normal Operation
(b) Input Overrange
(c) Input Overrange with Zero Integrator Cycle

The integrator output normally returns to 0 V at EOC (a), but an error voltage remains if the input is overranged (b). Adding a zero integrator cycle speeds overrange recovery (c).

Figure 6 demonstrates the difference between autozero and zero-integrator operation. During autozero, the buffer's input is connected to circuit common (Figure 6a). Disregarding offset voltage, the buffer's output will be zero volts. Any charge remaining on the integrator capacitor after deintegrate must discharge through RiNt, and the time constant is quite long. The zero-integrator phase speeds the error recovery by connecting the buffer input to comparator \#1's output. Since the comparator output swing is greater than plus/minus four volts, discharge time is greatly reduced. Zero integrator must be followed by autozero, so that the buffer offset is cancelled. Typically, if $20 \%$ of the normal autozero period is devoted to zero-integrator following an overrange, then the integrator capacitor will be discharged.
Integrating ADCs are suitable for both system and display applications. The system ADC is typically part of a microprocessor based system, with the ADC accessed via a data bus or input/output (I/O) port. System ADCs typically produce binary data, and have three-state, bus compatible outputs. Display converters, on the other hand, are most often used as the heart of a dedicated instrument such as a digital multimeter. Display converters typically operate with decimal data and have binary-coded decimal (BCD) or seven segment outputs for easy interface to a visual display.


Figure 6a: TSC500 Simplified Schematic During Auto-Zero


Figure 6b: TSC500 Simpllfied Schematic During Zero Integrate
Overrange recovery is slow in auto-zero because the buffer is connected to 0 V (a). The zero integrator phase connects the buffer to the comparator output to actively discharge the integrator (b).

The TSC500's flexibility permits it to be used in both system and display applications. Combined with a microprocessor I/O port, the TSC500 forms a binary ADC with resolution of 8 to 14 bits. Conversion rates of the binary ADC range from 400 down to 5 per second, while the high impedance signal inputs and differential reference ensure flexibility in measuring a variety of analog sensors.

When teamed with a single-chip microcomputer, on the other hand, the TSC500 can form an equally flexible display converter. Features which are difficult to implement with a dedicated display ADC become easy with the analog front end approach. Desireable features for a hand-held multimeter, for example, might include autoranging, bargraph display, relative measurements with decibel conversion, or programmable limits with buzzer alarm. Adding features in software can reduce development costs for a product family, as well as permitting product differentiation.
An example of the TSC500 used as a system ADC is shown in Figure 7. Only three active and ten passive components are required, in addition to the $\mu \mathrm{PI} / \mathrm{O}$ port, to form a very flexible ADC. Since the TSC500 is available in a 16-pin DIP, PCB area is actually less than that required for a dedicated but less flexible ADC.

All of the analog components, except the reference, are contained in the TSC500. The passive components are inexpensive, and critical tolerances are not required. The integrating capacitor, $\mathrm{Cint}_{\text {I }}$, must have very low dielectric absorption, so polypropylene is recommended. The other capacitors can be polypropylene, MYLAR, or other low leakage film type.
The ADC's reference voltage is provided by two TSC9491s, which operate like a 2.44 volt Zener diode. Requiring a minimum bias current of only $50 \mu \mathrm{~A}$, the TSC9491 is available in temperature coefficient grades of 50 or $100 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$. If the ADC's reference voltage is less than 1.22 V , only one TSC9491 is required.
Although the TSC500 requires $+/-5 \mathrm{~V}$ power supplies, the circuit operates with a single +5 V connection. A monolithic DC to DC converter, the TSC7660, combines with two electrolytic capacitors to convert a +5 V input into -5 V . The TSC500 only requires 1.5 mA of supply current, so the TSC7660 provides a voltage conversion efficiency of about 98\%. Eliminating a separate -5 V supply reduces power supply bulk and expense, as well as simplifying power distribution and PCB layout.

The $\mu \mathrm{P}$ I/O device is a Synertek SY6522, which contains two bidirectional 8-bit I/O ports, four interrupt control/handshake pins, two 16-bit timers and a shift register. Only four I/O bits, one interrupt input, and the timers are used for the ADC interface. The remainder of the I/O port functions are available for selecting multiplexed inputs, accessing a visual display, or other functions.

The TSC500/SY6522 interface only requires three digital connections, which is a significant advantage when the ADC is located some distance from the I/O port. Two SY6522 I/O bits, configured as outputs, control the TSC500's dual slope integration algorithm. The comparator output can either be read by polling an input port or by generating an interrupt. In most cases the interrupt would be used, of course, but input polling is useful while debugging software.


Figure 7: TSC500 Interface to a Typical $\mu \mathrm{P}$ I/O Port

The circuit makes use of both of the SY6522's counter/timers. Timer \#1 is used to generate the ADC clock pulses, while timer \#2 functions as the ADC's counter. The frequency output of timer \#1 therefore controls the ADC conversion speed, while the binary number loaded into the counter determines the ADC resolution. During deintegrate, the count in timer \#2 when the comparator output switches to a logic low state is proportional to the analog input voltage.
Timer \#1 operates in its "free running" mode to generate the ADC clock. In this mode, the $\mu$ P's clock is divided by a 16 -bit integer stored in the T1 latches. The result is a square wave output on pin PB7. The clock frequency can be modified, by changing the divider constant, to adjust conversion speed or to reject specific normal mode noise frequencies.
Counter/timer \#2 is programmed for its pulse counting mode. When a number is loaded into the T2 latches, the counter will decrement with each negative pulse on input PB6. Connecting PB7 to PB6 permits the counter to operate at the frequency programmed into Timer \#1. An interrupt flag is set when the counter underflows, signalling the end of each measurement cycle.
As mentioned previously, the TSC500 hardware combines with $\mu \mathrm{P}$ software to form an ADC. Software for the circuit, written in 6502 assembly language, is shown in Listing 1. The logic flow is shown in Flowchart 1. This program will produce a 12-bit conversion, but the resolution can easily be increased or decreased.


## Flowchart \#1

Before the actual conversion can begin, some housekeeping tasks must be completed. These tasks, not shown in the listing, include setting I/O ports, configuring timers, and clearing interrupt flags. Once initialization is completed, the analog-todigital conversion process can begin.
The conversion software begins by placing the TSC500 in its autozero mode. For a 12-bit converter the autozero cycle is 2048 counts, so the counter registers are loaded with this value. The counter immediately begins decrementing at the square wave frequency and the $\mu \mathrm{P}$ waits for the counter underflow that signals the end of autozero.
The signal integrate phase is identical to autozero, except for placing the TSC500 in signal integrate mode. The integrate cycle is also 2048 counts, and the integrate period is selected
to provide optimal normal mode noise rejection. After the signal integrate cycle is complete, deintegration begins and the analog input value is determined.
The deintegrate cycle begins by reading the comparator output. This action serves a dual purpose. First, the comparator state at the end of signal integrate establishes input polarity. Second, reading the input port resets the corresponding interrupt bit. The next negative edge on the comparator output will set the interrupt flag and signal the zero crossing.
Deintegrate continues by placing the TSC500 in its deintegrate mode and again loading the down counter. For a 12-bit conversion the counter value is 4096 . The software then begins testing for zero crossing and end of conversion.
In the deintegrate loop, a test is first made for zero crossing. If the interrupt bit which corresponds to the comparator is not set, then the program tests for counter underflow. The program continues to loop until either zero crossing or counter underflow occurs.

When zero crossing occurs, the contents of the down counter represent the analog conversion result. The counter value is therefore transferred to memory for further processing. A memory location is also incremented to indicate that zero crossing has occurred. This memory location can be tested during autozero if the user wishes to include an optional zerointegrator phase.
Rather than stopping and restarting the counter, the registers are read "on the fly." Several steps are required to ensure that data does not change between reading the high and low bytes. If the high order byte changes between readings, the result would be 256 counts of error. The program therefore reads the counter registers twice, and tests for a borrow occurring between the two read operations. If the high byte has changed, a correction is applied before data is stored in memory.
Once the conversion result is stored, the program again waits for the deintegrate phase to end. When the counter underflows, the conversion cycle is complete. The program loops back to autozero if another conversion is desired, or jumps to software which processes the ADC data. Since timer \#2 is a down counter, the stored data must be subtracted from 4096 to get the actual analog input.
The software shown in Listing 1 keeps the $\mu \mathrm{P}$ in a continuous loop during conversion. In normal practice the conversion would be interrupt driven, so that the $\mu \mathrm{P}$ would be free for other tasks. To convert the software to interrupt operation, routines must be added which will recognize interrupt sources and also keep track of the conversion phases.
The TSC500 interface only requires a small portion of the I/O port's available functions, so additional features are easy to add. Figure 8 shows one possible expansion by adding input multiplexers for eight differential analog signals. A four digit LED display is also included. The TSC701AM accepts BCD data, decodes the data to seven segment display format, and provides 28 LED segment driver outputs with 18 mA current capability. Placing CA2 in its pulse output mode will latch data into the TSC701AM simply by writing to port A. Four bits of I/O are still available for controlling motors, heaters, valves, etc., or for monitoring digital inputs.


Figure 8: 8-Channel Data Acquisition System

## TSC500 Comparator Behavior After Zero Crossing

The TSC500 comparator is designed to produce a negativegoing edge-triggered output which signals the end of conversion. This transition occurs during the deintegrate phase, when the integrator output passes through zero volts. In most cases, the result will be a single negative-going transition. Occasionally, however, and especially in a noisy electrical environment, the comparator may make more than one transition.

Multiple comparator pulses are seldom a problem in a microprocessor sytem, since most $\mu \mathrm{Ps}$ will not respond to a second interrupt until the first one is serviced. The service routine then disables the interrupt until the next deintegrate cycle, so additional comparator transitions are ignored.
Problems do occur, however, in circuits built with discrete logic. If the unbuffered negative comparator edge is used to transfer data to latches, for example, multiple transitions will produce erroneous data. More importantly, additional transitions during auto-zero and integrate cycles will make the latched data meaningless. Therefore, designers of non- $\mu \mathrm{P}$ TSC500 systems should provide logic which will ensure that end of conversion is only determined by the first negative comparator transition which occurs after the TSC500 is placed in deintegrate mode.
Photograph \#1 demonstrates the TSC500 comparator output at the end of a conversion. As the integrator output (top trace)
passes through zero volts, the comparator output (bottom trace) goes from a high to a low state. In this example, only a single negative-going transition was observed.

After zero crossing, Photograph \#1 shows that the integrator overshoots zero volts, continuing downward until the TSC500 is switched to zero-integrator mode. The Zl cycle rapidly discharges the overshoot error voltage, preparing the TSC500 for its next conversion cycle. After a short period of time in ZI, however, the comparator begins to oscillate. External circuitry which latches data at each falling edge of the comparator will now latch erroneous data. Additional gating of the comparator output, as outlined above, will prevent this error. (Note that the oscillations observed are comparator \#2. This does not imply that the ZI loop, which uses feedback from the output of comparator \#1, is unstable).


Photograph \#1

By using low-cost microprocessors and a program-controlled numerical-integration technique, you can achieve good noise rejection and take full advantage of the higher speeds offered by recently developed dual-slope A/D converters such as the TSC7109.
This and similar converters overcome the speed limitations imposed by logic-gate and analog-comparator delays in earlier dual-slope devices, and the modern units can operate at rates as high as 30 to 100 samples $/ \mathrm{sec}$. Nevertheless, operating them at their maximum conversion rates often makes it difficult or impossible to achieve the high normal-mode line-frequency rejection that dual-slope A/D converters inherently offer at slower conversion rates. Thus, noise considerations have often precluded use of these converters at their rated speeds especially in industrial environments, where line-frequency and other low-frequency noise components can be a particular problem.

## Normal-Mode Line-Frequency Rejection

To understand normal-mode line-frequency rejection in dual-slope A/D converters, consider a typical 12-bit converter (Figure 1a) and its timing diagram (Figure 1b) for one conversion cycle. Note that the conversion depends on charging the integrating capacitor during a fixed time interval; the number of counts necessary to discharge the capacitor to zero is proportional to the input voltage.

The integrating $A / D$ converter integrates the signal only in a certain time window, as Figure 1 b shows. This limited integration period results in normal-mode noise rejection only when the integration period is equal to one or more periods of the noise signal (Figure 2a). The time integral of this noise over integer multiples of the noise period is, of course, zero.
Normal-mode noise-rejection performance can thus be represented as a function (Figure 2b) that reaches peaks at the fundamental and harmonic frequencies of the period defined by the signal-integrate time $T$. The minimum period T , which must equal the noise period, has been the limiting factor for conversion speed. At 60 Hz , for example, the minimum signal-integrate time is 16.7 msec ; at 50 Hz , it's 20 msec .
Because the signal-integrate time is only a portion of the total conversion time, conversion rates are significantly less than $1 / T$. A standard, high-performance, dual-slope A/D converter includes a reference deintegrate phase, typically $2 T$ long, and an autozero period equal to the signal-integrate period T . The total conversion time is thus 4 T , which, for $60-\mathrm{Hz}$ rejection, yields a maximum conversion rate of 15 samples $/ \mathrm{sec}$; for 50 Hz , it yields 12.5 samples/sec.
The most serious constraint arises when you want to offer an instrument for international use that can reject both 60 and 50 Hz . This feature is attainable only when the signal-integrate period T can contain six cycles of $60-\mathrm{Hz}$ noise and five cycles of $50-\mathrm{Hz}$ noise. The resulting $100-\mathrm{msec}$ signal-integrate period dictates a $2.5-$ conversion $/ \mathrm{sec}$ rate.


Figure 1: A dual-slope A/D converter operates by charging a capacitor from the input voltage during a fixed time, then discharging it to zero. The number of clock periods in the discharge time corresponds to the analog input voltage. The size of the integrating time window determines which normal-mode noise signals are rejected.
(a)

(b)


Figure 2: In a dual-slope A/D converter, high normalmode noise rejection occurs when the integration period is a multiple of the noise signal's period.

You can, however, overcome the inherent conversion-speed limitation of integrating $A / D$ converters. A microprocessor with program-controlled numerical integration that complements the A/D converter's analog integration will speed dualslope conversion considerably.
You can achieve high normal-mode rejection for specific frequencies with this method if three conditions are met. First, the signal-integrate period must be defined such that noise integration takes place on a segmented basis. In Figure 3a, for example, the integrate window opens on a noise-waveform segment that's one-third of a period long.
Next, the second signal-integrate period must begin at a point corresponding exactly to the point at which the first one ended, and the third's beginning must correspond to the point at which the second ended. This condition can be met only if the $A / D$ converter has a fixed conversion time, irrespective of the signal input. Finally, the microprocessor must sum all three conversions to achieve the total integration of a cycle of noise. A consideration of all these constraints for the TSC7109 A/D converter, for example, leads to the relationship

$$
\mathrm{f}_{\mathrm{NOISE}}=\frac{1}{X T}=\frac{4 \mathrm{C}}{X}
$$

where $C$ is the conversion rate, $f$ the noise frequency and $X$ the number of conversion results added. $X$ must be an odd number; Figure $3 b$ shows why $X$ cannot be an even number. A frequency that would require an even number of samples is one at which the integrate window is locked in phase with the signal (ie, the converter and signal periods are synchronized). For $\mathrm{CV}=\left(\mathrm{f}_{\mathrm{NO}} \mathrm{ISE}\right)(\mathrm{X} / 4)$ and $\mathrm{X}=2$ (as in Figure 3b), the result is two times the error of one conversion.


Figure 3: Data-conversion systems employing a numerical-integration technique furnish noise rejection when an odd number of samples are summed (a). Adding the results of two conversions, though, can yield twice as much error as does one conversion (b) if the A/D converter and noise frequency are synchronized.


Figure 4: The normal-mode-rejection capability illustrated by the upper curve here demonstrates the effectiveness of taking nine conversion samples; the system that the curve represents rejects noise at all multiples of 10 Hz . The lower curve shows the result of acquiring only one sample and employing an 11.11-msec signalintegration period.

To achieve the desired normal-mode rejection, you must, therefore, sum an odd number of A/D-converter results. You can accomplish this summation with firmware or with userinteractive software. Consider an example using a TSC7109 A/D converter operating at 22.5 samples $/ \mathrm{sec}$. The equation yields the results in Table 1.
As Table 1 indicates, an A/D converter operating at 22.5 samples/sec can reject harmonics of 10 Hz if you maintain a rolling average of nine samples. This technique rejects 50 and 60 Hz ; it's equivalent to one sample taken at the rate of 2.5 samples $/ \mathrm{sec}$. The curves in Figure 4 show the normal-mode rejection resulting from 1-and 9-sample averages at the rate of 22.5 conversions/sec (or one sample at 2.5 conversions $/ \mathrm{sec}$ ).

Table 1: TSC7109 at 22.5 Samples/Sec

| fNOISE <br> (Fundamental) <br> In Hz | $\mathbf{X}$ <br> Samples Summed |
| :---: | :---: |
| 90 | 1 |
| 30 | 3 |
| 18 | 5 |
| 12.8 | 7 |
| 10 | 9 |



Figure 5: This 3 3/4-digit multimeter uses a numerical-integration technique to reject both $50-$ and $60-\mathrm{Hz}$ normalmode noise. Although the DMM's display updates at 2.5 samples $/ \mathrm{sec}$, conversions take place at 22.5 samples $/ \mathrm{sec}$.

What's the point, you may ask, of sampling at the higher rate if you must wait for the result during a 9-period numerical integration? After the first 9-period wait, the system's pipeline is full, and you can then obtain a new result for each cycle at the 22.5-samples/sec rate.

The numerical-integration technique has many practical applications. The Figure 5 circuit, for example, is a $33 / 4$ digit DMM that uses a TSC7109 13-bit A/D converter. The DMM updates the display at a 2.5 sample $/ \mathrm{sec}$ rate for easy readability, yet it converts at a 22.5 sample/sec rate for fast response during autoranging and continuity checking. Because the circuit averages nine samples, it rejects both $50-$ and $60-\mathrm{Hz}$ noise. Because it can carry a rolling average, the $\mu \mathrm{P}$ is capable of changing the number of conversions summed; it can therefore accommodate specific, user-programmable rejection frequencies.

Figure 6 shows connections for a system using the TSC7109 in conjunction with a 6502 processor and 6522 peripheral interface adapter. The adapter's programmable timer provides the $A / D$ converter's clock, thereby simplifying testing of noise rejection with different clock frequencies. This circuit allows you to evaluate numerical-integration-based designs using either a general-purpose $\mu \mathrm{P}$-development system or a prototyping board (eg, Rockwell's AIM-65). Figure 7 shows the assembly-language listing for the system; the flowchart appears in Figure 8.

Table 2: 16-Channel Multiplexer

| $\mathbf{X}$ | Channels Scanned |
| :---: | :---: |
| 3 | 13 |
| 5 | 16 |
| 7 | 15 |
| 9 | 10 |



Figure 6: You can evaluate numberical integration with the circuit detailed in this schematic. The 6522 peripheralinterface adapter provides clocking and the $\mu P$ interface for the dual-slope $A / D$ converter.

| 0941. ASM |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| 0000 |  |  |  |  |
| 0000 |  |  |  | ; SOFTMARE TO denonstrate numerical integration |
| 0000 |  |  |  | - USING THE TSC7109 INTERFACED TO A 6502 |
| 0000 |  |  |  | - MICROPROCESSOR VIA A 6522 I/O PORT |
| 0000 |  |  |  | ; ReSults stored at 'reslt in zero-page memory |
| 0008 |  |  |  | ; USER MUSt Provide interrupt vector froh the |
| 0000 |  |  |  | ; b522's cal interrupt to sve routine at "intsuc" |
| 0000 |  |  |  |  |
| 0000 |  |  |  | ;SYSTEM Equates |
| A800 | IOPT | Eay | OABOOH | ;ADDRESS OF 0522 :/O PORT |
| 0080 |  | ORG | 80h | ;RESERVE ZERO-PAGE MEMORY |
| 0080 | RESLT | DS | 3 | ;16-BIT ACCUMULATOR FOR RESULTS, 1 bYte For sign |
| 0083 | STORX | DS | 1 | ;STORAGE FOR LOOP COUNTER |
| 0084 | STORHI | DS | 1 | ;SAVE HIGH Byte |
| 0280 |  | OR6 | 0280H | ;SET UP L/O PORT TO CONTROL TSC7109 |
| 0280 A9C0 | CLOCK | LDA | ${ }^{3} \mathrm{COH}$ | ;P86 \& PB7 ARE OUTPUTS, |
| 02828 8000AB |  | STA | 109 T | - PB7 IS THE TIMER 1 OUTPut |
| 0285800288 |  | 5 SA | IOPT +2 | - (FOR 7109 Clock) |
| 0288 日00BAB |  | STA | LOPT +0 BH | ;SGUARE NAVE OUTPUT ON PB-7 |
| $0288 \mathrm{Ba912}$ |  | LDA | $1 / 2 \mathrm{H}$ | ; LOAD THE CONStant for |
| ${ }^{0280} 88004$ AB |  | STA | ${ }_{1097+4}$ | ; Clock ther |
| 0290205402 |  | JSR | SEtreg | ; IMItIALILE MEMORY REGISTERS |
| 029388054 B |  | STA | 10PT +5 | ; START THE 7109 Clock |
| 02968982 |  | LDA | 182 H | ;ENABLE INTERRUPT FROM |
| 0298 800EAB |  | STA | 10PT +0 EK | ; 6522 Cal input |
| 0298482303 |  | JMP | MAINPRg | ;1/O PORT SETUP COMPLETE, SO |
| 029 E |  |  |  | ; Junp to o.s. or to main progray |
| 029 E |  |  |  | ;interrupt service routine |
| 0280 |  | ORG | O2BOH |  |
| 02BO ADOOA8 | intsuc | LDA | 10PT | ;GET HIGH 8YTE |
| 0283 AA |  | tak |  | ;SAVE IT |
| 0284 290F |  | AND | *OFH | ; ZERO MSbs FOR ARITheEtic |
| 02868584 |  | STA | STORHI | ISAVE II |
| 028888 |  | ${ }^{1 \times 4}$ |  | ;GET SIEN BIT BACK |
| 02892910 |  | AnO | ${ }^{\text {H10H }}$ | ;ANALOG INPUT MEEATIVE? |
| 0288 F017 |  | BEP | SUBTR | \% YES, SO SUBTRACT |
| ${ }^{2} 28818$ |  | CLC |  | IRESULT POSITIVE 60 ADD |
| O2BE A5B0 |  | LDA | RESLT | ;GET LS BYTE OF THIS CONVERSION |
| 02 CO 600148 |  | ADC | 10PT+1 | ; ADO TO PREvIOUS READINGS |
| $02 C 38580$ |  | STA | RESLT | ; SAVE LS ByTE |
| 02051581 |  | LDA | RESLT+1 | ;GET MS byte of conversion |
| $02 C 76584$ |  | ADC | STORHI | ; ADD TO SUM |
| 02698581 |  | STA | RESLT+1 | - SAVE MS byte |
| 02CB A582 |  | LDA | RESLT+2 | \|GET SIGN |
| 02CD 6900 |  | ADC | 100 | ; ADO CARRY BIT, IF ANY |
| O2CF 8582 |  | STA | RESLT+2 | ; AND SAVE |
| 02 D 14 CE802 |  | JMP | LOOPCNT | ;JUHP TO TEST FOR 9 CONVERSIONS |
| 020438 | SUBTR | SEC |  | ; SET CARRY FOR SUBTRACTION |
| 02054580 |  | LDA | RESLT | ; POLARITY OF THIS CONVERSION |
| 0207 EDOLAB |  | SBC | 10PT+1 | - IS negative, So do a |
| 020A 8580 |  | STA | RESLT | - DDUBLE-PRECISION |
| O20C A581 |  | LDA | RESLT +1 | SUBRTACtion |
| O20E E584 |  | SBC | STORHt | $i$ - |
| 02508581 |  | STA | RESLT+1 |  |
| O2E2 A582 |  | ${ }^{\text {LDA }}$ | RESLT+2 | ; |
| O2E4 5990 |  | S日C | 100 | ; |
| 02E6 8582 |  | STA | RESLIT2 |  |
| $0258 \mathrm{C683}$ | LOPPCNT | DEC | Storx | ;HAVE HE DONE 9 CONVERS!ONS? |
| O2EA F001 |  | BER | DIVID | ; YES, SO MOM DIVIDE BY 9 |
| O2EC 40 |  | R71 |  | ( NO, so Return |
| O2ED |  | PABE |  |  |

Figure 7: This assembly-language listing for the $\mu P A / D-$ converter system in Figure 6 provides for 9 -sample numerical integration, thereby eliminating normalmode noise at frequencies that are multiples of 10 Hz .

## Adding Channels

By using analog multiplexers, you can take advantage of these speed-improvement techniques in multi-channel systems. Solving the equation given earlier for $X$ and using $X$ to determine the scan length (or number of channels), you keep the noise-segment alignment in proper phase. This segmented approach (for a 16 -channel system that requires the summation of three conversions) is shown in Figure 9. The scan length is found by dividing the number of available channels by X , taking the integer value, and then multiplying it by X and adding 1. Table 2 shows the relationship between the number of samples summed and the number of channels scanned for a 16-channel multiplexer.


Figure 8: This flowchart for Figure 7's assemblylanguage routine summarizes the code necessary to control the Figure 6 evaluation circuit.

A data-acquisition system using a 16 -channel multiplexer could use a TSC 7109 running at 25 conversions $/ \mathrm{sec}$ to reject all harmonics of 20 Hz (including, of course, 60 Hz , with a 5 -sample average taken in the microprocessor. The system would still respond to large signal deviations in a single conversion.
The change from analog signal integration of noise to hybrid analog/numerical integration entails some tradeoffs. The quantization error, for example, is always present; it can lead to a significant reduction in normal-mode rejection if the noise period is carved into too many segments. In addition, timing instability can create other error sources. For maximum stability, you must control the A/D converter's timing with a crystal oscillator.


Figure 9: You can add multichannel capability to the enhanced-speed A/D-converter designs employing $\mu$ P-based numerical integration.

# * TELEDYNE SEMICONDUCTOR 

Design Engineers sometimes have to interface our TSC7106 and similar ADCs to "non-ideal" sensors. A very common problem is that the sensor often does not give a "zero" output where the design wants a zero reading.
One example of a "non-ideal" sensor is a diode used as a temperature sensor. The diode typically changes $\mathbf{- 2} \mathrm{mV}$ per degree Celsius, but the change is from the diode's forward voltage of 600 mV or so. In order for the display to read "000" at 0.0 degrees, an offset must be provided.
The differential inputs of the TSC7106 yield an easy solution to the offset problem. Figure 1 shows a simple thermometer with a diode sensor. Because the diode voltage decreases as temperature increases, IN LO is connected to the diode temperature sensor. The $\mathbb{I N ~ H I ~ i n p u t ~ i s ~ c o n n e c t e d ~ t o ~ a ~ t r i m - ~}$ pot which is used to cancel the diode's forward voltage.
The offset problem gets a little more difficult, however, if a sensor requires a negative offset. The easiest way, shown in Figure 2, is to use a TSC9491 reference. This will provide an offset of up to -1.22 V . The only "trick" to this circuit is that Resistor R1 must source enough current for the TSC9491 plus a few extra microamps for the COMMON input.
Figure 2 also demonstrates the utility of the TSC7106 families' differential reference. The effective reference voltage is simply the difference between the REF HI and REF LO inputs. In this way, the same TSC9491 can be used to produce both input offset and reference voltages.

Positive Offset


Figure 1

## Negative Offset



Figure 2

The introduction of single-voltage EPROMS and dynamic RAMs has permitted designers to produce complete digital systems powered by a single 5 volt supply. One area which has not yielded to single-supply operation, however, is the RS-232 interface. If a system must communlcate with an RS-232 serlal device, such as a printer or another computer, a separate power supply is required.
The circult in Figure 1 provides an RS-232 driver without requiring a second power supply. Originally bullt for downloading files from an IBM PC to an AIM-65, the circuit is applicable to a wide variety of single-board computers as well as single chip microprocessors such as Intel's 8051. In 100-plece quantities the component cost is less than $\$ 3.00$, and pc board space is only a little more than is occupled by a 20-pin socket.
Understanding the circult's operation is easy. U1 is the CMOS TSC7660 DC-to-DC converter. It contains an oscillator and matrix of switches which convert the +5 volt supply to -5 volts. The optoisolator converts the TTL-level Input current into a voltage which swings between the plus and minus supply rails, producing RS-232 compatible output levels.
Resistor R1 determines the RS-232 output voltage swing. R1's value is determined by the input specifications of the receiving device, current transfer ratio of the optoisolator, and the driving circuit's output current capability.
The RS-232 input voltage spec is $\pm 3$ volts. The minimum input resistance of the MC1489, a typical RS-232 receiver,
is about $3 \mathrm{k} \Omega$. Therefore, 1 mA of current must be supplied, and R1 must be:

$$
R_{1}=\frac{5 V-3 V}{1 \mathrm{~mA}}=2 \mathrm{k} \Omega
$$

For reliable operation the optolsolator should be blased to saturation, so:

$$
\text { IOPTO }=\frac{10 \mathrm{~V}}{2 \mathrm{k} \Omega}+\frac{5 \mathrm{~V}}{3 \mathrm{k} \Omega}=6.6 \mathrm{~mA}
$$

Since the optoisolator's current transfer ratio is only $20 \%$, the LED current must be:

$$
I_{L E D}=\frac{6.6 \mathrm{~mA} * 100 \%}{20 \%}=33 \mathrm{~mA}
$$

This value is within the capability of the 7438 driver supplied with the AIM-65 computer. For interfacing to lower-power devices a higher gain optoisolator can be substituted. The 4N33 Darlington, for example, has a current transfer ratlo of $500 \%$, which reduces input drive current requirements to only 1.3 mA .
For a cable length of six feet, the circuit operates properly up to 9600 baud. Unfortunately, high baud rates are not always useable. This is because many computer prototyping boards seem to have software serial-communications routines which are designed for 110 baud teleprinters. These routines do not make use of the handshaking signals which RS-232 provides. Unless the serial communications routines are rewritten, lower baud rates may be required for proper operation.


This low cost circuit converts TTL-level signals to an RS-232 level without the expense of a negative power supply. The TSC7660's -5 V output permits the optoisolator to swing to RS-232 levels at up to 9600 baud.

## Application Brief 9 $\pm 5$ V Power Supply Operation with TSC7106A/TSC7107A By Dave Gillooly

The TSC7106A/7106 3 1/2 digit analog-to-digitial converters with liquid crystal display drive can be powered from $\pm 5 \mathrm{~V}$ power supplies easily. Low cost voltage regulators such as the LM7805 (+5 V) and LM7905 (-5 V) power the TSC7106A/ 7106 in Figure 1. Analog common, internally referenced to 3 V below the positive supply potential, is used to supply the converter reference.

If only +5 V is available the low cost TSC7660 DC to DC converter easily generates the -5 V supply as in Figure 2. A TSC7107A/7107 LED display converter can also be powered by a TSC7660.

An external voltage reference replaces the internal reference in Figure 3. Chip temperature variations caused by changing LED display drive current can cause full-scale drift if the internal reference does not have a low temperature coefficient. Input signal magnitude and the corresponding seven segment display code determine how many LED segment drivers are active. The TSC7107A features an improved low temperature drift internal voltage reference.

The TSC7107A is directly pin compatible with the first generation ICL7107 device and lowers temperature induced fullscale drift (See the TSC7107A Data Sheet Also).


Figure 1: TSC7106A/7106 Operates From $\pm 5$ V Power Supplies


Figure 2: TSC7660 Generates -5 V Power Supply


Figure 3: External Reference in $\pm 5$ V System

Many Teledyne Semiconductor products use displays, crystals and capacitors. A partial list of potential suppliers for components is given below. Although not exhaustive, the list
should help development. Additional vendors can be found in the U.S. Industrial Directory, Electronic Design's Gold Book, and Who's Who in Electronics.

## LED Displays

- AND

Burlingame, CA 94010
(415) 347-9916

TWX: 910-374-2353

- General Instrument

Opto Electronics Division
Palo Alto, CA 94304
(415) 493-0400

- Hewlett Packard

Opto Electronics
640 Page Mill Road
Palo Alto, CA 94304
(415) 857-5948

- Litronix

Cupertino, CA 95014
(408) 257-7910

TWX: 910-338-0022

## Oscillator Crystals

- Daiwa Sinku Corp.

Hirakacho, Kakogowa Hyogo, Japan 0794-26-3211

- International Piezo Ltd.

Hong Kong
3-351051
TELEX: 35454 XTAL HX

- Jameco

Belmont, CA
(415) 592-8097

TELEX: 176043

- Statek Co.

Orange, CA 92668
(714) 639-7810

TWX: 910-593-1355

## Piezoelectric Audio Transducers

- Murata Erie Marietta, GA 30067
(404) 952-9777

TWX: 810-766-1531

- Piezoelectric Products

Gulton Industries
Metuchen, NJ 08840
(201) 548-2800

## Liquid Crystal Displays

- Amperex

Slatersville, RI 02876
(401) 762-3800

TWX: 710-382-6332

- Crystaloid

Hudson, OH 44236
(216) 655-2429

- Epson

Torrance, CA 90505
(213) 534-0360

TELEX: 182412

- Hamlin

Lake Mills, WI 53551
(414) 648-2361

TWX: 910-260-3740

- Printed Circuits International

1145 Sonora Court
Sunnyvale, CA 94086
(408) 980-0591

- REFAC

Winsted, CT 06098-0809
(203) 379-2731

TWX: 710-449-6464

- UCE

Norwalk, CT 06855
(203) 838-7509

- Varitronix

VL Electronics
Los Angeles, CA 90027
(213) 661-8883

TELEX: 821-554

## Liquid Crystal Display Connectors

- Tecknit

129 Dermody Street
Cranford, NJ 07016
(201) 272-5500

TWX: 710-996-5951

## Polypropylene Capacitors

- International Components

Melville, NY 11747
(516) 293-1500

TELEX: 143130

- S\&EI Manufacturing

Northridge, CA 91324
(213) 349-4111

TWX: 910-493-1252

- Seacor

Westwood, NJ
(201) 666-5600

TELEX: 135354

- Sprague Electric

North Adams, MA
(413) 664-4411

- TRW Capacitors

Ogalla, NE
(308) 284-3611

- Wesco

Greenfield, MA 01301
(413) 774-4358

- West Lake Capacitors

West Lake Village, CA
(818) 889-4120

TWX: 910-494-4779

## Quad Flat Package Test Sockets

- Nepenthe Distribution

2471 East Bayshore, Suite 520
Palo Alto, CA 94303
(415) 856-9332

## Resistor Networks

- Caddock Electronics

1717 Chicago Avenue
Riverside, CA 92507
(714) 788-1700

TWX: 910-332-6108

This listing does not represent an endorsement of manufacturer's product or a guarantee of suitablity. Contact the supplier for specific product information.


SECTIION 16
Glossary of
Terms and Abbreviations

## Brief Glossary For TSC Products

## Analog-to-Digital Converter

Electronic device that converts Analog (continuous) information into a Digital word (number). Analog quantities can be temperature, pressure, weight, chemical concentration, noise level, and fluid level.
The Digital result can be a number in binary, decimal, or binary-coded-decimal (BCD).

## Auto-Zero

A self-correcting system that insures a Zero output of the ADC for a Zero input.

## Binary

Number system with only two values - 0 or 1 - in each numeric position. This is the number system used in computer systems.

## Binary-Coded-Decimal (BCD)

A number system whereby binary numbers are grouped in sets of four to represent decimal (Ten system) numbers. This system is shown below.

| BCD \# | Decimal \# |
| :--- | :---: |
| 0000 | 0 |
| 0001 | 1 |
| 0010 | 2 |
| 0011 | 3 |
| 0100 | 4 |
| 0101 | 5 |
| 0110 | 6 |
| 0111 | 7 |
| 1000 | 8 |
| 1001 | 9 |

This number system is useful for some $A / D$ converters intended to be used in displaying the output as decimal numbers.

## Bit

A single binary number unit, 0 or 1 . An 8 -bit number could appear as:

| 10011110 |  |
| :--- | :--- |
| or |  |
| 01000011 | $(158$ in decimal) |
|  | $(67$ in decimal $)$ |


| or any other combination |  |
| :---: | :---: |
| from | 00000000 |
| to |  |
|  | 11111111 |

## Code

Output format of A/D converter. Usually binary, $B C D$, or sign-magnitude binary.

## Digit

A single decimal number unit that can range in value from 0 to 9 . Thus, a $31 / 2$ digit A/D converter goes from 0000 to 1999; a $41 / 2$ digit $A / C$ converter can provide outputs from 00000 to 19999;
and a 3 digit converter can provide outputs from 000 to 999.
Note that the " $1 / 2$ digit" merely doubles the output range by adding a Most Significant Bit to the output.

## Display ADC

An A/D converter normally designed to convert and display the numeric value representing the analog signal. Display ADC's may have the Display Driver built in (as the TSC7106, 7107, 7116, 7117 have), or may provide multiplexed BCD for use by external drivers (the TSC14433, TSC7135, and TSC8750 do this).

## Least-Significant-Bit (or Digit)

The lowest number position

| for Decimal | 1287 |
| :---: | :---: |
|  | Least Significant Digit (LSD) |
| for Binary | 10010011 |
|  | Least Significant Bit (LSB) |

## Multiplexed

Signals sharing a common connection but separated in time are said to be multiplexed. Multiplexed BCD is characterized by the 4 BCD signal paths in which the appropriate digits are separated in time.

## Resolution

Number of output states offered by the A/D converter. For a binary ADC, the resolution is $2^{n}$; where $n$ equals the number of bits,

$$
\text { thus: } \quad \begin{array}{ll}
2^{8}=256 \\
& 2^{10}=1024 \\
& 2^{12}=4096 \\
& 2^{14}=16384 \\
& 2^{16}=65536
\end{array}
$$

For decimal and BCD ADCs, the resolution equals $10^{n}$; where n is the number of digits (see "Digit" definition).

## Sign

An additional output in some ADCs that are capable of measuring both + and - voltage. The sign bit identifies this polarity (typically, " 1 " for + and " 0 " for - ). The coding format resulting is called Sign-Magnitude Code.

## Glossary of Data Conversion Terms

Absolute Accuracy<br>The worst-case input to output error of a data converter referred to the NBS standard volt.

## Accuracy

The conformance of a measured value with its true value; the maximum error of a device such as a data converter from the true value. See relative accuracy and absolute accuracy.

## A/D Converter

Analog-to-digital converter. A circuit which converts an analog (continuous) voltage or current into an output digital code.

## Auto-Zero

A stabilization circuit which serves an amplifier or $A / D$ converter input offset to zero during a portion of its operating cycle.

## Bandgap Reference

A voltage reference circuit which is based on the principle of the predictable base-to-emitter voltage of a transistor to generate a constant voltage equal to the extrapolated bandgap voltage of silicon ( $\approx 1.22 \mathrm{~V}$ ).

## Binary Code

A positive weighted code in which a number is represented by

$$
N=a_{0} 2^{0}+a_{1} 2^{1}+a_{2} 2^{2}+a_{3} 2^{3}+\ldots+a_{n} 2^{n}
$$

where each coefficient "a" has a value of zero or one. Data converters use this code in its fractional form where:

$$
N=a_{1} 2^{-1}+a_{2} 2^{-2}+a_{3} 2^{-3}+\ldots a_{n} 2^{-n}
$$

and N has a fractional value between zero and one.

## Binary Coded Decimal (BCD)

A binary code used to represent decimal numbers in which each digit from 0 to 9 is represented by four bits weighted $8-4-2-1$. Only 10 of the 16 possible states are used.

## Bipolar Mode

For a data converter, when the analog signal range includes both positive and negative values.

## Busy Output

See Status Output

## Charge Balancing A/D Converter

An analog-to-digital conversion technique which employs an operational integrator circuit within a pulse generating feedback loop. Current pulses from the feedback loop are precisely balanced against the analog input by the integrator, and the sesulting pulses are counted for a fixed period of time to produce an output digital word. This technique is also called quantized-feedback.

## Clock

A circuit in an A/D converter that generates timing pulses which synchronize the operation of the converter.

## Common-Mode Rejection Ratio

For an amplifier, the ratio of differential voltage gain to common-mode voltage gain, generally expressed in dB.

$$
C M R R=20 \log _{10} \frac{A_{D}}{A_{C M}}
$$

where $A_{D}$ is differential voltage gain and $A \subset M$ is common mode voltage gain.

## Conversion Time

The time required for an A/D converter to complete a single conversion to specified resolution and linearity for a fullscale analog input change.

## Differential Linearity Error

The maximum deviation of any quantum (LSB change) in the transfer function of a data converter from its ideal size of FSR/2 ${ }^{n}$.

## Dual Slope A/D Converter

An indirect method of A/D conversion whereby an analog voltage is converted into a time period by an integrator and reference and then measured by a clock and counter. The method is relatively slow but capable of high accuracy.

## End of Conversion

## See Status Output

Frequency-To-Voltage (F/V) Converter
A device which converts an input pulse rate into an output analog voltage.

## Full-Scale Range (FSR)

The difference between maximum and minimum analog values for an A/D converter input or D/A converter output.

## Integral Linearity Error

The maximum deviation of a data converter transfer function from the ideal straight line with offset and gain errors zeroed. It is generally expressed in LSB's or in percent of FSR.

## Integrating A/D Converter

One of several types of $A / D$ conversion techniques whereby the analog input is integrated with time. This includes dual slope, triple slope, and charge balancing type A/D converters.

## Least Significant Bit (LSB)

The rightmost bit in a data converter code. The analog size of the LSB can be found from the converter resolution:

$$
\text { LSB Size }=\frac{\text { FSR }}{2^{n}}
$$

where FSR is full-scale range and n is the resolution in bits.

## Linearity Error

See Integral Linearity Error and Differential Linearity Error. Missing code
In an A/D converter, the characteristic whereby not all output codes are present in the transfer function of the converter. This is caused by a non monotonic D/A converter inside the

## Monotonicity

For a D/A converter, the characteristic of the transfer function whereby an increasing input code produces a continuously increasing analog output. Nonmonotonicity may occur if the converter differential linearity error exceeds $\pm 1$ LSB.

## Most Significant Bit (MSB)

The leftmost bit in a data converter code. It has the largest weight, equal to one half of full-scale range.

## Glossary of Data Conversion Terms

## Multiplying D/A Converter

A type of digital-to-analog converter In which the reference voltage can be varied over a wide range to produce an analog output which is the product of the input code and Input reference voltage. Multiplication can be accomplished in one, two, or four algebraic quadrants.

## Nolse Rejectlon

The amount of suppression of normal mode analog Input nolse of an A/D converter or other circult, generally expressed in dB. Good nolse rejection is a characteristic of Integrating type A/D converters.

## Offset Drift

The change with temperature of analog zero for a data converter operating in the blpolar mode. It is generally expressed in ppm $/{ }^{\circ} \mathrm{C}$ of FSR.

## Parallel Type A/D Converter

An ultra-fast method of A/D conversion which uses an array of $2^{n}-1$ comparators to directly implement a quantizer, where $n$ is the resolution in bits. The quantizer is followed by a decoder circult which converts the comparator outputs into binary code.

## Power Supply Sensitivity

The output change in a data converter caused by a change in power supply voltage. Power supply sensitivity is generally specified in \%/V or in \%/\% supply change.

## Ratiometric A/D Converter

An analog-to-digital converter which uses a variable reference to measure the ratio of the input voltage to the difference.

## Relatlve Accuracy

The worst case input to output error of a data converter, as a percent of full-scale, referred to the converter reference. The error consists of offset, galn, and linearity components.

## Resolution

The smallest change that can be distinguished by an $A / D$ converter or produced by a D/A converter. Resolution may be stated in percent of full-scale, but is commonly expressed as the number of blts $n$ where the converter has $2^{n}$ possible states.

## Status Output

The logic output of an A/D converter which Indicates whether the device is in the process of making a conversion or the conversion has been completed and output data is ready. Also called busy output or end of conversion output.

## Temperature Coefflclent

The change in analog magnitude with temperature, expressed in ppm $/{ }^{\circ} \mathrm{C}$.

## Three-State Output

A type of a/D converter output used to connect to a data bus. The three output states are logic 1, logic 0 , and off. An enable control turns the output on or off.

## Voltage-To-Frequency (V/F) Converter

A device which converts an analog voltage into a train of digital pulses with frequency proportional to the input voltage.

## Zero Drift

The change with temperature of analog zero for a data converter operating in the unipolar mode. It is generally expressed in $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$.


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| Edmonton, AB T6E 5W5 | $10-8385$ St. George St. |
| 403/437-2755 | Vancouver, BC V5X 4P3 |
| TWX: 610-831-1101 | $604 / 324-6831$ |
|  | TWX: 610-922-5032 |

## Ontario

Future Electronics
82 St. Regis Cresant N.
Downsview, ON M3J 123
416/638-4771
Future Electronics
1050 Baxter Rd.
Ottawa, ON K2C 3P2
613/820-8313

## Quebec

Future Electronics
237 Humus Blva.
Pointe Claire, QB H9R 5C7
514/694-7710
TWX: 610-421-3500

## International Representatives and Distributors

| Argentina | France |
| :---: | :---: |
| Tinko SA | Tekelec Airtronic SA |
| Aisina 1633 | Cité des Bruyères |
| 1088 Buenos Aires | Rue Carle Vernet |
| Argentina | F-92310 Sèvres |
| Telephone: 49-6060 | Telephone: 01-5347535 |
| TLX: 17825 SENIS AR | TLX: 204552 |
| Australia | Germany |
| Promark Electronics Pty. Ltd. Suite 102, 6-8 Clarke Street Crows Nest, NSW 2065 <br> Australia <br> Telephone: 439-6571 or 439-6965 TLX: 20474 | Adelco Elektronik GmbH |
|  | Boxhoimstr. 5 |
|  | Telephone: 04106-2024 |
|  | Telephone: 04106-2024 <br> TLX• 2180619 |
|  |  |
|  | Emtron |
|  | Electronic Vertriebs GmbH |
| Belgium | Waldstr. 55 |
| Microtron PVBA/SPRL <br> Tremelobaan 131 <br> B-2850 Keerbergen <br> Telephone: 016-534186 <br> TLX: 22606 | Telephone: 06152-6003 |
|  | TLX: 4191175 |
|  | Ing. T. Henskes GmbH |
|  | Badenstedter Str. 9 |
|  | 3000 Hannover 91 |
|  | Telephone: 0511-456082 |
| Brazil | TLX: 923509 |
| Hitech Comerciale Industrial Av. Eng. Luiz Carlos Berrini, Conjunto 111/121 Brooklin <br> Telephone: (011) 533-9566 TLX: 391-53288 | Hot Elektronik |
|  | Wendelsteinweg 11 <br> Postfach 1261 |
|  | 8028 Taufkirchen - Potzham |
|  | Telephone: 089-6121092 |
|  | TLX: 529528 |
|  | Metronik GmbH |
| Denmark | Kapellenstr. 9 |
|  | 8025 Unterhaching |
| Nordisk Elektronik AS Tranformervej 17 DK-2730 Herlev Telephone: 02-842000 TLX: 35200 | Telephone: 089-6114063 |
|  | TLX: 529524 |
|  | Rein Elektronik GmbH |
|  | Lötscher Weg 66 |
|  | 4054 Nettetal 1 |
|  | Telephone: 02153-733-0 |
| Finland | TLX: 854251 |
| Fintronic OY $A B$ | Semitron W. Röck GmbH |
| Melkonkatu 24A | Im Gut 1 |
| SF-00210 Helsinki 21 | 7891 Kussaberg 6 |
| Telephone: 80-6926022 | Telephone: 07742-7011 |
| TLX: 124224 | TLX: 7921472 |

## Isreal (Representative)

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15, Kineret Street
Bney-Brak
P.O. Box 20168

Tel-Aviv 61200
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Telephone: 03-708174/5
TLX: 342107

## Italy

Eledra 3S Spa
Viale Elvezia 18
I-20154 Milano
Telephone: 02-349751
TLX: 332332
314155

## Japan

Tomen Electronics Corp.
1-1, Uchisaiwai-Cho 2-Chome
Chiyoda-Ku, Tokyo 100
Telephone: (03) 506-3694
TLX: J-23548
Sil-Walker Inc.
1-1, Shinjuku 5-Chome
Shinjuku-Ku, Tokyo 160
Telephone: (03) 341-3651
TLX: 0232-3398

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Vine-Overseas Trading Corp.
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266-1663/265-9875/269-0832
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## Mexico

Dicopel
Tochtli 368
Fracc Ind. San Antonio
Azcapotzalco C.P. 02760 Mexico D.F.
Telephone: 561-32-11
TLX: 1773780 DICOME

## International Representatives and Distributors

| Netherlands | Sweden | United Kingdom |
| :---: | :---: | :---: |
| Alcom Electronics bv | Nordisk Elektronik AB Huvudstagatan 1 <br> P.O. Box 1409 <br> S-17127 Solna <br> Telephone: 08-7349770 <br> TLX: 10547 | Macro Marketing Ltd. |
| Esse Baan 1 |  | Burnham Lane |
| NL-2908 LJ Capelle a/d IJssel |  | Slough, Berks. SL1 6LN |
| Telephone: 010-519533 |  | Telephone: 06286-4422 |
| TLX: 26160 |  | TLX: 847945 |
| New Zealand |  | Phoenix Electronics <br> (Airdrie) Ltd. <br> Western Buildings <br> Vere Road <br> Kirkmuirhill <br> Lanarkshire, Scotland <br> Telephone: 0555-892393 <br> TLX: 777404 |
|  | Switzerland |  |
| Protessional Electronics Ltd. 22A, Milford Rd., Milford, Auckland <br> Telephone: 493-048/029 <br> TLX: NZ21084 | ENA AG <br> Hermetschloostr. 75 $\mathrm{CH}-8048$ Zurich Telephone: 01-645757 TLX: 822303 |  |
|  |  |  |
|  |  |  |
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| South Africa | Omni Ray AG <br> Industriestr. 31 <br> CH-8305 Dietlikon <br> Telephone: 01-8352111 <br> TLX: 53239 | Semicomps Ltd. Halifax Road |
| Fairmont Electronics (Pty) Ltd. 4th Fl., 312 Kent Avenue, Ferndale Randburg 2194, South Africa Telephone: (011) 789-1230/4 TLX: 8-24842 |  | Keighley |
|  |  | West Yorkshire BD21 5HR Telephone: 0535-65191 |
|  |  | $\begin{aligned} & \text { Telephone: } 0 \\ & \text { TLX: } 517343 \end{aligned}$ |
|  | Taiwan | Semiconductor Supplies International Ltd. |
| Spain | Timkuo Taiwan Ltd. 8F-2, 157 Fu Hsing S. Road | Dawson House <br> 128/130 Carshalton Road Sutton, Surrey SM1 4RS |
| Amitron S.A. <br> Avenida Valladolid, 47-A <br> E-28008 Madrid | Sec. 2, Taipei <br> Telephone: (02) 709-2246 <br> TLX: 26206 | $\begin{aligned} & \text { Telephone: 01643-1126 } \\ & \text { TLX: } 946650 \end{aligned}$ |
| $\begin{aligned} & \text { Telephone: 01-2479313 } \\ & \text { TLX: } 45550 \end{aligned}$ |  | Trident Microsystems Ltd. 53 Ormside Way Holmethorpe Industrial Estate Redhill, Surrey RH1 2LS Telephone: 0737-65900 TLX: 8953230 |

## A-TELEDYNE SEMICONDUCTOR

1300 Terra Bella Avenue •P.0. Box 7267 • Mountain View, CA 94039-7267 •(415) 968-9241


[^0]:    ADDRESS INPUTS $\left(A_{N}\right)=0$ (LATCHES NOT SHOWN)

[^1]:    TSC500/Microcomputer Display ADC

[^2]:    1. Approximately 5 conversions/sec.
[^3]:    Notes:

    1. Functional operation is not implied.
    2. Limit input current to under $100 \mu \mathrm{~A}$ if input voltages exceed supply voltage.
    3. Full Scale Voltage $=2.000 \mathrm{~V}$.
    4. $\mathrm{V}_{\mathrm{IN}}=0.0000 \mathrm{~V}$.
    5. $0^{\circ} \mathrm{C} \leq T_{A} \leq+70^{\circ} \mathrm{C}$.
    6. External Reference Temperature Coefficient less than $0.01 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$.
[^4]:    Note: *Assumes a positive polarity input signal. SWRI would be closed for a negative input signal.

[^5]:    Multivibrator clrcult at Pin 21 (Initlate Conversion) strobes converter at rates slower than the normal freerun mode. ( $\tau=R_{x} C_{x}$ )

[^6]:    Notes:

    1. Full temperature range
    2. $\mathrm{IIN}=0$.
    3. Full temperature range. IOUT $=10 \mathrm{~mA}$.
    4. IOUT $=10 \mu \mathrm{~A}$
    5. 10 Hz to 100 kHz .
    6. $5 \mu \mathrm{~s} \mathrm{~min}$. positive pulse width and $0.5 \mu \mathrm{~s} \mathrm{~min}$. negative pulse width. $\mathrm{T}_{\mathrm{r}}=\mathrm{t}_{\mathrm{f}}=20 \mathrm{~ns}$.
[^7]:    $L=$ Logic 0
    H = Logic 1
    L* $=$ Output NMOS ON
    $H^{*}=$ Output NMOS OFF
    X = Don't Care
    $\sqrt{ } \sqrt{=}$ Transition from Low to High
    $\mathrm{D}_{1}, \mathrm{D}_{2}, \ldots \mathrm{D}_{16}=$ Data Inputs at Clock Time T-N. Data is Inverted at the Parallel Outputs.

[^8]:    Circuit uses frequency-to-voltage-to-frequency conversion, with intermediate stage of gain between conversions, for multiplying input frequency by any number. Digital-to-analog converter is programmed digitally, by thumbwheel switches or microprocessor, for coarse selection of frequency-multiplying factor; 741 provides fine gain, enables choice of non-integer multiplication values.

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